

# 1986 FIELD INVESTIGATION AND SUPPLEMENTAL REMEDIAL INVESTIGATION REPORT

VOLUME I

FRENCH LIMITED SITE  
CROSBY, TEXAS

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***RESOURCE ENGINEERING***

1986 FIELD INVESTIGATION REPORT  
FRENCH LIMITED SITE

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## EXECUTIVE SUMMARY

Several field investigations have been conducted at the French Limited Site since December, 1982. The most recent consolidation of the various investigation reports was published as the draft CERCLA Remedial Investigation (RI) report in June, 1986. This draft was subsequently accepted by EPA, as the final RI Report for the site pending resolution of certain issues to be addressed in the 1986 Field Investigation. Generally, there have been common interpretations of the factual data base. However, in certain areas, limited and/or conflicting data have been reported by the different studies. A 1986 Field Investigation was proposed by the French Limited Task Group and approved by EPA, to broaden the technical data base and investigate four specific areas. A description of these four areas of expanded investigation, and the results of the 1986 Investigation, is as follows:

- 1) PCB Concentration Distribution in Sludge - This task was designed to identify maximum PCB concentrations in the lagoon sludges. It was also designed to assess the possibility of segregating sludges containing different PCB concentration levels, if there should be a requirement for different disposal methods for different concentration levels.

Only 1 sample location in the lagoon reported a PCB concentration over 500 ppm. This location near the southern shore of the lagoon, reported a 693 ppm PCB concentration. A subsequent re-extraction and re-analysis of the same sample reported 144 PCB concentration. This variability of analytic results precludes a firm conclusion that the sample exceeds 500 ppm PCB concentration.

It is clearly feasible to remove this "spot" of sludge separately from the remaining lagoon sludge, should separate disposal methods be required.

2. Contaminated Soil Volume Assessment - This task provided additional soil contamination analysis data to update the contaminated soil volume estimate. Estimates of contaminated soil volume were made based on four different decontamination cleanup objectives. The results are as follows:

ESTIMATED CONTAMINATED SOIL VOLUME

<u>Decontamination Objective (ppm-PNA's)</u>	<u>Volume (Cubic Yards)</u>
1 ppm	267,000
10 ppm	51,000
100 ppm	35,400
1000 ppm	25,500

3. Alluvial Remnant Assessment - The purpose of this task was to identify the extent and configuration of alluvial remnant material separating the French Lagoon and the Riverdale water supply wells. The degree of hydraulic communication that exists across this alluvial remnant material was also assessed.

Clay material in the Alluvial remnant area may have originated from the underlying Beaumont Formation, but it has been reworked and mixed with sand to such an extent that it does not retain compositional qualities of the parent formation. The discontinuous configuration of the remnant, combined with the composition of its material was found to retard but not prevent future lateral contaminant migration between French Limited and the Riverdale.

4. Deep Aquifer Hydrogeologic Assessment - Previous geologic investigations have suggested that a confining aquitard exists under the French Limited Lagoon that hydrologically isolates the shallow Alluvial zone from the regional Deep Aquifer. However, the previous investigations also detected trace level contamination in the first Deep Aquifer below the site.

This task was designed to provide supplemental geologic, hydrogeologic, and chemical analysis information to

support a detailed analysis of the aquitard's hydrologic integrity. Additionally the investigation would identify the source and extent of trace contamination in the Deep Aquifer.

Performance of these investigations resulted in a conclusion that the aquitard does prevent vertical migration of contaminants from the Alluvial zone into the Deep Aquifer. It was further determined that trace contamination existing in the Deep Aquifer had migrated downward by means of leakage around certain of the artificial penetrations in the area. Additionally, the investigations provided hydrogeologic characteristic data for both the shallow and Deep Aquifers.

## 1.0 INTRODUCTION

Several field investigations have been conducted at the French Limited Superfund site since December, 1982. These investigations have been documented in various reports. The most recent consolidation was published as the Draft CERCLA Remedial Investigation (RI) Report in June, 1986. This draft was subsequently accepted by EPA, as the final RI Report for the site, pending resolution of certain issues to be addressed in the 1986 field investigation. A significant technical data base has been generated by these previous investigations, and numerous conclusions have been drawn, as reported in the draft RI report.

Some data interpretations have been modified after detailed technical review by the Environmental Protection Agency (EPA) and the French Limited Task Group. In general, this review has resulted in a common interpretation of the factual data base. However, there are certain areas where limited and/or conflicting data were developed during the various investigatory programs. As a result, a 1986 Field Investigation Program was proposed by the French Limited Task Group and approved by the EPA, to broaden the technical data base in four specific areas. A brief description of these four expanded investigative areas is as follows:

- Identify the maximum PCB concentration in the lagoon sludges, and assess the possibility of segregating sludges containing different PCB concentration levels.

- Identify the volume of contaminated soils underlying and surrounding the lagoon sludges.
- Identify the extent and configuration of an alluvial remnant (buried clay ridge) within the alluvium separating the French Limited Lagoon and Riverdale water supply wells, and assess its impact on the hydraulic connection of the two locations, through the shallow aquifer.
- Assess the The hydrogeology of the deep aquifer located approximately 120 feet below grade at the site, and provide identification of contaminant migration pathways which might impact it.

The purpose and scope of the 1986 field investigation is further described in the following sections, which also include the results of the various tests and analyses.

An overall plan view of the French Limited site is shown on the Plate 1 - Base Map in Attachment 1. The location of the various monitor wells at the site are also included.

All field tasks and analytical programs were conducted in accordance with existing safety and QA/QC procedures developed and used during previous field investigation activities at the French Limited site.

## 2.0 ASSESSMENT OF LAGOON SLUDGE PCB CONCENTRATIONS

### 2.1 Purpose of PCB Concentration Survey

Previous investigations have established that PCB contamination exists at the French Limited site, and that the higher concentrations of PCBs tend to be located in the far western portion of the lagoon. However, the previous sampling and analytical programs lacked sufficient detail to determine the optimum disposal method requirements for the PCB contaminated sludges.

The 1986 PCB Sampling and Analysis Survey was designed to provide detailed PCB concentration information. The survey, established in a lateral and vertical grid pattern, covered the far western end of the lagoon where maximum PCB concentrations are indicated. The PCB concentration data obtained in this survey will then be available to prepare a PCB disposal plan that segregates and isolates sludges containing high PCB concentrations (over 500 ppm) from those containing lower concentrations, should this be required.

This survey incorporated a program of sample splits for analysis at three different laboratories, and repeat analysis of the same samples at one of the laboratories in order to establish a data base illustrating the degree of variability in analytical results obtained from the same samples.

## 2.2 Scope of PCB Concentration Survey

2.2.1 Sludge Sample Collection - After PCB concentration information from previous investigations was reviewed, it was determined that a sample grid extending eastward 350 feet from the western end of the lagoon would cover the area where PCB concentrations over 500 ppm might be expected. A sampling grid was established in that area of the lagoon on approximately 50 by 50 foot centers. Samples were collected at 22 locations on this grid, as shown in Figure 2-1, at the following depths:

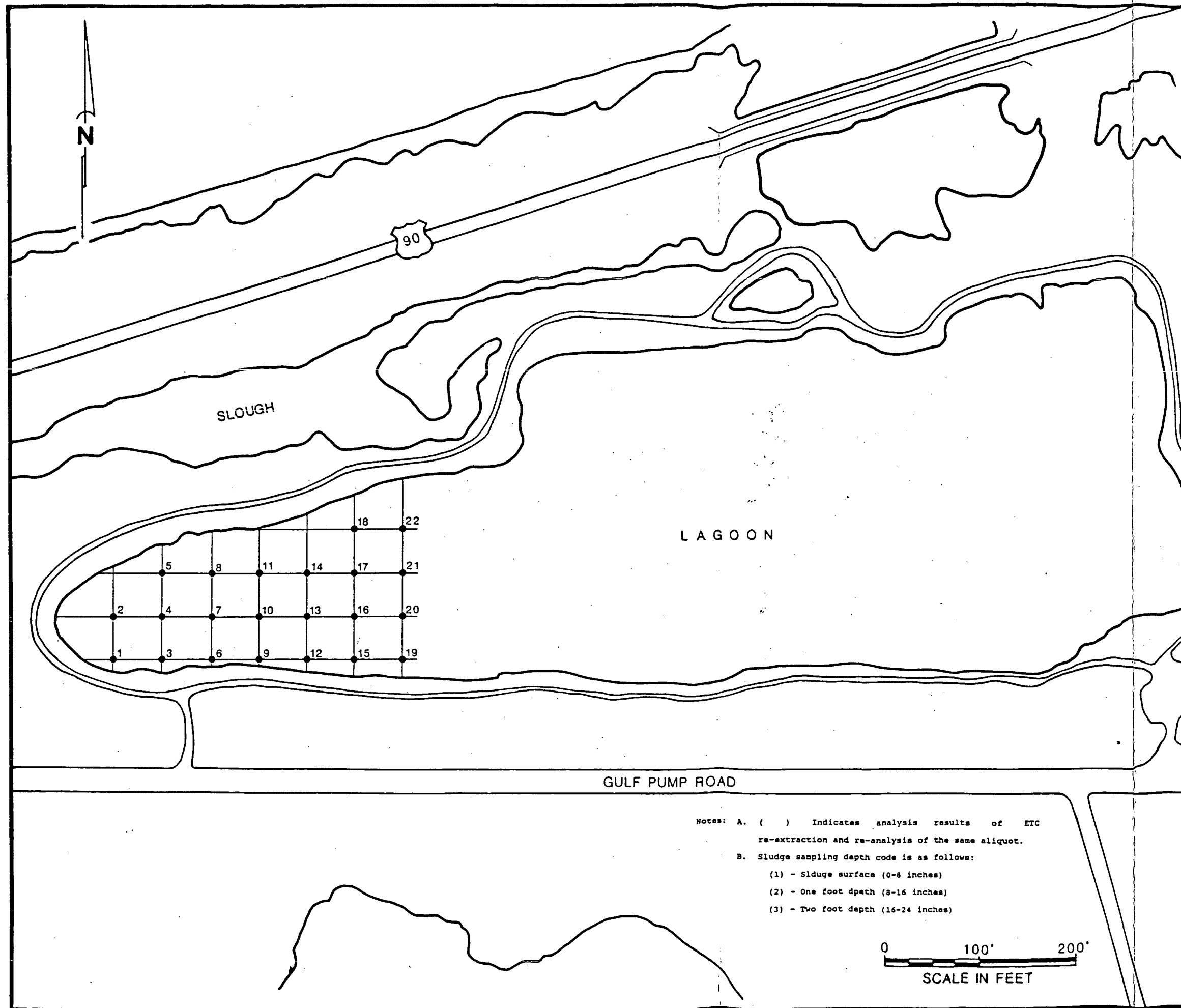
Depth 1 - Sludge surface samples (0 to 8 inches)

Depth 2 - One foot depth samples (8 to 16 inches)

Depth 3 - Two foot depth samples (16 to 24 inches)

Collection of samples was accomplished using a 2-inch PVC piston sampler to retrieve 24-inch long sample cores from the lagoon sludge. Samples from each of the three depth intervals were extruded into individual stainless steel compositing bowls and blended prior to placement into specially prepared sample containers. Consistent with approved sampling protocol, all sample collection and compositing equipment was decontaminated between samples using rinses of a detergent, water, acetone, and then water.





# LAGOON SLUDGE PCB ANALYTICAL RESULTS

Sample Point	Depth	TOTAL PCB'S (ppm)		
		ETC	Rocky Mountain	Radian
1	1	105 (277)	77	160
	2	73.1		
	3	315 (353)		
2	1	59.5		
	2	14.6	28	38
	3	20.5		
3	1	ND		
	2	28.7		
	3	17.8	3.3	12
4	1	44.9	57	84
	2	72.1		
	3	39.4		
5	1	21.7		
	2	21.7		
	3	4.7		
6	1	32.9		
	2	37.7		
	3	20.6		
7	1	24.4		
	2	4.18		
	3	16.6		
8	1	25	9.3	28
	2	ND		
	3	ND		
9	1	ND		
	2	ND(31)	34	120
	3	ND		
10	1	35.8		
	2	7.57		
	3	17.7		
11	1	7.17		
	2	ND	2.3	3.8
	3	15.2		
12	1	243 (471)		
	2	693 (144)		
	3	244 (151)		
13	1	19.3		
	2	ND	36	48
	3	6.67		
14	1	41.4		
	2	40.3		
	3	13.5		
15	1	98.6 (200)		
	2	No Sludge		
	3	No Sludge		
16	1	21.4		
	2	3.42		
	3	8.70		
17	1	9.45		
	2	3.46	2.0	2.4
	3	ND		
18	1	34.4		
	2	41.6		
	3	No Sludge		
19	1	8.96		
	2	38.5		
	3	No Sludge		
20	1	10.58	6.1	37
	2	12.3		
	3	13.1		
21	1	ND		
	2	ND		
	3	ND		
22	1	2.88		
	2	ND		
	3	No Sludge		



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

FIGURE 2-1  
LAGOON SLUDGE  
PCB SAMPLING LOCATIONS  
AND RESULTS  
FRENCH LIMITED

DRAWN BY: BH DATE: 11-3-86 PROJECT NO: 275-14

The grid consisted of 22 sampling locations, with 3 sampling depths at each location, resulting in a total of 66 samples. However, there were 5 sample points that had no sludge present; thus, no samples were collected.

Of the 61 samples collected, 10 were randomly selected to be analyzed by 2 separate independent laboratories specified by the EPA (Radian and Rocky Mountain), in addition to being analyzed in the laboratory that performed the analytical work for REI (Environmental Testing and Certification - ETC). Each of these 10 sample splits was taken simultaneously from the same homogenized composites, and placed into identically prepared containers. Complete chain-of-custody documentation accompanied each individual sample.

After receipt of the analytical results from the three laboratories, ETC was requested to re-extract and re-analyze seven samples. These samples were randomly selected by REI, but they included two samples that had previously been analyzed by all three laboratories and five samples that had been analyzed only by ETC. The location and depth's of the samples that were analyzed by all three laboratories, and those that were re-analyzed by ETC is shown on Figure 2-1.

#### 2.2.2 Laboratory PCB Analysis Method Control

To ensure results were comparative from the three laboratories performing PCB analyses, the sample preparation, extraction, and analysis methodologies were

specified to all laboratories. These procedural instructions are shown in Appendix 1. All samples were analyzed using Gas Chromatograph/Electron Capture Detector (GC/ECD) techniques, with results reported in dry weight concentrations.

### 2.3 PCB Concentration Analysis Results

The results of the PCB analysis of lagoon sludge are summarized on Figure 2-1. Presented are analytical results from the three laboratories and the lagoon grid pattern for reference regarding sample location. Data provided in parentheses under the ETC column show the analytic results for samples which were re-extracted and re-analyzed by ETC.

The laboratory reports are provided in the following Appendices:

Appendix 2 - ETC PCB Analytical Results

Appendix 3 - Rocky Mountain PCB Analytical Results

Appendix 4 - Radian PCB Analytical Results

A review of the analytical data presented in Section 2-3 was performed to evaluate the statistical significance of the results. This evaluation verified that all results for sample splits analyzed by all three labs were statistically valid. A statistical evaluation of the results where only two analyses data points are available can not be performed.

#### 2.4 PCB Concentration Assessment Conclusions

Review of the analytical data leads to the following conclusions regarding the PCB concentration survey of the French Limited Site.

- Only one (1) sample (Location 12 - Depth 2) location reflected a PCB concentration over 500 ppm. This sample, from the 8 to 16 inch depth, reported 693 ppm PCBs.  
However, when this sample was re-extracted and re-analyzed, it reported a 144 ppm PCB concentration. The variability of analytical results at this sample point precludes a firm conclusion that the concentration exceeds 500 ppm.
- Only three (3) sample locations (Locations 1, 12 and 15) indicate PCB concentrations over 100 ppm.
- It is clearly feasible to remove the "spot" of sludge at sample Location 12 from the lagoon, separately from the remaining sludge. Should it become necessary. This ability to segregate sludge that contains a PCB concentration in excess of 500 ppm would allow a separate and/or different remedial method as compared to the method used for the remaining sludge.

- Comparison of the sludge's PCB concentration analytic results from the three laboratories, and the re-analysis by ETC, indicates a degree of variability. However, study of the data does show that high PCB results were present at sample Location 12 and re-analysis also showed relatively high concentrations. Low concentrations shown in the first analysis tended to be confirmed (Sample Location 9) by the re-analysis.

### 3.0 ASSESSMENT OF CONTAMINATED SOIL VOLUMES

3.1 Purpose of Contaminated Soil Volume Survey - Several estimates of the volume of contaminated soils underlying the French Limited Site have been developed during previous field investigations. These estimates were based on visual observation, limited analytical quantification of soil contaminants, and assumed decontamination objectives. The most recent lagoon boring program (1985) obtained gas chromatography/mass spectroscopy (GC/MS) analytical data for underlying soils. The data indicates that base/neutral priority pollutants, specifically polynuclear aromatics (PNAs), could be an acceptable indicator of contamination due to their mobility and persistence in the subgrade soil environment. The volume estimate reported in the 1985 Remedial Investigation Report was based upon an assumed decontamination objective of 1 ppm PNAs.

The purpose of this 1986 assessment is to develop additional soil contamination analytical data and use it, in combination with the existing data to update the underlying and surrounding contaminated soil volume calculation.

3.2 Scope of Contaminated Soil Volume Survey - Previous studies (lagoon borings and resistivity profiling) at the site have indicated that the permeable strata adjacent to the lagoon may be pathways of radial contaminant migration. To better define the extent of this migration, and thus better quantify

the contaminated soil volumes, samples from ten (10) borings located around the perimeter of the lagoon were collected to augment the analytical data base. Additionally, soil samples were taken during the installation of two (2) monitor wells (REI 10-3 and REI 11).

Due to the hydraulic pressures present in the subgrade sand zones, hollow stem auger equipment could not be utilized for advancing these borings, as was specified in the project work plan. Instead, rotary wash techniques were used. Soil samples were collected using split spoon and Shelby tube samplers on a continuous basis from the surface to the depth at which the confining clay stratum was encountered. Samples from each boring were selected for chemical analysis based upon a combination of visual inspection, HNU screening, and physical observation of stratum breaks between permeable zones and clay strata.

All samples for chemical analysis were placed into pre-cleaned 16 ounce wide-mouthed jars, refrigerated, and transported to the laboratory for analysis. Split samples were offered to the EPA for their independent analysis.

Following completion, each boring was pressure grouted to the surface with a cement/bentonite slurry and all drilling fluids and cuttings were placed into the lagoon. Logs of these borings are shown in Appendix 5. The locations of these borings and the monitor wells that were sampled are shown on Figure 3-1.

In addition to the 60 samples collected during the dike boring program, soil samples retained from the 1985 Field Investigation were analyzed to quantitatively identify some of the base/neutral (PNA) contaminants present. The location of these 1985 lagoon borings is also shown on Figure 3-1.

The volume of contaminated soil was calculated using base/neutral organics concentrations as the indicator parameter. Separate calculations were performed using 1, 10, 100 and 1000 ppm as the decontamination objective.

3.3 Soil Analysis - All samples were analyzed using standard GC/MS techniques for base/neutral priority pollutant compounds in soils.

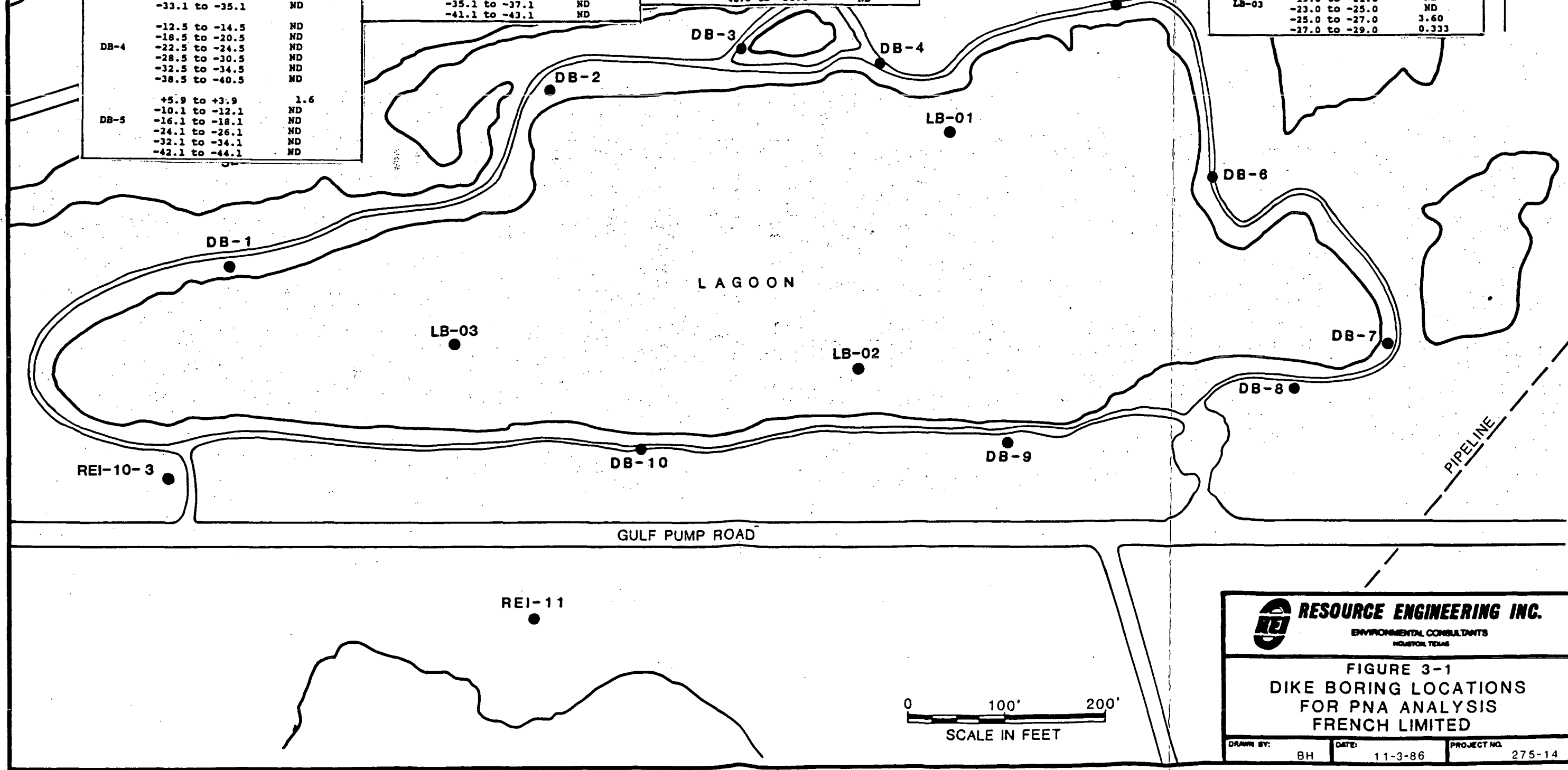
3.4 Contaminated Soil Volume Results - Analytical results of the subgrade dike soils and the retained samples from the 1985 lagoon boring program are shown on Figure 3-1. Laboratory reports for the contaminated soil analyses are provided in Appendix 6.

These data indicate that a large percentage of the soils which constitute the earthen dike have less than 1 ppm of base/neutral organic contamination (PNAs). Additionally, only two dike boring locations exhibited total base/neutral concentrations in excess of 10 ppm. The volumes of contaminated soil calculated in the 1985 Remedial Investigation report were based upon the assumption that all of the soils within the dike volumes were contaminated with organics over 1 ppm.



# SOIL CONTAMINATION ANALYSIS

BORING	SAMPLE DEPTH (Feet MSL)	PNA's (ppm)	BORING	SAMPLE DEPTH (Feet MSL)	PNA's (ppm)	BORING	SAMPLE DEPTH (Feet MSL)	PNA's (ppm)	BORING	SAMPLE DEPTH (Feet MSL)	PNA's (ppm)	BORING	SAMPLE DEPTH (Feet MSL)	PNA's (ppm)
DB-1	-14.7 to -16.7	ND	DB-6	+2.2 to +0.2	ND	DB-9	-17.3 to -19.3	4.9	REI-11	-18.1 to -20.1	ND	LB-01	-12.4 to -13.9	0.459
	-18.7 to -20.7	0.84		-13.8 to -15.8	0.07		-25.3 to -27.3	0.25		-22.1 to -24.1	ND		-13.9 to -15.9	1.148
	-26.7 to -28.7	ND		-23.8 to -25.8	ND		-31.3 to -33.3	2846.5		-38.1 to -40.1	0.67		-15.9 to -17.9	1.257
	-30.7 to -32.7	0.64		-33.8 to -35.8	ND		-39.3 to -41.3	.5		-40.1 to -42.1	1.54		-17.9 to -19.9	1.521
	-42.7 to -44.7	ND		-37.8 to -39.8	ND									
DB-2	-46.7 to -48.7	ND	DB-7	-12.5 to -14.5	ND	DB-10	-14.1 to -16.1	0.48				LB-02	-16.5 to -18.5	1650.000
	-14.6 to -16.6	ND		-24.5 to -26.5	ND		-20.1 to -22.1	0.60					-20.0 to -21.5	2.066
	-20.6 to -22.6	0.52		-28.5 to -30.5	ND		-28.1 to -30.1	2.0					-22.0 to -23.5	4.097
	-24.6 to -26.6	ND		-32.5 to -34.5	ND		-36.1 to -38.1	ND					-24.0 to -25.5	1.182
	-30.6 to -32.6	ND		-42.5 to -44.5	ND								-27.5 to -29.0	ND
DB-3	-34.6 to -36.6	ND	DB-8	-13.1 to -15.1	ND	REI 10-3	+10.4 to +12.4	271					-29.0 to -31.0	0.462
	-15.1 to -17.1	ND		-19.1 to -21.1	ND		-9.6 to -11.6	2.4					-31.0 to -32.5	0.462
	-29.1 to -31.1	ND		-21.1 to -23.1	4.08		-14.6 to -16.6	2.0				LB-03	-15.0 to -17.0	1.342
	-31.1 to -33.1	ND		-35.1 to -37.1	ND		-24.6 to -26.6	0.7					-17.0 to -19.0	ND
	-33.1 to -35.1	ND		-41.1 to -43.1	ND		-34.6 to -36.6	0.6					-19.0 to -21.0	ND
DB-4	-12.5 to -14.5	ND					-48.6 to -50.6	ND					-23.0 to -25.0	ND
	-18.5 to -20.5	ND											-25.0 to -27.0	3.60
	-22.5 to -24.5	ND											-27.0 to -29.0	0.333
	-28.5 to -30.5	ND												
	-32.5 to -34.5	ND												
DB-5	-38.5 to -40.5	ND												
	+5.9 to +3.9	1.6												
	-10.1 to -12.1	ND												
	-16.1 to -18.1	ND												
	-24.1 to -26.1	ND												
	-32.1 to -34.1	ND												
	-42.1 to -44.1	ND												



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**FIGURE 3-1**  
**DIKE BORING LOCATIONS**  
**FOR PNA ANALYSIS**  
**FRENCH LIMITED**

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The 1986 estimates of the contaminated soil volumes were made based on decontamination objectives of 1, 10, 100 and 1000 ppm. The calculations for each of the four cases were made by utilizing the known dimensions of the lagoon, and the depth of contaminated soil as determined from the soil analysis data. Detailed calculations for the four cases are provided in Appendix 7.

The results of these calculations are summarized in Table 3-1 as follows:

Table 3-1  
Estimated Contaminated Soil Volumes

<u>Decontamination Objectives (ppm-PNAs)</u>	<u>Volume (cubic yards)</u>
1 ppm	267,000
10 ppm	51,000
100 ppm	35,400
1000 ppm	25,500

These estimates show a 523% decrease in the volumes of contaminated soil when the decontamination objective is increased from 1 ppm to 10 ppm. The relative difference in contaminated soil volumes is still significant (60% decrease) when the decontamination objective is raised from 10 ppm to 100 PNAs. A 72% decrease occurs when the decontamination objective is raised from 100 ppm to 1000 ppm PNAs.

The significance of choosing a decontamination objective on the volume of contaminated soils is illustrated in the contaminated soil volume table (Table 3-1). Typical choices for PNA decontamination objectives (i.e., 100 or 1000 ppm) has a relatively insignificant impact on the volume of soil considered to be "contaminated."

#### 4.0 ALLUVIAL REMNANT ASSESSMENT

4.1 Purpose - The purpose of the Alluvial Remnant Assessment Task in the French Limited site 1986 Field Investigation Program was to identify the extent and configuration of alluvial remnant material separating the waste lagoon and the Riverdale water supply wells. The study also assesses the impact of the alluvial remnant material on the hydraulic connection between the shallow aquifer in these two locations.

Subsurface field investigation programs conducted at the French Limited site have produced much information describing the shallow geology (< 50 feet) immediately adjacent to the waste lagoon; however, the details of that geologic data base decrease significantly outside the immediate vicinity of the lagoon.

A previous interpretation of the depositional history within the alluvium tentatively suggested that there may be two geologically recent, parallel, alluvial channels segregated by an older, less permeable, alluvial remnant deposit. This tentative interpretation, based upon limited stratigraphic and soil property data, suggested that this remnant deposit could possibly provide a natural containment and migration barrier between the French Limited site's lagoon and the Riverdale water well locations. The 1986 assessment task is designed to augment the geologic data base of the area between the lagoon and Riverdale, and to accurately describe the alluvial remnant

materials structure. The interpretive tools used to delineate the remnant's configuration and structural extent included cone penetrometer soundings, soil confirmation borings, electric borehole geophysics and geotechnical soils analysis.

#### 4.2 Procedure

4.2.1 Phase I - The first phase of the alluvial remnant material's assessment consisted of a cone penetrometer survey of twenty-eight (28) soundings (CPT-1 through CPT-28) set on three traversals between French Limited and Riverdale. The locations of the penetrometer soundings are shown on Plate 2 in Attachment 2. Each sounding was pushed to a depth of 70 feet, or until cone refusal, and was pressure grouted upon completion of the penetration. Subsequent sounding locations were selected by inferring the lithology from the computerized field reports of sleeve friction and tip resistance. These were plotted on the computer housed inside the cone penetrometer truck.

4.2.2 Phase II - The second phase of the assessment program consisted of installing eight (8) confirmation borings (R-1 through R-8). These borings were placed adjacent to cone sounding locations to provide validation of the inferred lithologic materials and to obtain soil samples for geotechnical analysis. See Plate 2 in Attachment 2 for the boring locations. A mud rotary drilling rig, using a potable water and bentonite powder as a mud, was used to advance the

borings. Each boring was continuously sampled, visually logged and electric logged, (resistivity, spontaneous potential, gamma and neutron) to a depth of 60 feet. All borings were pressure grouted with a cement-bentonite slurry on completion of the geophysical logging. The visual description of each confirmation boring, its geophysical log, and nearest cone sounding log are presented in Appendix 8. The confirmation boring and its corresponding cone penetrometer sounding are as follows:

<u>Cone Sounding</u>	<u>Corresponding Confirmation Borings</u>
CPT-10	R-1
CPT-2	R-2
CPT-4	R-3
CPT-6	R-4
CPT-17	R-5
CPT-18	R-6
CPT-21	R-7
CPT-24	R-8

The logs for all the cone penetrometer soundings (CPT-1 through CPT-28) are shown in Appendix 9.

Soil samples were retained while drilling the confirmation borings and analyzed for their appropriate geotechnical properties. Sandy soils were sieved to determine their grain size; clays and silts were analyzed by direct shear analysis and Atterberg limit determinations. The geotechnical test reports are presented in Appendix 10.

4.2.3 Phase III - In the third phase of the program, four piezometers (MR-1 through MR-4) were installed in the upper alluvial sand, with the mud rotary drilling rig. The locations of these piezometers are shown on Plate 2 in Attachment 2. The piezometers were constructed of 4-inch flush-jointed PVC Schedule 40 pipe with a Triloc 0.010-inch slotted screen. The top of each casing was notched to provide a common reference point for water level measurements and surveyed for its elevation to Benchmark NGS #S109, 1984. Construction details for each piezometer are presented in Appendix 11. The purpose of the piezometers was to allow water level measurement in the uppermost aquifer at points in the alluvial deposit area. These water level readings were then used in assessing the degree of hydraulic separation across the alluvial remnant material.

4.3 Results - Since a predominantly clay formation such as the Beaumont is subjected to subareal dessication and compaction, its soil properties change. Although the Beaumont may be the parent material for the alluvial remnants, the alluvial material has been reworked, winnowed, and placed in a different depositional environment than its parent formation. Using this hypothesis, one possible method to identify the contact between the Beaumont formation and the overlying clay soils or remnant material is to examine the cone penetrometer and geophysical logs for baseline shifts. Baseline shift

occurs when the physical and qualitative properties of a unit are markedly different from those of an adjacent unit, even though the units may be lithologically similar.

Cone penetrometer sounding traversals were set along Gulf Pump Road, along Hickory Street in Riverdale, and on a north-south line tangent to GW-02 and GW-07, as shown on Plate 2 in Attachment 2. Cross-sections based on interpretations of the sounding traces, using baseline shifts and confirmation borings as correlation aids, are shown in Figures 4-1, 4-2 and 4-3.

By compiling the information from the cone penetrometer survey, the confirmation borings, the geotechnical tests, and the data from previous investigations, a more detailed interpretation of the extent and configuration of the alluvial remnant material can be made. An interpretation of the cross-sections constructed from the cone penetrometer soundings suggests that parallel alluvial channels "etch" the surface of the Beaumont clay as they increase both their sinuosity and meandering across the eroded peneplain. Between these channels exist older alluvial deposit remnants. These deposit remnants consist of reworked clay alluvium which uncomfortably overlies the Beaumont formation and is incised by minor sand channels. The minor channels move eastward as the sinuosity of the oxbow channel increases. These channels were later covered with silt and clay when the oxbow was starved by the meandering stream. A careful analysis of the cone







WEST  
C

EAST  
C'

CPT-27  
EL. 17.75' (MSL)

CPT-26  
EL. 17.54' (MSL)

CPT-25  
EL. 19.09' (MSL)

CPT-24  
EL. 16.54' (MSL)

CPT-23  
EL. 16.14' (MSL)

CPT-22  
EL. 15.03' (MSL)

CPT-21  
EL. 14.69' (MSL)

ELEVATION IN FEET (MEAN SEA LEVEL)

20  
10  
0  
-10  
-20  
-30  
-40  
-50  
-60

20  
10  
0  
-10  
-20  
-30  
-40  
-50  
-60

SAND

SAND

CLAYEY SAND

CLAYEY SAND

CLAY/  
SILTY CLAY

CLAY/SILTY CLAY

CLAY

SILTY CLAY

SAND

SILTY CLAY  
SANDY SILT

SILTY CLAY

SANDY SILT

SILTY SAND

SANDY SILT  
CLAYEY SAND

SILTY CLAY

CLAY

SILTY SAND

CLAYEY SILT

CLAYEY SILT

SILTY CLAY

SILTY SAND

SILTY CLAY

SANDY SILT

SILTY CLAY

SANDY SILT

SILTY SAND

CLAYEY SAND

CLAYEY SILT

SILTY SAND

CLAYEY SAND

CLAYEY SILT

CLAYEY SAND

CLAYEY SILT

CLAYEY SAND

SILTY CLAY

SILTY CLAY

SILTY CLAY

0 60 120  
HORIZONTAL SCALE (FEET)

NOTE: Lithology inferred from cone penetrometer soundings and confirmation borings of The 1988 Field Investigation.



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FIGURE 4-3  
1986 FIELD INVESTIGATION  
CROSS SECTION C-C'  
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CHK'D BY:

DATE: 11-25-86  
REVISED:

PROJECT NO: 275-14  
DWG. NO:

penetrometer sounding traces confirm the geologic makeup of the material above the Beaumont clay is a complex assembly of interfingered sand and clay-based materials. Although the material encountered at CPT 10 (adjacent to GW-02 and GW-27) confirmed boring logs from previous investigations, the geometry of the remnant as previously interpreted could not be confirmed. The composition of the material at -15 to -50 MSL has clay as a major component at some cone penetrometer sounding points, however, the clay content of this zone varies both in thickness and continuous areal extent.

Geotechnical tests performed on the soil samples retained from the confirmation borings indicate the alluvial remnant material is of a different grain size and composition from the underlying Beaumont formation. The alluvial remnant material is coarser and has a lower liquid limit, plastic limit, and plasticity index than the Beaumont clay material. Grain size analysis of sand taken from a confirmation boring (R-8) in Riverdale showed the sand to be finer and more silty than sand taken from a different channeling event which occurred across the bulk of the remnant material near the French Limited site (R-2 and R-3). A summary of the geotechnical testing results for each sample interval are listed in Table 4-1, and complete test reports are shown in Appendix 10.

TABLE 4-1

ALLUVIAL REMNANT MATERIAL  
SUMMARY OF GEOTECHNICAL ANALYSIS DATA

French Limited Sand

<u>Boring</u>	<u>Depth (ft.)</u>	<u>#60 Sieve % Retained</u>
R-2	8-10	91.2
R-2	10-12	94.9
R-3	4-6	62.6
R-3	14-16	70.8

Riverdale Sand

<u>Boring</u>	<u>Depth (ft.)</u>	<u>#60 Sieve % Retained</u>
R-8	4-6	40.8

Alluvial Remnant Material

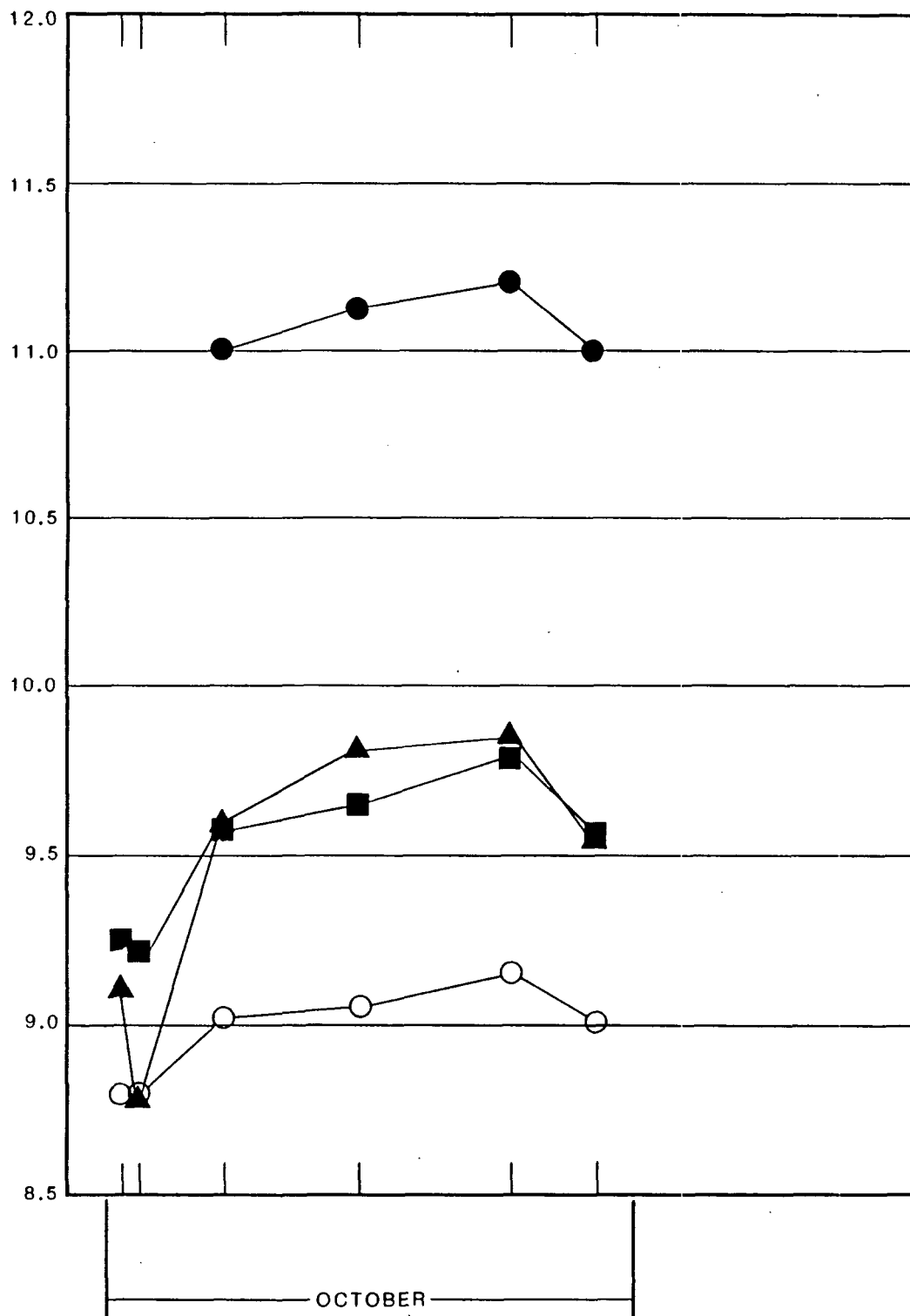
<u>Boring</u>	<u>Depth (ft.)</u>	<u>Liquid Limit</u>	<u>Plastic Limit</u>	<u>Plastic Index</u>	<u>% Less Than #200</u>
R-2	22-24	49.5	16.8	32.7	20.3
R-2	38-40	-	-	-	25.0
R-3	22-24	41.0	15.7	25.3	-
R-3	34-36	25.2	13.9	11.3	47.0
R-8	22-24	41.5	15.2	26.3	-
R-8	40-42	24.0	15.7	8.3	35.1

Beaumont Clay Upper Contract

<u>Boring</u>	<u>Depth (ft.)</u>	<u>Liquid Limit</u>	<u>Plastic Limit</u>	<u>Plastic Index</u>	<u>% Less Than #200</u>
R-2	48-50	-	-	-	20.5
R-3	46-48	66.0	27.4	38.6	-

A study of the near surface sand deposits in the French Limited alluvial zone indicates there is an unconfined sand with up to two buried artesian channel sands. All sands above the Beaumont Formation appear to have a weak hydraulic connection. This connection is illustrated by the hydrograph of the water levels of the four Riverdale piezometers. (See Figure 4-4). The water levels of these four piezometers were affected in a similar fashion by atmospheric events such as rainfall, drought, and barometric pressure over the period of measurement in October, 1986. Piezometer MR-1 (total depth, 8 feet) was set near GW-07, a well screened in the upper permeable zone (14 to 24 feet below surface) to determine whether the sand seam detected on cone penetrometer traces yielded a change in hydrostatic head. Preliminary water level readings have shown a difference in head of at least two feet between the two wells. (See Figure 4-5.)

4.4 Conclusions - Clay material found approximately 20 feet below the surface may have originated from the Beaumont Formation; however, it has been reworked and mixed with sand to such an extent that it does not retain compositional qualities of the parent formation. Although the methods and



10-1 CLUSTER PUMP TEST 10/04/86 - 10/14/86

MSL (T.O.C.)

- MR-1 18.75
- ▲ MR-2 13.28
- MR-3 11.69
- MR-4 12.45



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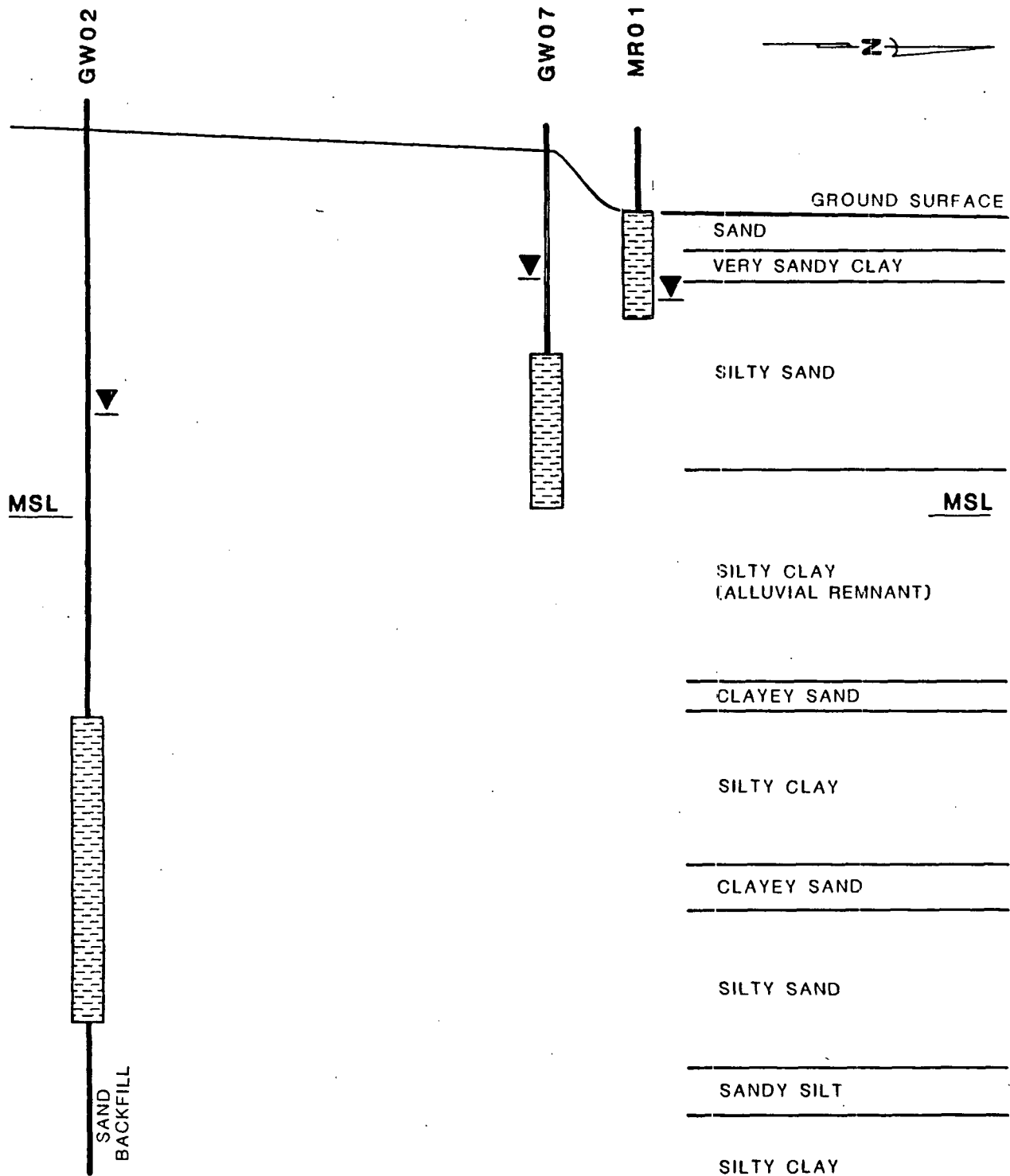
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**FIGURE 4-4**  
**HYDROGRAPHS RIVERDALE**  
**PIEZOMETERS (OCTOBER, 1986)**  
**FRENCH LIMITED**

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DATE: 11/6/86

PROJECT NO. 275-14-06



STRATIGRAPHY GENERALIZED FROM  
CONFIRMATION BORING R-1,  
ADJACENT TO CPT 10.



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FIGURE 4-5

WATER LEVELS - 10/29/86

FRENCH LIMITED

DRAWN BY: RLS

DATE: 11/5/86

PROJECT NO. 275-14-06



characteristics of the deposition of the alluvial remnant material represent a standard geologic model for a fluvial system, the discontinuous configuration of the material is not adequate to provide an absolute unqualified lateral migration barrier between French Limited and Riverdale. The presence of this material and other interspersed clay, sand, and silt seams does provide localized, hydraulic separation. Supply wells in the shallow alluvium (less than 50 feet) would have to overcome these localized anomalies with an extremely high pumping rate, over an extended period to induce water from the French Limited site into the Riverdale home supply wells.

## 5.0 DEEP AQUIFER HYDROGEOLOGY ASSESSMENT

5.1 Purpose - The existence of a confining aquitard beneath the French Limited Lagoon, that would hydraulically isolate the alluvial zone from the regional Deep Aquifer, is important in evaluating several potential remedial alternatives for the site. Previous geologic investigations have suggested that such an aquitard exists, and that its hydraulic integrity will prevent the vertical migration of contamination away from the site. However, these previous investigations also detected trace level contamination in the regional Deep Aquifer below the site. The presence of this trace contamination suggests that hydraulic communication exists across the aquitard, from either artificial penetrations or natural migration.

Review of the data base from previous investigations led EPA, and the French Limited PRP Group, to conclude that a 1986 Field Investigation should be performed to:

- First, supplement the existing geologic data base by performing a series of pumping tests designed to provide a positive "stress" test of the aquitard's hydraulic integrity in the area of the French Limited site. Additionally, while performing these pumping tests, data would be collected for calculation of the deep aquifer's hydraulic characteristics.

- Second, implement a program of ground water analysis designed to identify the source of trace contamination in the deep aquifer.

The purpose of these investigations would be to assess the integrity of the aquitard underlying the French Limited Site.

5.2 Scope - The investigative tasks performed during the deep aquifer hydrogeology assessment are summarized as follows:

1. Before performing the pumping tests, it was necessary to remove and seal an existing well known as the "Murphy Well." This well had been discovered previously, near an abandoned structure on the Murphy property, and was suspected of being a source of vertical hydraulic communication across the aquitard.
2. A second Deep Aquifer pumping test, referred to as the "REI-3 Cluster" test, was performed utilizing a pumping well located approximately 650 feet down gradient (south) of the French Limited Lagoon's southern shore. This was also an extended run test (3 days) designed to measure the aquitard's vertical hydraulic integrity at that location. Data were also collected for calculating Deep Aquifer characteristics.

3. The Deep Aquifer pumping test referred to as the "REI-10 Cluster" test was performed utilizing a pumping well located approximately 75 feet south of the French Limited Lagoon's southern shore. This downgradient location adjacent to the lagoon was utilized to perform an extended duration (7 day) "stress test" of the aquitard's vertical hydraulic integrity. Additionally, during the test, data were obtained for calculating Deep Aquifer characteristics.
4. During an initial attempt to perform the "REI 10 Cluster" Deep Aquifer pumping test, an anomaly was observed in the shallow aquifers hydraulic response. After review and further investigation, it was concluded that the nearby artificial penetration (Monitor Well GW-25) should be removed and sealed before proceeding with the test.
5. A third Deep Aquifer pumping test identified as the "REI-12 Cluster" test, was planned utilizing a pumping well located north of Highway 90. This upgradient test was designed to stress the aquitard while observing the shallow aquifer for evidence of vertical hydraulic communication. This test was not

performed as described in the work plan. Review of the results from the REI 10-1 Run #2 Test, and the preliminary drawdown test performed on REI 12-1 concluded that this upgradient test would not greatly supplement the data already obtained from the preceding tests, so the test was eliminated.

6. Groundwater potentiometric maps of the French Limited site's Deep Aquifer were prepared using water level data from a network of old, as well as newly installed monitor wells. Two maps were prepared based on data obtained on two separate dates. The maps show the Deep Aquifer groundwater gradient, and "mounding" effects that exist in the area.
7. Groundwater samples were collected from six (6) monitor wells, and analyzed for contaminant concentrations by (GC/MS). Results from these analyses provided data to support final determination of Deep Aquifer contamination levels, and to help identify contaminant migration pathway into the Deep Aquifer.

A complete description of the activities, approach, procedures utilized, and results obtained from these investigations are described in the following sections of this report.

5.3 Murphy Well Removal - The 1985 Field Investigations Scope of Work included a pumping test of the Deep Aquifer utilizing a well (REI 3-4) located approximately 650 feet south of the French Limited Lagoon's southern shore. Results of this test indicated a potential boundary condition or source of artificial recharge near the pumping well. Investigation identified an abandoned water well northeast of REI 3-4 on the Murphy property. See Plate 1 in the Attachment 1 for location. The well was found beneath vegetation and rubble from the original structure on the property. The well was constructed of 3-inch galvanized steel pipe cut off beneath the surface of a small concrete pad. No grout material was in evidence at the surface of the well, and the concrete pad was not functioning as a surface seal.

The down-hole portion of a jet-pump was removed from the well without difficulty, and a cased-hole electric log was run to identify potential problems that might be encountered during removal of the well.

The well casing was pulled using conventional water well workover equipment. One hundred ninety (190) feet of 3-inch galvanized casing and ten (10) feet of 3-inch stainless

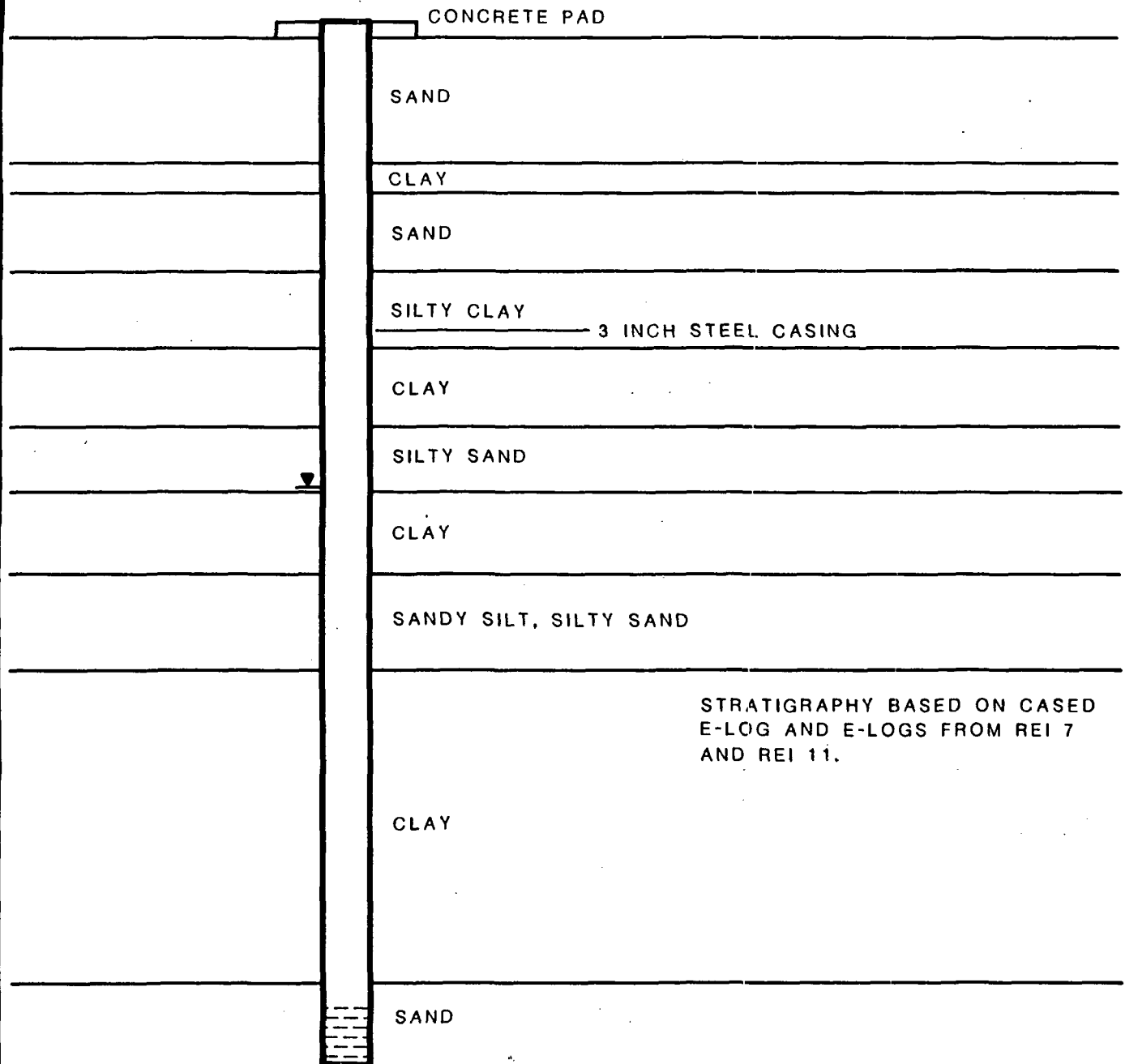
steel screen were removed from the well bore. Close observation during removal of the casing found that no cement or grout adhered to the piping. The borehole was reamed to an 8-inch diameter with a rotary wash rig to a depth of 205 feet. Again, no evidence of grout was observed during the drilling process. The borehole was then pressure grouted to the surface using tremie rods and a neat cement. Following settling, additional cement was added to seal the borehole to the surface. Figure 5-1 illustrates the construction of the Murphy well as it was found before removal.

5.4 Installation of Piezometers and Monitor Wells - The objectives for the design and installation of the piezometers and monitor wells of the 1986 French Limited Field Investigation were two-fold:

1. Design a program of wells to add geologic data between the surface and the Deep Aquifer in and about the French Limited Site;

2. Design and construct a series of shallow wells and piezometers to test the ability of a given clay layer (-67 to -80 MSL) to act as an aquitard beneath the French Limited Lagoon. See Plate 1, field investigation map, in Attachment 1 for the location of all monitor well and piezometers.

5.4.1 Deep Aquifer Monitor Well Installation - The Deep Aquifer monitor well installation program consisted of adding three monitor wells (REI 10-1, REI-11, and REI 12-1) to



STRATIGRAPHY BASED ON CASED  
E-LOG AND E-LOGS FROM REI 7  
AND REI 11.

JET PUMP AT SURFACE

WATER LEVEL TAKEN 05/28/86

TOP OF SCREEN 190 FT. BELOW GRADE  
BOTTOM OF SCREEN 200 FT. BELOW GRADE

SLOT SIZE UNKNOWN

WELL REMOVED FROM SERVICE 07/07/86

VERTICAL SCALE : 1"=30'

CASING PULLED, 8 INCH BORE OVER-REAMED  
TO 205 FT., BORE PRESSURE GROUTED  
THROUGH RODS



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FIGURE 5-1

MURPHY WELL CONSTRUCTION

FRENCH LIMITED

DRAWN BY: RLS

DATE: 11/5/86

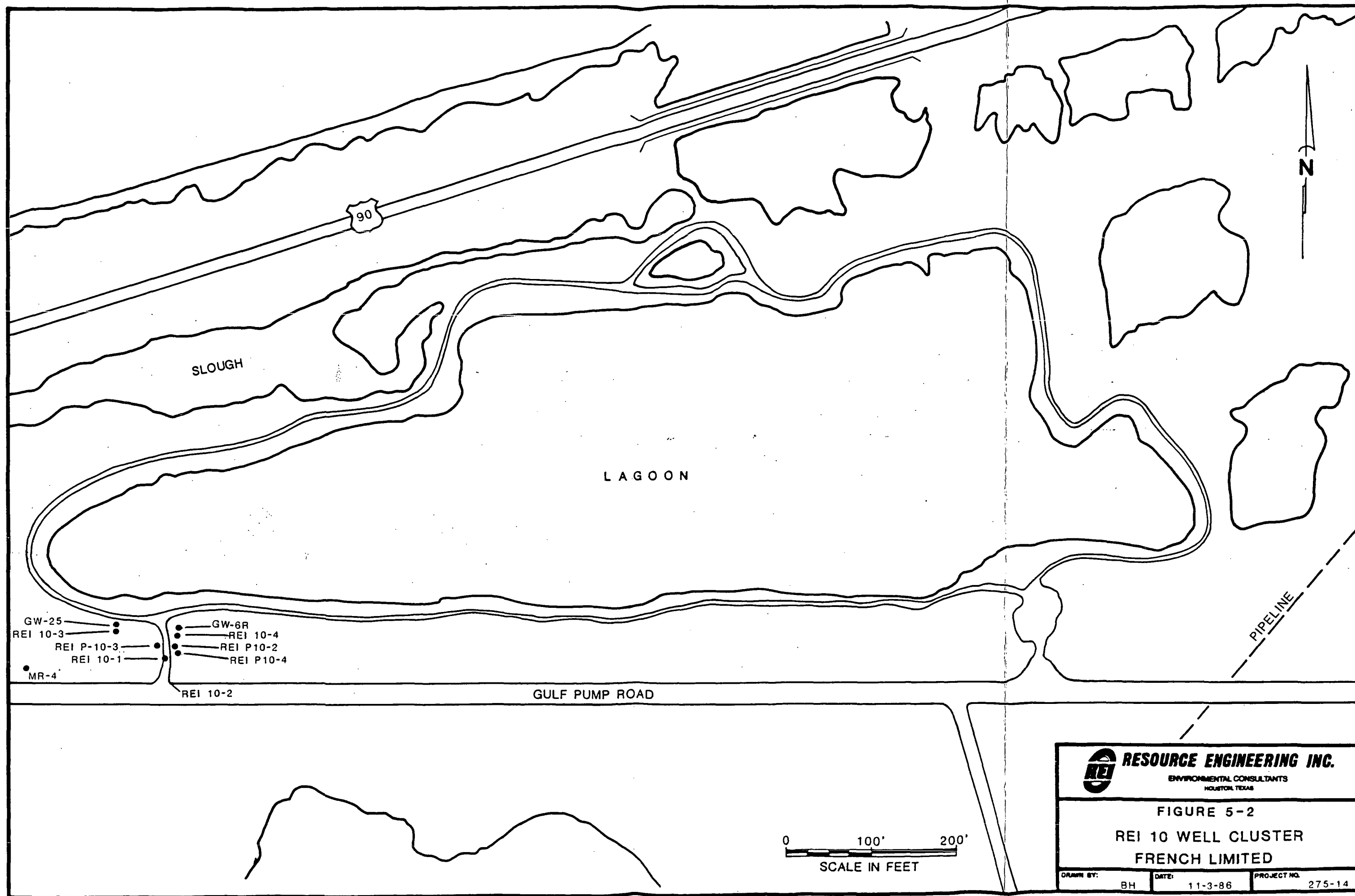
PROJECT NO. 275-14-06




the four monitor wells which existed at the start of the 1986 Field Investigation (GW-12, GW-25, REI 3-4, REI 7). The locations of these new wells were selected to provide information for potentiometric maps and to provide optimal spacing distances for the pumping tests performed during the investigation.

Each monitor well bore was advanced with a mud rotary drilling rig, using bentonite powder and potable water as a drilling mud. Monitor wells and piezometers in the REI 10 cluster (see Figure 5-2 for location) required the addition of coarse mica as a fluid circulation loss additive, due the head generated by the French Limited lagoon and the coarseness of the material encountered while drilling. An eight (8) inch surface casing was pushed to the first significant clay layer and grouted in place. The drilling fluid from the upper formations was pumped into 55 gallon drums for return to the French Limited Lagoon, prior to advancing a smaller diameter hole for installation of the monitor well. Each monitor well was constructed of four (4) inch flush jointed schedule 40 Triloc PVC blank and 0.010-inch Triloc PVC screen. Each screen length was custom cut in the field, so only the discrete permeable zone was screened.

5.4.2 Shallow Aquifer Monitor Wells and Piezometer Installation - The REI 10 cluster of monitor wells and piezometers was designed to test the degree of vertical



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<b>FIGURE 5-2</b> <b>REI 10 WELL CLUSTER</b> <b>FRENCH LIMITED</b>		
DRAWN BY:	DATE:	PROJECT NO.
BH	11-3-86	275-14

hydraulic connection between the zone of French Limited alluvium and the Deep Aquifer. Three shallow monitor wells (REI 10-2, REI 10-3, and REI 10-4) were placed near REI 10-1 in the third shallow sand zone below the surface, resting on the first significant clay (approximately -34 feet MSL). Each monitor well was constructed of four (4) inch flush jointed Triloc Schedule 40 PVC, 0.010-inch slot screen and casing. Temporary 10-inch casing was used while drilling, in addition to circulation loss materials (MICA), to minimize excessive sloughing in the bore while drilling.

The three piezometers installed to characterize the qualities of the aquitard (REI P10-2, REI P10-3, and REI P10-4), were advanced to the first massive, low silt, clay (approximately -67 MSL). Six (6) inch flush jointed PVC surface casing was pushed to that depth and grouted in place. Drilling fluids were removed from the casing with an air compressor and the remainder of the bore (2 to 12 feet) was advanced using only potable water as a drilling fluid. Each piezometer has two (2) feet of open screen and is positioned at a different interval in the clay or in the first two(2) feet of the silt directly below the clay. Soil compaction test results from this clay interval are presented in Appendix 10. The REI-12 cluster of wells was designed to test an area north of Highway 90 for hydraulic connection between the alluvium and the Deep Aquifer. One shallow monitor well, (REI 12-2) was

placed near REI 12-1 Deep Aquifer well to support this test. Installation and construction was similar to the shallow wells, as described above.

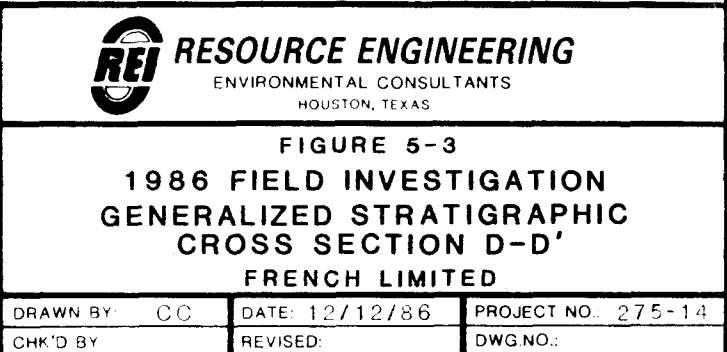
All monitor well construction logs (with the well elevation survey) and geophysical logs are presented in Appendices 12 and 13, respectively.

5.4.3 Monitor Well Development - The shallow and deep aquifer wells were developed by using a submersible pump. Conductivity, pH, and temperature readings were taken after the removal of each volume of development water until the readings stabilized. Step drawdown tests were performed on new pumping wells (REI 10-1 and REI 12-1), to estimate the pumping rate and the ability of the formation to recharge after the stress of pumping. See Appendix 23 for description of the pumping test step drawdown data that resulted from these tests.

5.4.4 Monitor Well Post-Construction Analysis - Information gathered during the design and construction of the 1986 Field Investigation Monitor Wells was integrated with data generated from previous Deep Aquifer investigations. Geophysical logs from those previous investigations are included in Appendix 13.

A cross-section diagram depicting the stratigraphy across the site is presented as Figure 5-3. This diagram is an interpretation of geophysical spontaneous potential and resistivity traces logged from bores penetrating the Deep Aquifer prior to setting a monitor well.

D'



Common procedure, field equipment, installation details, measuring methods, and other activities are described as follows:

5.5.1 Pretest Activities - The pumping tests were performed utilizing newly installed monitor wells, in addition to wells installed during previous investigations. These new wells were developed using a submersible, electric-driven pump following procedures described in the French Limited Site Investigation Report of June, 1986.

The flow rate to be used during each pumping test was selected based on review of drawdown test data, preliminary pumping test data; or data from the 1985 Field Investigation. The selected flow rate was picked to provide balance among the various test objectives. These objectives consisted of 1) maintaining a constant flow rate throughout the test; 2) avoiding "cavitation" or breaking suction" on the pump; and 3) maximizing hydraulic "stress" on the aquitard during the available test duration. Proper balancing of these factors supported achievement of the test objectives to evaluate potential connection between the Shallow Alluvial zone and the Deep Aquifer, and to obtain data for calculation of Deep Aquifer characteristics. Pumping flow rate information from previous investigations was also used in making the test flow rate decision.

Pumps were installed by REI personnel, or by subcontractors supervised by REI. The pump installation was designed to minimize addition of artifactual constituents to the wells. Dedicated hoses and polypropylene rope were secured together with nylon ties for the REI 3-4 cluster test pump. The large volume pump necessary for the REI 10 cluster test was installed, and suspended on 2-inch PVC pipe. New disposable PVC gloves were used to handle the equipment while lowering pumps into the wells. A flow meter was installed in the pump discharge piping, after each pump installation.

An In-Situ, Inc. Hydrologic Analysis System-Model SE-200 computer was utilized to monitor and record the water levels in observation wells during the tests. This system is a fully automated data acquisition system that utilizes pressure transducers as the water level detection devices. A detailed description of the In-Situ SE-200 computer system and the pressure transducers is provided in the In-Situ Operating Manual Information shown in Appendix 15. Each In-Situ pressure transducer was installed after first measuring the depth to static water level from the well's casing datum. This measurement was made to the nearest 0.01 feet, and documented with the well number in the field logbook, together with the transducer's serial number, scale factor, and range. The transducer was lowered into the well while measuring its cable length, again to the nearest 0.01 feet. The 50 pounds

per square inch gauge (PSIG) range transducers used on the Deep Aquifer wells were installed from 40 to 50 feet below static water surface, as measured from the well datum. The 10 PSIG range transducers utilized on the shallow Alluvial zone wells were installed 10 to 12 feet below static water surface, as measured from the well datum. The transducer cable was secured to the well casing using tape, and its final installed depth recorded in the field logbook.

The well opening was covered to prevent entrance of precipitation. The transducer cable was color coded to ensure proper well identification, and routed to the In-Situ SE-200 computer for connection to the selected data recording channel. The transducer installed in a pumping well was suspended inside a 3/4-inch PVC pipe, which in turn was suspended in the well to minimize turbulence effects on the measurement. The transducer for wells having potential water contamination was placed in 3/4-inch PVC pipe; a special stainless steel connector was used to seal the transducer and its cable. This prevented well water contact with the transducer and cable, except for the transducer sensing tip, which protruded through the special connector and was coated with a Teflon/Silicone grease.

Background water level measurements from each observation well involved in the pumping test were recorded using both manual measuring methods and the In-Situ SE-200



computer. Fluctuations in these levels were monitored to document natural fluctuations in the zones observed and to determine when the water-bearing zones of interest had equilibrated after artificial disturbances caused by previous pumping tests or drilling activities. A Weather-Measure Metrograph with a 7-day reading drum graph was used to record temperature, relative humidity, and barometric pressure. This metrograph was maintained during all phases of the tests, including the background, drawdown, and recovery phases.

5.5.2 Test Execution - Upon the start of the drawdown phase of the test the flow rate was monitored constantly for the initial 2 to 3 hours. These flow rate readings were recorded every 5 to 10 minutes on the appropriate field data sheets. Adjustments were made to maintain the flow rate to within 10% of the selected test design rate. Correct flow rates were usually achieved in less than 1 minute after the start of each test. After the initial 3 hours, Flow meter readings were documented every 15 to 30 minutes through the remainder of the test.

Flow rates were maintained constant if possible, for a minimum of 12 hours after initiating the test, to maximize reliability of the data used for quantifying aquifer characteristics. After the initial 12 hours, flow rates were reduced to prevent pump cavitation due to breakage of pump suction in the pumping well, if it became necessary.

During the pumping test, water levels in the wells were measured and recorded by the In-Situ SE-200 computer using its preprogrammed logarithmic data recording schedule. This schedule is:

Interval Between Measured Water Levels	Aquifer Test Elapsed Time
1 second .....	0 to 10 seconds
5 seconds .....	10 to 60 seconds
20 seconds .....	1 to 10 minutes
2 minutes .....	10 to 100 minutes
20 minutes .....	100 to 1000 minutes
60 minutes .....	1000 to 10000 minutes
200 minutes .....	10000 to 99999 minutes

The computer also provides an option for collecting data at shorter intervals for one well. The computer was programmed to designate the pumping well for this special treatment option in all of the tests.

Manual water level measurements taken and recorded periodically throughout the test provided a quality assurance cross-check of the quality of data recorded by the computer system. A Well Wizard Series 6000 well sounder was used to collect the manual measurements. This instruments inherent design accuracy is to 0.01 feet.

As the pumping test progressed, the various test data were monitored and evaluated for conditions which would require adjustments in test conditions or procedure. The

data that were monitored included comparison of the manual water level measurement with the computer data, and computer-plotted well level drawdown curves.

The In-Situ computer data and the manual water level measurements were continued during the "Recovery" phase of the test, after the pump was shut off. The In-Situ computer program was reset to the beginning of its preprogrammed data recording schedule so that early, crucial recovery data could be recorded at a frequent interval. Water level monitoring during the recovery phase was continued until sufficient data was obtained for determination of aquifer characteristics.

5.5.3 Post-Test Activities - After completion of the recovery phase, the field test activities were concluded and the In-Situ computer removed to the office for unloading the test data tapes. The computer's data were compared to manual level readings as a quality control check to ensure its accuracy. This comparison included plotting manual measurements and computer measurements on log-log and semi-log paper to determine if the resulting response curves indicated significant differences. When significant variances were noted, records were studied for indications of equipment failure, and measurement or transcription error. To minimize transcription errors, data tapes from the In-Situ SE-200 computer were loaded directly into a Lotus spreadsheet PC program to perform the repetitive calculations efficiently and accurately.

The required range of aquifer characteristic values was calculated using several methods and, after all graphical methods and calculations had been completed, they were checked for accuracy by a second person.

The data were then hand plotted on both log-log and semi-log Keuffel and Esser (K+E) graph paper for analysis. Due to the voluminous nature of the data generated, it was practical for only certain data to be plotted. The plots were then checked for accuracy.

The two methods of analysis for the drawdown data were the Theis non-equilibrium solution (Theis, 1935; Heath and Trainer, 1981) and the time vs. drawdown modification to Theis' non-equilibrium solution by Cooper and Jacob (Driscoll, 1981). The recovery data were also analyzed by both of these methods, using the assumption of Theis' Correlary, and the residual drawdown plot solution (after Driscoll). For the log-log plots, the resulting curves were matched using a reverse type curve provided in the U.S. Department of Interior: Ground Water Manual, A Water Resources Technical Publication, 1981; (Figure 5-5). This type curve was used instead of a leaky type curve (e.g., after Walton, Theis) because most of the curves generated from the data were non-leaky. Only that portion of the curve plot considered to be applicable was utilized in the hydrogeologist's interpretation of where curves matched the type curve.

Similarly, for the semi-log plots, only the representative data were utilized to identify a straight-line intersect from each plot. In some cases, two intersects were identified and also considered to provide a range for variation.

Aquifer characteristics were calculated, using the data obtained from the plots. The formulas used are specifically cited by each solution method employed. Some additional data, are necessary within the calculations, such as flow rate (Q) were taken from the pumping test results. Where necessary, adjusted values were used, as indicated, to compensate for some of the uncontrollable events that occurred during the tests.

The saturated thickness of the aquifer (b) was determined, using the screen length of each observation well for consistency.

Results from calculations for transmissivity and hydraulic conductivity were expressed in both English Standard Units and SI-Metric Units, for convenience.

#### 5.6. REI 3-4 Run #1 Pumping Test

5.6.1 Purpose - The major objective of this test was to qualitatively evaluate the potential hydraulic connection of the Alluvial Zone and the Deep Aquifer. These test results would also be compared with the results of the more sophisticated REI-10 cluster test to evaluate the areal extent of the aquitard(s).

Aquifer characteristics had been previously determined at this location in a pumping test which was described in the French Limited Remedial Investigation Report June 1986. As indicated in the 1986 Field Investigation Work Plan, aquifer characteristics (transmissivity, storativity, and hydraulic conductivity) of the Deep Aquifer would be redetermined from data collected during this test.

5.6.2 Description of Test - The test's operational parameters and well construction information are described in Table 5-1. Further installation and construction details for REI 10-1 and REI 11 are described in Section 5.4. Details of REI 3-4, REI 7, REI 3-1, REI 3-2 and REI 3-3 installation and construction are described in the Remedial Investigation Report June 1986 for the French Limited Site.

Monitor Wells REI 3-1, REI 3-2, and REI 3-3 are located at small radial distances from REI 3-4 in conformance with the Neuman-Witherspoon field test requirements. Water levels were observed in these three wells for possible responses to the drawdown of the Deep Aquifer. The remaining observation wells (REI 11, REI 7, REI 10-1) and REI 3-4 were monitored for data used in determining aquifer characteristics.

5.6.3 Results - The 2.5 gpm test flow rate used at the start of the test was selected based on information from the 1985 pumping test, and it was intentionally set at a high rate based on a desire to maximize "stress" on the aquitard in

TABLE 5-1

REI 3-4 RUN #1 PUMPING TEST PARAMETERS

DURATION OF PUMPING: From 8-20-86 @ 21:00 to 8-21-86 @ 03:00  
(360 min.)

DURATION OF RECOVERY: From 8-21-86 @ 03:00 to 8-21-86 @ 16:20  
(810 min.)

## COMMENTS

PUMPING WELL: REI 3-4	REI 3-4 is screened 25 ft across the Deep Aquifer. The top of screen is located approx. 120 ft below the surface.
PUMP INTAKE LOCATION:	130 ft (approx.) below the surface.
OBSERVATION WELLS:	
REI 3-4	Screened 25 ft across the Deep Aquifer (RADIUS = 0.16 ft).
REI 7	Screened 15 ft across the Deep Aquifer (RADIUS = 682.67 ft).
REI 10-1	Screened 25.3 ft across the Deep Aquifer (RADIUS = 784.360 ft).
REI 11	Screened 16.58 across the Deep Aquifer (RADIUS = 446.391 ft).
REI 3-3	Screened 14 ft across the Alluvial Aquifer.
REI 3-2	Screened 5 ft across a shallow water-bearing zone, below REI 3-3.
REI 3-1	Screened 10 ft across a shallow water-bearing zone, below 3-2.

## FLOW RATE DATA SUMMARY

Flow Rate (gpm)	From	To	Comments
2.5	8-20-86 @21:00	8-20-86 @21:21	Designated pumping rate.
2.1-1.65	8-20-86 @21:00	8-20-86 @03:07	Steady decrease in pumping rate because of decline in head.
0	8-21-86 @03:07		Recovery phase started because flow rate would have caused pump to break suction.

Pumping Rate Monitoring: Dwyer Series VFC Visifloat Flowmeter  
(range = 0.6 to 6.0 gpm, accuracy  $\pm$  0.005.

the available pumping test duration. However, this high flow rate could not be maintained constant throughout the test because: 1) the flow rate caused sufficient drawdown to limit the pumping capacity, and 2) the flow rate exceeded the specific capacity of the well. This would have caused the pump to break suction prior to test completion, if the flow rate had not been reduced. Discussion on terminating this test began within 20 minutes after it began, and it was actually terminated after approximately 360 minutes of drawdown. Data from this test were not evaluated for the potential connection of the zones nor for aquifer characteristics.

#### 5.7 REI 3-4 Run #2 Pumping Test

5.7.1 Purpose. The purpose of this test was the same as that described for Run #1, in Section 5.6.1.

5.7.2 Description of Test - The test's operating parameters and well construction information are described in Table 5-2. The same observation wells monitored during REI 3-4 Test Run #1 were also monitored in this test. (See Section 5.6.2.) The REI 3-4 Run #2 Test was started using a 1.6 gpm flow rate which was maintained constant for approximately 28.5 hours. At that time, it became necessary to adjust the flow to 1.4 gpm to prevent the pump from breaking suction. This 1.4 gpm flow rate was maintained for the remainder of the test.



TABLE 5-2

REI 3-4 RUN #2 PUMPING TEST PARAMETER

DURATION OF PUMPING: From 8-21-86 @ 16:30 to 8-24-86 @ 17:00  
(4349.7 min.)

DURATION OF RECOVERY: From 8-24-86 @ 17:00 to 8-25-86 @ 08:54  
(954.580 min.)

## COMMENTS

PUMPING WELL: REI 3-4 REI 3-4 is screened 25 ft across the Deep Aquifer. The top of screen is located approx. 120 ft below the surface.

PUMP INTAKE LOCATION: 130 ft (approx.) below the surface.

OBSERVATION WELLS:

REI 3-4 Screened 25 ft across the Deep Aquifer (RADIUS = 0.16 ft).

REI 7 Screened 15 ft across the Deep Aquifer (RADIUS = 682.67 ft).

REI 10-1 Screened 25.3 ft across the Deep Aquifer (RADIUS = 784.360 ft).

REI 11 Screened 16.58 across the Deep Aquifer (RADIUS = 446.391 ft).

REI 3-3 Screened 14 ft across the Alluvial Aquifer.

REI 3-2 Screened 5 ft across a shallow water-bearing zone, below REI 3-3.

REI 3-1 Screened 10 ft across a shallow water-bearing zone, below 3-2.

## FLOW RATE DATA SUMMARY

Flow Rate (gpm)	From	To	Comments
1.6	8-21-86 @16:30	8-22-86 @21:11	Designated pumping rate. Rate remains within 10% of 1.6 gpm.
1.1-1.9	8-22-86 @21:11	8-22-86 @21:15	Flow oscillated widely due to imminent breakage of suction in the pumping well.
1.4	8-22-86 @21:15	8-24-86 @17:00	Flow stabilized. Rate remained within 10% of 1.4 gpm. The rate was increased to 1.45 between 8-24-86 @07:30 and 8-24-86 @12:19.
0	8-24-86 17:00		Recovery phase started based on study of drawdown curves.

Pumping Rate Monitoring: Dwyer Series VFC Visifloat Flowmeter  
(range = 0.6 to 6.0 gpm, accuracy  $\pm$  0.005).

5.7.3 Results. The level measurement data from the In-Situ SE-200 Computer were processed into calculation data sheets for the test, which are provided in Appendix 16. The drawdown and recovery curves and aquifer characteristics calculations are shown in Attachment 5.

A. Connection Evaluation - No drawdown reaction was observed in REI 3-1, REI 3-2, or REI 3-3, during the 3 day duration of the test, which could be attributed to drawdown of the Deep Aquifer. Assessment of the fluctuations observed in these three wells during the test indicates they were affected by several factors: atmospheric pressure changes, precipitation, and earth tides. (See discussion of earth tides in Section 5-10.3). Tidal effects seem to have been the dominant cause of the fluctuations observed in REI 3-1, REI 3-2 and REI 3-3; however, these effects appear to have been retarded and sometimes overridden by precipitation events. In one incident, after a major rainfall event had begun, the water levels in all three wells were observed to rise significantly. This recharge response initially occurred in the shallowest well, REI 3-3, then in REI 3-2 (deeper than REI 3-3), and then in REI 3-1, the deepest. The observed lag time is probably a function of the difference in the well depths. The relatively rapid responses of all three wells indicate that the three zones are in weak hydraulic communication. The surface water pond adjacent to the REI 3 cluster is the

probable source for both the recharge and intercommunication between the zones monitored by REI 3-1, REI 3-2 and REI 3-3.

B. Aquifer Characterization - The hydrologic characteristics of the aquifer were derived from analysis of the data collected from four observation wells. The values for the hydrologic characteristics were calculated using methods described in Section 5.5.3. A summary of the results of those calculations is presented in Table 5-3. Transmissivity and storativity were calculated from the drawdown data using the 1.6 gpm flow rate that was maintained during the first 28.5 hours of the tests drawdown period. An adjusted flow rate of 1.4 gpm was maintained for the last 44 hours of the test. In the recovery data calculations, the adjusted flow rate,  $Q_r = 1.4$  gpm was used to determine transmissivity and storativity.

1. Transmissivity - The transmissivity of the Deep Aquifer was determined to range from  $9.17 \times 10^0$  gpd/ft ( $1.32 \times 10^{-6}$  m<sup>2</sup>/sec) to  $8.89 \times 10^2$  gpd/ft ( $1.28 \times 10^{-4}$  m<sup>2</sup>/sec) based on the most representative data. (See the discussion in Section 5.10.3 for further details). This relatively large range (almost three orders of magnitude) indicates that the Deep Aquifer may not be homogenous. The variations in grain size and thickness documented in the boring log data (see Appendix 12) also support this conclusion. The transmissivity values appear to increase areally from REI 3-4 toward REI 11 and REI 10-1 (north). The difference between the values of the latter two observation wells is relatively small.

TABLE 5-3

REI 3-4 RUN #2 PUMPING TESTHYDROGEOLOGIC CHARACTERISTICS SUMMARY

Observation Well	Analysis Method	Transmissivity (T)		Storativity (S)	Hydraulic Conductivity (K)	
		gpd/ft	m <sup>2</sup> /sec		gpd/ft <sup>2</sup>	cm/sec
REI 3-4						
Drawdown	Log-Log	1.41 x 10 <sup>1</sup>	2.03 x 10 <sup>-6</sup>	3.77 x 10 <sup>-1</sup>	6.13 x 10 <sup>-1</sup>	2.89 x 10 <sup>-5</sup>
	Semi-log	1.53 x 10 <sup>1</sup>	2.20 x 10 <sup>-6</sup>	2.83 x 10 <sup>-1</sup>	6.65 x 10 <sup>-1</sup>	3.14 x 10 <sup>-5</sup>
Recovery	Log-Log	9.17 x 10 <sup>0</sup>	1.32 x 10 <sup>-6</sup>	-	3.99 x 10 <sup>-1</sup>	1.88 x 10 <sup>-5</sup>
	Semi-log <sup>a</sup>	9.91 x 10 <sup>0</sup>	1.42 x 10 <sup>-6</sup>	-	4.31 x 10 <sup>-1</sup>	2.03 x 10 <sup>-5</sup>
	Semi-log <sup>b</sup>	1.01 x 10 <sup>1</sup>	1.45 x 10 <sup>-6</sup>	-	-	-
REI-11						
Drawdown	Log-Log	8.82 x 10 <sup>2</sup>	1.27 x 10 <sup>-4</sup>	1.11 x 10 <sup>-4</sup>	5.36 x 10 <sup>1</sup>	2.53 x 10 <sup>-3</sup>
	Semi-log	7.94 x 10 <sup>2</sup>	1.14 x 10 <sup>-4</sup>	8.71 x 10 <sup>-5</sup>	4.83 x 10 <sup>1</sup>	2.28 x 10 <sup>-3</sup>
		8.89 x 10 <sup>2</sup>	1.28 x 10 <sup>-4</sup>	9.76 x 10 <sup>-5</sup>	5.41 x 10 <sup>1</sup>	2.55 x 10 <sup>-3</sup>
Recovery	Log-Log	6.17 x 10 <sup>2</sup>	8.87 x 10 <sup>-5</sup>	-	3.75 x 10 <sup>1</sup>	1.77 x 10 <sup>-3</sup>
	Semi-log <sup>a</sup>	6.43 x 10 <sup>2</sup>	9.24 x 10 <sup>-5</sup>	-	3.91 x 10 <sup>1</sup>	1.84 x 10 <sup>-3</sup>
	Semi-log <sup>b</sup>	7.01 x 10 <sup>2</sup>	1.01 x 10 <sup>-4</sup>	-	-	-
REI 7						
Drawdown	Log-Log	-	-	-	-	-
	Semi-log	1.97 x 10 <sup>3</sup>	2.84 x 10 <sup>-4</sup>	6.07 x 10 <sup>-4</sup>	1.32 x 10 <sup>2</sup>	6.20 x 10 <sup>-3</sup>
Recovery	Log-Log	*	*	-	*	*
	Semi-log <sup>a</sup>	2.40 x 10 <sup>3</sup>	3.45 x 10 <sup>-4</sup>	-	1.60 x 10 <sup>2</sup>	7.54 x 10 <sup>-3</sup>
	Semi-log <sup>b</sup>	2.78 x 10 <sup>3</sup>	4.00 x 10 <sup>-4</sup>	-	-	-
REI 10-1						
Drawdown	Log-Log	-	-	-	-	-
	Semi-Log	9.89 x 10 <sup>2</sup>	1.42 x 10 <sup>-4</sup>	4.69 x 10 <sup>-5</sup>	3.91 x 10 <sup>1</sup>	1.84 x 10 <sup>-3</sup>
		1.06 x 10 <sup>3</sup>	1.52 x 10 <sup>-4</sup>	8.06 x 10 <sup>-5</sup>	4.17 x 10 <sup>1</sup>	1.97 x 10 <sup>-3</sup>
Recovery	Log-Log	5.63 x 10 <sup>2</sup>	8.10 x 10 <sup>-5</sup>	-	2.23 x 10 <sup>1</sup>	1.05 x 10 <sup>-3</sup>
	Semi-log <sup>a</sup>	6.35 x 10 <sup>2</sup>	9.13 x 10 <sup>-5</sup>	-	2.51 x 10 <sup>1</sup>	1.18 x 10 <sup>-3</sup>
	Semi-log <sup>b</sup>	6.59 x 10 <sup>2</sup>	9.47 x 10 <sup>-5</sup>	-	-	-

\* Could Not Determine

a - residual drawdown vs. t/t'

b - residual recovery vs. time

2. Storativity - Storativity values ranged from  $8.71 \times 10^{-5}$  to  $3.77 \times 10^{-1}$ . Confined aquifers generally exhibit low storativities in a range from  $1 \times 10^{-5}$  to  $1 \times 10^{-3}$ . (Driscoll, 1986). The relatively high storativity value obtained from REI 3-4 may be due to a transition in the geologic characteristics (e.g., grain size, thickness).

3. Hydraulic Conductivity - The values for hydraulic conductivity ranged from  $3.99 \times 10^{-1}$  gpd/ft<sup>2</sup> ( $2.89 \times 10^{-5}$  cm/sec) to  $5.4 \times 10^1$  gpd/ft<sup>2</sup> ( $2.55 \times 10^{-3}$  cm/sec). These values represent an average hydraulic conductivity; the Deep Aquifer, as identified by boring log data, is stratified (non-homogeneous). Comparisons with the charts (Attachment 5) provided by both Driscoll (1986) and the U.S. Department of Interior: Ground Water Manual (1981) show that this range compares with the hydraulic conductivities of a silt or sandy silt to a well-sorted, medium-grained sand.

C. Boundary Conditions - An evaluation of the observation well data and the drawdown and recovery curve plots indicates boundary conditions were observed. At first glance, the log-log curve plots of REI 3-4 appear to be representative of a leaky confined aquifer. The log-log and semi-log plots of the other observation wells, however, seem to indicate the Deep Aquifer is non-leaky and is almost an "ideal aquifer." A more plausible explanation for these apparent inconsistencies is that REI 3-4 may be located very close to

where the Deep Aquifer decreases significantly in either lateral extent, or thickness, and/or experiences changes in grain size (i.e., located within an area of low transmissivity). Support for this explanation is provided by the differences in the transmissivity values calculated for REI 3-4 as compared to the values for the other observation wells (Table 5-3). The REI 3-4 values are two orders of magnitude lower than the values obtained from REI-11 and REI 10-1. (Additional information obtained in subsequent tests provided further supporting evidence that the Deep Aquifer is bounded.)

Thus, apparent leaky conditions observed in REI 3-4 may have been caused by the influence of a diverse aquifer which exhibits much higher transmissivities at other nearby locations and resulting in the observation of an apparent recharge boundary (Freeze and Cherry, 1979).

#### 5.8 REI 10-1 Run #1 Pumping Test

5.8.1 Purpose - The major objective of this test was to qualitatively evaluate the potential hydraulic connection between the Alluvial zone and the Deep Aquifer. In addition, characteristics of the Deep Aquifer (transmissivity, storativity, and hydraulic conductivity) would be determined from this test. Characteristics of the aquitard would also be determined, using the field method described in Neuman and Witherspoon (1972) as shown in Appendix 17, if drawdown responses were observed in the piezometers installed in the aquitard.

5.8.2 Description of Test - The test's operational parameters and well construction information are described in Table 5-4. Additional installation and construction details for REI 10-1, REI 11, REI 12-1, REI 10-2, REI 10-3, REI 10-4, P10-2, P10-3 and P10-4 are described in Subsection 5.4. The installation and construction details for GW-25, REI-7 and REI 3-4 are described in the Remedial Investigation Report June, 1986 for the French Limited Site. The new REI 10 cluster wells and piezometers were located to conform with the Neuman-Witherspoon field test requirements, i.e., at as small radial distances from the pumping well (REI 10-1) as practically possible.

A premise of the test design was that piezometers P10-2, P10-3 and P10-4 would measure any response through the aquitard, to drawdown in the Deep Aquifer, if indeed, the aquitard were leaky. REI 10-2, REI 10-3, and REI 10-4 were monitored for possible response in the Alluvial Zone, to drawdown of the Deep Aquifer during the test. The remaining observation wells (REI-11, REI-7, REI 3-4, REI 12-1) and the pumping well were monitored to obtain data for determining aquifer characteristics.

The initially selected flow rate for this test (20 gpm), which was maintained for the first 12 hours of the drawdown phase had to be adjusted. At approximately 11 hours of elapsed time, an increase in drawdown rate was observed in

TABLE 5-4

## REI 10-1 RUN #1 PUMPING TEST PARAMETERS

DURATION OF PUMPING: From 9-15-86 @ 13:00 to 9-16-86 @ 16:30  
(1650.6 min.)

DURATION OF RECOVERY: From 9-16-86 @ 16:30 to 9-19-86 @ 07:37  
(3786.6 min.)

PUMPING WELL: REI 10-1 REI-10 is screened 25.3 ft across the Deep Aquifer. The top of screen is located approx. 122.5 ft below the surface.

PUMP INTAKE LOCATION: 138 ft (approx.) below the surface.

## OBSERVATION WELLS:

REI 10-1	Screened 25 ft across the Deep Aquifer (RADIUS = 0.16 ft).
REI 7	Screened 15 ft across the Deep Aquifer (RADIUS = 1012.704 ft).
REI 11	Screened 16.58 ft across the Deep Aquifer (RADIUS = 427.782 ft).
REI 3-4	Screened 25 ft across the Deep Aquifer (RADIUS = 784.360 ft).
GW-25	Screened 5 ft across the deep Aquifer (RADIUS = 66.670 ft).
REI 12-1	Screened 36.5 ft across the Deep Aquifer (RADIUS = 1492.112 ft).
P10-2	Screened 2.01 ft across an intermediate silt (RADIUS = 20.845 ft).
P10-3	Screened 2.00 ft across an intermediate clay (RADIUS = 20.220 ft).
P10-4	Screened 2.00 ft across an intermediate clay (RADIUS = 20.053 ft).
REI 10-2	Screened 13.75 ft across the Alluvial Zone.
REI 10-3	Screened 10.30 ft across the Alluvial Zone.
REI 10-4	Screened 12.80 ft across the Alluvial Zone.

## FLOW RATE DATA SUMMARY

Flow Rate (gpm)	From	To	Comments
19-20.3	9-15-86 @13:00	9-16-86 @03:00	Designated pumping rate was 20 gpm, it remained within 10% of 20 gpm.
19-14.5	9-16-86 @03:00	9-16-86 @10:43	Flow was steadily decreased so that drawdown in the pumping well would not exceed 50 ft.
12.0	9-16-86 @10:43	9-16-86 @13:02	Flow was held steady at 12 gpm.
12.0-14.7	9-16-86 @13:02	9-16-86 @16:30	Flow was steadily increased in an attempt to again reach 50 ft of drawdown in the pumping well.
0	9-16-86 @16:30		Recovery phase started.



the pumping well. It later became apparent that, if this increase continued, the drawdown in the well would pass below the top of the screen, causing cavitation. The flow rate was adjusted periodically in order to maintain the drawdown at a safe level above the screened interval. This test was terminated after only 27.5 hours of drawdown due to the observation of an anomaly in the response of REI 10-3.

5.8.3 Results - The level measurement data from the In-Situ SE-200 computer were processed into calculation data sheets for the test; these are provided in Appendix 18. The drawdown and recovery response curve plots, and aquifer characteristics calculations are shown in Attachment 6.

A. Connection Evaluation - Anomalous water level fluctuations were observed in REI 10-3 during this test. After 3.5 hours of elapsed time, the transducer measurements indicate that REI 10-3 was experiencing drawdown. REI 10-2, REI 10-3, and REI 10-4 are located within close proximity of each other and are screened in the same zone; thus, water level fluctuations of all three wells were expected to be similar.

In comparison, with the possible exception of a disturbance observed in the initial 10 minutes of the test, REI 10-2 and REI 10-4 fluctuated synchronously from other influences, not associated with the anomaly.

The piezometers P10-3 and P10-4, which are both screened in the clay aquitard, exhibited minor fluctuations within a 0.03 feet range. The water levels in

P10-2, however, rose 0.10 feet, in the initial 10 minutes of the test, and then began to respond somewhat erratically. (The initial rise may have been caused by the phenomenon known as the Noordbergum effect. See Subsection 5.9.3 for a detailed description of this effect.) An assessment of the fluctuations in REI 10-3 and P10-2 and those in the other observation wells was made while this test was in progress.

After reviewing the data, and deliberating over potential causes and sources for the anomaly, it was postulated that leakage around an artificial penetration, located near REI 10-3, was the probable cause for both the anomaly and the erratic fluctuations observed in P10-2. The potential for connection between the shallow Alluvial zone and the Deep Aquifer by leakage through the aquitard was ruled out because of: 1) the relatively rapid responses of REI 10-3 and P10-2; and 2) the lack of drawdown response in either P10-3 and P10-4. This test was terminated after 27.5 hours of drawdown. An additional drawdown test was conducted, after partial recovery of the Deep Aquifer, to determine whether the observed anomaly could be repeated. Results of this test, which lasted for approximately 3.5 hours, were, however, inconclusive. (See Appendix 24)

B. Aquifer Characterization - The hydrologic characteristics of the aquifer were derived from an analysis of data collected from six observation wells. The values for the hydrologic characteristics are presented in Table 5-5. The

TABLE 5-5

REI 10-1 RUN #1 PUMPING TEST  
HYDROLOGIC CHARACTERISTICS SUMMARY

Observation Well	Analysis Method	Transmissivity (T)		Storativity (S)	Hydraulic Conductivity (K)	
		gpd/ft	m <sup>2</sup> /sec		gpd/ft <sup>2</sup>	cm/sec
REI 10-1 Drawdown	Log-Log	$9.55 \times 10^2$	$1.37 \times 10^{-4}$	$1.24 \times 10^{-4}$	$3.77 \times 10^1$	$1.78 \times 10^{-3}$
	Semi-log	$1.08 \times 10^3$	$1.55 \times 10^{-4}$	$1.92 \times 10^{-4}$	$4.26 \times 10^1$	$2.01 \times 10^{-3}$
GW-25 Drawdown	Log-Log	$1.57 \times 10^3$	$2.26 \times 10^{-4}$	$2.10 \times 10^{-4}$	$3.14 \times 10^2$	$1.48 \times 10^{-2}$
	Semi-log	$1.77 \times 10^3$	$2.55 \times 10^{-4}$	$2.08 \times 10^{-4}$	$3.54 \times 10^2$	$1.67 \times 10^{-2}$
		$6.14 \times 10^2$	$8.83 \times 10^{-5}$	$2.01 \times 10^{-3}$	$1.23 \times 10^2$	$5.79 \times 10^{-3}$
REI 11 Drawdown	Log-Log	$2.05 \times 10^3$	$2.94 \times 10^{-4}$	$1.44 \times 10^{-4}$	$1.24 \times 10^2$	$5.87 \times 10^{-3}$
	Semi-log	$1.53 \times 10^3$	$2.20 \times 10^{-4}$	$8.65 \times 10^{-5}$	$9.30 \times 10^1$	$4.39 \times 10^{-3}$
		$7.03 \times 10^2$	$1.01 \times 10^{-4}$	$1.34 \times 10^{-4}$	$4.27 \times 10^1$	$2.02 \times 10^{-3}$
REI 3-4 Drawdown	Log-Log	$9.67 \times 10^2$	$1.39 \times 10^{-4}$	$6.72 \times 10^{-5}$	$4.20 \times 10^1$	$1.98 \times 10^{-3}$
	Semi-log	$8.12 \times 10^2$	$1.17 \times 10^{-4}$	$5.27 \times 10^{-5}$	$3.53 \times 10^1$	$1.67 \times 10^{-3}$
REI 7 Drawdown	Log-Log	$1.28 \times 10^3$	$1.84 \times 10^{-4}$	$5.96 \times 10^{-4}$	$8.54 \times 10^1$	$4.02 \times 10^{-3}$
	Semi-log	$2.36 \times 10^3$	$3.39 \times 10^{-4}$	$3.71 \times 10^{-4}$	$1.57 \times 10^2$	$7.41 \times 10^{-3}$
REI 12-1 Drawdown	Log-Log	$3.07 \times 10^2$	$4.41 \times 10^{-5}$	$4.27 \times 10^{-5}$	$8.35 \times 10^0$	$3.94 \times 10^{-4}$
	Semi-Log	$7.00 \times 10^2$	$1.01 \times 10^{-4}$	$3.60 \times 10^{-5}$	$1.91 \times 10^1$	$8.98 \times 10^{-4}$

calculations for transmissivity and storativity values were made using a 20.0 gpm flow rate. This flow rate was maintained constant for the first 12.5 hours of the test. The initial flow rate was maintained within 10 percent of the 20.0 gpm rate, until it was gradually decreased, to 18.0 gpm. A  $\pm 10$  percent fluctuation tolerance is considered acceptable to obtain accurate hydrologic characteristics (Stallman, 1983). For this reason, only the early portion of the data from the log-log plots and the semi-log plots were considered to be reliable and useable in the analysis. Recovery data were not analyzed because of the variable flow rate during drawdown.

1. Transmissivity - The transmissivity of the Deep Aquifer was determined to range from  $7.03 \times 10^2$  gpd/ft ( $1.01 \times 10^{-4}$  m<sup>2</sup>/sec) to  $2.05 \times 10^3$  gpd/ft ( $2.94 \times 10^{-4}$  m<sup>2</sup>/sec), based on the most reliable data (from REI-11 and REI 10-1). Transmissivities in this range are characteristic of aquifers with a fair to good potential use as a source for domestic well supplies, but a poor potential for usages requiring large volumes, such as irrigation; this is based on a comparison with the table in Attachment 7. See U.S. Dept of Interior, Ground Water Manual, 1981.

2. Storativity - Storativity values ranged from  $8.65 \times 10^{-5}$  to  $1.24 \times 10^{-4}$ . The values obtained from GW-25, REI 3-4, REI 7 and REI 12 are not considered to be reliable. (See Subsection 5.9.3.)

3. Hydraulic Conductivity - The hydraulic conductivities ranged from  $3.77 \times 10^1$  gpd/ft<sup>2</sup> ( $1.78 \times 10^{-3}$  cm/sec) to  $1.24 \times 10^2$  gpd/ft<sup>2</sup> ( $5.87 \times 10^{-3}$  cm/sec.). These values represent an average hydraulic conductivity; the Deep Aquifer, as identified by boring log data, is stratified (nonhomogeneous). Comparisons with the charts (See Attachment 8) provided by both Driscoll (1986) and the U.S. Department of Interior Ground Water Manual (1981) show that this range is comparative to the hydraulic conductivity of a well-sorted, medium-grained sand.

C. Boundary Conditions - An evaluation was not conducted on the boundary conditions observed in this test. Flow rates were variable after 12 hours of elapsed time, so the data collected after that time cannot be considered reliable. These are the data necessary to make accurate interpretations of boundary conditions.

#### 5.9 REI 10-1 Run #2 Test

5.9.1 Purpose - The objective of this test was the same as that described REI 10-1 for Run #1, in Subsection 5.8.1

5.9.2 Description of Test. The tests operational parameters and well construction information are described in Table 5-6. Additional installation and construction details for REI 10-1, REI 11, REI 12-1, REI 10-2, REI 10-3, REI 10-4, P10-2, P10-3 and P10-4 are described in Subsection 5-4. The installation and construction details for REI-7 and REI 3-4 are

TABLE 5-6

REI 10-1 RUN #2 PUMPING TEST PARAMETERS

DURATION OF PUMPING: From 10-7-86 @ 09:00 to 10-14-86 @ 11:00  
(10210.6 min.)

DURATION OF RECOVERY: From 10-14-86 @ 11:10 to 10-17-86 @ 11:04  
(4214.8 min.)

## PUMPING WELL: REI 10-1

REI 10-1 is screened 25.3 ft across the Deep Aquifer. The top of screen is located approx. 122.5 ft below the surface.

## PUMP INTAKE LOCATION:

138 ft (approx.) below the surface.

## OBSERVATION WELLS:

## REI 10-1

Screened 25 ft across the Deep Aquifer (RADIUS = 0.16 ft).

## REI 7

Screened 15 ft across the Deep Aquifer (RADIUS = 1012.704 ft).

## REI 11

Screened 16.58 ft across the Deep Aquifer (RADIUS = 427.782 ft).

## REI 3-4

Screened 25 across the Deep Aquifer (RADIUS = 784.360 ft).

## REI 12-1

Screened 36.5 ft across the Deep Aquifer (RADIUS = 1492.112 ft).

## P10-2

Screened 2.01 ft across an intermediate silt (RADIUS = 20.845 ft).

## P10-3

Screened 2.00 ft across an intermediate clay (RADIUS = 20.220 ft).

## P10-4

Screened 2.00 ft across an intermediate silt (RADIUS = 20.053 ft).

## REI 10-2

Screened 13.75 ft across the Alluvial Aquifer.

## REI 10-3

Screened 10.30 ft across the Alluvial Aquifer.

## REI 10-4

Screened 12.80 ft across the Alluvial Aquifer.

## FLOW RATE DATA SUMMARY

Flow Rate (gpm)	From	To	Comments
unknown	10-07-86 @09:00	10-07-86 @11:45	Flow meter was not working
17	10-07-86 @11:45	10-07-86 @18:08	Flow was measured with a 5 gallon bucket, and remained within 10% of 17 gpm..
40	10-07-86 @18:08	10-07-86 @18:09	Flow was raised for one minute in an effort to flush out the flow meter.
17	10-07-86 @18:09	10-14-86 @11:10	Flow was measured with a 5 gallon bucket, and remained within 10% of 17 gpm for the remainder of the test.
0	10-14-86 @11:10		Recovery phase started.

Pumping Rate Monitoring: Flow rate was measured at the pump discharge with a 5 gallon bucket and stop watch (accuracy = 0.2 gpm).

described in the Remedial Investigation Report of June, 1986 for the French Limited Site. GW-25 was removed from service prior to this test run, and thus was not monitored.

During this test, a malfunction in the flow meter used to monitor flow rate from the pumping well was discovered after approximately 4 hours of elapsed time. It is not known whether this malfunction occurred before the test began or sometime during the initial 4 hours of the test. A 17 gpm flow rate with  $\pm$  10 percent fluctuation was maintained, using a calibrated bucket and a stop watch for the remainder of the test.

5.9.3 Results - The level measurement data from the In-Situ SE-200 computer was processed into calculation data sheets for the test which are provided in Appendix 19. The drawdown and recovery response curves plots, and aquifer characteristics calculations are shown in Attachment 9.

A. Connection Evaluation - No significant (drawdown) reaction was observed in the alluvial wells (REI 10-2, REI 10-3, and REI 10-4) or piezometers (P10-3 and P10-4), that could be attributed to the 7 days of drawdown in the Deep Aquifer. Some nonrelated water level fluctuations were observed, however.

An assessment of the water level fluctuations, in the shallow wells REI 10-2, REI 10-3, and REI 10-4 and the piezometers P10-3 and P10-4, indicates there are

probably three major influences which caused the fluctuations observed: recharge by precipitation, barometric pressure changes, and earth tides.

Recharge from precipitation events was observed in the shallow wells when water levels rose after significant rainfall events. The on-site lagoon is the probable source of hydraulic communication causing the response to precipitation in the shallow wells. Little or no responses were observed in the piezometers which could be attributed directly to the precipitation events.

Major changes in barometric pressure appear to have caused some level changes in the shallow wells. The lack of any significant response to small barometric changes can be attributed to the fact that these wells are screened in a weakly confined water-bearing zone. Piezometers P10-3 and P10-4 do not appear to have responded to any barometric pressure changes.

Earth tides appear to have been the cause for many of the fluctuations observed in the shallow wells. The Dictionary of Geologic Terms (American Geologic Institute, 1976) defines an earth tide as "the rising and falling of the surface of the solid earth in response to the same forces that produce the tides of the sea." These tides are recognizable by their semi-daily cycle (1 day = 24 hours, 20 minutes). Semi-daily cycles in water level fluctuations were observed in both the shallow wells and P10-2. These cycles were more



evident in the shallow wells, perhaps because of their hydraulic connection to the nearby surface impoundment. Influences by earth tides on water level fluctuations have been described and documented in the technical literature (e.g., Theis, 1939).

The fluctuations in P10-2 water level are more complex. In the early 1 to 5 minutes of the test, a rise in the water level was observed. For the remainder of the drawdown phase, its fluctuations appear to have been influenced by similar factors affecting the other shallow wells. Then, at the end of the drawdown phase, a drop in the water level was observed when the pump was turned off. These apparent responses to the starting and stopping of the pump may be attributed to the "Noordbergum effect" (Verruijt, 1969; and Wolff, 1970). This effect is described as a response to increases in the pore pressure within finer grained sediments of strata. The strain induced by the initial pumping of an aquifer, or by the turning the pump off, is transferred across the finer grained confining strata, causing the water level of wells screened in the strata to rise. P10-3 and P10-4 may have also been influenced later in the test by this effect.

B. Aquifer Characterization - The hydrologic characteristics of the aquifer were derived from analysis of the data collected from five observation wells during the REI 10-1 Run #2 test. The resulting values for the hydrologic characteristics are shown in Table 5-7.

TABLE 5-7

REI 10-1 RUN #2 PUMPING TEST  
HYDROLOGIC CHARACTERISTICS SUMMARY

Observation Well	Analysis Method	Transmissivity (T)		Storativity (S)	Hydraulic Conductivity (K)	
		gpd/ft	m <sup>2</sup> /sec		gpd/ft <sup>2</sup>	cm/sec
REI 10-1	Drawdown	Log-Log	1.02 x 10 <sup>3</sup>	1.47 x 10 <sup>-4</sup>	1.31 x 10 <sup>-4</sup>	4.03 x 10 <sup>1</sup>
		Semi-log	*	*	*	1.90 x 10 <sup>-3</sup>
	Recovery	Log-Log	8.29 x 10 <sup>2</sup>	1.19 x 10 <sup>-4</sup>	-	3.28 x 10 <sup>1</sup>
		Semi-log <sup>a</sup>	2.13 x 10 <sup>3</sup>	3.06 x 10 <sup>-4</sup>	-	8.41 x 10 <sup>1</sup>
		Semi-log <sup>b</sup>	7.87 x 10 <sup>2</sup>	1.13 x 10 <sup>-4</sup>	-	3.97 x 10 <sup>-3</sup>
REI-11	Drawdown	Log-Log	1.27 x 10 <sup>3</sup>	1.83 x 10 <sup>-4</sup>	1.14 x 10 <sup>-4</sup>	7.72 x 10 <sup>1</sup>
		Semi-log	8.23 x 10 <sup>2</sup>	1.18 x 10 <sup>-4</sup>	1.17 x 10 <sup>-4</sup>	5.01 x 10 <sup>1</sup>
			6.34 x 10 <sup>2</sup>	9.12 x 10 <sup>-5</sup>	1.73 x 10 <sup>-4</sup>	3.85 x 10 <sup>1</sup>
	Recovery	Log-Log	8.51 x 10 <sup>2</sup>	1.22 x 10 <sup>-4</sup>	-	5.17 x 10 <sup>1</sup>
		Semi-log <sup>a</sup>	7.81 x 10 <sup>2</sup>	1.12 x 10 <sup>-4</sup>	-	4.75 x 10 <sup>1</sup>
		Semi-log <sup>b</sup>	8.00 x 10 <sup>2</sup>	1.15 x 10 <sup>-4</sup>	-	2.44 x 10 <sup>-3</sup>
REI 3-4	Drawdown	Log-Log	1.03 x 10 <sup>3</sup>	1.48 x 10 <sup>-4</sup>	6.44 x 10 <sup>-5</sup>	4.48 x 10 <sup>1</sup>
			7.22 x 10 <sup>2</sup>	1.04 x 10 <sup>-4</sup>	6.56 x 10 <sup>-5</sup>	3.14 x 10 <sup>1</sup>
		Semi-log	6.97 x 10 <sup>2</sup>	1.00 x 10 <sup>-4</sup>	6.26 x 10 <sup>-5</sup>	3.03 x 10 <sup>1</sup>
	Recovery	Log-Log	9.32 x 10 <sup>2</sup>	1.34 x 10 <sup>-4</sup>	-	4.05 x 10 <sup>1</sup>
		Semi-log <sup>a</sup>	8.42 x 10 <sup>2</sup>	1.21 x 10 <sup>-4</sup>	-	3.66 x 10 <sup>1</sup>
		Semi-log <sup>b</sup>	9.01 x 10 <sup>2</sup>	1.30 x 10 <sup>-4</sup>	-	1.91 x 10 <sup>-3</sup>
REI 7	Drawdown	Log-Log	1.86 x 10 <sup>3</sup>	2.67 x 10 <sup>-4</sup>	5.77 x 10 <sup>-4</sup>	1.24 x 10 <sup>2</sup>
		Semi-log	1.64 x 10 <sup>3</sup>	2.36 x 10 <sup>-4</sup>	4.25 x 10 <sup>-4</sup>	1.09 x 10 <sup>2</sup>
	Recovery	Log-Log	1.57 x 10 <sup>3</sup>	2.26 x 10 <sup>-4</sup>	-	1.05 x 10 <sup>2</sup>
		Semi-log <sup>a</sup>	2.40 x 10 <sup>3</sup>	3.45 x 10 <sup>-4</sup>	-	1.60 x 10 <sup>2</sup>
		Semi-log <sup>b</sup>	2.78 x 10 <sup>3</sup>	4.00 x 10 <sup>-4</sup>	-	4.95 x 10 <sup>-3</sup>
						7.54 x 10 <sup>-3</sup>
REI-12	Drawdown	Log-Log	4.81 x 10 <sup>2</sup>	6.92 x 10 <sup>-5</sup>	4.45 x 10 <sup>-5</sup>	1.31 x 10 <sup>1</sup>
		Semi-Log	4.49 x 10 <sup>2</sup>	6.46 x 10 <sup>-5</sup>	3.28 x 10 <sup>-5</sup>	1.22 x 10 <sup>1</sup>
	Recovery	Not analyzed				

\* Could Not Determine

a - residual drawdown vs. t/t'

b - residual recovery vs. time

1. Transmissivity - The transmissivity values were calculated from the drawdown data based on the assumption that a constant 17 gpm flow rate was maintained throughout the drawdown test. See the discussion in Subsection 5.9.2. The same assumption was made for analyzing the recovery data.

Transmissivity of the Deep Aquifer was determined to range from  $7.81 \times 10^2$  gpd/ft. to  $2.13 \times 10^3$  gpd/ft based on the most reliable data (from REI 11 and REI 10-1) of this test.

2. Storativity - Storativity values ranged from  $1.14 \times 10^{-4}$  to  $1.73 \times 10^{-4}$ . The values obtained from REI 3-4, REI-7 and REI-12 are not considered to be reliable.

3. Hydraulic Conductivity - The values for hydraulic conductivity ranged from  $3.28 \times 10^1$  gpd/ft<sup>2</sup> ( $1.55 \times 10^{-3}$  cm/s) to  $8.41 \times 10^1$  gpd/ft<sup>2</sup> ( $3.97 \times 10^{-3}$  cm/s). These values represent an average hydraulic conductivity because the Deep Aquifer, as identified by boring log data, is stratified (nonhomogeneous). Comparisons with the charts (Attachment 8) provided by both Driscoll (1986) and the U.S. Department of Interior, Ground Water Manual (1981) show that this range is comparative to the hydraulic conductivity of a well-sorted, medium-grained sand.

C. Boundary Conditions - An evaluation of the observation well data and the curve plots indicate a negative boundary was observed. The log-log plots all generally yield curves that approach the "ideal aquifer" type of curve. The lithologic data in boring logs indicate that the Deep Aquifer underlying the French Limited site is stratified and consists of various grain sizes; thus, it is not ideal.

When the residual-drawdown plots ( $H_{res}$  vs.  $t/t'$ ) of the observation wells are extended towards the origin, all generally intercept the abscissa below the origin, where the ordinate approaches 1. This is representative of a bounded aquifer, i.e., an aquifer of limited extent (after Driscoll, 1986).

The transmissivity values determined for REI 3-4 from this test are two orders of magnitude higher than those obtained in the REI 3 cluster test (Table 5-3). This was probably caused by the apparent nearby negative boundary conditions which will yield higher than normal transmissivity values in wells located near the boundary because of excessive drawdown (Driscoll, 1986).

#### 5.10 Conclusion from Deep Aquifer Pumping Tests

5.10.1 Connection Evaluation - The purpose of these Deep Aquifer pumping tests was to determine whether a confining layer exists between the Alluvial zone and the Deep Aquifer which hydraulically isolates these two units. A possible

hydraulic connection of these two units had been postulated after trace contamination was identified in samples collected from monitor well GW-25, which was screened in the Deep Aquifer.

The 1986 Deep Aquifer pumping tests do not provide evidence to support the conclusion that the two units are hydraulically connected within the near vicinity of the French Limited site. Rather, the data support the conclusion that an aquitard (or aquitards) lies between the Alluvial zone and the Deep Aquifer, thereby isolating the two units, within the near vicinity of the French Limited site.

Evaluation of the final test data showed no drawdown responses during any of the tests in either the piezometers P10-2, P10-3, P10-4, screened in a shallow confining clay aquitard between the two units of interest or the observation wells, REI 3-1, REI 3-2, REI 3-3, REI 10-2, REI 10-3, REI 10-4, screened in the Alluvial and other shallow zones, while stressing it with Deep Aquifer drawdown. The Neuman-Witherspoon field method could not be utilized to determine the hydraulic properties (hydrologic characteristics, such as hydraulic diffusivity) of the aquitard because no drawdown responses were observed in any of the piezometers during the REI 10-1 Run #2 test.

Observation made during REI 10-1 Run #1 indicated that REI 10-3 quickly responded to the pumping of the Deep Aquifer. Similar responses were also observed, though to a lesser degree, in REI 10-2, REI 10-4, and P10-2. An evaluation

of these responses postulated that an artificial penetration, located very near REI 10-3, was at least one possible source for the anomolous responses. The artificial penetration (GW-25) was drilled out and sealed with a cement-bentonite grout, after review of all pertinent data and performance of another test for the anomolous response. This test produced inclusive results. After equilibration of the aquifer, REI 10-1 Run #2 was performed; no drawdown responses were observed in either the shallow Alluvial zone wells (including REI 10-3) or the piezometers. During Run #2 water levels in REI 10-3 fluctuated similarly to REI 10-2 and REI 10-4, while during Run #1, the behavior of the fluctuations in REI 10-3 was significantly different in comparison to REI 10-2 and REI 10-4. These different results, in Run #1 and Run #2, provide additional support to the conclusion that leakage through the artificial penetration, located near REI 10-3, caused the anomaly observed.

5.10.2 Aquifer Characterization - A description of the Deep Aquifer hydrologic characteristics (transmissivity, storativity, hydraulic conductivity) based on the data obtained in all of the pumping test is contained in the individual results sections.

The aquifer characteristics determined from some of the observation wells may not be reliable or representative of the aquifer. Some of the values determined

from REI 3-4 may not be reliable because of its apparent location with respect to a transition in the Deep Aquifer. The high transmissivity values obtained from REI 3-4 in the REI 10 cluster tests were the result of the artificially greater drawdown observed at this location.

Values from REI-7 are not reliable because it is only partially screened across the upper portion of the Deep Aquifer. This is the cause for its delayed response, relative to its radial distance from the pumping well, in comparison with the initial responses and radial distances for the other observation wells.

REI 12-1 has the greatest radial distance of all the observation wells. It is also located where the Deep Aquifer increases in thickness. Because of these factors, the characteristics determined from REI-12-1 may not be representative of the Deep Aquifer underlying the French Limited site.

A. Transmissvity - The transmissivity values obtained from the most reliable data fall within the narrow range (less than one order of magnitude) of difference from  $6.17 \times 10^2$  gpd/ft to  $2.05 \times 10^3$  gpd/ft. Transmissivities in this range are generally characteristic of aquifers with a fair to good potential use as sources for domestic water supplies.

Transmissivities from REI 3-4 ranged from  $9.17 \times 10^0$  gpd/ft to  $1.03 \times 10^3$  gpd/ft, with a difference of more than two orders of magnitude. The lower values determined from the REI 3-4 Run #2 test data are considered to be more representative of the aquifer at that location. These lower values, ranging from  $9.17 \times 10^0$  gpd/ft to  $1.53 \times 10^1$  gpd/ft, are indicators of a significant difference in transmissivity within the Deep Aquifer, i.e., an apparent negative boundary condition.

B. Storativity - The storativity values ranged widely from  $3.28 \times 10^{-5}$  to  $3.77 \times 10^{-1}$ . The high value (obtained from REI 3-4, in the REI 3-4 Run #2 test) seems to be an anomaly in comparison with other values considered reliable. However, the presence of higher transmissive zones at REI 11 and REI 10-1 would have caused recharge to the lower transmissive area near REI 3-4. This would then result in artificially high storativities (after Driscoll, 1986).

C. Hydraulic Conductivity - The hydraulic conductivities obtained from the test data vary over a range of nearly three orders of magnitude. Some of the results may not be representative because of assumptions made in determining the saturated thickness (see Subsection 5.5.3). The hydraulic conductivity value from REI 12-1 and REI-7 are not considered to be representative of the Deep Aquifer.



Using the more reliable data, the hydraulic conductivities, ranged from  $3.99 \times 10^{-1}$  gpd/ft<sup>2</sup> ( $1.88 \times 10^{-5}$  cm/sec) to  $1.24 \times 10^2$  gpd/ft<sup>2</sup> ( $5.87 \times 10^{-3}$  cm/sec) The former value was obtained from REI 3-4, in the REI 3-4 Run #2 test; the latter was obtained from REI 11, in the REI 10-1 Run #1 test. Comparisons with the charts (See Attachment 8) provided by both Driscoll (1986) and the U.S. Department of Interior: Ground Water Manual (1981) show that this range is comparative to the hydraulic conductivities ranging from a silt to a well-sorted, medium-grained sand.

5.10.3 Boundary Conditions - The data from all the tests seem to support the interpretation that a transition occurs in the Deep Aquifer, in the proximity of REI 3-4. This caused a bounded aquifer response in many of the observation wells. This interpretation offers a plausible explanation for the large differences in the specific capacities of REI 3-4 and REI 10-1, indicated by the different optimum pumping rate used in each respective test, as well as many other observations made from the data.

#### 5.11 Monitor Well GW-25 Removal

5.11.1 Removal Decision Basis - During the 1986 Field Investigation, several factors indicated that monitor well GW-25 could be a possible source of vertical leakage between the shallow Alluvial zone, and Deep Aquifer. These factors are as follows:

- First, during the initial attempt to perform the "REI 10 Cluster" pumping test, a shallow Alluvial zone response was observed in monitor well REI 10-3 after pumping from the Deep Aquifer. This REI 10-3 response occurred promptly after the pumping test created drawdown in GW-25. Efforts to confirm the anomolous response in REI 10-3 were made by performing a second test, after partial equilibration of the aquifer. This test proved to be inconclusive. See Section 5.8 for a complete description of this activity.

- Secondly, Deep Aquifer water level measurements were taken on August 19, 1986 and a groundwater potentiometric map prepared as described in Subsection 5.4. The map showed that a minor "mounding" effect was occurring in the GW-25 area (Plate 3, Attachment 3).

- Third, analysis (GC/MS) of groundwater samples from six (6) Deep Aquifer monitor wells was performed, and the GW-25 well sample reported the presence of trace contamination, while the other wells sampled indicated no pertinent contamination concentrations. This investigation is reported in Section 5.12 of this report.

Upon review of these results, a field decision was made to remove and seal monitor well GW-25. The procedure used, and the findings, as this decision was implemented, are described in the following subsection. GW-25 was installed on May 15-18, 1984.

5.11.2 Removal Procedure and Findings - The objectives of GW-25 well removal were to resolve the question of leakage from the shallow Alluvial zone into the Deep Aquifer via this artificial conduit, and to observe details of GW-25 construction so that potential reasons for this downward leakage could be noted.

The planned method to achieve this was to drill a boring of sufficient diameter to remove all PVC and any original grout from the borehole, and to fill the resulting hole to ground surface with an impervious cement and bentonite grout. The original boring was ten (10) inches in diameter to a depth of 58 feet to accommodate the surface casing, and six (6) inches in diameter from a 58-foot depth to 152 feet below the surface. To ensure that the drill bit used to destroy the well would not be deflected away from the well, a 1 foot long guiding rod was welded to the nose of the 5.5 inch diameter bit. This rod fit inside the PVC well pipe to guide the drill and maintain center. It was planned that after the PVC pipe had been removed, the boring would be reamed with a 12 or 14 inch diameter drill bit to remove the 6-inch diameter surface casing, and any remaining grout. After the boring had been reamed into natural materials, it was planned that the hole would be tremie grouted to the surface with a mixture of 96% cement and 4% bentonite jel (by weight).

All removed materials and fluids were to be disposed of in the French Limited Lagoon. The removal of GW-25 was begun on September 19, 1986 and the final seal grouting completed on September 29, 1986.

The actual removal was performed using a mud rotary drill rig, under the supervision of an REI hydrogeologist. The actual well removal procedures were adjusted from the planned methods as field decisions were made based on conditions encountered. Decisions which affected the removal methods were made by the REI hydrogeologist in consultation with the driller, the PRP representative, and other REI engineers. These adjustments from planned procedures were primarily aimed at maintaining the drilling within the original well boring.

All equipment used, observations, and decisions were documented in a field book. Photographs of crucial portions of the removal process were taken. Samples of well and grout materials brought to the surface were retained and inspected for signs of degradations.

During the drilling out process, it was found that the grout material was not providing an effective seal around the well casing and piping. Based on these observations it appeared that downward leakage from the shallow Alluvial zone to the Deep Aquifer could have occurred because of an inadequate grout seal of the well annulus.

A detailed log of the GW-25 drilling and grout process, and the observations regarding conditions found, is shown in Appendix 20.

#### 5.12 Deep Aquifer Ground Water Analysis

5.12.1 Introduction - The 1986 Field Investigation installed three (3) additional Deep Aquifer Monitoring Wells for use in the various Deep Aquifer assessment tasks (REI 10-1, REI 11, REI 12-1). Installation and development of the new wells was performed as described in Subsection 5.4.

A Deep Aquifer Ground Water Analysis task was then implemented, which included the sampling of a total of six (6) monitor wells (REI 3-4, REI 7, REI 10-1, REI 11, REI 12-1 and GW-25). See the French Limited Site Map shown on Plate 1 in Attachments 1, for the location of these wells. Ground Water Samples were analyzed by GC/MS for priority pollutants. Approximate distances to each monitor well location from the nearest lagoon shoreline, and its direction from the lagoon, are shown as follows:

<u>Well Number</u>	<u>Distance From Lagoon(Feet)</u>	<u>Direction From Lagoon</u>
REI 3-4	650	South
REI 7	200	South
REI 10-1	75	South
REI 11	230	South
REI 12-1	490	North
GW-25	50	South

5.12.2 Sampling and Analysis - Prior to sampling, each well was purged of a minimum of three well volumes of water. Samples were collected using a Teflon bailer which was decontaminated prior to each use in accordance with standard procedures described in the French Limited Remedial Investigation Report of June, 1986. All sample containers used were specially prepared, sealed and labeled for laboratory analysis. Analytical parameters consisted of GC/MS priority pollutant Volatiles, Acid Extractables, and Base/Neutral Extractable Fractions.

5.12.3 Analytical Results - A summary of the analytical results of the groundwater sampling is provided in Table 5-8. The laboratory analytical reports are provided in Attachment 21.

5.12.4 Conclusions - The analytical data indicate that monitoring wells REI 3-4, REI 7, REI 11, and REI 12 contained no detectable concentrations of contaminants that were considered pertinent to the assessment. A concentration of 140 ppb of bis(2 ethylhexyl)phthalate) was reported at REI -7, but this was discounted because it is a common component of PVC piping materials. Monitor Well GW-25 was sampled during the 1984 and 1985 well sampling program and found to show trace contamination. As a result, REI 10-1 was installed 75 feet from GW-25 to assist in assessing the extent of that trace contamination.

Table 5-8

Deep Aquifer Ground Water Analytical Results

<u>Parameter</u>	<u>Monitor Well</u>					
	<u>REI 3-4</u>	<u>REI 7</u>	<u>REI 10-1</u>	<u>REI 11</u>	<u>REI 12</u>	<u>GW-25</u>
<u>Volatile Organics (ug/l)</u>						
Benzene	ND	ND	ND	ND	ND	101
Chloroethane	ND	ND	ND	ND	ND	56.1
1,1-Dichloroethane	ND	ND	ND	ND	ND	87.1
Ethylbenzene	ND	ND	ND	ND	ND	16.1
Toluene	ND	ND	ND	ND	ND	42.0
1,2-Trans-dichloroethylene	ND	ND	ND	ND	ND	17.8
Vinyl chloride	ND	ND	ND	ND	ND	226
<u>Acid Fraction (ug/l)</u>						
2,4-Dimethylphenol	ND	ND	ND	ND	ND	3.15
Phenol	ND	ND	4.16	ND	ND	89.2
<u>Base/Neutral Fraction</u> <u>(ug/l)</u>						
Bis(2-ethylhexyl)						
phthalate	ND	140	ND	ND	ND	11.7
Napthalene	ND	140	ND	ND	ND	7.83

Note: All other priority pollutant parameters reported not detected (ND)

The 1986 sample from GW-25 was found to contain a total of 546.0 ppb volatiles, 92.0 ppb acid compounds, and 19.6 ppb base/neutral compounds. REI 10-1 was found to contain 4.2 ppb of phenol.

These data, in conjunction with the known characteristics of the lower aquifer, indicate that contamination at GW-25 is probably the result of a vertical leak at that location. The 4.2 ppb of phenol found in REI 10-1 is probably the result of extended purging during the well development phase drawing contaminants from GW-25. If general contamination of the lower aquifer existed, REI 10-1 would be expected to contain much higher contaminant concentrations.



## 6.0 SHALLOW ALLUVIAL ZONE ASSESSMENT

6.1 Purpose - The objective of the REI 3-3 pumping test was to determine the hydrologic characteristics of the shallow Alluvial zone (transmissivity, storativity, hydraulic conductivity).

6.2 Scope - An aquifer characterization test was conducted at the REI 3-3 well cluster in 1985, and described in the French Limited Site Remedial Investigation Report of June, 1986. This pumping test was of short duration (approximately 73 minutes) and was based on using only 2 observation wells.

The task for the 1986 Field Investigation was designed to repeat the test at REI 3-3, using 3 observation wells and extending the test duration to approximately 15 hours.

### 6.3 Pumping Test Procedures

6.3.1 Pre-Test Activities - Before the start of the pumping test at REI 3-3, the following preparatory tasks were performed.

An additional observation point for the pumping test was provided by installing a new well, REI 3-5 approximately 40 feet from REI 3-3. This well was screened across the same zone as REI 3-3 and piezometer P 3-3. The description of its construction is provided in Appendix 12 and its boring log is provided in Appendix 13. The well was fully developed, in accordance with procedures described in the French Limited Site Remedial Investigation Report of June, 1986.

A second step in the pre-test activities was selection of a test flow rate which would provide adequate stress for determining aquifer characteristics. The specific capacity data that had been derived from the previous REI 3-3 pump test (described in the Remedial Investigation Report; June 1986) was used. A 3.0 gpm flow rate was selected and used in the 1986 test.

An electric submersible pump was installed in REI 3-3, with dedicated hoses and polypropylene rope secured together by nylon ties. This pump had been decontaminated prior to installation. Clean disposable gloves were worn when handling both the pump and the hose to prevent the addition of artifactual constituents to REI 3-3.

Water level measurements were taken from REI 3-3, REI 3-5, and P 3-3 before and after the pump was installed to determine background static water levels. The equilibration of the water level in REI 3-3 after pump installation was also monitored.

6.3.2 Test Execution - Immediately before starting the test, all watches used in the test were synchronized for time accuracy. After the pump was started discharge flow was regulated to the specified 3.0 gpm flow rate, within less than 1 minute of the starting time.

The flow rate was monitored constantly during the initial and critical 2 to 3 hours. During this period, readings were collected and documented approximately every 5 to

10 minutes on the appropriate record sheets. After this initial period, the flow meter readings were documented approximately every 15 to 30 minutes through the remainder of the test. Adjustments were made throughout the test, as necessary, to maintain the flow rate to within  $\pm 10$  percent of the 3.0 gpm rate.

Drawdown and recovery data were collected from REI 3-3, REI 3-5, and P 3-3 during the test. The changes in the water levels of these three observation wells were measured with a dedicated Well Wizard Series 6000 well sounder at each well. Experienced pump test personnel collected these measurements on logarithmic time intervals as directed by the on-site hydrogeologist. These readings were collected with a  $\pm 0.01$  ft. accuracy objective, and were documented on appropriate record sheets for each well.

Progress of the pumping test was monitored by plotting data as it was collected during the test, on log-log and semi-log graph paper.

6.3.3 Post-Test Activities - After field activities were completed, the drawdown and recovery data were computed with a programmed Hewlett-Packard HP-41CX. These data were checked for errors as part of quality assurance. The computed data were then plotted by hand on K+E 8-1/2 x 11 log-log and semi-log graph paper for analysis. These plots were also checked for accuracy.

The two methods of analysis for the drawdown data were the Theis non-equilibrium solution (Theis, 1935; Health and Trainer, 1981) and the time vs. drawdown modification to the Theis non-equilibrium solution by Cooper and Jacob (Driscoll, 1981). The recovery data were also analyzed by both of these methods, using the assumption of Theis' corollary, and the residual drawdown plot solution (Driscoll, 1981).

For the log-log plots, the resulting curves were matched using a reversed type curve provided in the U.S. Department of Interior: Ground Water Manual, A Water Resources Technical Publication (1981; Figure 5-5). Only the portion of each curve plot considered to be reliable was utilized in the hydrogeologist's interpretation of where the curve matched the type curve.

For the semi-log plots, the most reliable data was selected to identify a straight-line intersect from the plots. In some cases, two intersects were identified and considered to provide a range.

The aquifer characteristics were calculated using the data obtained from the plots. The formulas used are specifically cited by each solution method employed. Some additional data necessary for the calculations, such as the flow rate ( $Q$ ), were taken from the pumping test results.

The saturated thickness of the aquifer (b) was determined using the screen length of each observation well for consistency.

Results for transmissivity and hydraulic conductivity were expressed in both English Standard Units and SI-Metric units for convenience.

#### 6.4 REI 3-3 Pumping Test

6.4.1 Description of the Test - The test's operational parameters and observation well information are described in Table 6-1. Installation and construction details for REI 3-5 are provided in Appendix 12. The installation and construction details for REI 3-3 and P 3-3 are provided in the Remedial Investigation Report (June, 1986) for the French Limited site.

REI 3-3, REI 3-5, and P 3-3 are all screened across the uppermost unit of the Alluvial zone. This shallow unit was previously described in the Remedial Investigation Report (June, 1986) as being unconfined. At the time the 1986 pumping test was conducted, this unit appeared to be confined, or at least semi-confined, at the REI 3 cluster location. This observation is based upon the static water level measurements collected from the observation wells prior to beginning the test. The surface water pond, located adjacent to this well cluster (approximately 60 to 100 feet away) is probably responsible for these conditions. A significant recharge boundary was observed at 55 to 60 minutes into the test, as

TABLE 6-1

TEST NAME: REI 3-3 PUMPING TEST

DURATION OF PUMPING: From 8-11-86 @ 1830 to 8-12-86 @ 0915  
(885 minutes)

DURATION OF RECOVERY: From 8-12-86 @ 0915 to 8-12-86 @ 1130  
(135 minutes)

COMMENTS

PUMPING WELL: REI 3-3 REI 3-3 is screened 14 ft across the Alluvial zone. The top of screen is located 8.5 ft below the surface.

PUMP INTAKE LOCATION: 18 ft (approx.) below the surface.

OBSERVATION WELLS:

REI 3-3 Screened 14 ft across the Alluvial zone (RADIUS = 0.16 ft).

REI P-3-3 Screened 14 ft across the Alluvial zone (RADIUS = 12.42 ft).

REI 3-5 Screened 15 ft across the Alluvial zone (RADIUS = 39.33 ft).

FLOW RATE DATA SUMMARY

<u>Flow Rate</u> (gpm)	<u>From</u>	<u>To</u>	<u>Comments</u>
3.0	8/11/86 @ 18:30	8/12/86 @ 09:15	Flow was maintained within $\pm 10\%$ of 3.0 gpm.

Pumping Rate Monitoring: Dwyer Series VFC Visifloat Flowmeter (range = 0.6 to 6.0 gpm, accuracy  $\pm 0.005$ ).

represented in the log-log and semi-log drawdown plots from the observation wells. The surface water pond would appear to be the likely source for the observed recharge. This recharge boundary was also observed in the REI 3-3 pumping test, conducted during the 1985 field investigation.

6.4.2 Results - The hydrological characteristics of the shallow Alluvial zone were derived from an analysis of data collected from three observation wells. The values for the hydrologic characteristics are presented in Table 6-2. The calculations for transmissivity and storativity values were made using a 3.0 gpm flow rate. This flow rate was maintained constant with  $\pm 10$  percent or less fluctuation throughout the drawdown phase of the test. Recovery data were also analyzed for the determination of characteristics.

A. Aquifer Characteristics

1. Transmissivity - The transmissivity of the Alluvial zone was determined to range from  $2.42 \times 10^2$  gpd/ft. ( $3.48 \times 10^{-5}$  m<sup>2</sup>/sec) to  $1.58 \times 10^3$  ( $1.58 \times 10^{-4}$  m<sup>2</sup>/sec), based on the most reliable data from REI 3-5. Transmissivities in this range are characteristic of aquifers with a fair to good potential use as a source for domestic well supplies, but poor potential for usages requiring large volumes, such as irrigation; this is based on a comparison with the table in Attachment 7. (Source: U.S. Department of Interior, Ground Water Manual, 1981). The transmissivity

TABLE 6-2  
REI 3-3 Pumping Test - Hydrologic Characteristics Summary

Observation Well	Analysis Method	Transmissivity (T)		Storativity (S)	Hydraulic Conductivity (K)	
		gpd/ft	m <sup>2</sup> /sec		gpd/ft <sup>2</sup>	cm/sec
REI 3-3	Drawdown	*	*	*	*	*
		5.21 x 10 <sup>2</sup>	7.49 x 10 <sup>-5</sup>	3.66 x 10 <sup>0</sup>	3.72 x 10 <sup>1</sup>	1.75 x 10 <sup>-3</sup>
	Recovery	Log-Log	7.16 x 10 <sup>2</sup>	1.03 x 10 <sup>-4</sup>	5.12 x 10 <sup>1</sup>	2.41 x 10 <sup>-3</sup>
		Semi-Log a	6.71 x 10 <sup>2</sup>	9.65 x 10 <sup>-5</sup>	4.79 x 10 <sup>1</sup>	2.26 x 10 <sup>-3</sup>
			6.66 x 10 <sup>2</sup>	9.57 x 10 <sup>-5</sup>	-	-
		Semi-Log b	8.77 x 10 <sup>2</sup>	1.26 x 10 <sup>-4</sup>	-	-
REI 3-5	Drawdown	Log-Log	6.14 x 10 <sup>2</sup>	8.83 x 10 <sup>-5</sup>	4.04 x 10 <sup>1</sup>	1.90 x 10 <sup>-3</sup>
		Semi-Log	7.76 x 10 <sup>2</sup>	1.12 x 10 <sup>-4</sup>	5.11 x 10 <sup>1</sup>	2.41 x 10 <sup>-3</sup>
	Recovery	Log-Log	1.07 x 10 <sup>3</sup>	1.54 x 10 <sup>-4</sup>	7.07 x 10 <sup>1</sup>	3.33 x 10 <sup>-3</sup>
		Semi-Log a	1.00 x 10 <sup>3</sup>	1.44 x 10 <sup>-4</sup>	6.60 x 10 <sup>1</sup>	3.11 x 10 <sup>-3</sup>
		Semi-Log b	4.58 x 10 <sup>3</sup>	2.28 x 10 <sup>-4</sup>	-	-
			1.11 x 10 <sup>3</sup>	1.52 x 10 <sup>-4</sup>	-	-
P 3-3	Drawdown	Log-Log	2.42 x 10 <sup>2</sup>	3.48 x 10 <sup>-5</sup>	1.73 x 10 <sup>1</sup>	8.15 x 10 <sup>-4</sup>
		Semi-Log	3.34 x 10 <sup>2</sup>	4.81 x 10 <sup>-5</sup>	2.39 x 10 <sup>1</sup>	1.13 x 10 <sup>-3</sup>
	Recovery	Log-Log	3.78 x 10 <sup>2</sup>	5.43 x 10 <sup>-5</sup>	2.70 x 10 <sup>1</sup>	1.27 x 10 <sup>-3</sup>
		Semi-Log a	5.14 x 10 <sup>2</sup>	7.40 x 10 <sup>-5</sup>	3.67 x 10 <sup>1</sup>	1.73 x 10 <sup>-3</sup>
		Semi-Log b	5.58 x 10 <sup>2</sup>	8.02 x 10 <sup>-5</sup>	-	-

\* could not determine  
- not analyzed



values obtained from REI 3-3 are somewhat less, but generally fall within the range of values from REI 3-5. The values from P 3-3 are significantly lower than both REI 3-3 and REI 3-5.

These values may be artificially lower because of its relatively shorter distance from the surface water pond as compared to the other wells. The location of an observation well near a recharge source will cause transmissivity values to be artificially lower (Driscoll, 1981). This is opposite of the effect which would be caused by a negative boundary condition, as observed in the Deep Aquifer pumping tests at the REI 10 cluster.

2. Storativity -- The storativity values obtained ranged from  $1.30 \times 10^{-3}$  (from REI 3-5) to  $3.66 \times 10^0$  (from REI 3-3). The latter value, because it is greater than 1 (an impossible value) indicates that significant recharge occurred during the test (Driscoll, 1981). Using the most reliable data, the highest storativity value obtained was  $9.31 \times 10^{-3}$ . The overall range of these storativities would be considered to be relatively high for a confined aquifer.

3. Hydraulic Conductivity - The reliable values for hydraulic conductivity ranged from  $3.72 \times 10^1$  gpd/ft<sup>2</sup> ( $1.75 \times 10^{-3}$  cm/sec) to  $7.07 \times 10^1$  gpd/ft<sup>2</sup> ( $3.33 \times 10^{-3}$  cm/sec). These values represent an average hydraulic conductivity; the Alluvial zone is stratified (non-homogenous) as identified in the boring log data. Comparison with the charts (see Attachment 8) provided by both Driscoll (1986) and

the U.S. Department of Interior: Ground Water Manual (1981), shows that the range compares with the hydraulic conductivity of silty sand of fine-grained sand.

6.5 Conclusions REI 3-3 Pumping Test - The aquifer characteristics for the shallow Alluvial zone may be best represented by those values obtained from REI 3-5. The values from REI 3-3 generally support the data obtained from REI 3-5; however, because REI 3-3 was utilized as the pumping well during the test, the values from it would have to be considered to be less reliable than values from observation wells.

The results obtained from P 3-3 cannot be considered reliable because of its proximity to an apparent recharge source (the surface water pond). In particular transmissivity values, were found to be much lower than the other two observation wells; this is probably the result of recharge rather than a variation in characteristics.

Detailed construction details apparently do not exist for P 3-3. In order to solve for hydraulic conductivity, an assumed value of 14.0 ft. (the same as REI 3-3) was used for the saturated thickness (b), in the calculations. The transmissivity values indicate the Alluvial zone has a fair to good potential use for domestic water supplies, but a poor potential use for larger volume usages such as irrigation; this is based on the comparison with the table in Attachment 7.

The storativity values from the test are not considered to be reliable, i.e., representative of the Alluvial zone, because of the recharge conditions observed. A significant recharge boundary was observed initially at 55 to 60 minutes into the test. The surface water pond, located adjacent to the REI 3 well cluster, is considered to be the likely source for the recharge conditions.

The hydraulic conductivities determined from the results of the tests are comparative to the hydraulic conductivity of a silty sand or fine-grained sand. The boring logs of REI 3-5 and REI 3-3 generally supports this identification.

The aquifer characteristics were determined based on the assumption that confined aquifer conditions had existed at the time of the test, as was indicated by data collected prior to the test. Previously, the upper unit of the Alluvial zone had been expected to be unconfined. It would appear, then, that the confined conditions observed at the REI 3-3 may be localized, due to the effects of the surface water pond. It is also possible that, because of the apparent hydrologic connection between the shallow zone and the surface water pond, seasonal fluctuations of the water level in the surface water pond caused by precipitation, may cause the condition of the shallow zone to vary from confined to unconfined periodically. Thus, when this variation occurs, it then can also be assumed that the aquifer characteristics may also vary to some degree

from those values obtained during this test. Given that "ground-water hydrology is dynamic and an inexact science," (U.S. Department of Interior: Ground Water Manual, 1981; pg. 65) the values for characteristics at this location should not be considered as absolute values, but rather as approximations, within  $\pm 1$  order of magnitude of the true values.

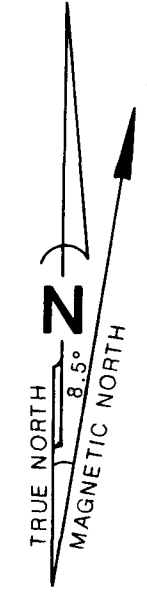
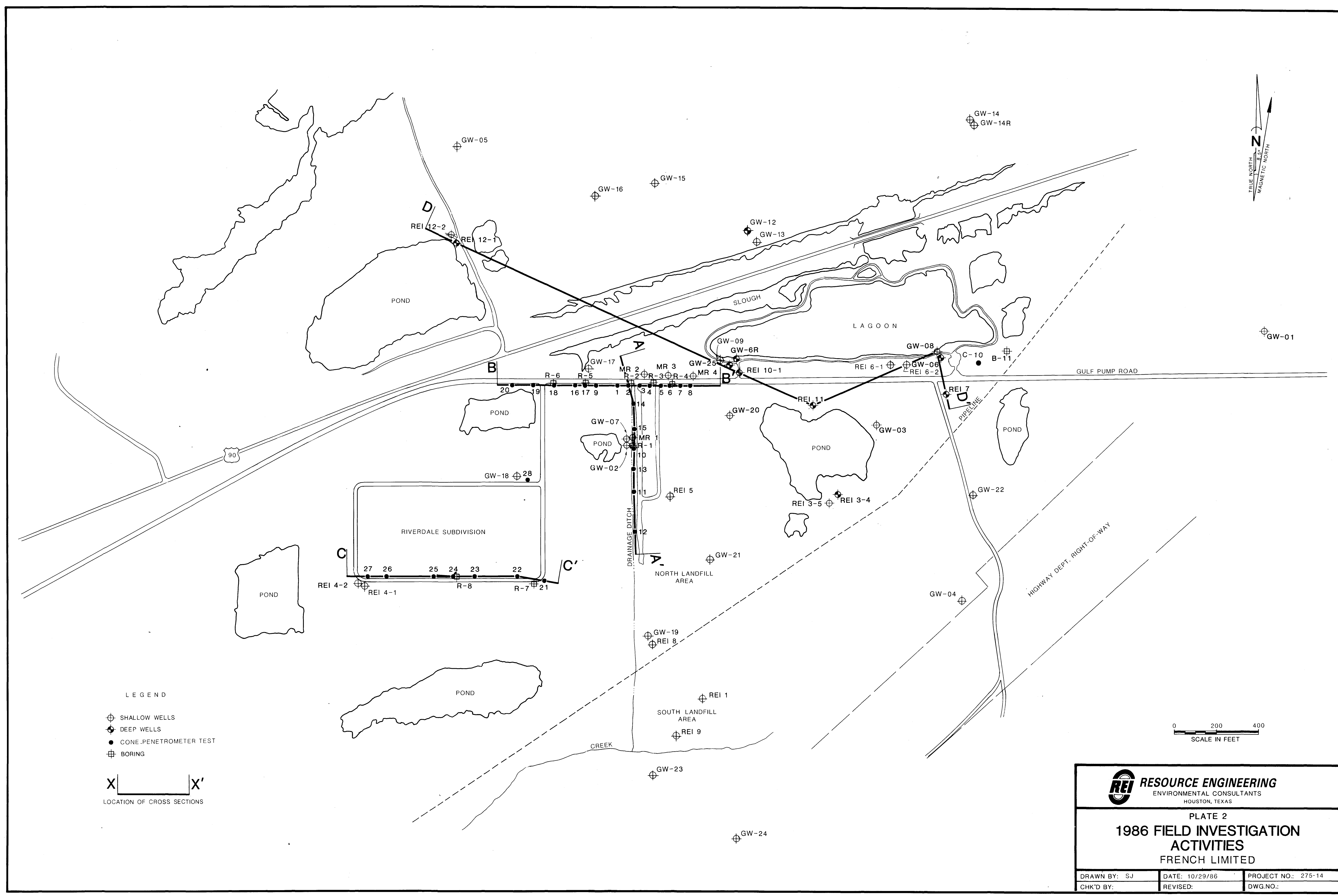
Attachment 1

Plate 1 - Site Location Map



Attachment 2

Plate 2 - 1986 Field Investigation Map

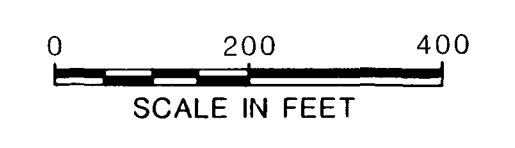


LEGEND

- ⊕ SHALLOW WELLS
- ⊙ DEEP WELLS
- CONE PENETROMETER TEST
- ⊞ BORING

X|X'

LOCATION OF CROSS SECTIONS




**RESOURCE ENGINEERING**  
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

PLATE 2  
**1986 FIELD INVESTIGATION  
ACTIVITIES**  
FRENCH LIMITED

DRAWN BY: SJ	DATE: 10/29/86	PROJECT NO.: 275-14
CHK'D BY:	REVISED:	DWG. NO.:



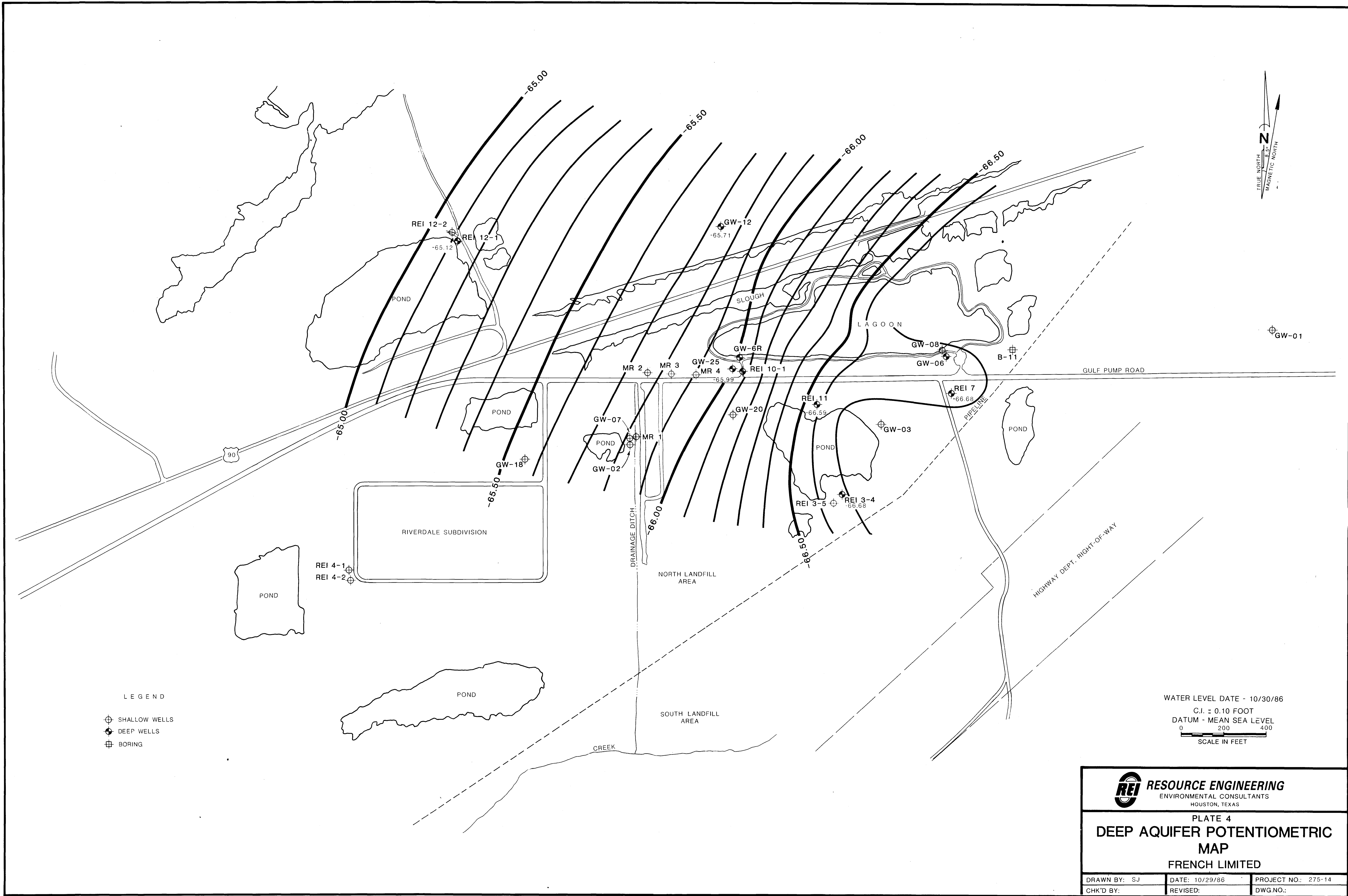
Attachment 3

Plate 3 - Deep Aquifer Potentiometric Map  
8/19/86



Attachment 4

Plate 4 - Deep Aquifer Potentiometric Map  
10/30/86



LEGEND

- ⊕ SHALLOW WELLS
- ⊕ DEEP WELLS
- ⊕ BORING

WATER LEVEL DATE - 10/30/86  
C.I. = 0.10 FOOT  
DATUM - MEAN SEA LEVEL  
0 200 400  
SCALE IN FEET

**REI** **RESOURCE ENGINEERING**  
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

PLATE 4  
**DEEP AQUIFER POTENTIOMETRIC  
MAP**  
FRENCH LIMITED

DRAWN BY: SJ	DATE: 10/29/86	PROJECT NO.: 275-14
CHK'D BY:	REVISED:	DWG. NO.:

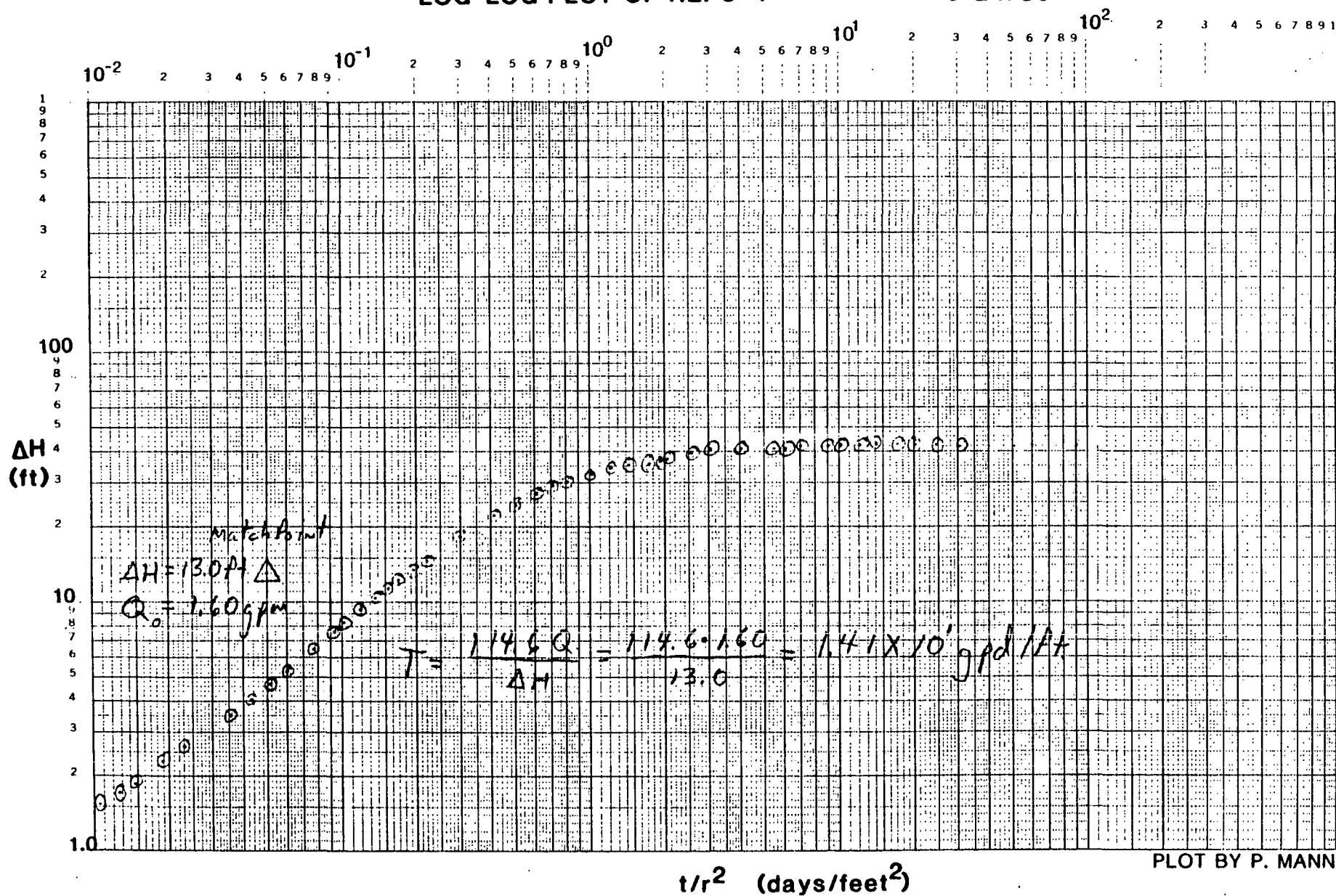
Attachment 5

REI 3-4 Run #2 Pumping Test  
Response Curves and Aquifer  
Characteristics Calculations

REI 3-4 RUN #2 PUMP TEST - DRAWDOWN

LOG-LOG PLOT OF REI 3-4

8/21/86



# CALCULATIONS AND COMPUTATIONS

SHEET 1 OF 1

PROJECT: FRENCH LTD

JOB NO.: 274-14

SUBJECT: REI 3-4 Run #2 Calc. for REI 3-4

COMPUTED BY: DRS DATE: 11-7-86

CHECKED BY: DD DATE: 11-15-86

## Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$\Delta H = 13.0 \text{ ft.} \quad T = \frac{(114.6)(1.60)}{13.0} = 1.41 \times 10^1 \text{ gpd/ft}$$

$$Q = 1.60 \text{ gpm}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 2.03 \times 10^{-6} \text{ m}^2/\text{s}$$

## Log-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 5.0 \times 10^{-2} \text{ days/ft}^2$$

$$T = 1.41 \times 10^1 \text{ gpd/ft}$$

$$S = \frac{(1)(1.41 \times 10^1)(5.0 \times 10^{-2})}{1.87} = 3.77 \times 10^{-1}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 1.41 \times 10^1 \text{ gpd/ft}$$

$$b = 23.0 \text{ ft}$$

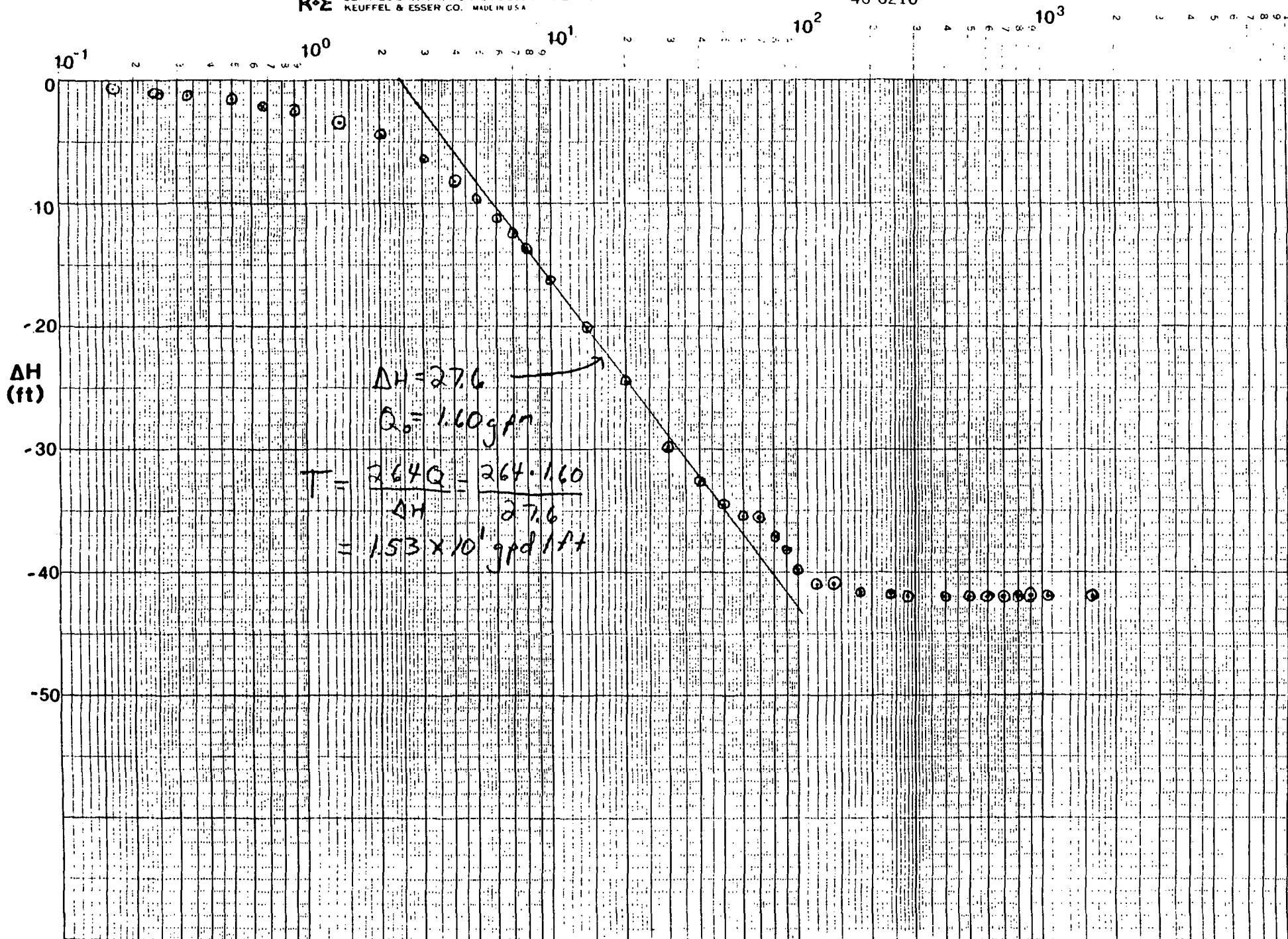
$$K = \frac{1.41 \times 10^1}{23.0} = 6.13 \times 10^{-1} \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 2.89 \times 10^{-5} \text{ cm/s}$$

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t (min)

46 6210



REI 3-4 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 3-4  
8/21/86

PLOT BY S. CAYLOR



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 3-4 Run #2 Calc for REI 2-4

COMPUTED BY: DRG DATE: 11-12-77

CHECKED BY: DD DATE: 11-19-81

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H}$$

$$Q = 1.60 \text{ gpm}$$

$$\Delta H = 27.6 \text{ ft} \quad T = \frac{(264)(1.60)}{27.6} = 1.53 \times 10^1 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 2.20 \times 10^{-6} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.3 T t_0}{r^2}$$

$$r = 0.166 \text{ ft.}$$

$$t_0 = 2.45 \text{ min.} / 1440 = 1.70 \times 10^{-3} \text{ days}$$

$$T = 1.53 \times 10^1 \text{ gpd/ft}$$

$$S = \frac{(0.3)(1.53 \times 10^1)(1.70 \times 10^{-3})}{(0.166)^2} = 2.83 \times 10^{-1}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 1.53 \times 10^1 \text{ gpd/ft}$$

$$b = 23.0 \text{ ft}$$

$$K = \frac{1.53 \times 10^1}{23.0} = 6.65 \times 10^{-1} \text{ gpd/ft}^2$$

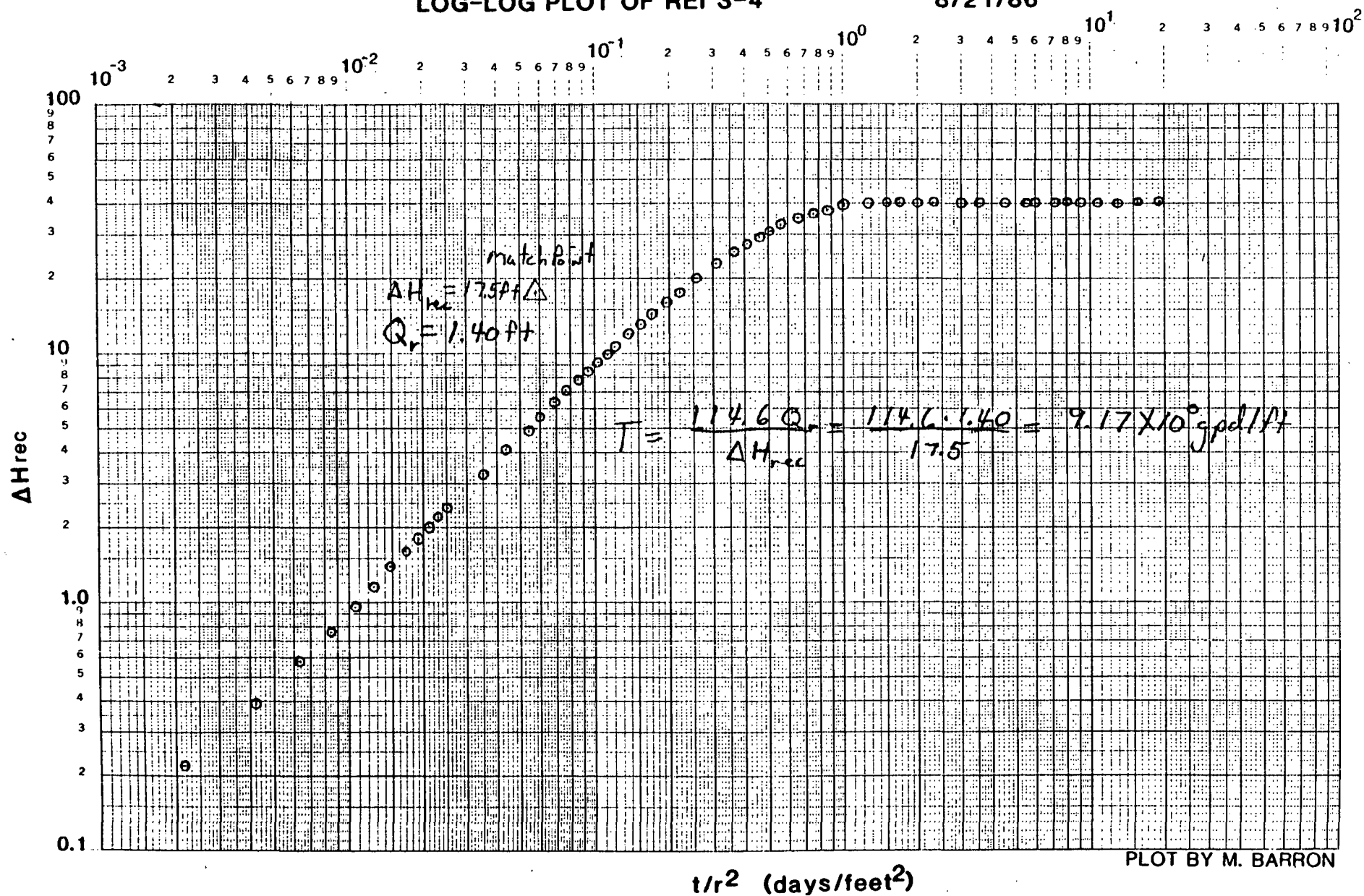
$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 3.14 \times 10^{-5} \text{ cm/s}$$

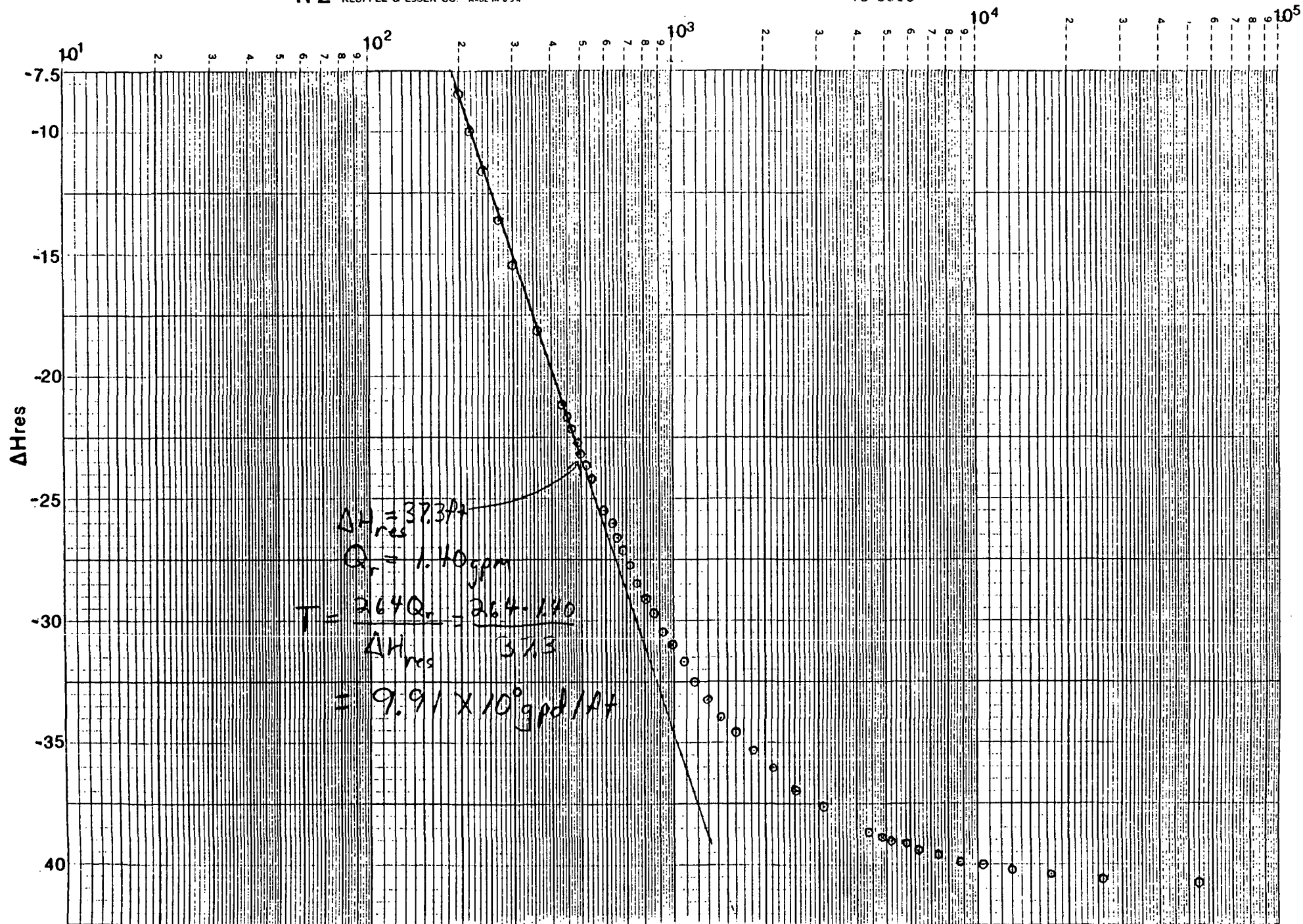
**ERT**

REI 3-4 RUN #2 PUMP TEST - RECOVERY

LOG-LOG PLOT OF REI 3-4

8/21/86





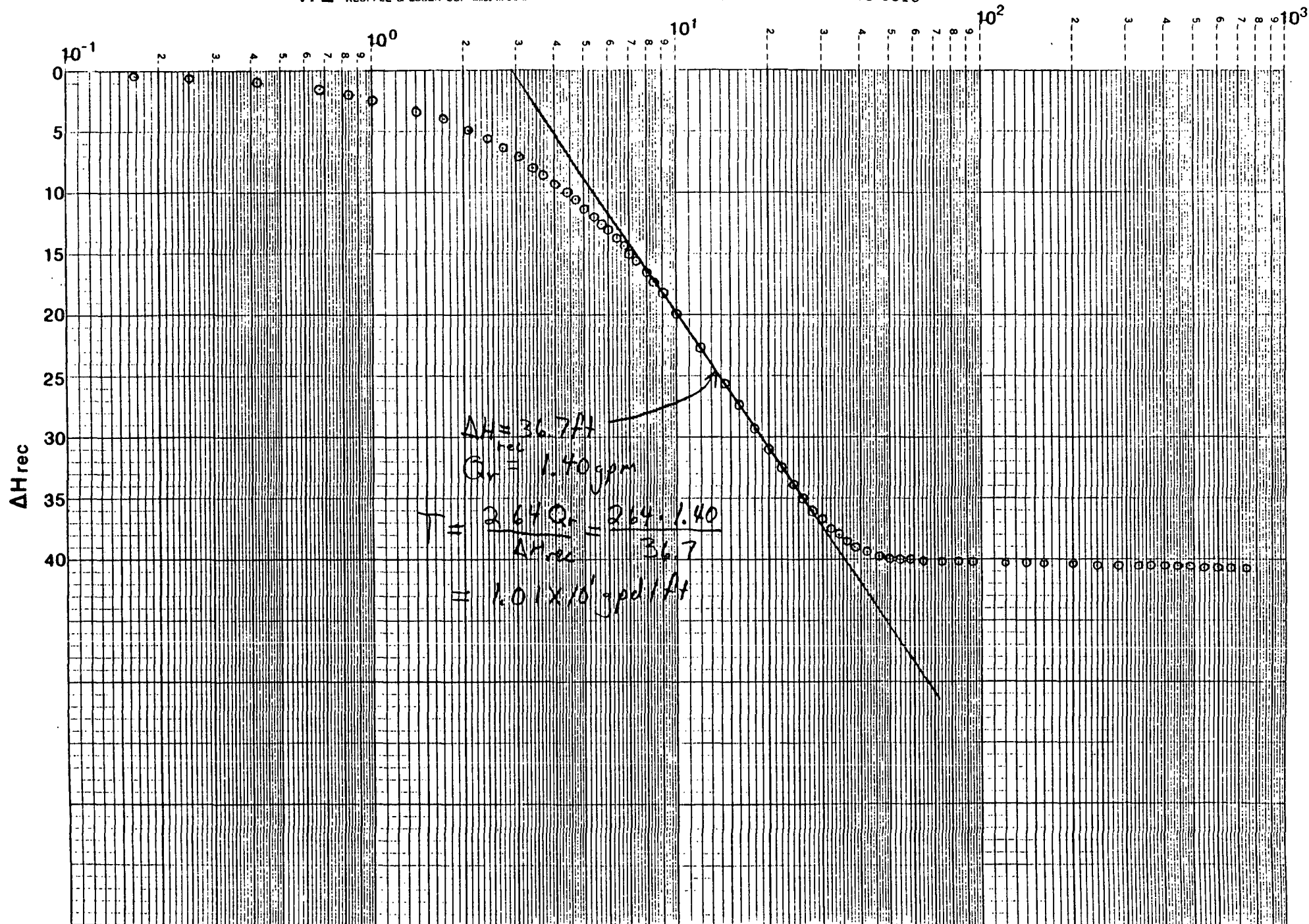
REI 3-4 RUN #2 PUMP TEST - RECOVERY  
SEMI-LOG PLOT OF REI 3-4

8/21/86

PLOT BY M. BARRON

t(min)

46 6010



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FREEMAN LTD.

JOB NO.: 275-14

SUBJECT: REI 3-4 Run #2 Calc for REI 3-4

COMPUTED BY: DRS DATE: 11-17-80

CHECKED BY: DD DATE: 11-18-80

## Log-Log solution for Transmissivity - Recovery

$$Transmissivity (T) = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$\Delta H = 17.3 \text{ ft}$$

$$Q = 1.40 \text{ gpm}$$

$$T = \frac{(114.6)(1.40)}{17.3} = 9.17 \times 10^0 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7} = 1.32 \times 10^{-6} \text{ m}^2/\text{s}$$

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \text{ where } b \text{ is the screened thickness in feet.}$$

$$T = 9.17 \times 10^0 \text{ gpd/ft}$$

$$b = 23.0 \text{ ft}$$

$$K = \frac{9.17 \times 10^0}{23.0} = 3.99 \times 10^{-1} \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 1.88 \times 10^{-5} \text{ cm/s}$$

## Semi-Log(a) solution for Transmissivity - Recovery

$$Transmissivity (T) = \frac{264 Q}{\Delta H_{res}}$$

$$Q = 1.40 \text{ gpm}$$

$$\Delta H_{res} = 37.3 \text{ ft}$$

$$T = \frac{(264)(1.40)}{37.3} = 9.91 \times 10^0 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7} = 1.42 \times 10^{-6} \text{ m}^2/\text{s}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 574-16

SUBJECT: PEI 3-4 Run #2 Calc for PEI 3-4

COMPUTED BY: DFK DATE: 1-17-88

CHECKED BY: DD DATE: 1-19-88

Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 9.91 \times 10^0 \text{ gpd/ft}$$

$$b = 23.0 \text{ ft}$$

$$K = \frac{9.91 \times 10^0}{23.0} = 4.31 \times 10^{-1} \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 2.03 \times 10^{-5} \text{ cm/s}$$

Semi-Log( $\epsilon$ ) solution for Transmissivity - Recovery

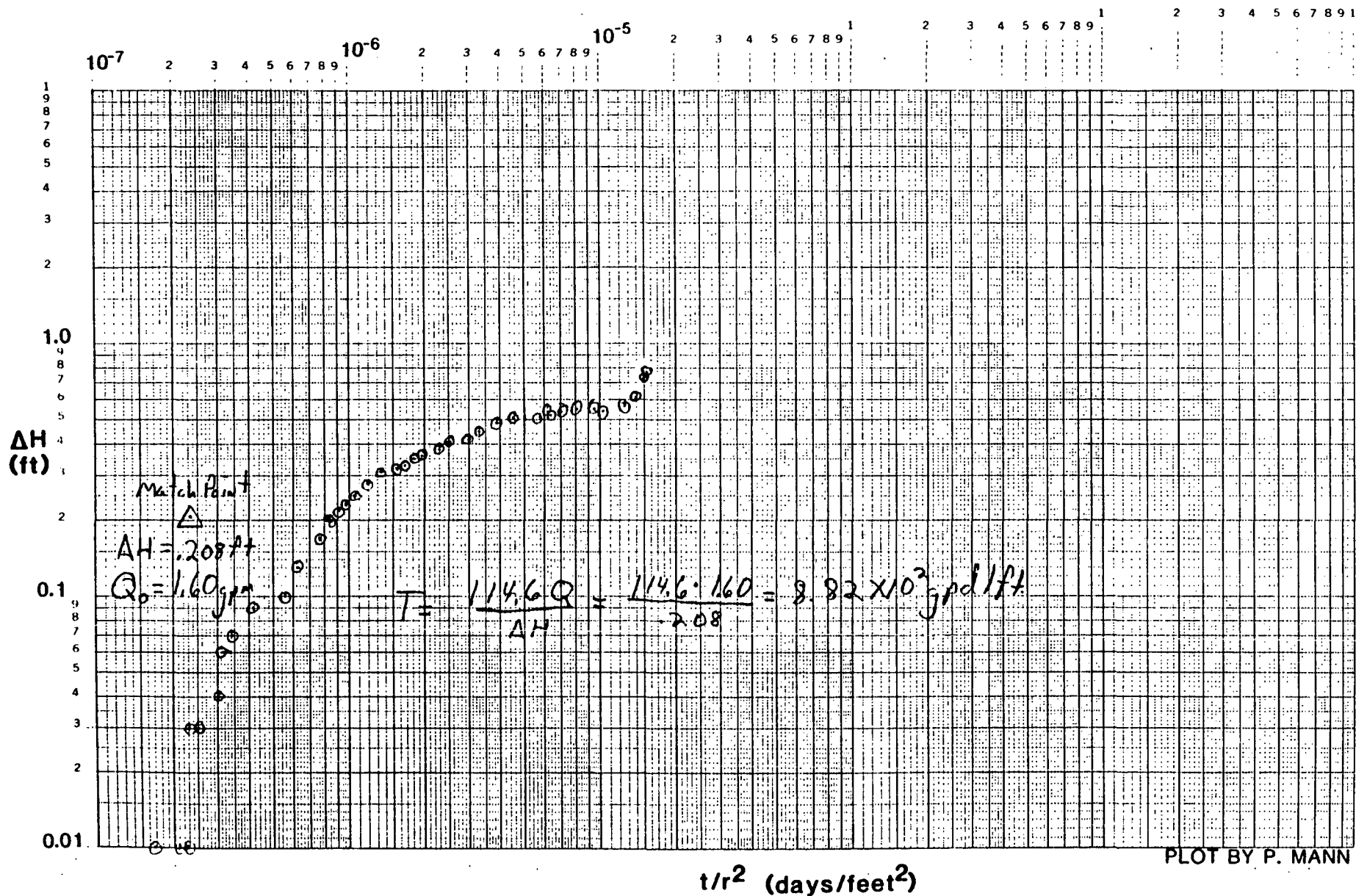
$$\text{Transmissivity (T)} = \frac{26.4 Q}{4h_{rec}}$$

$$Q = 1.40 \text{ gpm}$$

$$4h_{rec} = 36.7 \text{ ft} \quad T = \frac{(26.4)(1.40)}{36.7} = 1.01 \times 10^1 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.422 \times 10^{-7} = 1.45 \times 10^{-6} \text{ m/s}$$

REI 3-4 RUN #2 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI-11 8/21/86



# CALCULATIONS AND COMPUTATIONS

SHEET 2 OF       

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 3-4 Run #2 Calc. for REI 11

COMPUTED BY: DRG DATE: 11-17-82

CHECKED BY: DD DATE: 11-19-82

## Log-Log solution for Transmissivity - Drawdown

$$T = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$\Delta H = 0.208 \text{ ft}$$

$$Q = 1.60 \text{ gpm}$$

$$T = \frac{(114.6)(1.60)}{0.208} = 8.82 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 1.27 \times 10^{-4} \text{ m/s}$$

## Log-Log solution for Storativity - Drawdown

$$S = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 2.35 \times 10^{-7} \text{ days/ft}^2$$

$$T = 8.82 \times 10^2 \text{ gpd/ft}$$

$$S = \frac{(1)(8.82 \times 10^2)(2.35 \times 10^{-7})}{1.87} = 1.11 \times 10^{-4}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 8.82 \times 10^2 \text{ gpd/ft}$$

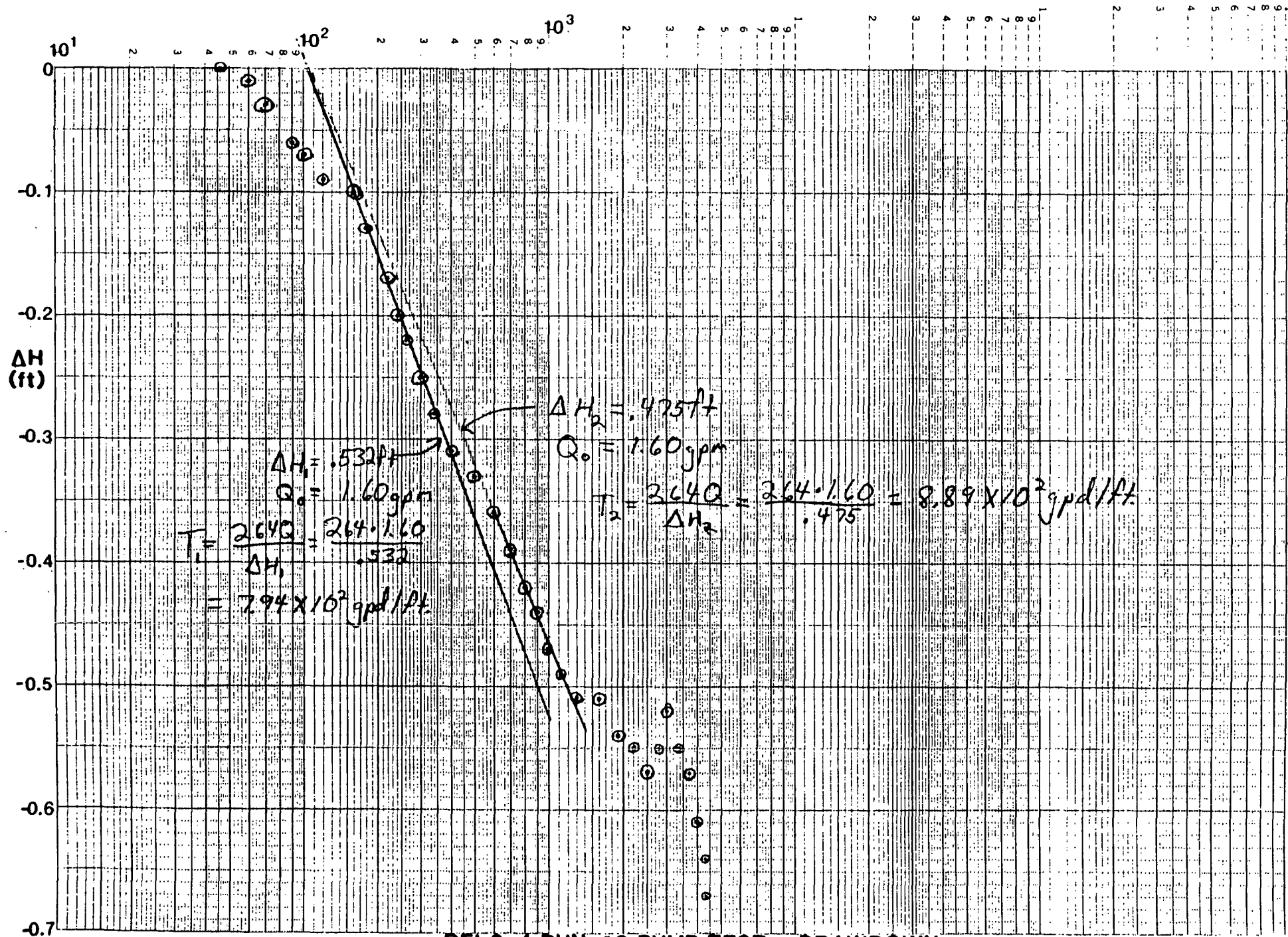
$$b = 16.45 \text{ ft}$$

$$K = \frac{8.82 \times 10^2}{16.45} = 5.36 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 2.53 \times 10^{-3} \text{ m/s}$$

**ERT**





# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 238-14

SUBJECT: REI 3-4 Run #2 Calc for REI 11

COMPUTED BY: DRG DATE: 11-17-80

CHECKED BY: DD DATE: 11-17-80

Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264Q}{\Delta H}$$

$$Q = 1.60 \text{ gpm}$$

$$\Delta H_1 = 0.532 \text{ ft} \quad T_1 = \frac{(264)(1.60)}{0.532} = 7.94 \times 10^2 \text{ gpd/ft}$$

$$\Delta H_2 = 0.475 \text{ ft} \quad T_2 = \frac{(264)(1.60)}{0.475} = 8.89 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7}$$

$$= 1.14 \times 10^{-4} \text{ m}^2/\text{s}$$

$$= 1.22 \times 10^{-4} \text{ m}^2/\text{s}$$

Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.3 T t_0}{r^2}$$

$$r = 446.391 \text{ ft}$$

$$t_{01} = 105 \text{ min} / 1440 = 7.29 \times 10^{-2} \text{ days}$$

$$T_1 = 7.94 \times 10^2 \text{ gpd/ft}$$

$$t_{02} = 105 \text{ min} / 1440 = 7.29 \times 10^{-2} \text{ days}$$

$$T_2 = 8.89 \times 10^2 \text{ gpd/ft}$$

$$S_1 = \frac{(0.3)(7.94 \times 10^2)(7.29 \times 10^{-2})}{(446.391)^2} = 8.71 \times 10^{-5}$$

$$S_2 = \frac{(0.3)(8.89 \times 10^2)(7.29 \times 10^{-2})}{(446.391)^2} = 9.76 \times 10^{-5}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FREIGHT LTD

JOB NO.: 275-14

SUBJECT: PEI 2-4 Run #2 Calc for PEI 11

COMPUTED BY: DD DATE: 11-17-82

CHECKED BY: DD DATE: 11-19-82

Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T_1 = \boxed{7.94 \times 10^2 \text{ gpd/ft}}$$

$$b = 16.45 \text{ ft}$$

$$K = \frac{7.94 \times 10^2}{16.45} = \boxed{4.83 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = \boxed{2.28 \times 10^{-3} \text{ cm/s}}$$

$$T_2 = \boxed{8.89 \times 10^2 \text{ gpd/ft}}$$

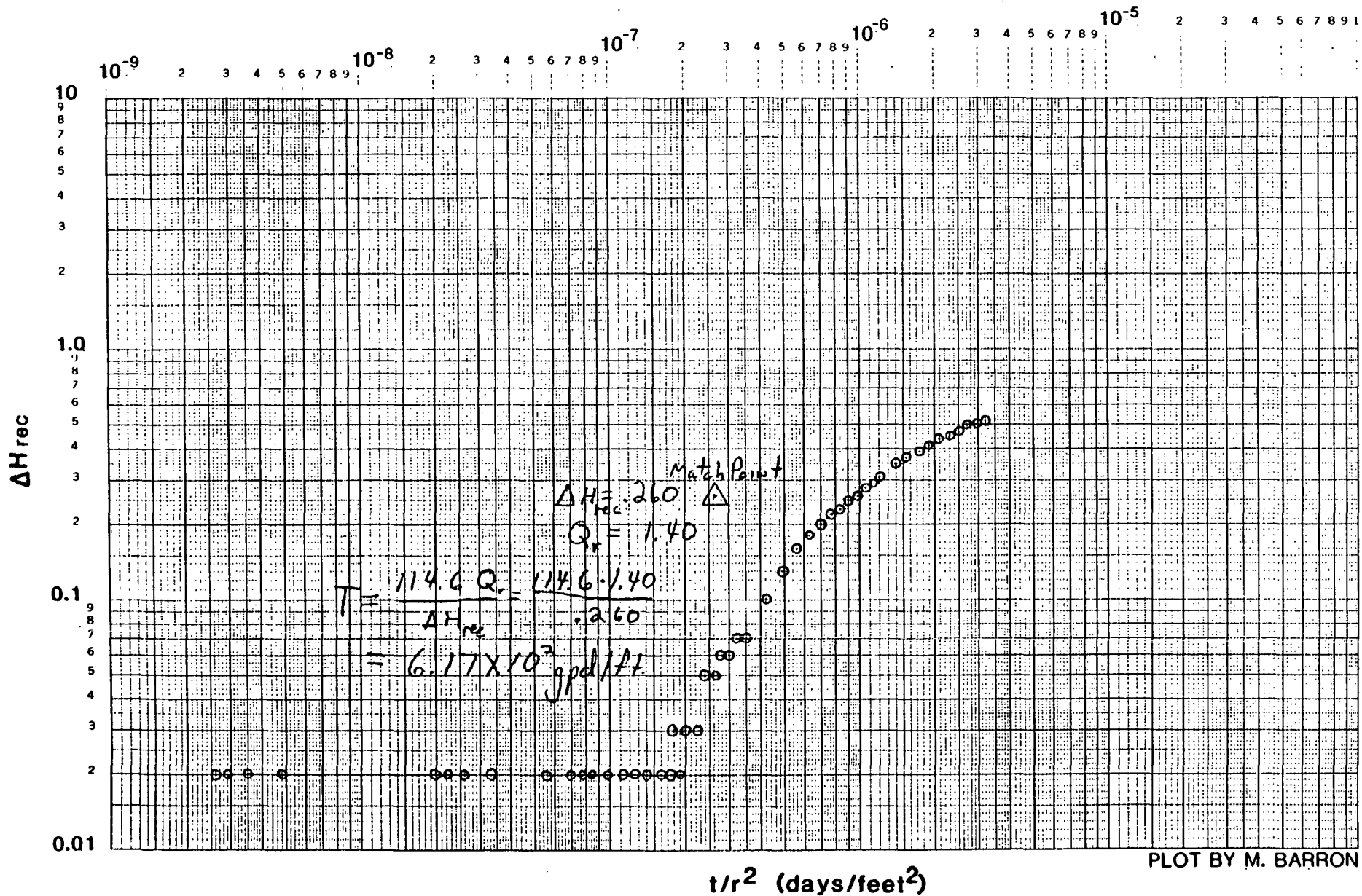
$$b = 16.45 \text{ ft}$$

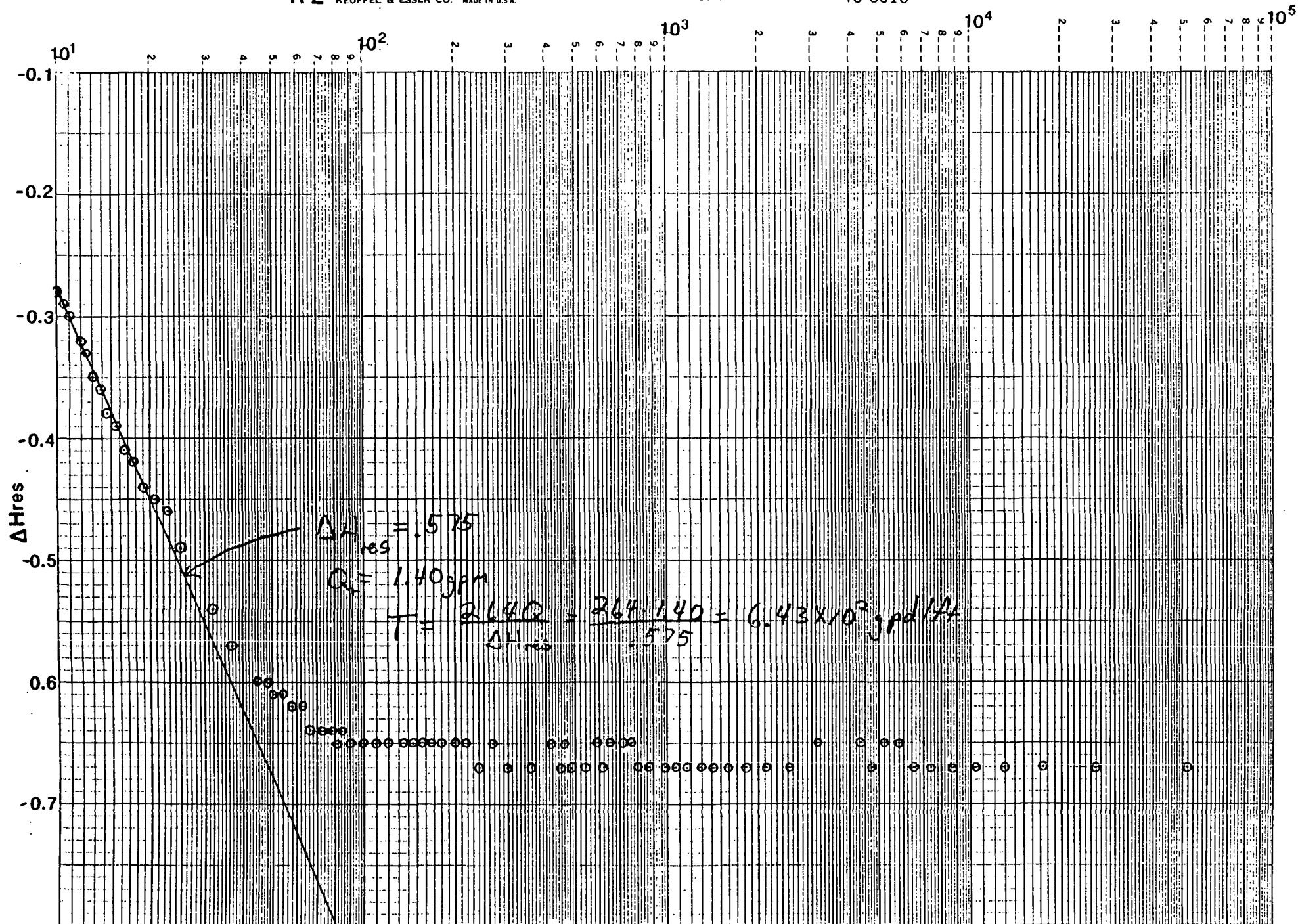
$$K = \frac{8.89 \times 10^2}{16.45} = \boxed{5.41 \times 10^1 \text{ gpd/ft}^2}$$

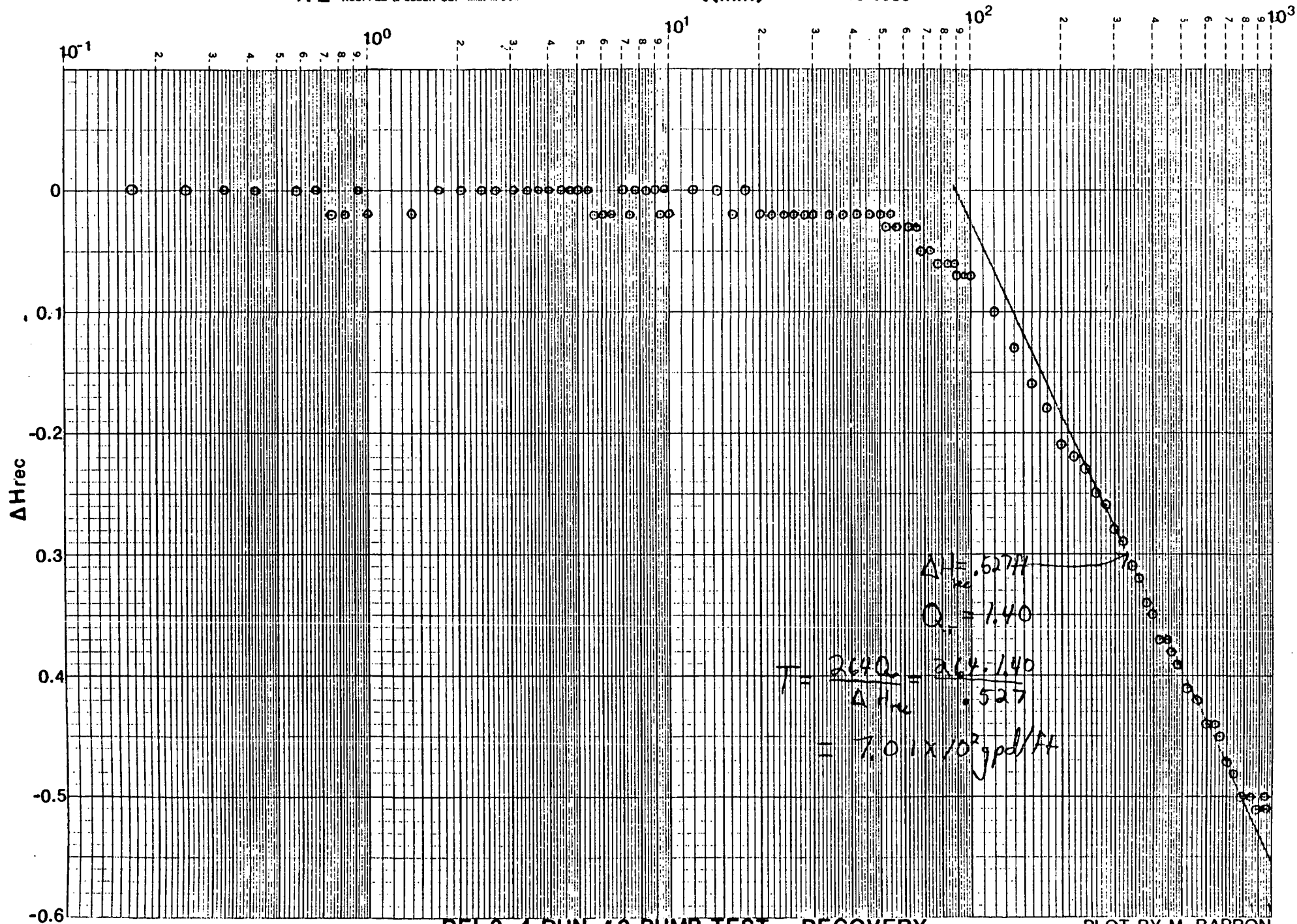
$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = \boxed{2.55 \times 10^{-3} \text{ cm/s}}$$

REI 3-4 RUN #2 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF REI-11

8/21/86







# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FREIGHT LTD.

JOB NO.: 275-10

SUBJECT: PFI 3-4 Pump 2 Calc for REF 11

COMPUTED BY: DRS DATE: 11/1/88

CHECKED BY: DD DATE: 11/1/88

## Log-Log solution for Transmissivity - Recovery

$$Transmissivity (T) = \frac{114.6 Q W(u)}{\Delta h}$$

where  $W(u) = 1$

$$\Delta h = 0.260 \text{ ft}$$

$$Q = 1.40 \text{ gpm}$$

$$T = \frac{(114.6)(1.40)}{0.260} = 6.17 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.422 \times 10^{-7} = 8.87 \times 10^{-5} \text{ m}^2/\text{s}$$

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 6.17 \times 10^2 \text{ gpd/ft}$$

$$b = 16.45 \text{ ft}$$

$$K = \frac{6.17 \times 10^2}{16.45} = 3.75 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 1.77 \times 10^{-3} \text{ cm/s}$$

## Semi-Log(u) solution for Transmissivity - Recovery

$$Transmissivity (T) = \frac{264 Q}{\Delta h_{res}}$$

$$Q = 1.40 \text{ gpm}$$

$$\Delta h_{res} = 0.575 \text{ ft}$$

$$T = \frac{(264)(1.40)}{0.575} = 6.43 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.432 \times 10^{-7} = 9.24 \times 10^{-5} \text{ m}^2/\text{s}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 275-16

SUBJECT: REI 3-4 Pump = 2 Calc for REI 11

COMPUTED BY: PCS DATE: 11/27/86

CHECKED BY: DD DATE: 11/28/86

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = \boxed{6.43 \times 10^2 \text{ gpd/ft}}$$

$$b = 16.45 \text{ ft}$$

$$K = \frac{6.43 \times 10^2}{16.45} = \boxed{3.91 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = \boxed{1.84 \times 10^{-3} \text{ cm/s}}$$

## Semi-Log(b) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H_{\text{rec}}}$$

$$Q = 1.40 \text{ cfm}$$

$$\Delta H_{\text{rec}} = 0.527 \text{ ft} \quad T = \frac{(264)(1.40)}{0.527} = \boxed{7.01 \times 10^2 \text{ gpd/ft}}$$

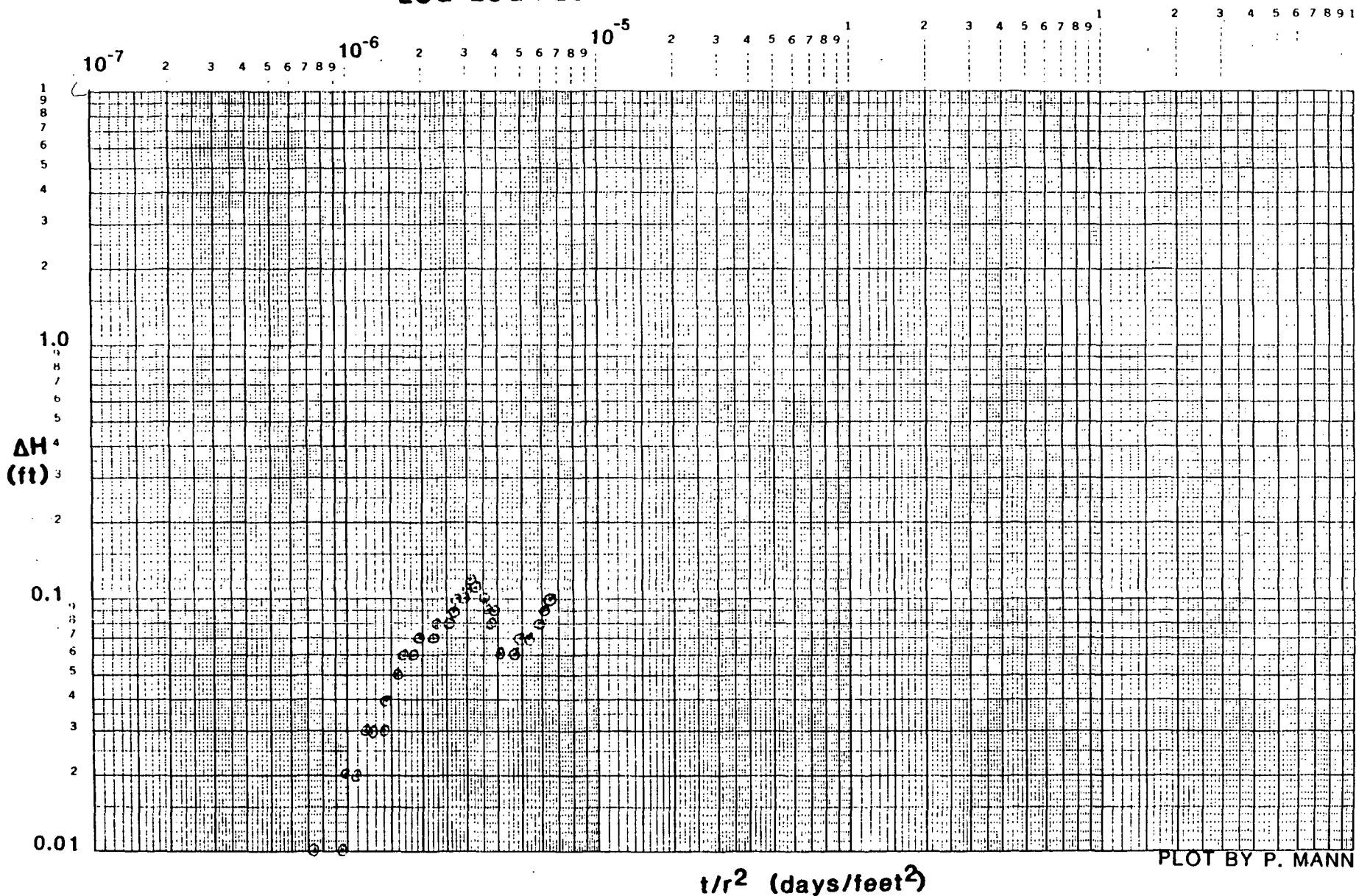
$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = \boxed{1.01 \times 10^{-4} \text{ m}^2/\text{s}}$$

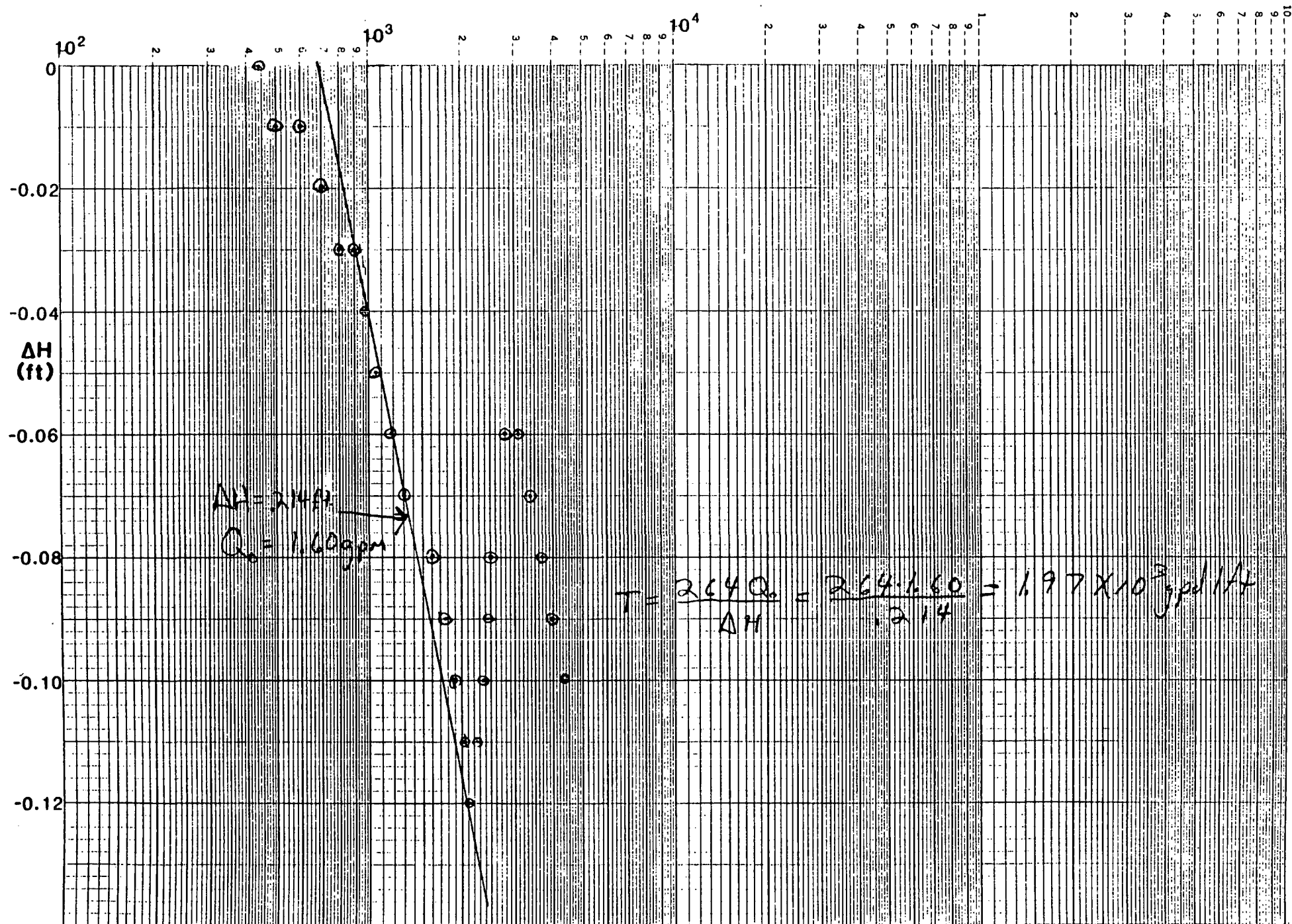


REI 3-4 RUN #2 PUMP TEST - DRAWDOWN

LOG-LOG PLOT OF REI-7

8/21/86





# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 3-4 Run #2 Calc for REI 7

COMPUTED BY: DRG DATE: 11-17-20

CHECKED BY: DD DATE: 11-18-20

Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H}$$

$$Q = 1.60 \text{ gpm}$$

$$\Delta H = 0.214 \text{ ft}$$

$$T = \frac{(264)(1.60)}{0.214} = 1.97 \times 10^3 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.432 \times 10^{-7} = 2.84 \times 10^{-4} \text{ m}^2/\text{s}$$

Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.3 T t_0}{r^2}$$

$$r = 682.670 \text{ ft}$$

$$t_0 = 690 \text{ min} / 1440 = 4.79 \times 10^{-1} \text{ days}$$

$$T = 1.97 \times 10^3 \text{ gpd/ft}$$

$$S = \frac{(0.3)(1.97 \times 10^3)(4.79 \times 10^{-1})}{(682.670)^2} = 6.07 \times 10^{-4}$$

Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 1.97 \times 10^3 \text{ gpd/ft}$$

$$b = 15.0 \text{ ft}$$

$$K = \frac{1.97 \times 10^3}{15.0} = 1.32 \times 10^2 \text{ gpd/ft}^2$$

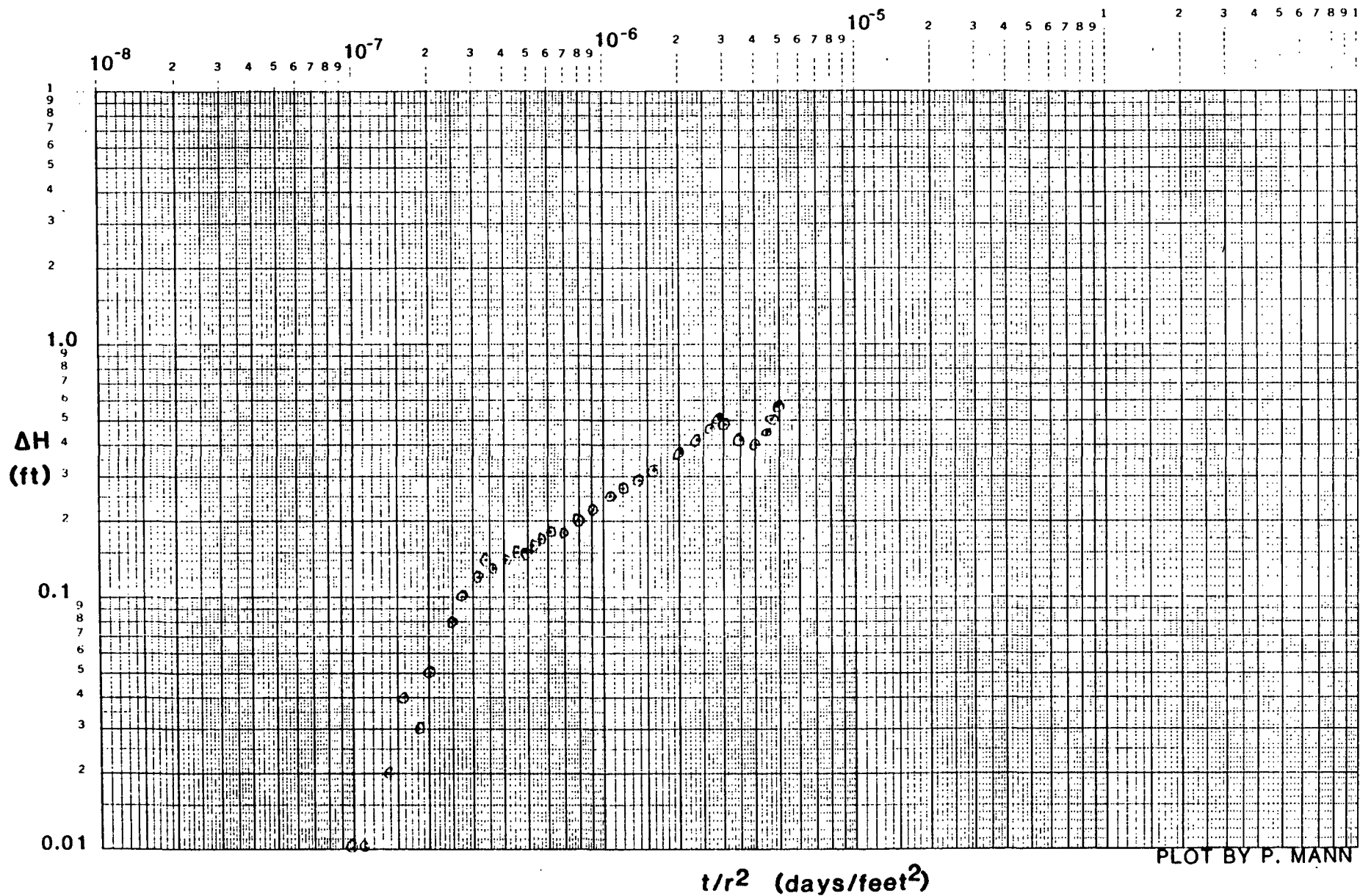
$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 6.20 \times 10^{-5} \text{ cm/s}$$

**ERT**

REI 3-4 RUN #2 PUMP TEST - DRAWDOWN

LOG-LOG PLOT OF REI 10-1

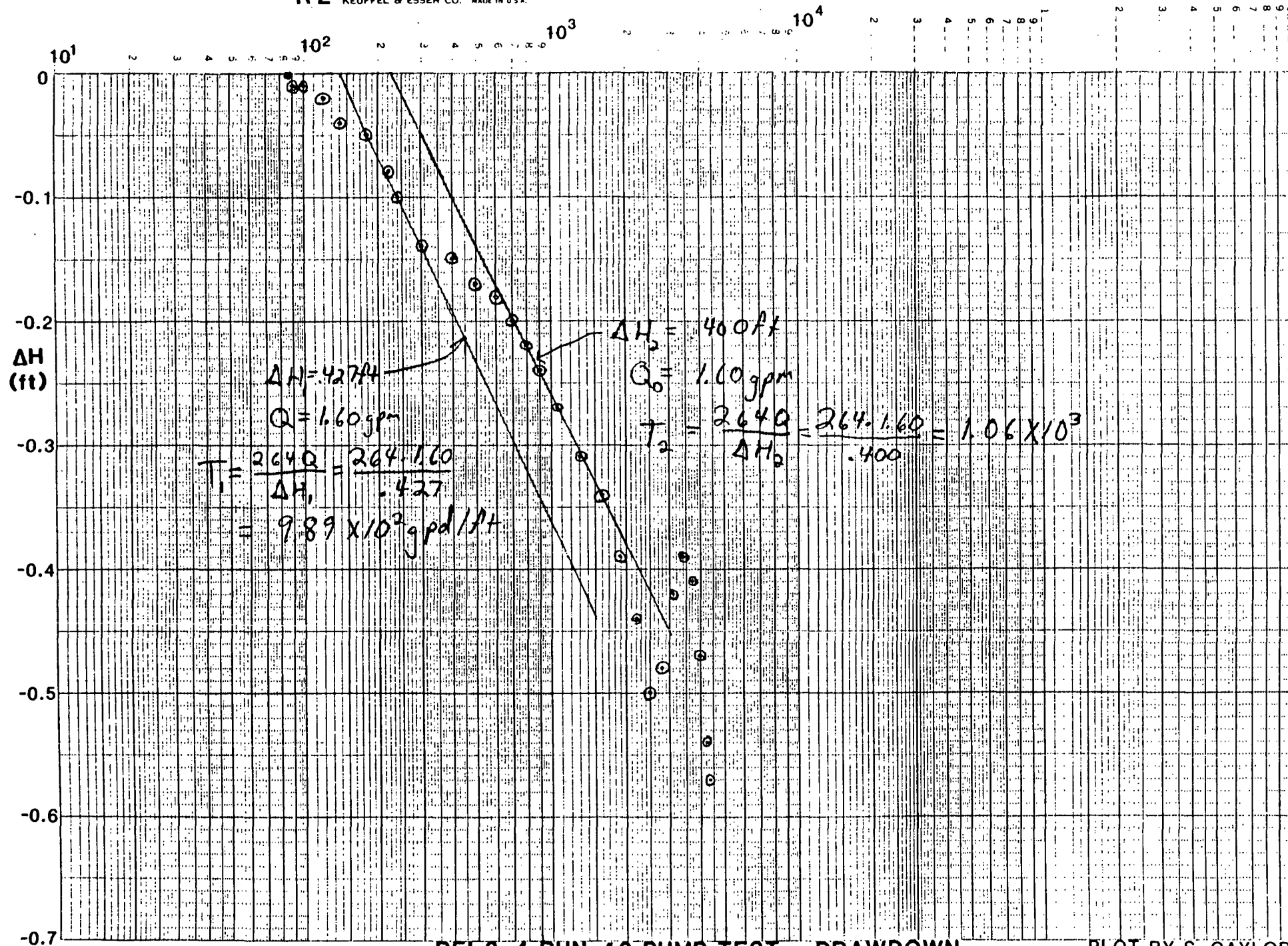
8/21/86



K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

46 6210



REI 3-4 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 10 1 8/21/86

PLOT BY S. CAYLOR

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 274-10

SUBJECT: REI 3-4 Run #2 Calc. for REI 10-1

COMPUTED BY: DRK DATE: 11-17-88

CHECKED BY: DD DATE: 11-19-88

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264Q}{\Delta H}$$

$$Q = 1.60 \text{ gpm}$$

$$\Delta H_1 = 0.427 \text{ ft} \quad T_1 = \frac{(264)(1.60)}{0.427} = 9.89 \times 10^2 \text{ gpd/ft}$$

$$\Delta H_2 = 0.400 \text{ ft} \quad T_2 = \frac{(264)(1.60)}{0.400} = 1.06 \times 10^3 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.432 \times 10^{-7} =$$

$$1.42 \times 10^{-6} \text{ m}^2/\text{s}$$

$$1.52 \times 10^{-4} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storage - Drawdown

$$\text{Storage (S)} = \frac{0.3 T t_c}{r^2}$$

$$r = 784.360 \text{ ft}$$

$$t_{c1} = 140 \text{ min} / 1440 = 9.72 \times 10^{-2} \text{ days}$$

$$T_1 = 9.89 \times 10^2 \text{ gpd/ft}$$

$$t_{c2} = 225 \text{ min} / 1440 = 1.56 \times 10^{-1} \text{ days}$$

$$T_2 = 1.06 \times 10^3 \text{ gpd/ft}$$

$$S_1 = \frac{(0.3)(9.89 \times 10^2)(9.72 \times 10^{-2})}{(784.360)^2} = 4.69 \times 10^{-5}$$

$$S_2 = \frac{(0.3)(1.06 \times 10^3)(1.56 \times 10^{-1})}{(784.360)^2} = 8.06 \times 10^{-5}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 575-10

SUBJECT: PEI 2-11 Run #2 Calc for PEI 10-1

COMPUTED BY: DD DATE: 11-19-81

CHECKED BY: DD DATE: 11-19-81

Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T_1 = \boxed{9.89 \times 10^2 \text{ gpd/ft}}$$

$$b = 25.30 \text{ ft}$$

$$K = \frac{9.89 \times 10^2}{25.30} = \boxed{3.91 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{ Conversion Factor } 4.713 \times 10^{-5} = \boxed{1.84 \times 10^{-3} \text{ cm/s}}$$

$$T_2 = \boxed{1.06 \times 10^3 \text{ gpd/ft}}$$

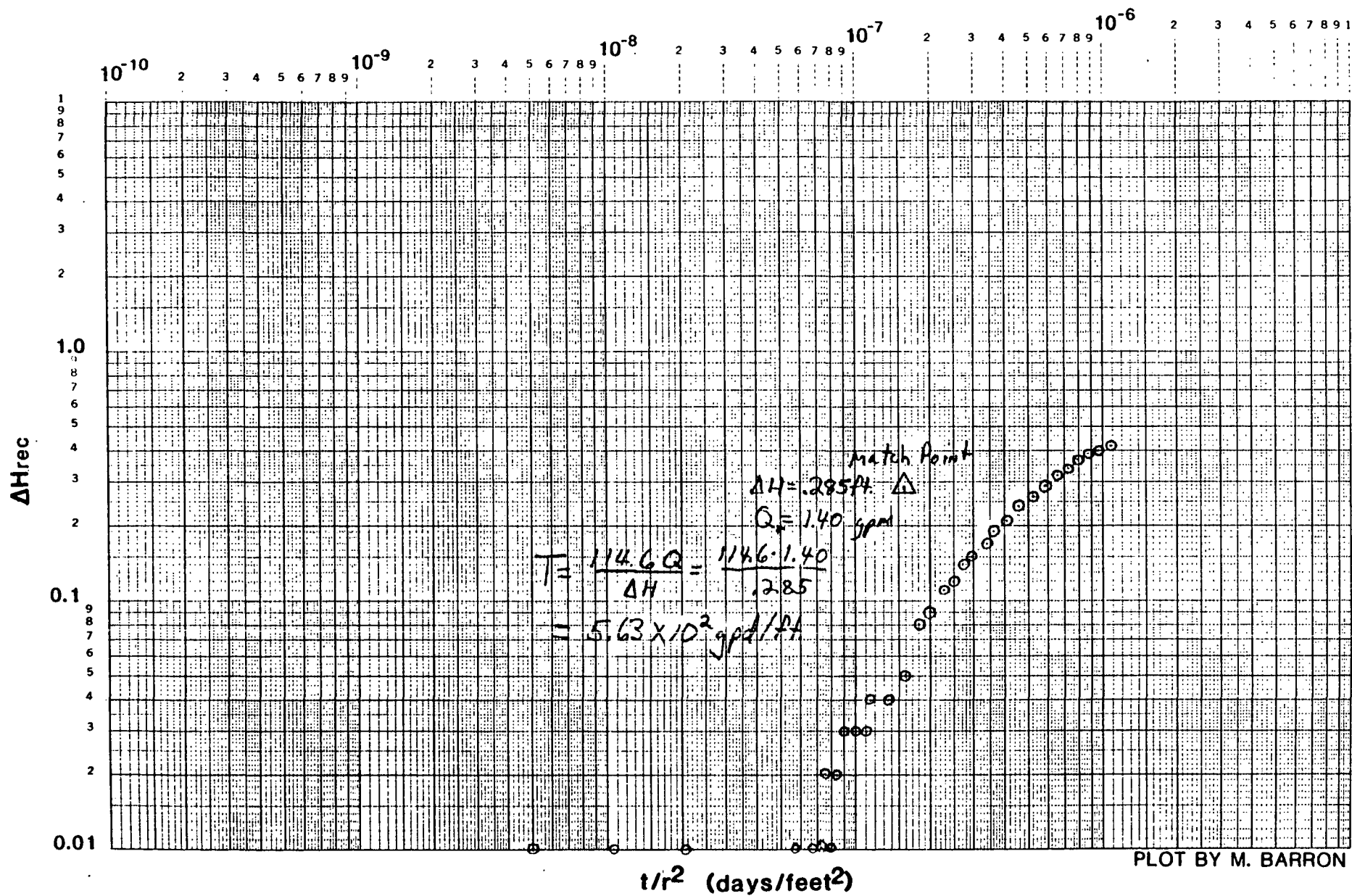
$$b = 25.30 \text{ ft}$$

$$K = \frac{1.06 \times 10^3}{25.30} = \boxed{4.17 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{ Conversion Factor } 4.713 \times 10^{-5} = \boxed{1.97 \times 10^{-3} \text{ cm/s}}$$

**ERT**

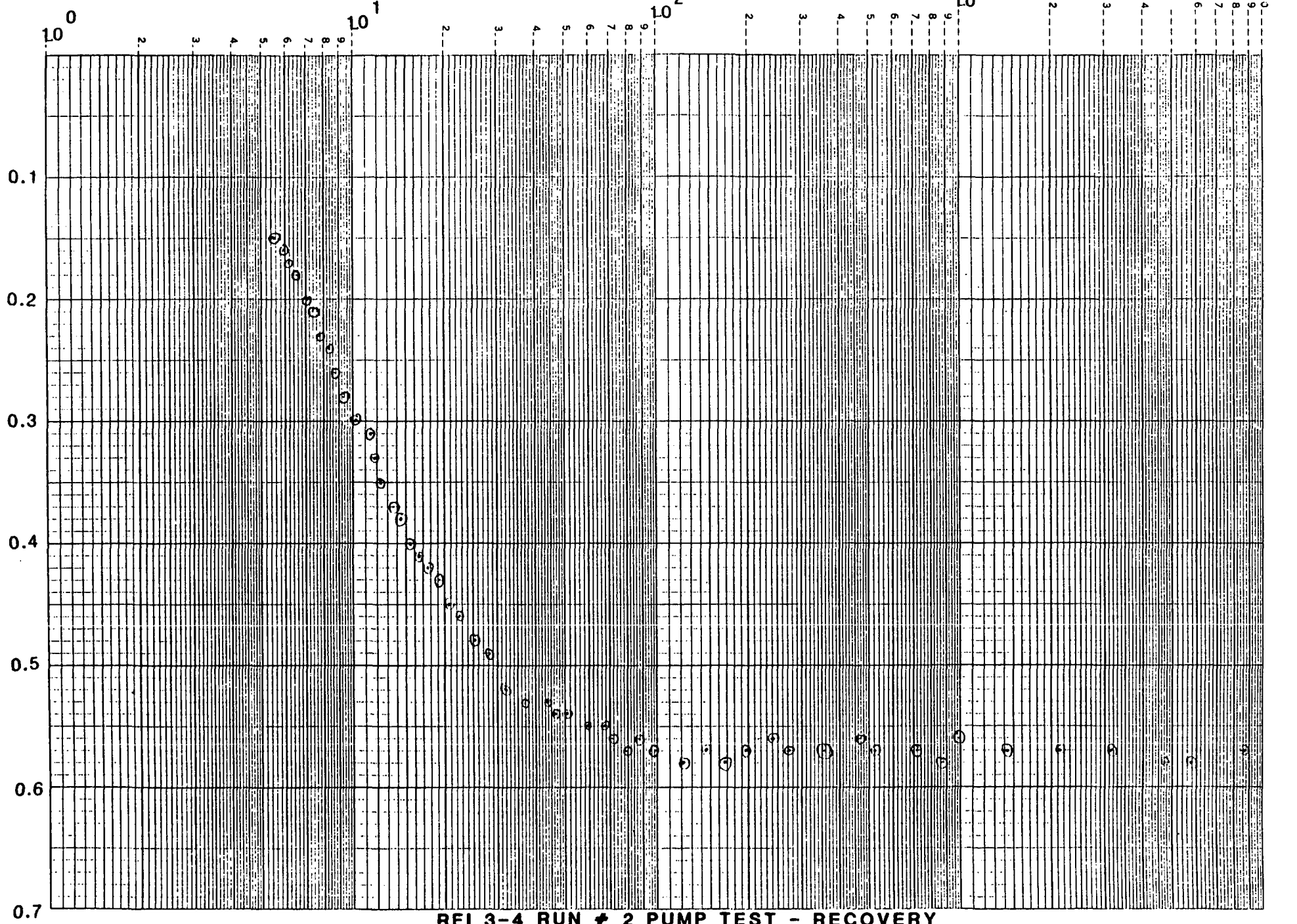
**8/21/86**





$t/t'$

46 6010



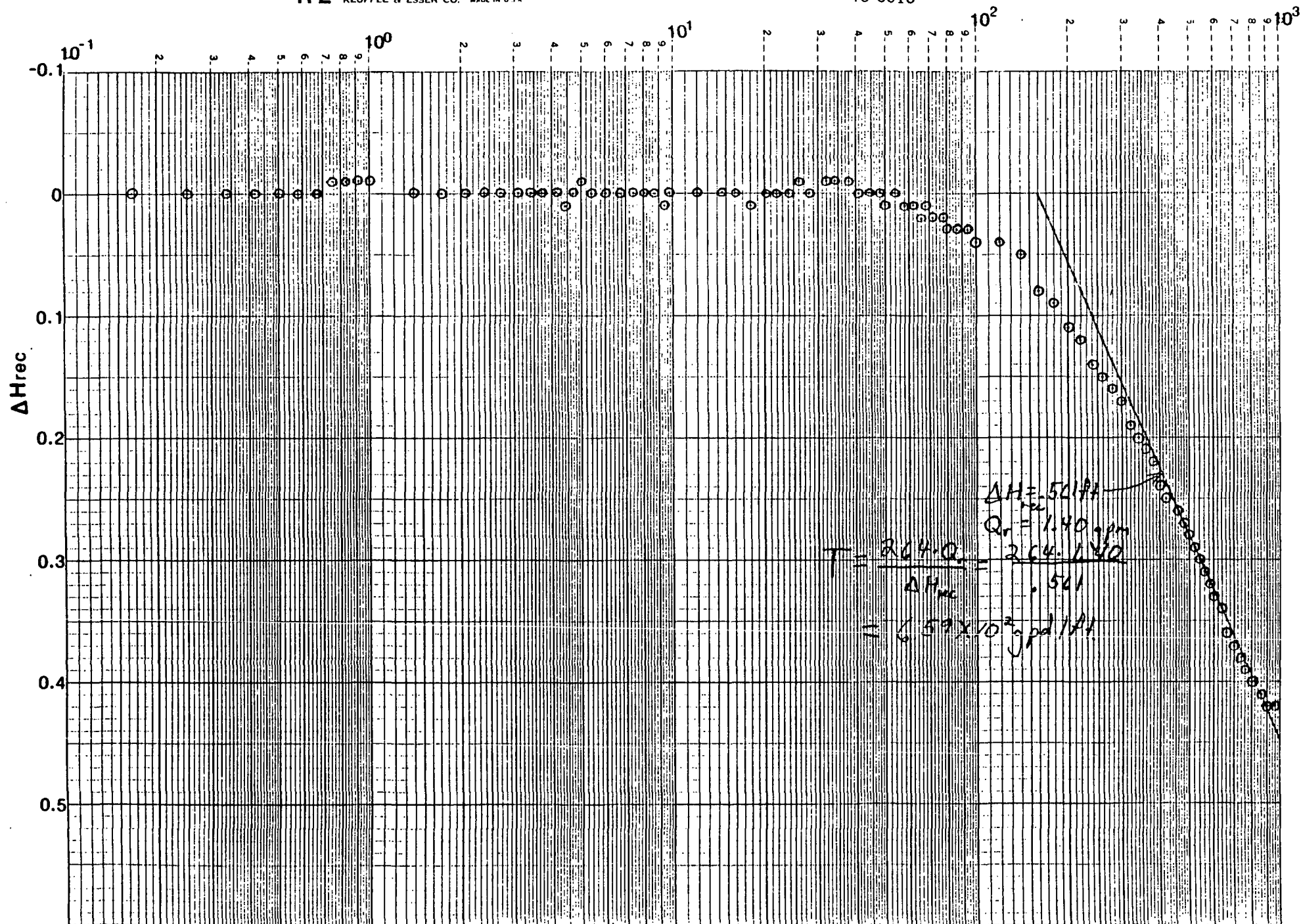
REI 3-4 RUN # 2 PUMP TEST - RECOVERY

SEMI-LOG PLOT OF REI 10-1

8/21/88

t(min)

46 6010



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: ERF/CH LTD

JOB NO.: 275-16

SUBJECT: REI 3-4 Run #2 Calc for REI 10-1

COMPUTED BY: DR DATE: 12-14

CHECKED BY: DD DATE: 11-19-80

Log-Log solution for Transmissivity - Recovery

$$\text{Transmissivity } (T) = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$\begin{aligned} \Delta H &= 0.285 \text{ ft} \\ Q &= 1.40 \text{ gpm} \end{aligned} \quad T = \frac{(114.6)(1.40)}{0.285} = 5.63 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 8.10 \times 10^{-5} \text{ m}^2/\text{s}$$

Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 5.63 \times 10^2 \text{ gpd/ft}$$

$$b = 25.30 \text{ ft}$$

$$K = \frac{5.63 \times 10^2}{25.30} = 2.23 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.713 \times 10^{-5} = 1.05 \times 10^{-3} \text{ cm/s}$$

Semi-Log (a) solution for Transmissivity - Recovery

$$\text{Transmissivity } (T) = \frac{264 Q}{\Delta H_{res}}$$

$$Q = 1.40 \text{ gpm}$$

$$\Delta H_{res} = 0.582 \text{ ft} \quad T = \frac{(264)(1.40)}{0.582} = 6.35 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 9.13 \times 10^{-5} \text{ m}^2/\text{s}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FPE INC. LTD.

JOB NO.: 274-14

SUBJECT: PEI 3-4 Run #2 Calc for REI 10-1

COMPUTED BY: JPS DATE: 1-12

CHECKED BY: JD DATE: 1-12-86

Solution for Hydraulic Conductivity - Recovery

$$R = \frac{I}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = \boxed{6.35 \times 10^2 \text{ gpd/ft}}$$

$$b = 25.30 \text{ ft}$$

$$R = \frac{6.35 \times 10^2}{25.30} = \boxed{2.51 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = \boxed{1.18 \times 10^{-3} \text{ cm/s}}$$

Semi-Log(E) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264Q}{\Delta H_{rec}}$$

$$Q = 1.40 \text{ gpm}$$

$$\Delta H_{rec} = 0.561 \text{ ft} \quad T = \frac{(264)(1.40)}{0.561} = \boxed{6.59 \times 10^2 \text{ gpd/ft}^2}$$

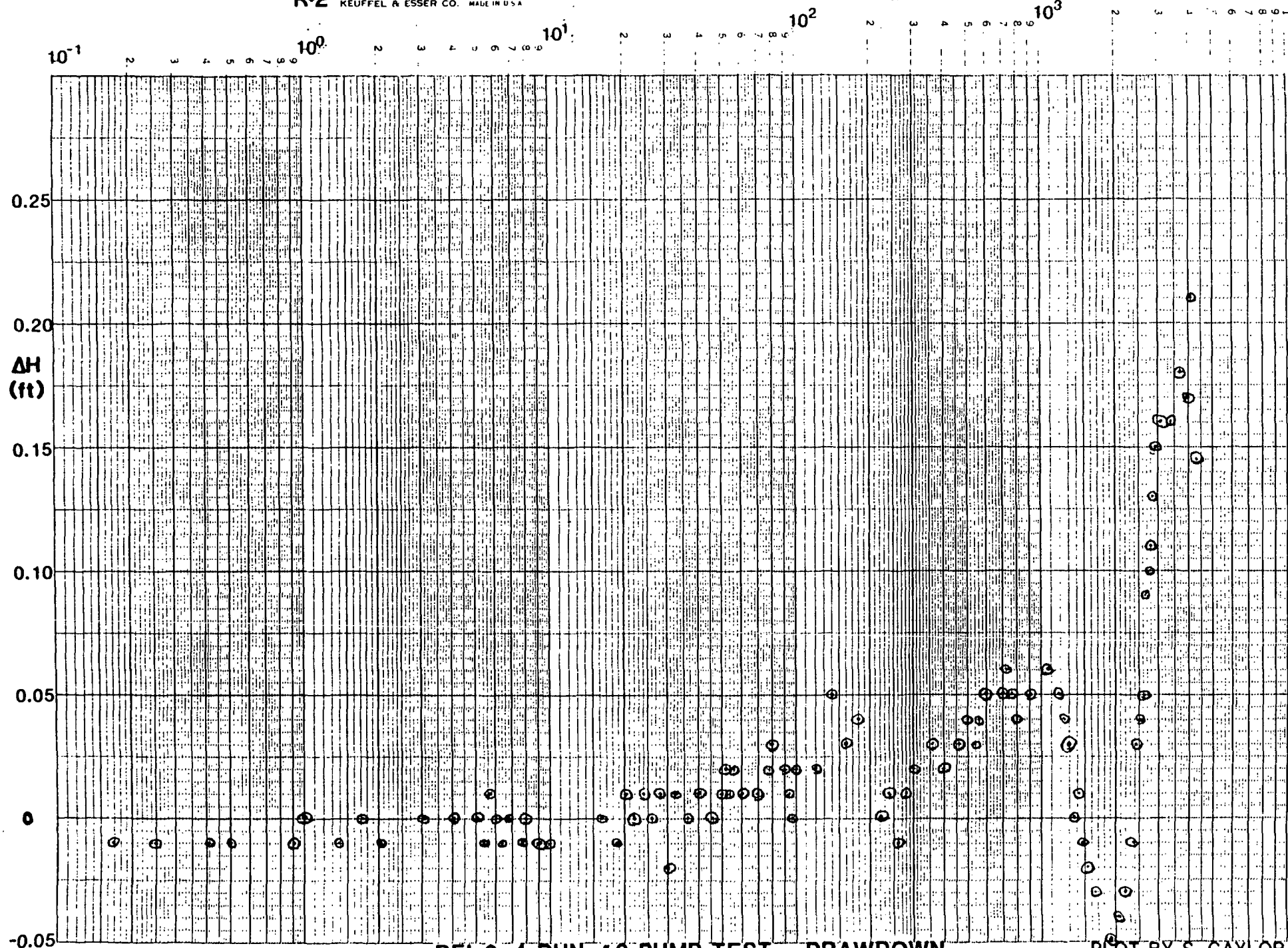
$$\times \text{Conversion Factor } 1.428 \times 10^{-7} = \boxed{9.47 \times 10^{-5} \text{ m}^2/\text{s}}$$

**ERT**

K&E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

46 6210



REI 3-4 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 3-4

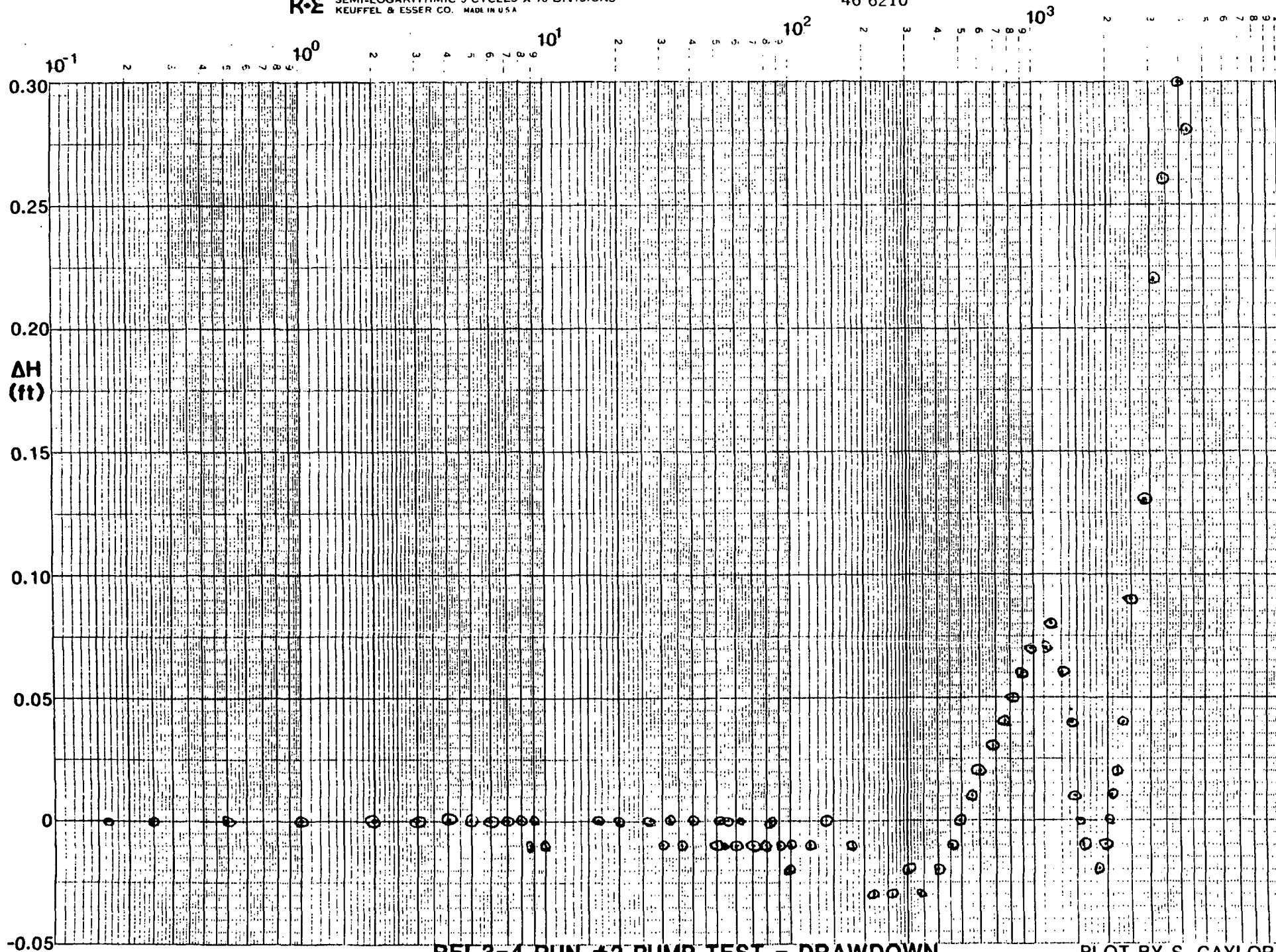
8/21/86

PLOT BY S. CAYLOR

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

46 6210



REI 3-4 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 3-2

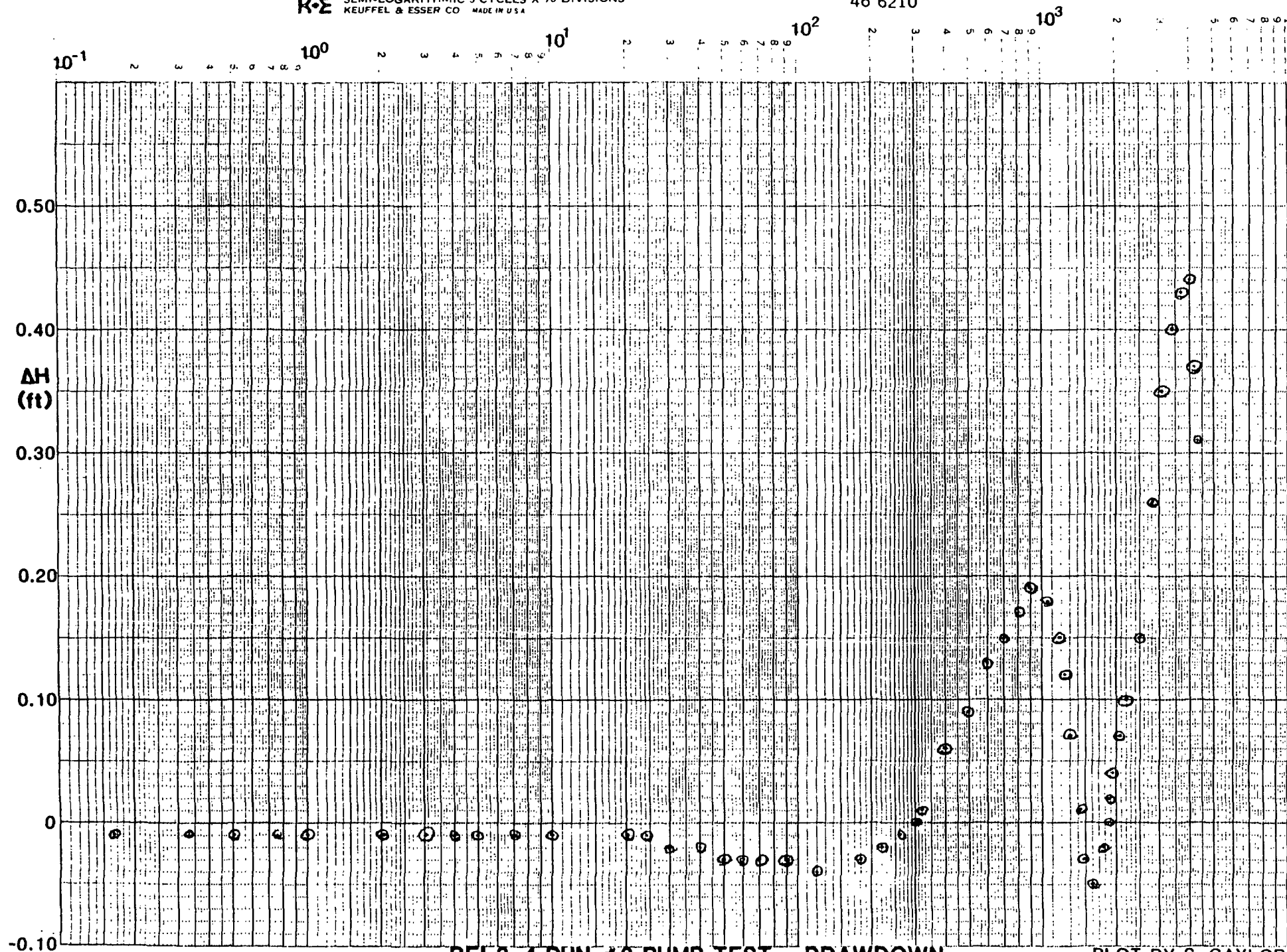
8/21/86

PLOT BY S. CAYLOR

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

46 6210



REI 3-4 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 2-2

8/21/86

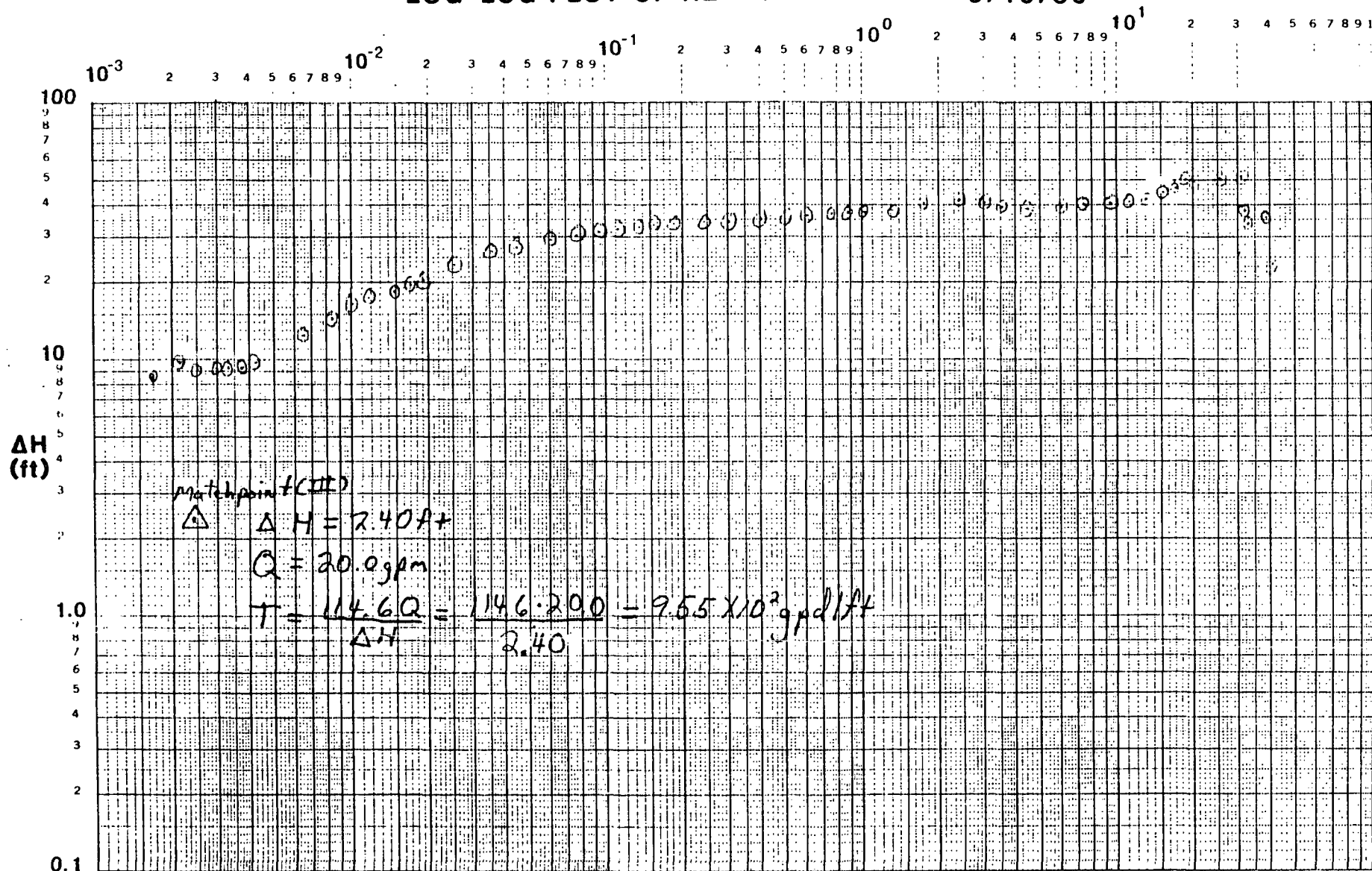
PLOT BY S. CAYLOR

Attachment 6

REI 10-1 Run #1 Pumping Test  
Response Curves and Aquifer  
Characteristics Calculations



REI 10-1 RUN #1 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI 10-1 9/15/86



PLOT BY T. BOCCA

$t/r^2$  (days/feet<sup>2</sup>)

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 27-14

SUBJECT: REI 10-1 RUD=1 Calc. for REI 10-1

COMPUTED BY: DES DATE: 11-1-81

CHECKED BY: DD DATE: 11-1-81

Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$Q = 20.0 \text{ gpm}$$

$$\Delta H = 2.40 \text{ ft} \quad T = \frac{(114.6)(20.0)}{2.40} = 9.55 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7} = 1.27 \times 10^{-4} \text{ m}^2/\text{s}$$

Log-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 2.42 \times 10^{-7} \text{ days/ft}^2$$

$$T = 9.55 \times 10^2 \text{ gpd/ft}$$

$$S = \frac{(1)(9.55 \times 10^2)(2.42 \times 10^{-7})}{1.87} = 1.24 \times 10^{-4}$$

Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is tie screened thickness in feet.}$$

$$T = 9.55 \times 10^2 \text{ gpd/ft}$$

$$b = 25.30 \text{ ft}$$

$$K = \frac{9.55 \times 10^2}{25.30} = 3.77 \times 10 \text{ gpd/ft}^2$$

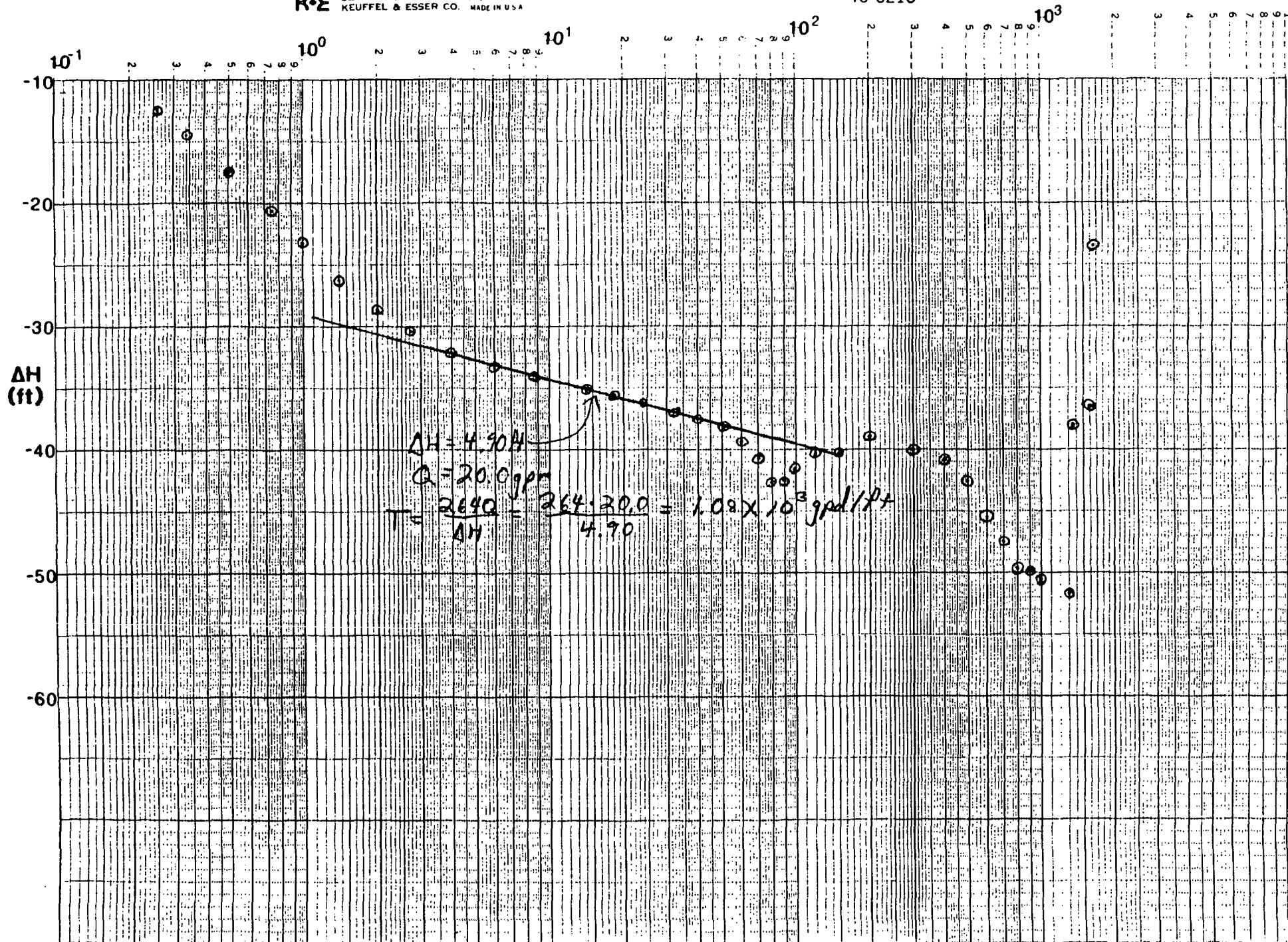
$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 1.78 \times 10^{-5} \text{ cm/s}$$

**ERT**

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

46 6210



REI 10-1 RUN #1 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 10-1

0/15/86

PLOT BY T. BOCCA

# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-1 Pur #1 Calc for REI 10-1

COMPUTED BY: DRG DATE: 11-8-86

CHECKED BY: DD DATE: 11-9-86

## Semi-Log solution for Transmissivity - Drawdown

$$Transmissivity (T) = \frac{264Q}{\Delta H}$$

$$Q = 20.0 \text{ gpm}$$

$$\Delta H = 4.90 \text{ ft} \quad T = \frac{(264)(20.0)}{4.90} = 1.08 \times 10^3 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 1.55 \times 10^{-4} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storativity - Drawdown

$$Storativity (S) = \frac{0.3 T t_0}{r^2}$$

$$r = 0.166 \text{ ft}$$

$$t_0 = 2.35 \times 10^{-5} \text{ min.} / 1440 = 1.63 \times 10^{-8} \text{ days}$$

$$T = 1.08 \times 10^3 \text{ gpd/ft}$$

$$S = \frac{(0.3)(1.08 \times 10^3)(1.63 \times 10^{-8})}{(0.166)^2} = 1.92 \times 10^{-4}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 1.08 \times 10^3 \text{ gpd/ft}$$

$$b = 25.30 \text{ ft}$$

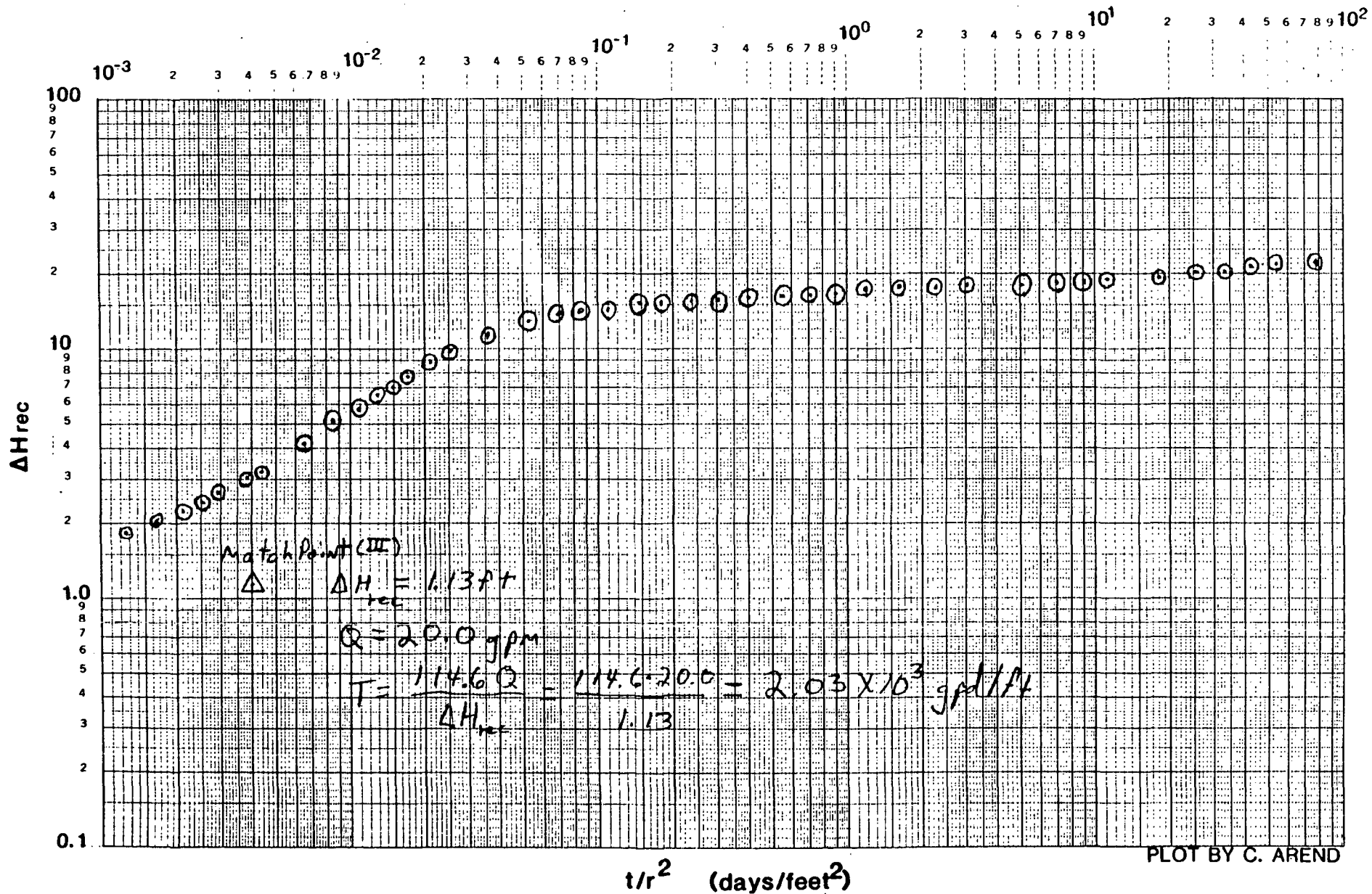
$$K = \frac{1.08 \times 10^3}{25.30} = 4.26 \times 10^{-1} \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 2.01 \times 10^{-5} \text{ cm/s}$$

**ERT**

REI 10-1 RUN #1 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF REI 10-1

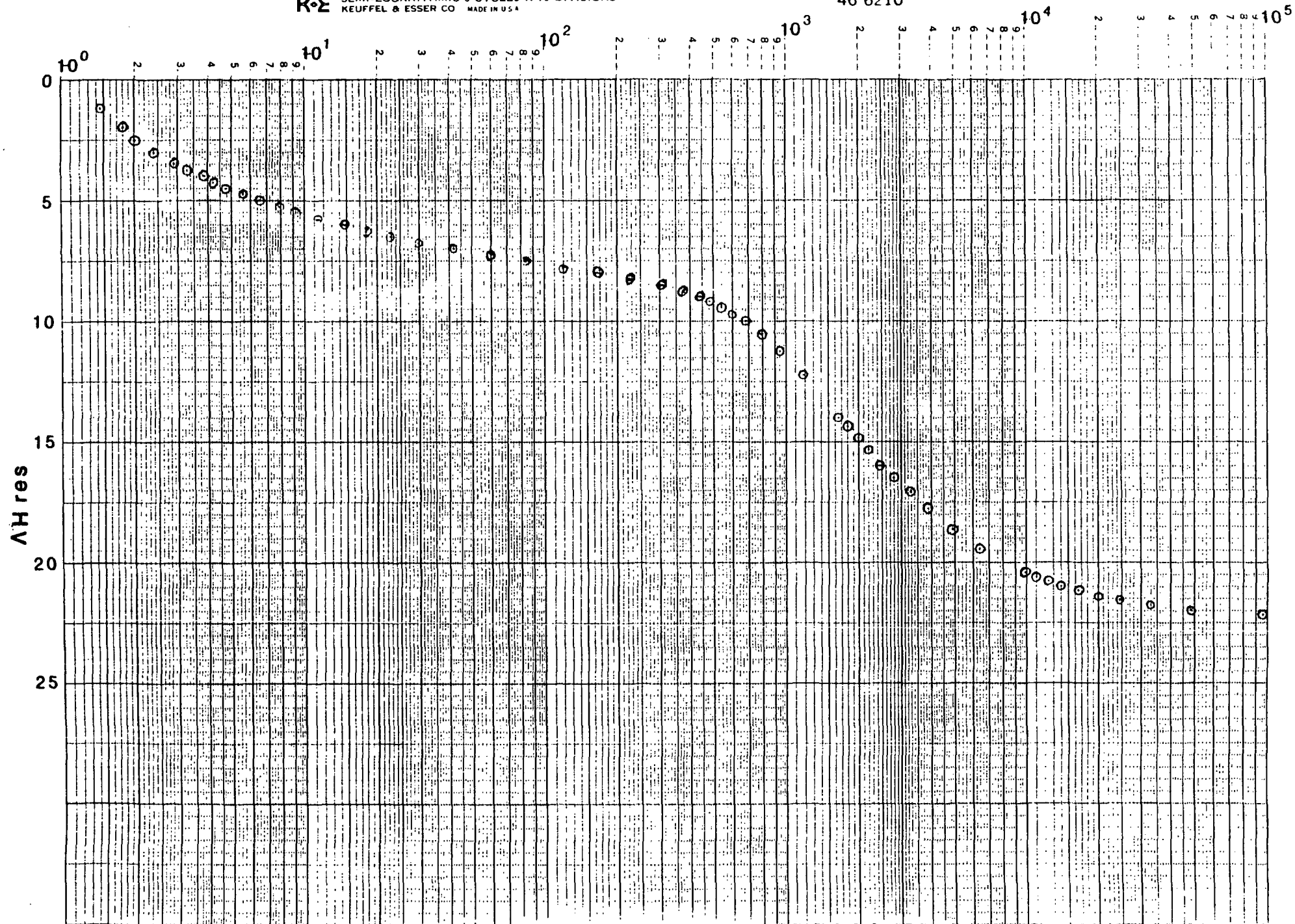
9/15/86



K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

$t/t'$

46 6210



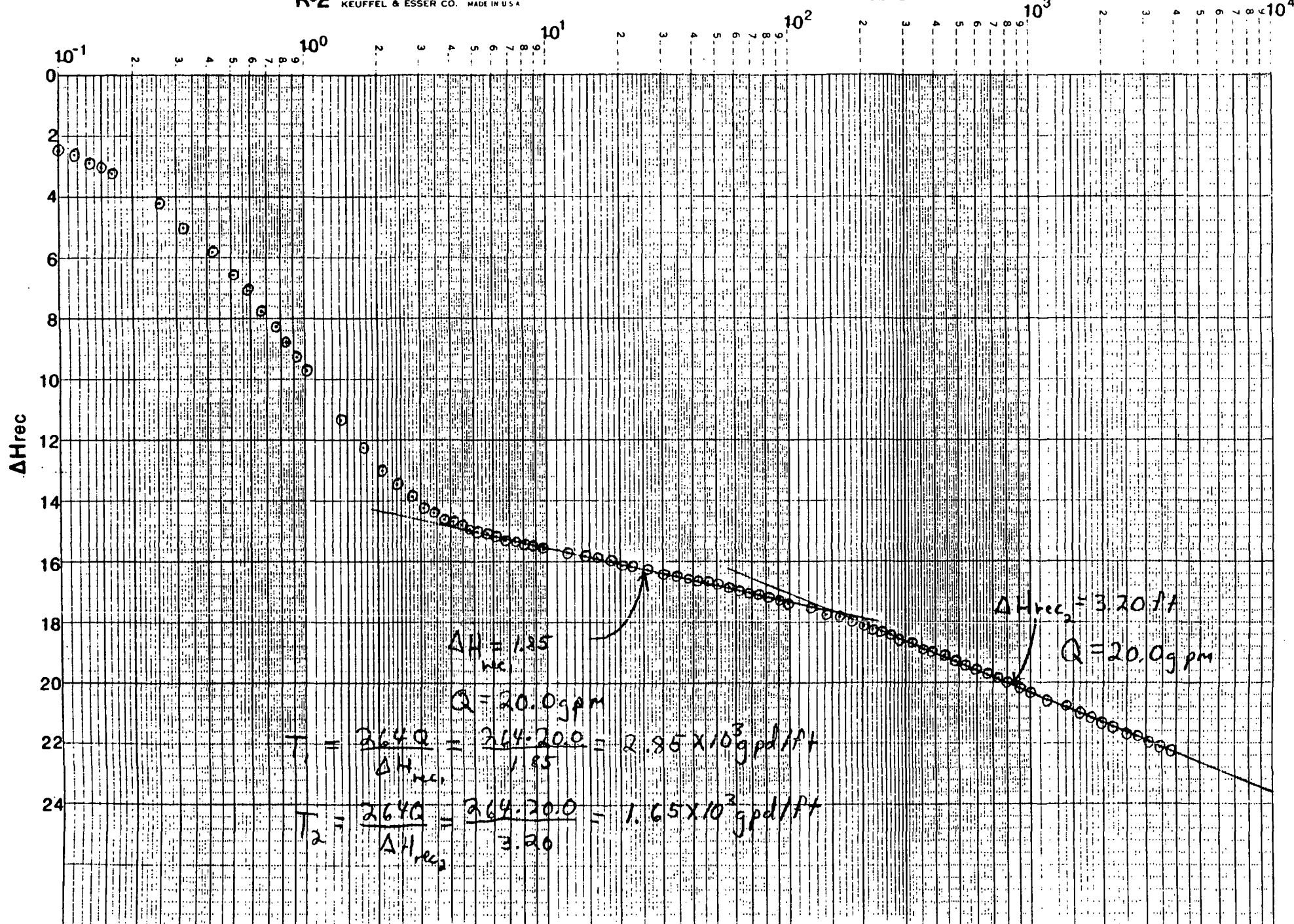
REI 10-1 RUN #1 PUMP TEST - RECOVERY  
SEMI-LOG PLOT OF REI 10-1  
9/15/86

PLOT BY M. BARRON

K·E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

46 6210

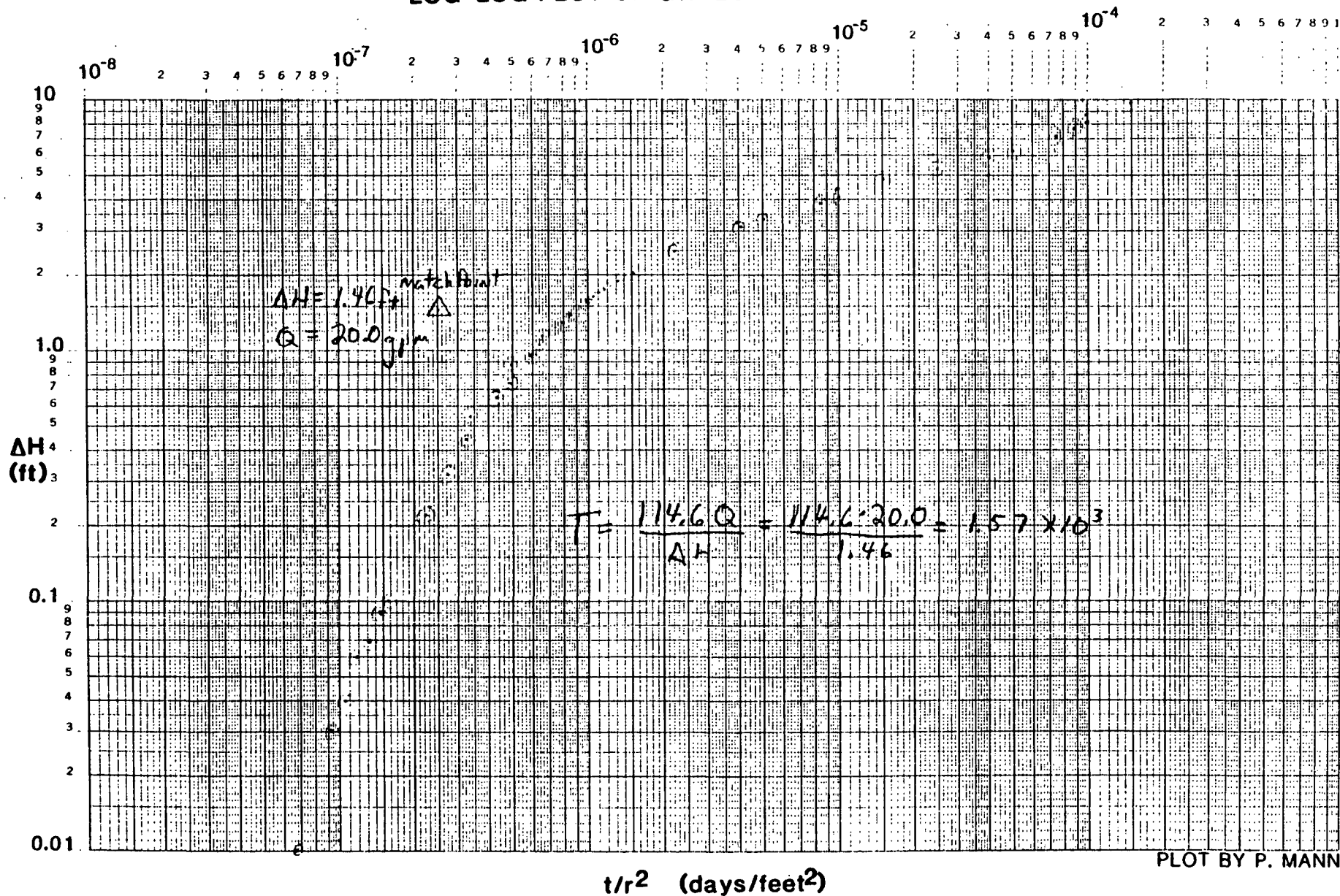


REI 10-1 RUN #1 PUMP TEST - RECOVERY  
SEMI-LOG PLOT OF REI 10-1 01/15/86

PLOT BY D. GABRYSCH



REI 10-1 RUN #1 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF GW-25 9/15/86



PLOT BY P. MANN



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FREING, LTD

JOB NO.: 275-14

SUBJECT: PEI 10-1 Pump = 1 Calc for GV-25

COMPUTED BY: DEE DATE: 11-11-86

CHECKED BY: DD DATE: 11-11-86

## Log-Log solution for Transmissivity - Drawdown

$$Transmissivity (T) = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$Q = 20.0 \text{ gpm}$

$\Delta H = 1.46 \text{ ft} \quad T = \frac{(114.6)(20.0)}{1.46}$

$1.57 \times 10^3 \text{ cfd/ft}$

$\times \text{Conversion Factor } 1.432 \times 10^{-7} = 2.25 \times 10^{-4} \text{ m}^2/\text{s}$

## Log-Log solution for Storativity - Drawdown

$$Storativity (S) = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$t/r^2 = 2.50 \times 10^{-7} \text{ days/ft}^2$

$T = 1.57 \times 10^3 \text{ cfd/ft}$

$S = \frac{(1)(1.57 \times 10^3)(2.50 \times 10^{-7})}{1.87} = 2.10 \times 10^{-4}$

## Solutions for Hydraulic Conductivity (K)

$K = \frac{T}{b}$  where  $b$  is the screened thickness in feet

$T = 1.57 \times 10^3 \text{ cfd/ft}$

$b = 5.0 \text{ ft}$

$K = \frac{1.57 \times 10^3}{5.0} = 3.14 \times 10^2 \text{ cfd/ft}^2$

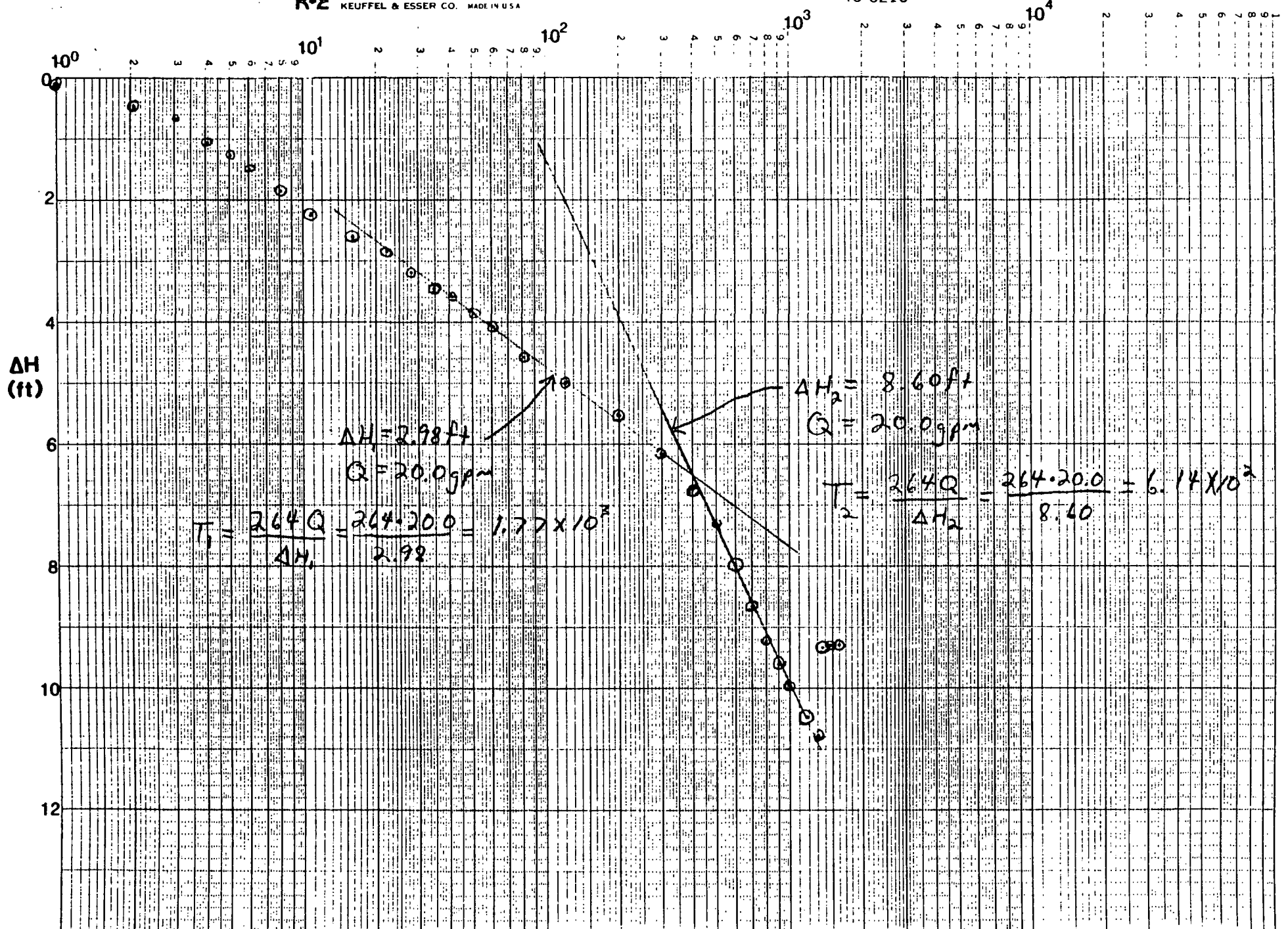
$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 1.48 \times 10^{-2} \text{ cm/s}$

**ERT**

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

46 6210



REF 10-1 RUN #1 PUMP TEST - DRAWDOWN

PLOT BY S. CAYLOR

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 274-14

SUBJECT: REI 10-1 Run #1 Calc for GW-25

COMPUTED BY: DRG DATE: 11-19-84

CHECKED BY: DD DATE: 11-19-84

Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264Q}{\Delta H}$$

$$Q = 20.0 \text{ gpm}$$

$$\Delta H_1 = 2.98 \text{ ft} \quad T_1 = \frac{(264)(20.0)}{2.98}$$

$$1.77 \times 10^3 \text{ gpd/ft}$$

$$\Delta H_2 = 8.60 \text{ ft} \quad T_2 = \frac{(264)(20.0)}{8.60}$$

$$6.14 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7} =$$

$$2.55 \times 10^{-4} \text{ m}^2/\text{s}$$

$$8.83 \times 10^{-5} \text{ m}^2/\text{s}$$

Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.3Tt_0}{r^2}$$

$$r = 66.670 \text{ ft}$$

$$t_{01} = 2.5 \text{ min} / 1440 = 1.74 \times 10^{-3} \text{ days}$$

$$T_1 = 1.77 \times 10^3 \text{ gpd/ft}$$

$$t_{02} = 70 \text{ min} / 1440 = 4.86 \times 10^{-2} \text{ days}$$

$$T_2 = 6.14 \times 10^2 \text{ gpd/ft}$$

$$S_1 = \frac{(0.3)(1.77 \times 10^3)(1.74 \times 10^{-3})}{(66.670)^2} = 2.08 \times 10^{-4}$$

$$S_2 = \frac{(0.3)(6.14 \times 10^2)(4.86 \times 10^{-2})}{(66.670)^2} = 2.01 \times 10^{-3}$$

ERT

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FREIGHT LTD.

JOB NO.: 271-14

SUBJECT: REI 10-1 Run #1 Calc. for Gb-25

COMPUTED BY: DRG DATE: 11-15-80

CHECKED BY: DD DATE: 11-19-80

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T_1 = 1.77 \times 10^3 \text{ gpd/ft}$$

$$b = 5.0 \text{ ft}$$

$$K = \frac{1.77 \times 10^3}{5.0} = 3.54 \times 10^2 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 1.67 \times 10^{-2} \text{ cm/s}$$

$$T_2 = 6.14 \times 10^2 \text{ gpd/ft}$$

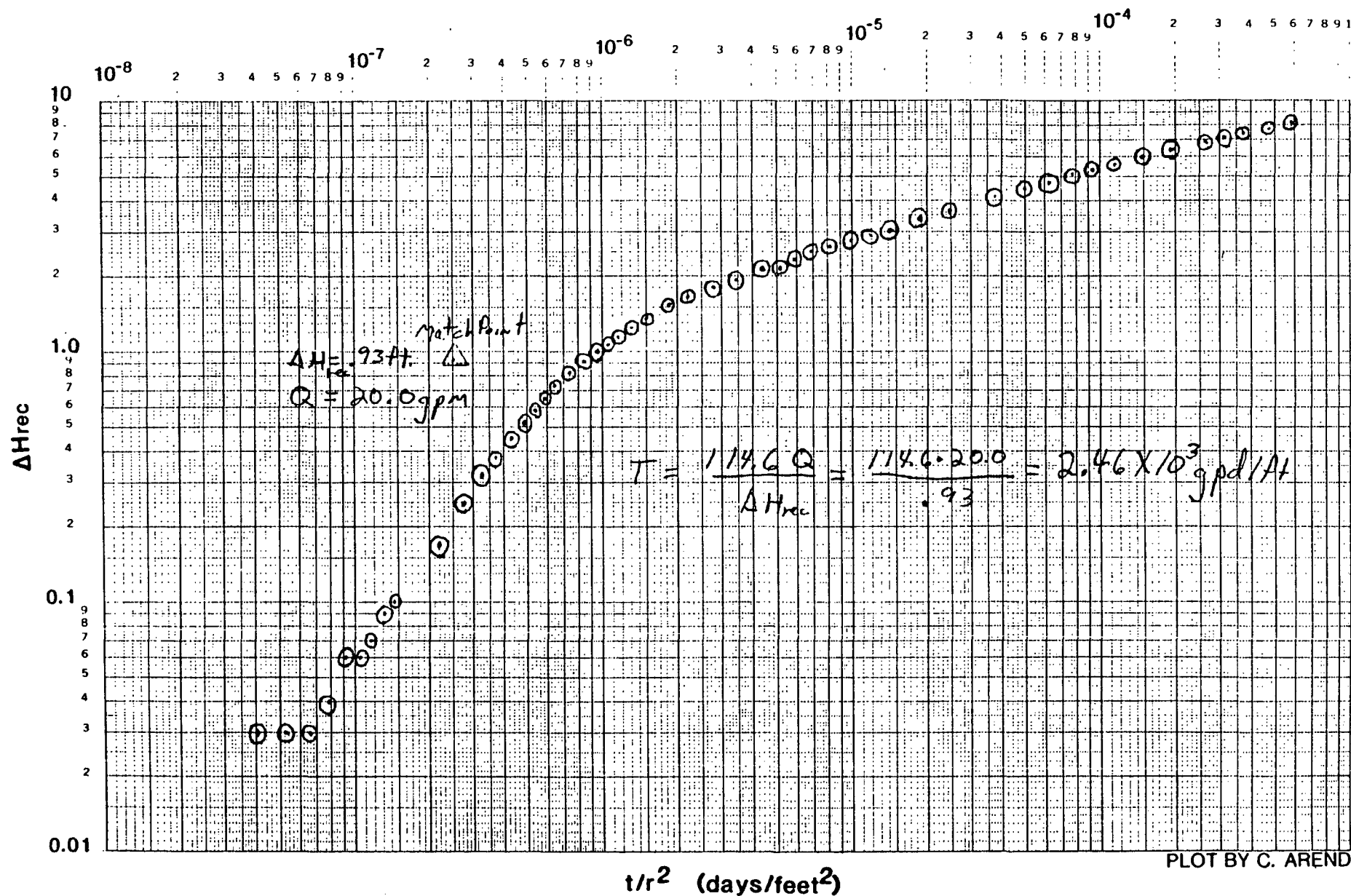
$$b = 5.0 \text{ ft}$$

$$K = \frac{6.14 \times 10^2}{5.0} = 1.23 \times 10^2 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 5.79 \times 10^{-3} \text{ cm/s}$$

**ERT**

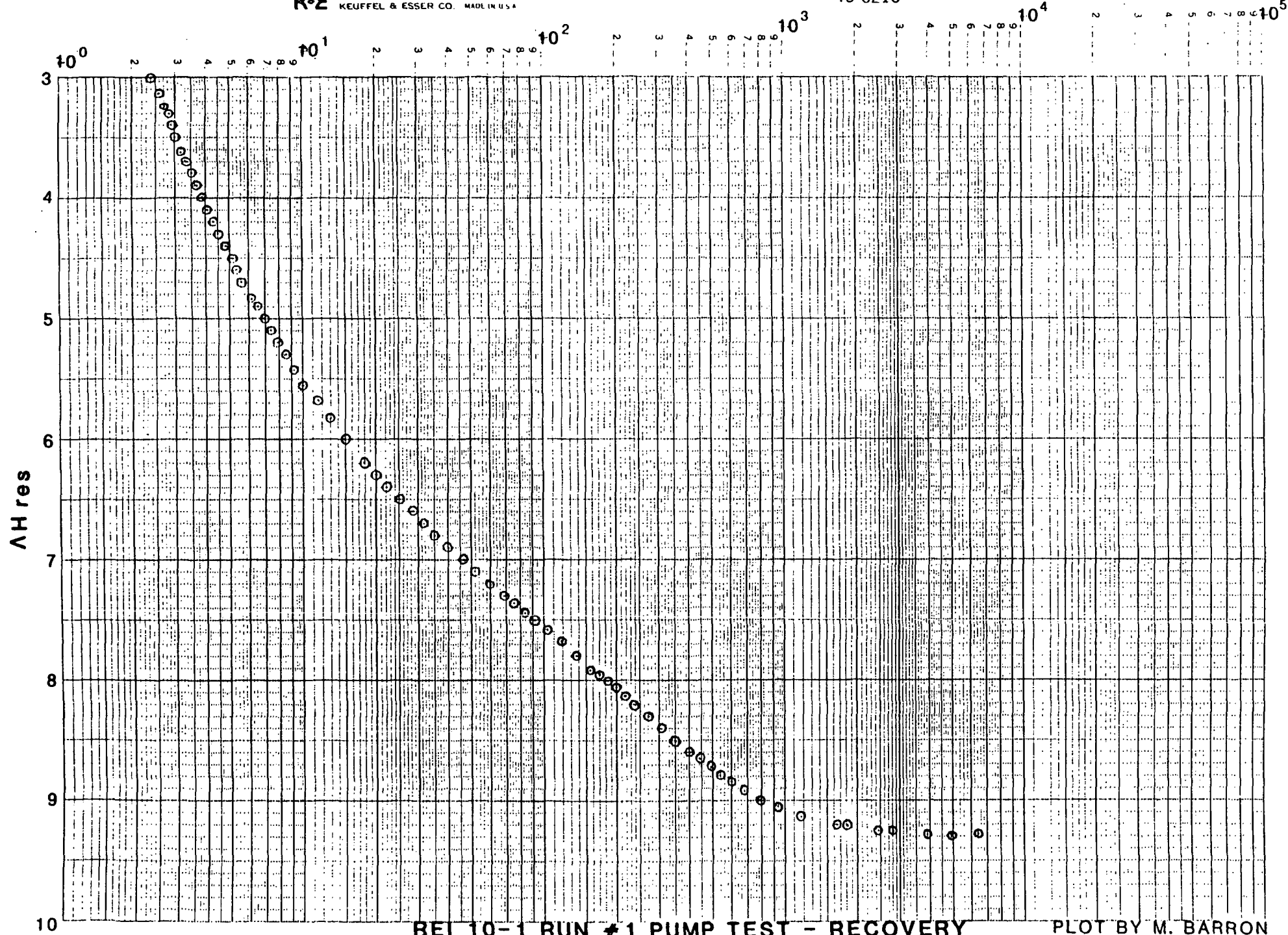
REI 10-1 RUN #1 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF GW-25 9/15/86



K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

$t/t'$

46 6210



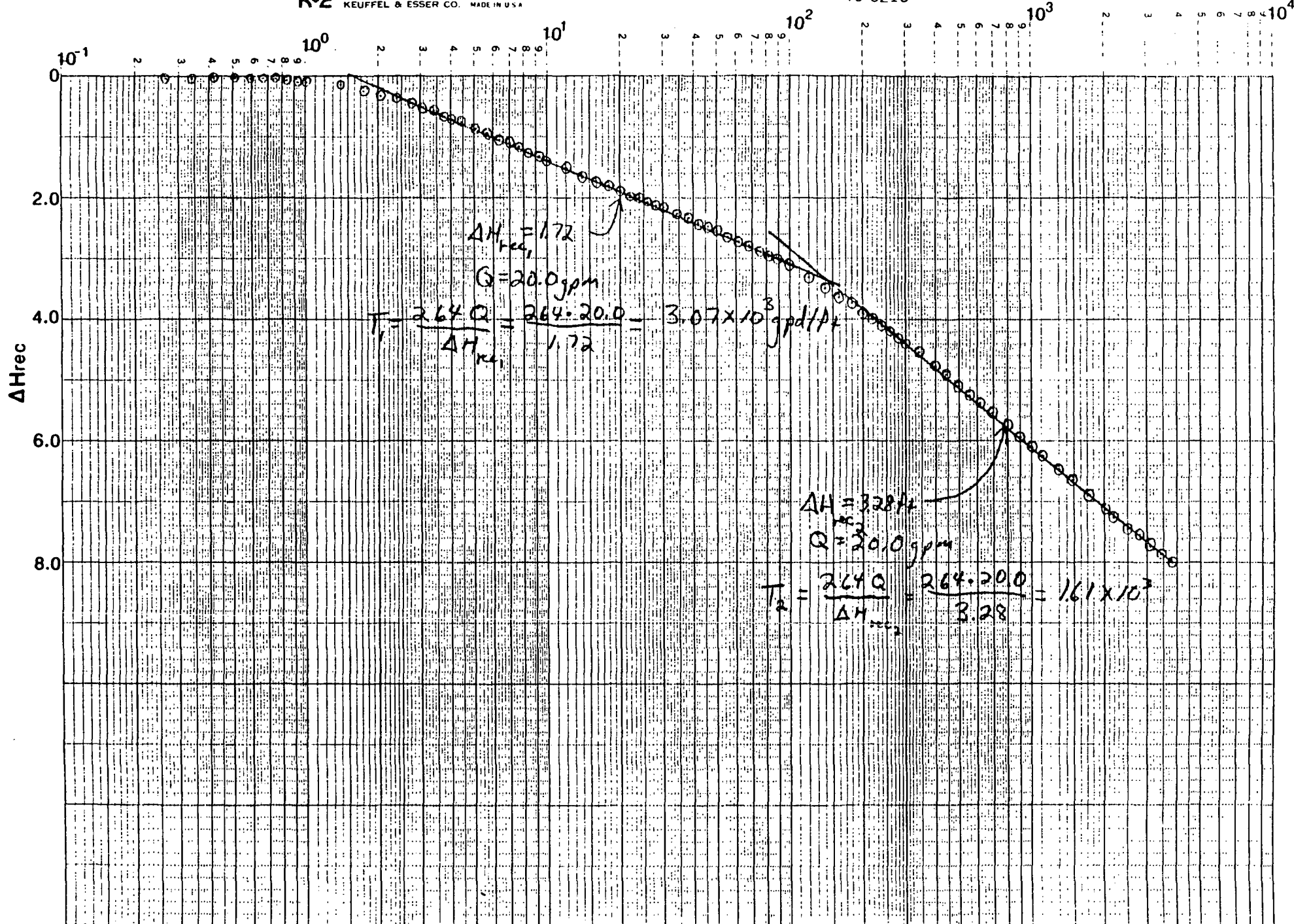
REI 10-1 RUN #1 PUMP TEST - RECOVERY

PLOT BY M. BARRON

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

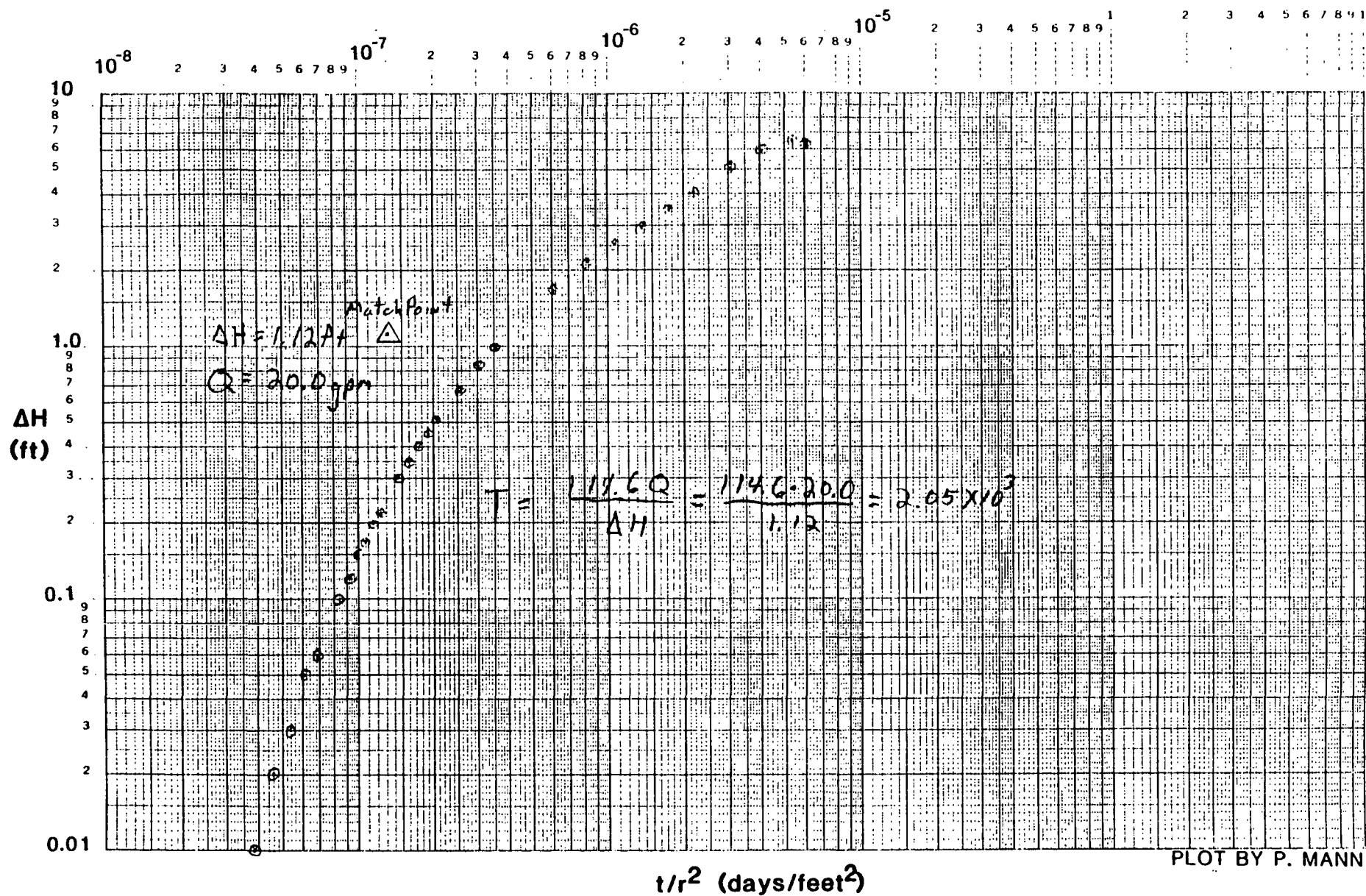
t(min)

46 6210



REI 10-1 RUN #1 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI-11

9/15/86





# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FEEDS 1-2

JOB NO.: 274-14

SUBJECT: PEI 12-1 Pur. #1 Calc. for PEI 11

COMPUTED BY: DRS DATE: 11-15-83

CHECKED BY: DD DATE: 11-15-83

## Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta h}$$

where  $W(u) = 1$

$$Q = 20.0 \text{ gpm}$$

$$\Delta h = 1.12 \text{ ft}$$

$$T = \frac{(114.6)(20.0)}{1.12} = 2.05 \times 10^3 \text{ gpd/ft}$$

$$\gamma \text{ Conversion Factor } 1.432 \times 10^{-2} = 2.94 \times 10^{-4} \text{ m}^2/\text{s}$$

## Log-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 1.32 \times 10^{-7} \text{ days/ft}^2$$

$$T = 2.05 \times 10^3 \text{ gpd/ft}$$

$$S = \frac{(1)(2.05 \times 10^3)(1.32 \times 10^{-7})}{1.87} = 1.44 \times 10^{-4}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

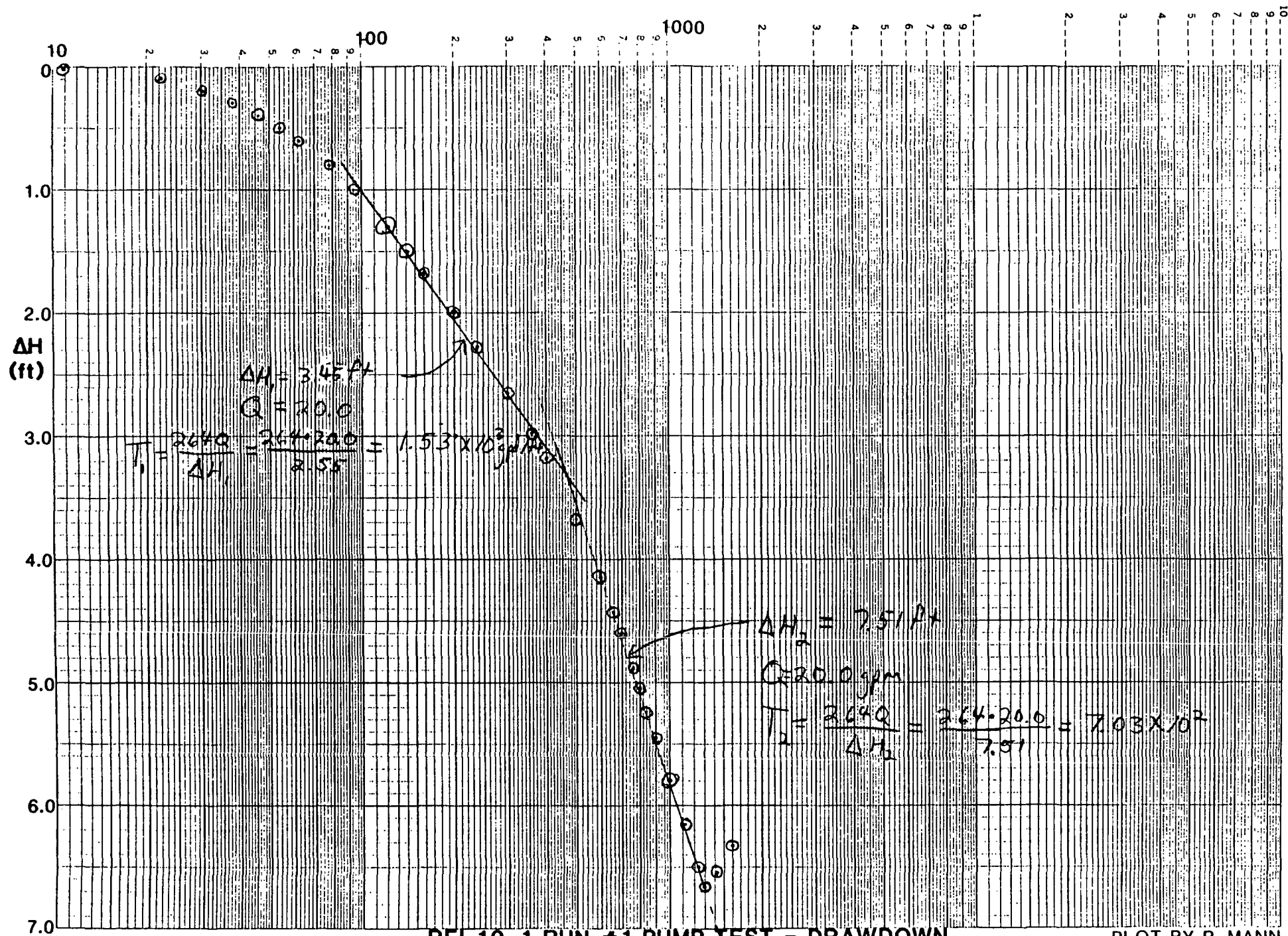
$$T = 2.05 \times 10^3 \text{ gpd/ft}$$

$$b = 16.45 \text{ ft}$$

$$K = \frac{2.05 \times 10^3}{16.45} = 1.24 \times 10^2 \text{ gpd/ft}^2$$

$$\lambda \text{ Conversion Factor } 4.715 \times 10^{-2} = 5.87 \times 10^{-3} \text{ cm/s}$$

**ERT**



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 272-14

SUBJECT: REI 10-1 Run #1 Calc for REI 11

COMPUTED BY: DB DATE: 1-19-84

CHECKED BY: DB DATE: 1-19-84

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity } (T) = \frac{264Q}{\Delta H}$$

$$Q = 20.0 \text{ gpm}$$

$$\Delta H_1 = 3.45 \text{ ft} \quad T_1 = \frac{(264)(20.0)}{3.45} = 1.53 \times 10^3 \text{ gpd/ft}$$

$$\Delta H_2 = 7.51 \text{ ft} \quad T_2 = \frac{(264)(20.0)}{7.51} = 7.03 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.432 \times 10^{-7} =$$

$$2.20 \times 10^{-4} \text{ m}^2/\text{s}$$

$$1.01 \times 10^{-4} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity } (S) = \frac{0.2 T t_0}{r^2}$$

$$r = 427.782 \text{ ft}$$

$$t_{01} = 51 \text{ min} / 1440 = 3.54 \times 10^{-2} \text{ days}$$

$$T_1 = 1.53 \times 10^3 \text{ gpd/ft}$$

$$t_{02} = 167 \text{ min} / 1440 = 1.16 \times 10^{-1} \text{ days}$$

$$T_2 = 7.03 \times 10^2 \text{ gpd/ft}$$

$$S_1 = \frac{(0.2)(1.53 \times 10^3)(3.54 \times 10^{-2})}{(427.782)^2} = 8.65 \times 10^{-5}$$

$$S_2 = \frac{(0.2)(7.03 \times 10^2)(1.16 \times 10^{-1})}{(427.782)^2} = 1.34 \times 10^{-4}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FPE 004 672

JOB NO.: 275-14

SUBJECT: PEI 10-1 Pump Calc for REI 11

COMPUTED BY: LP DATE: 11-1-88

CHECKED BY: DD DATE: 11-4-88

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T_1 = \boxed{1.53 \times 10^3 \text{ gpd/ft}}$$

$$b = 16.45 \text{ ft}$$

$$K = \frac{1.53 \times 10^3}{16.45} = \boxed{9.30 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = \boxed{4.39 \times 10^{-5} \text{ cm/s}}$$

$$T_2 = \boxed{7.03 \times 10^2 \text{ gpd/ft}}$$

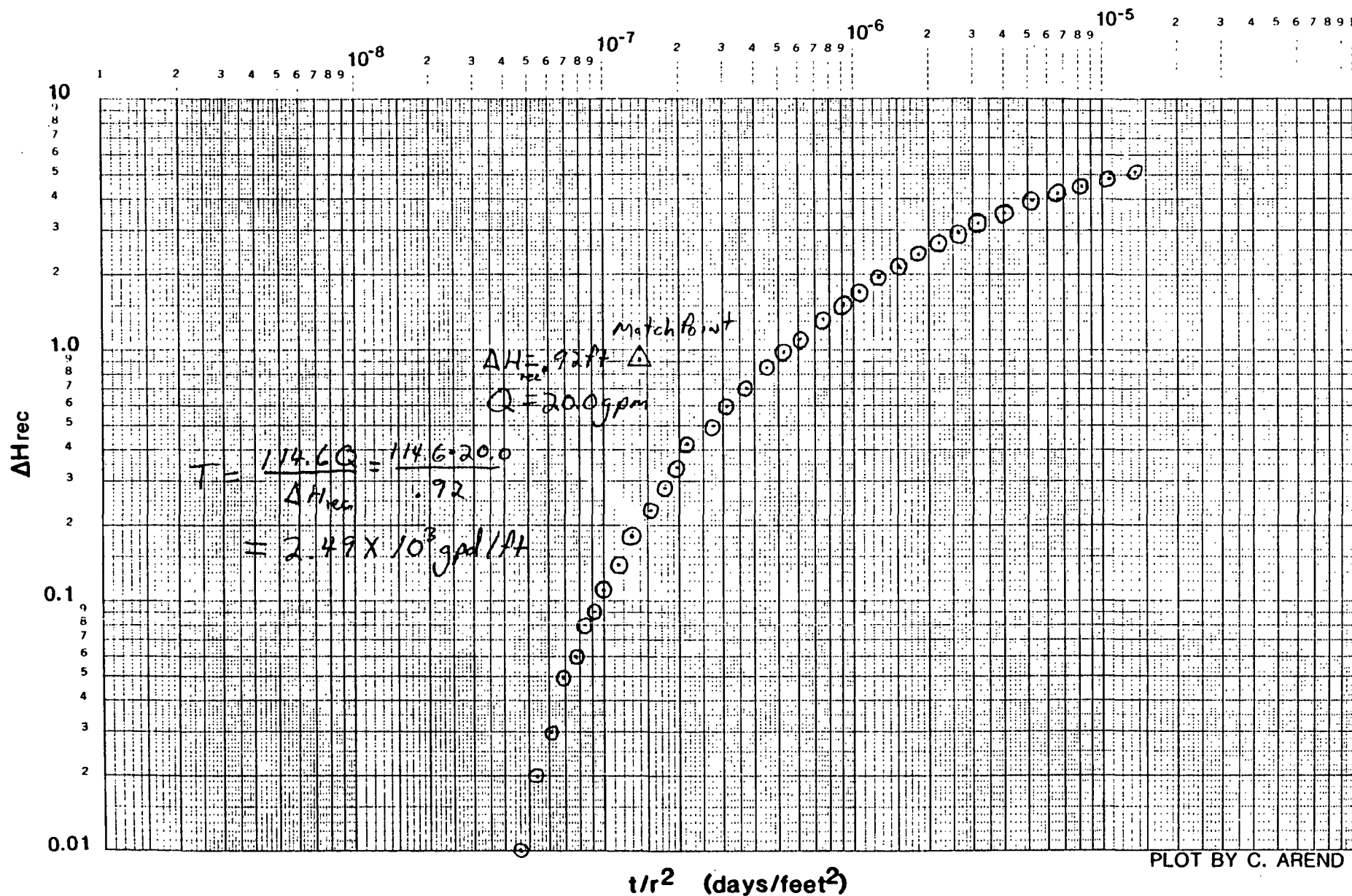
$$b = 16.45 \text{ ft}$$

$$K = \frac{7.03 \times 10^2}{16.45} = \boxed{4.27 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = \boxed{2.02 \times 10^{-5} \text{ cm/s}}$$

REI 10-1 RUN #1 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF REI-11

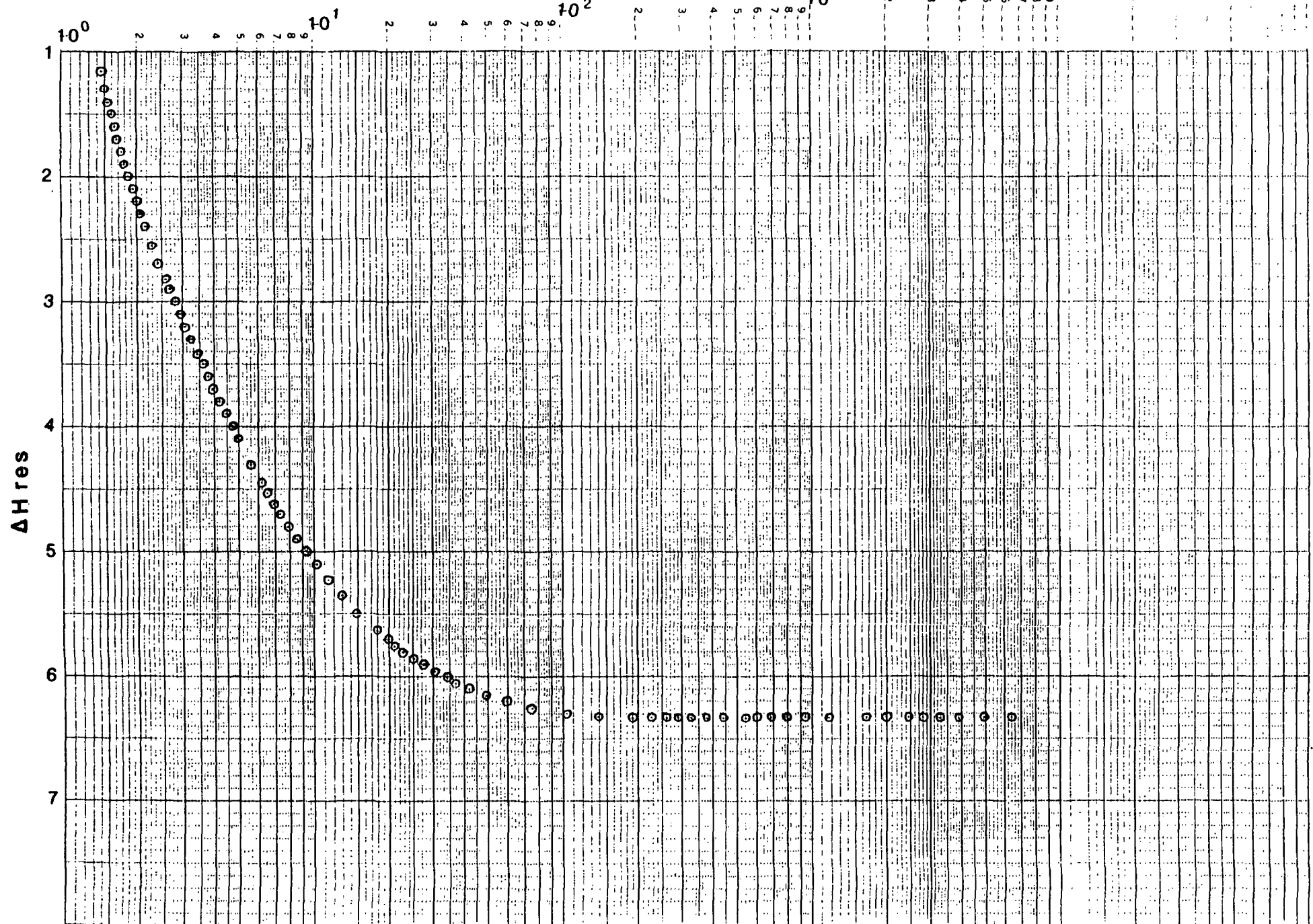
9/15/86



K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

$t/t'$

46 6210



REI 10-1 RUN #1 PUMP TEST - RECOVERY

PLOT BY M. BARRON

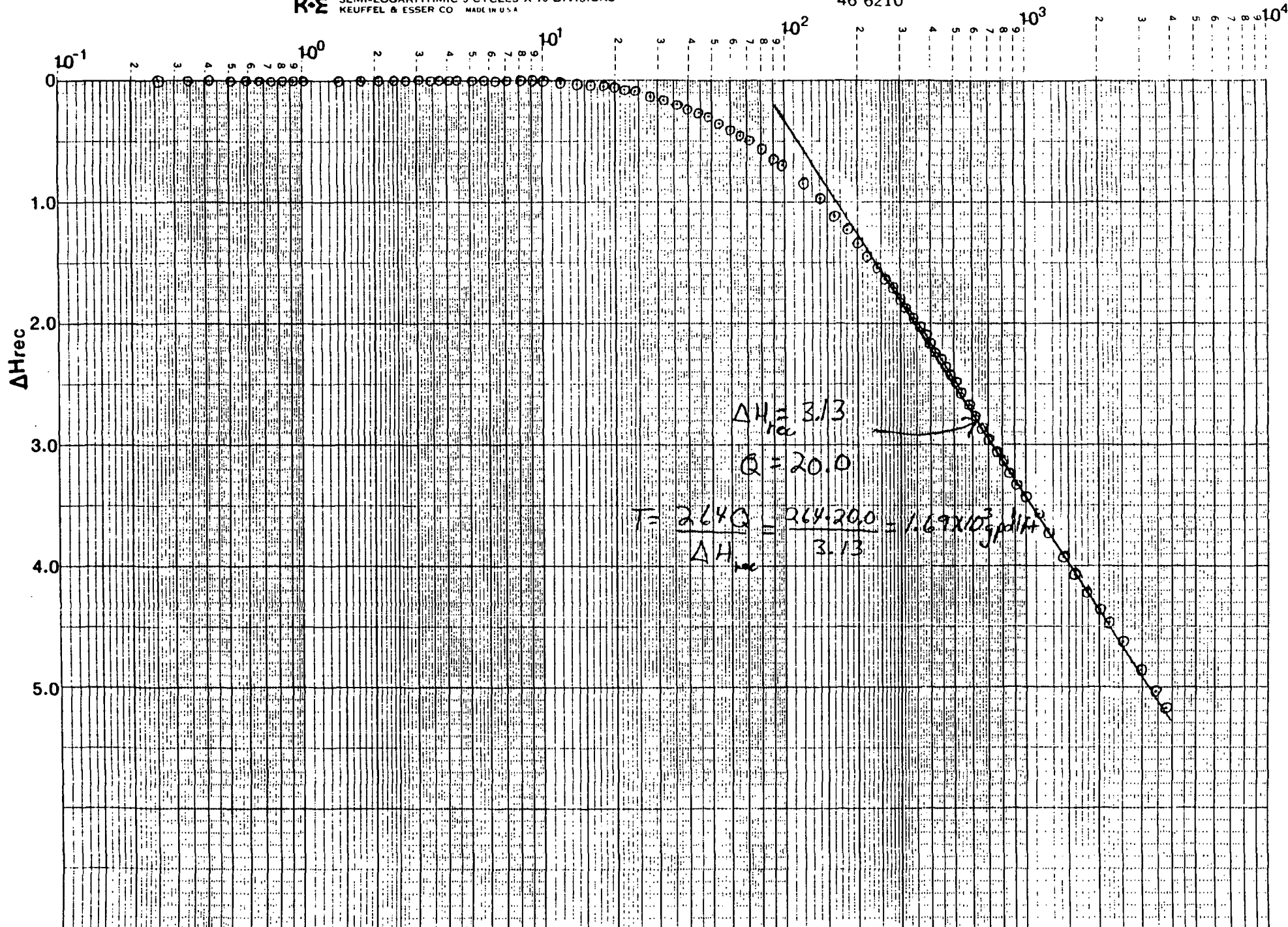
SEMI-LOG PLOT OF REI 10-1

2/15/86

K-Σ SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t (min)

46 6210

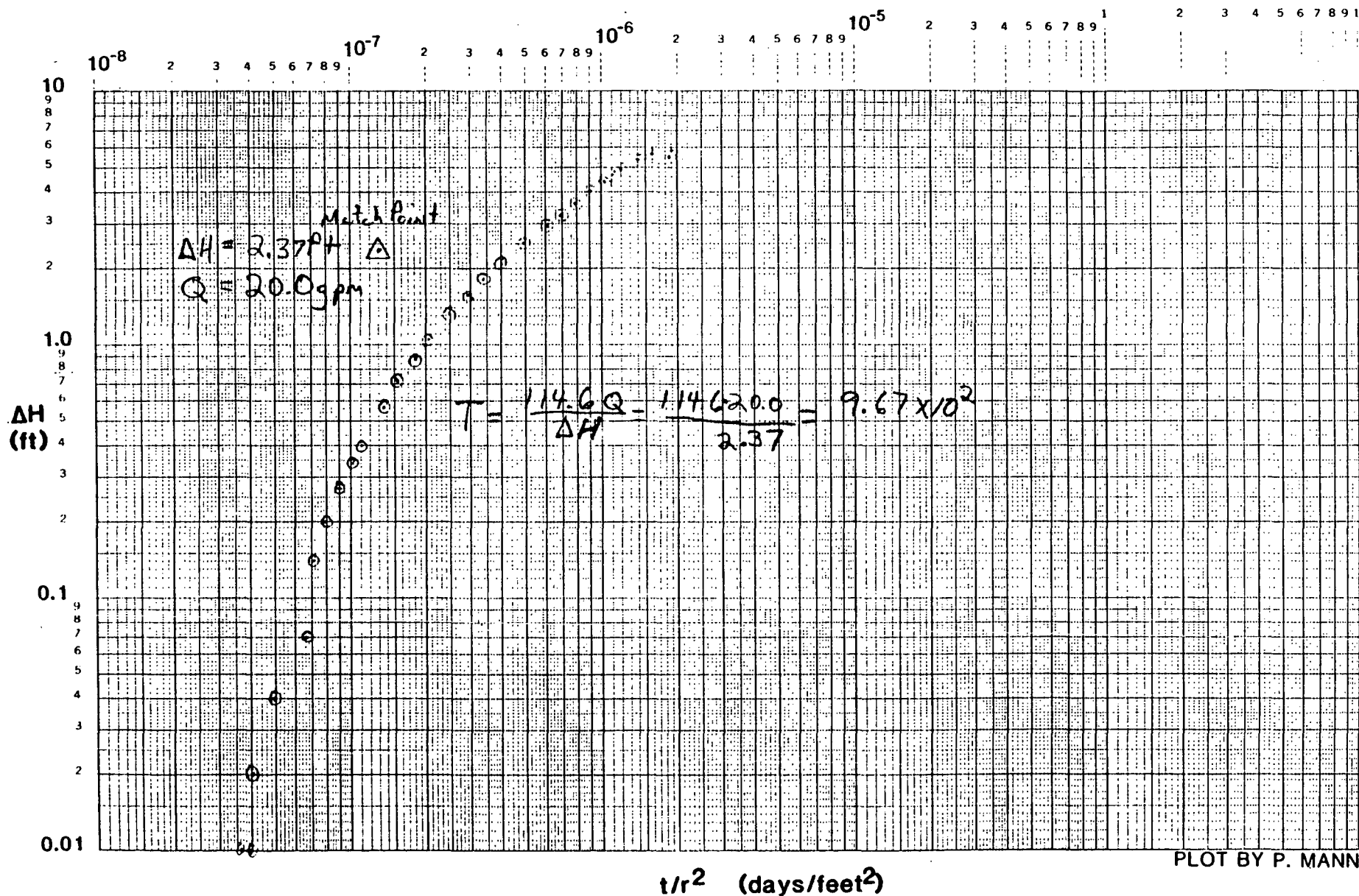


REI 10-1 RUN #1 PUMP TEST - RECOVERY

PLOT BY D. GABRYSCH

REI 10-1 RUN #1 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI 3-4

9/15/86





# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #1 Calc for REI 3-4

COMPUTED BY: DCG DATE: 11-12-81

CHECKED BY: DD DATE: 11-16-81

## Log-Log solution for Transmissivity - Drawdown

$$T = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$Q = 20.0 \text{ gpm}$$

$$\Delta H = 2.37 \text{ ft}$$

$$T = \frac{(114.6)(20.0)}{2.37} = 9.67 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.432 \times 10^{-7} = 1.39 \times 10^{-4} \text{ m}^2/\text{s}$$

## Log-Log solution for Storativity - Drawdown

$$S = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 1.30 \times 10^{-7} \text{ days/ft}^2$$

$$T = 9.67 \times 10^2 \text{ gpd/ft}$$

$$S = \frac{(1)(9.67 \times 10^2)(1.30 \times 10^{-7})}{1.87} = 6.72 \times 10^{-5}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 9.67 \times 10^2 \text{ gpd/ft}$$

$$b = 23.0 \text{ ft}$$

$$K = \frac{9.67 \times 10^2}{23.0} = 4.20 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 1.98 \times 10^{-3} \text{ in s}$$

**ERT**

**9/15/86**

# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FRENCH LTD

JOB NO.: 275-14

SUBJECT: PEI 10-1 Run #1 Calc for REI 3-4

COMPUTED BY: DRS DATE: 11-19-82

CHECKED BY: JD DATE: 11-18-82

Semi-Log solution for Transmissivity-Drawdown

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta h}$$

$$Q = 20.0 \text{ gpm}$$

$$\Delta h = 6.50 \text{ ft}$$

$$T = \frac{(264)(20.0)}{6.50} = 8.12 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 1.17 \times 10^{-4} \text{ m}^2/\text{s}$$

Semi-Log solution for Storativity-Drawdown

$$\text{Storativity (S)} = \frac{0.3 T t_0}{r^2}$$

$$r = 784.360 \text{ ft}$$

$$t_0 = 192 \text{ min} / 1440 = 1.33 \times 10^{-1} \text{ days}$$

$$T = 8.12 \times 10^2 \text{ gpd/ft}$$

$$S = \frac{(0.3)(8.12 \times 10^2)(1.33 \times 10^{-1})}{(784.360)^2} = 5.27 \times 10^{-5}$$

Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 8.12 \times 10^2 \text{ gpd/ft}$$

$$b = 23.0 \text{ ft}$$

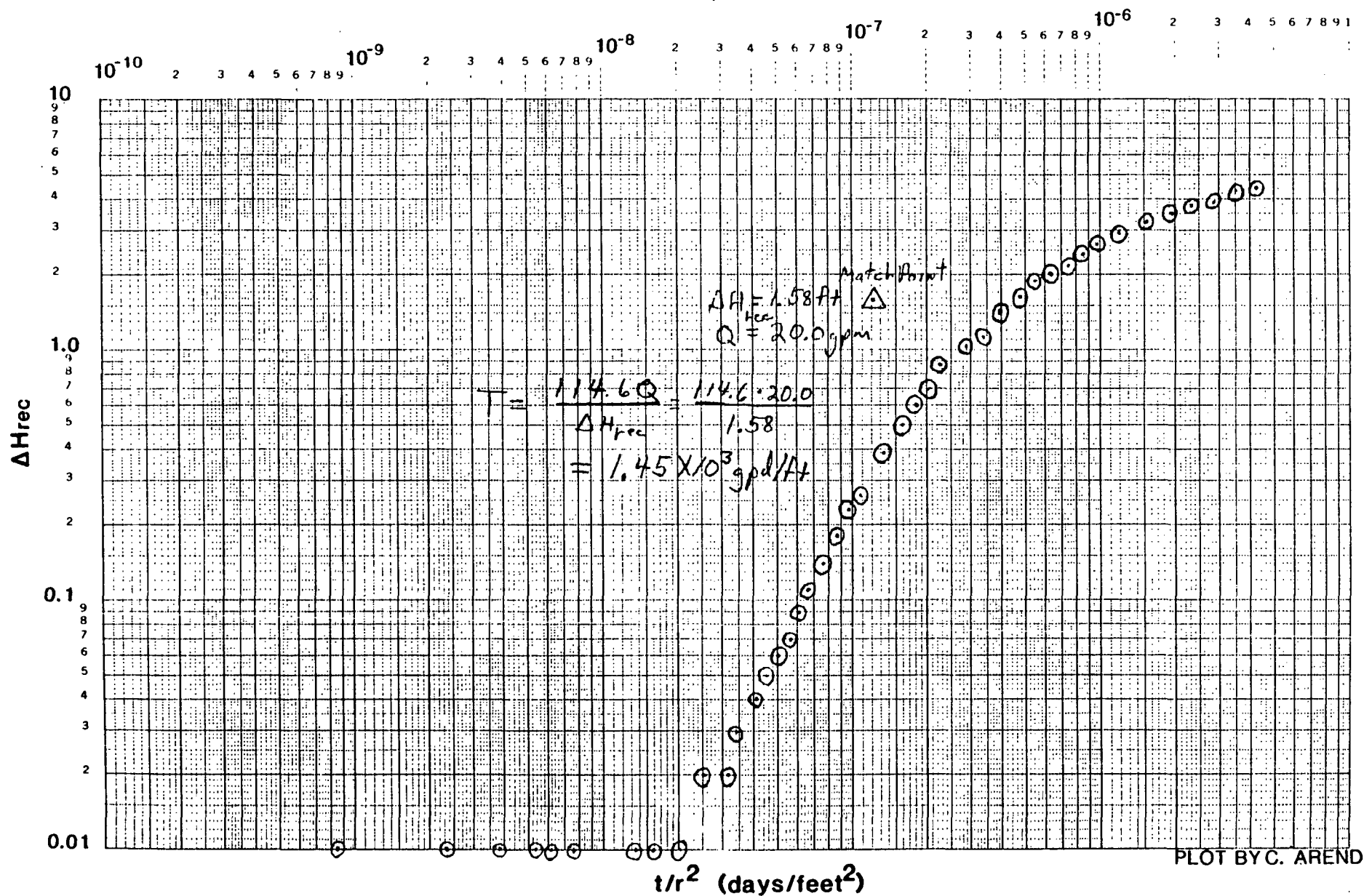
$$K = \frac{8.12 \times 10^2}{23.0} = 3.53 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 1.67 \times 10^{-3} \text{ cm/s}$$

**ERT**

REI 10-1 RUN #1 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF REI 3-4

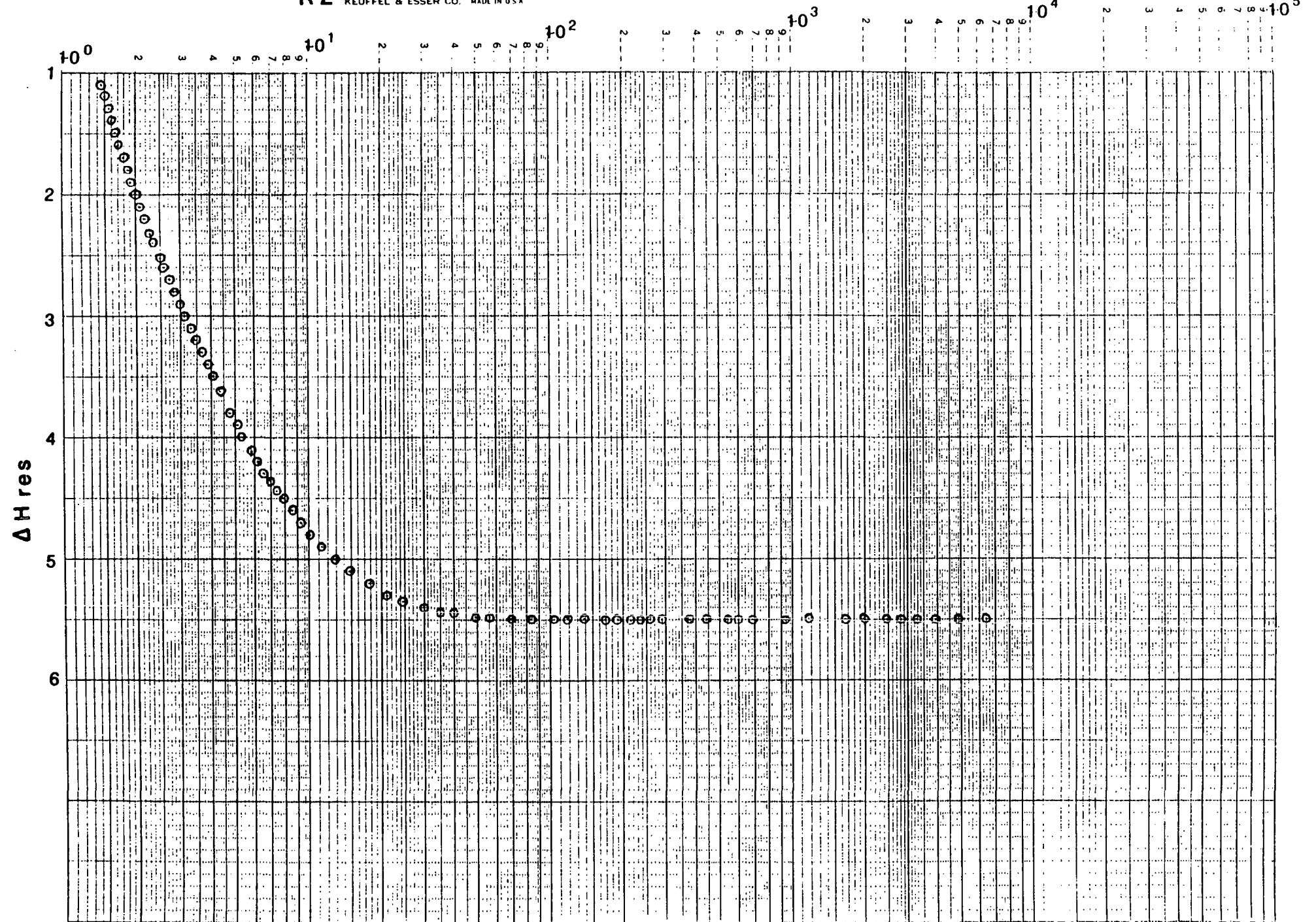
9/15/86



K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

$t/t'$

46 6210



REI 10-1 RUN #1 PUMP TEST - RECOVERY  
SEMI-LOG PLOT OF REI 2-1

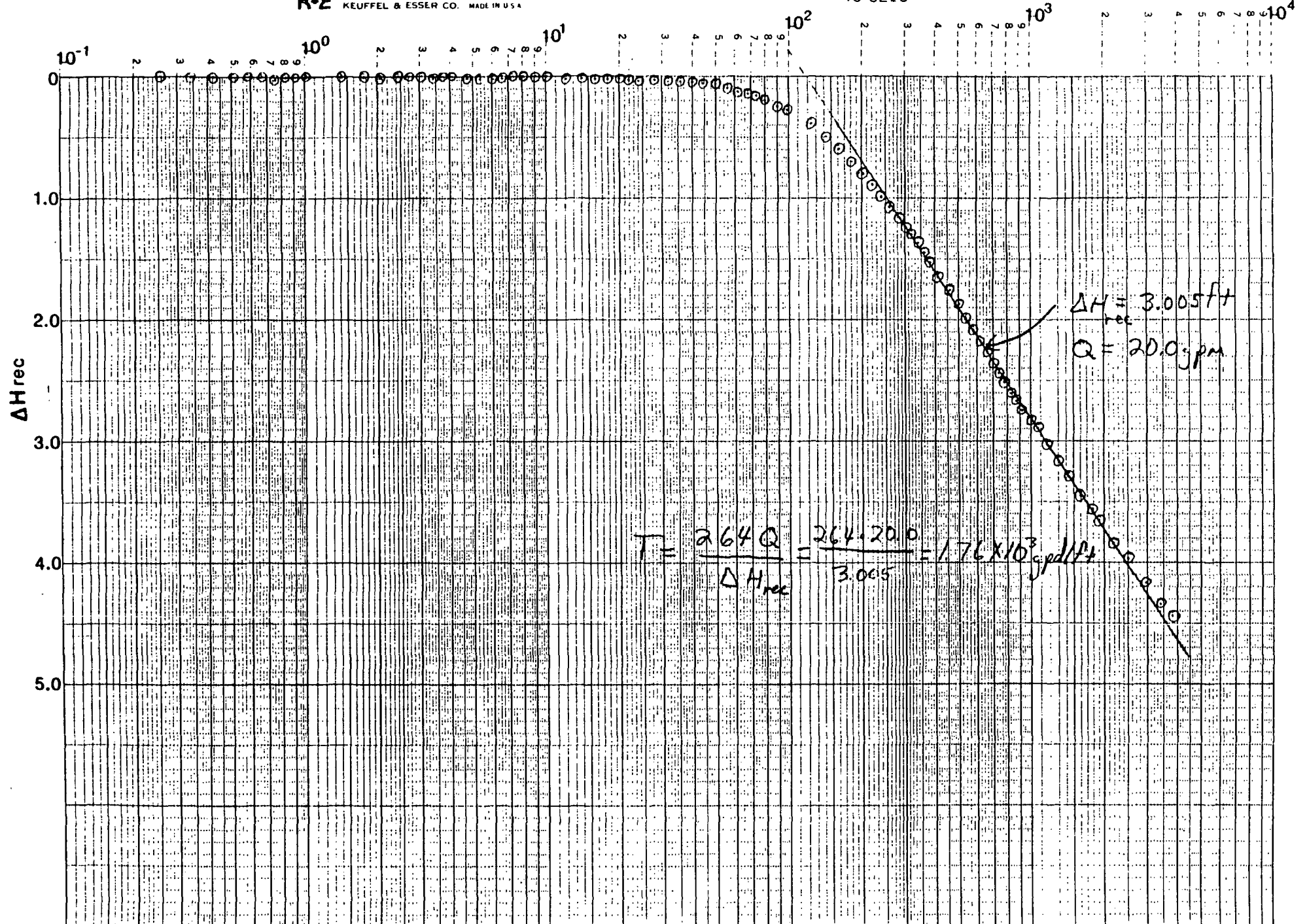
PLOT BY M. BARRON

2/15/66

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

46 6210

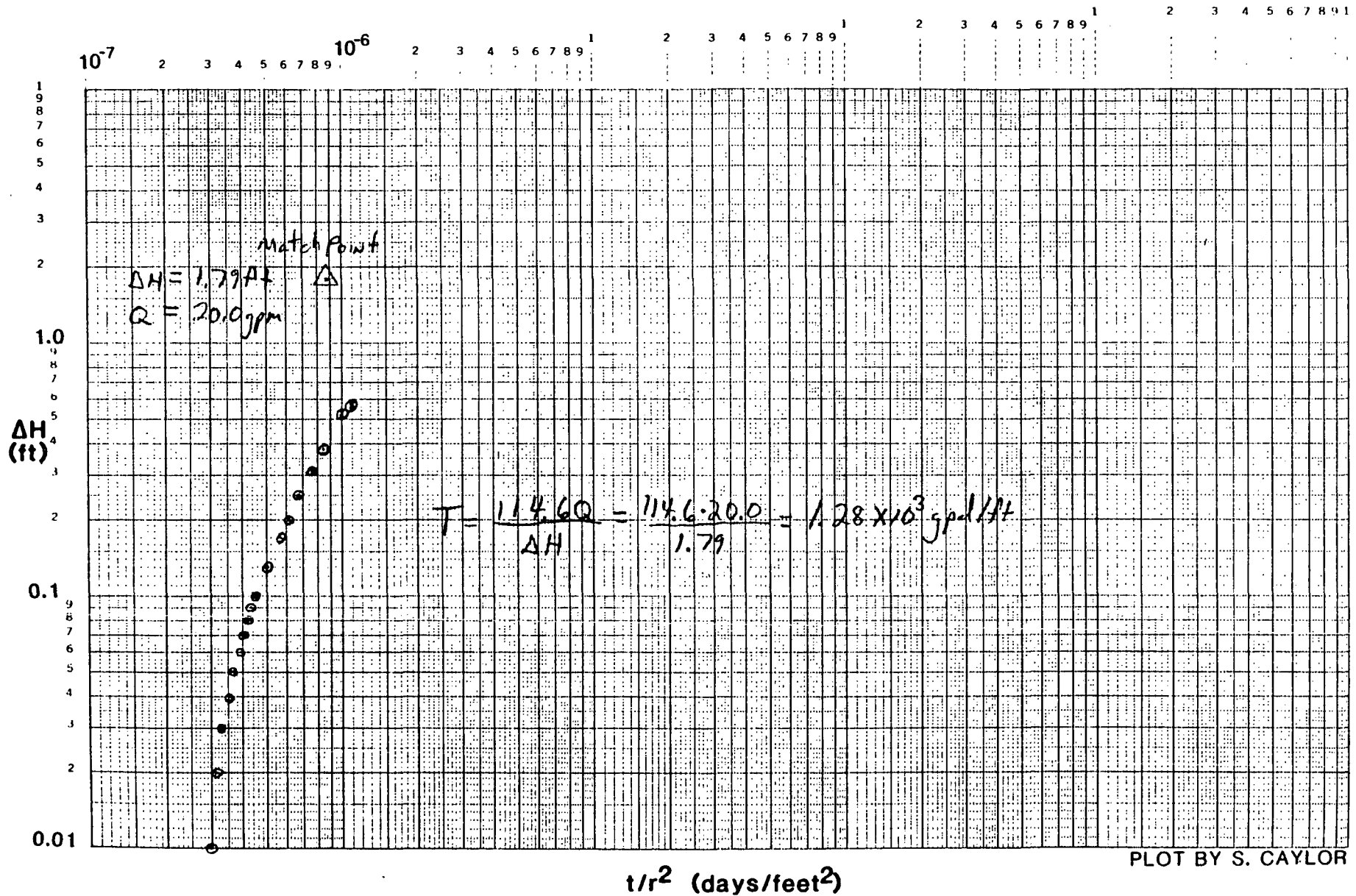


REI 10-1 RUN #1 PUMP TEST - RECOVERY

PLOT BY D. GABRYSCH

REI 10-1 RUN #1 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI-7

9/15/86



# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FEEDCH LTI

JOB NO.: 275-15

SUBJECT: PEI 10-1 Run #1 Calc for PEI 7

COMPUTED BY: DD DATE: 11-15-86

CHECKED BY: DD DATE: 11-15-86

## Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$Q = 20.0 \text{ gpm}$$

$$\Delta H = 1.79 \text{ ft} \quad T = \frac{(114.6)(20.0)}{1.79} = 1.28 \times 10^3 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 1.84 \times 10^{-4} \text{ m}^2/\text{s}$$

## Log-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 8.70 \times 10^{-7} \text{ days/ft}^2$$

$$T = 1.28 \times 10^3 \text{ gpd/ft}$$

$$S = \frac{(1)(1.28 \times 10^3)(8.70 \times 10^{-7})}{1.87} = 5.96 \times 10^{-4}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 1.28 \times 10^3 \text{ gpd/ft}$$

$$b = 15.0 \text{ ft}$$

$$K = \frac{1.28 \times 10^3}{15.0} = 8.54 \times 10^1 \text{ gpd/ft}^2$$

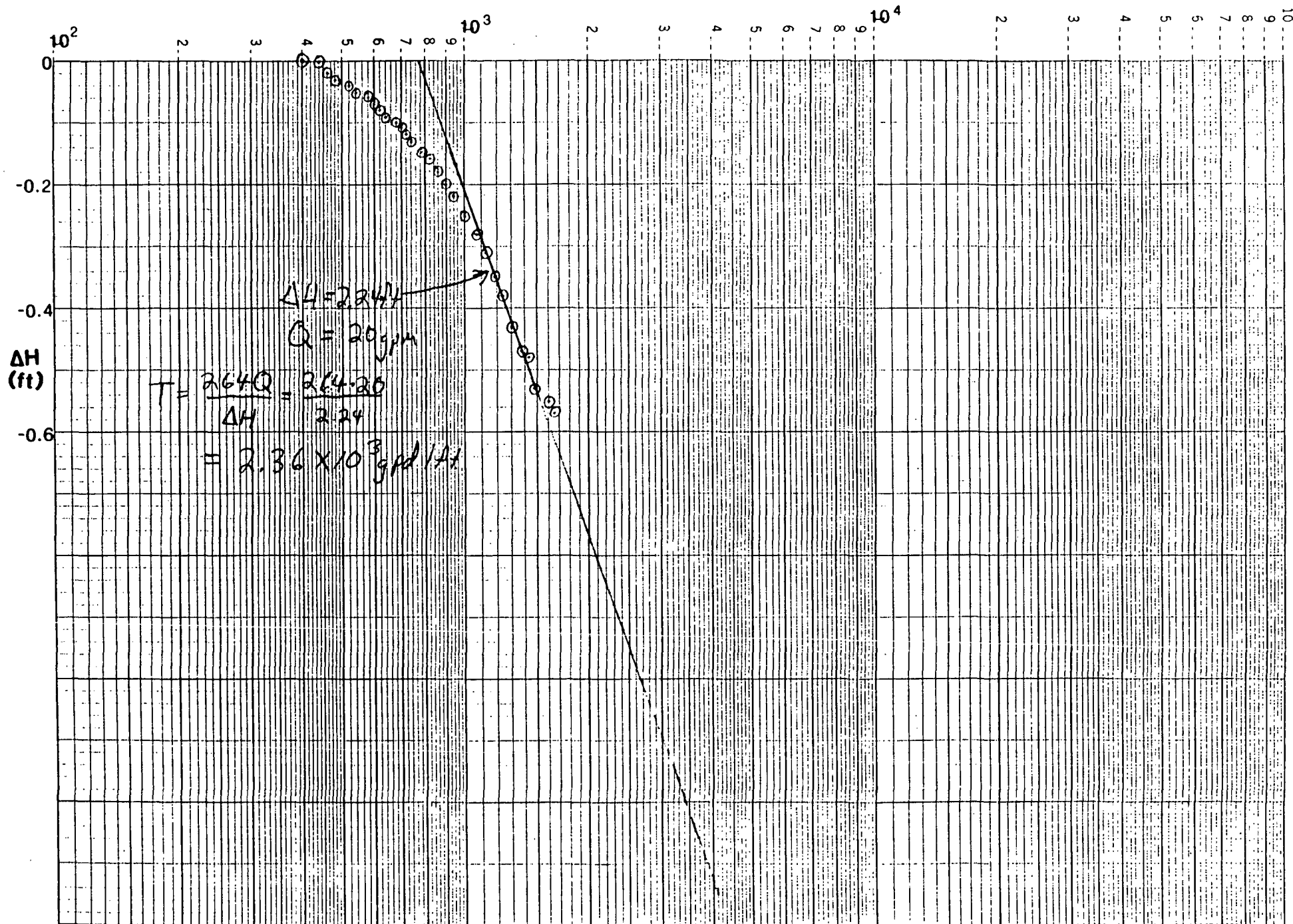
$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 4.02 \times 10^{-3} \text{ cm/s}$$

**ERT**



t(min)

46 5490



REI 10-1 RUN #1 PUMP TEST - DRAWDOWN

PLOT BY D. GABRYSCH

SEMI-LOG PLOT OF REI 7

9/15/86

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 276-14

SUBJECT: REI 10-1 Run #1 Calc for REI 7

COMPUTED BY: DD DATE: 11/9/80

CHECKED BY: DD DATE: 11/9/80

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity } (T) = \frac{264 Q}{\Delta H}$$

$$Q = 20.0 \text{ gpm}$$

$$\Delta H = 2.24 \text{ ft} \quad T = \frac{(264)(20.0)}{2.24} = 2.36 \times 10^3 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.422 \times 10^{-7} = 3.39 \times 10^{-4} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity } (S) = \frac{0.2 T t_e}{r^2}$$

$$r = 1012.704 \text{ ft}$$

$$t_e = 775 \text{ min.} / 1440 = 5.32 \times 10^{-1} \text{ days}$$

$$T = 2.36 \times 10^3 \text{ gpd/ft}$$

$$S = \frac{(0.2)(2.36 \times 10^3)(5.32 \times 10^{-1})}{(1012.704)^2} = 3.71 \times 10^{-2}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 2.36 \times 10^3 \text{ gpd/ft}$$

$$b = 15.0 \text{ ft}$$

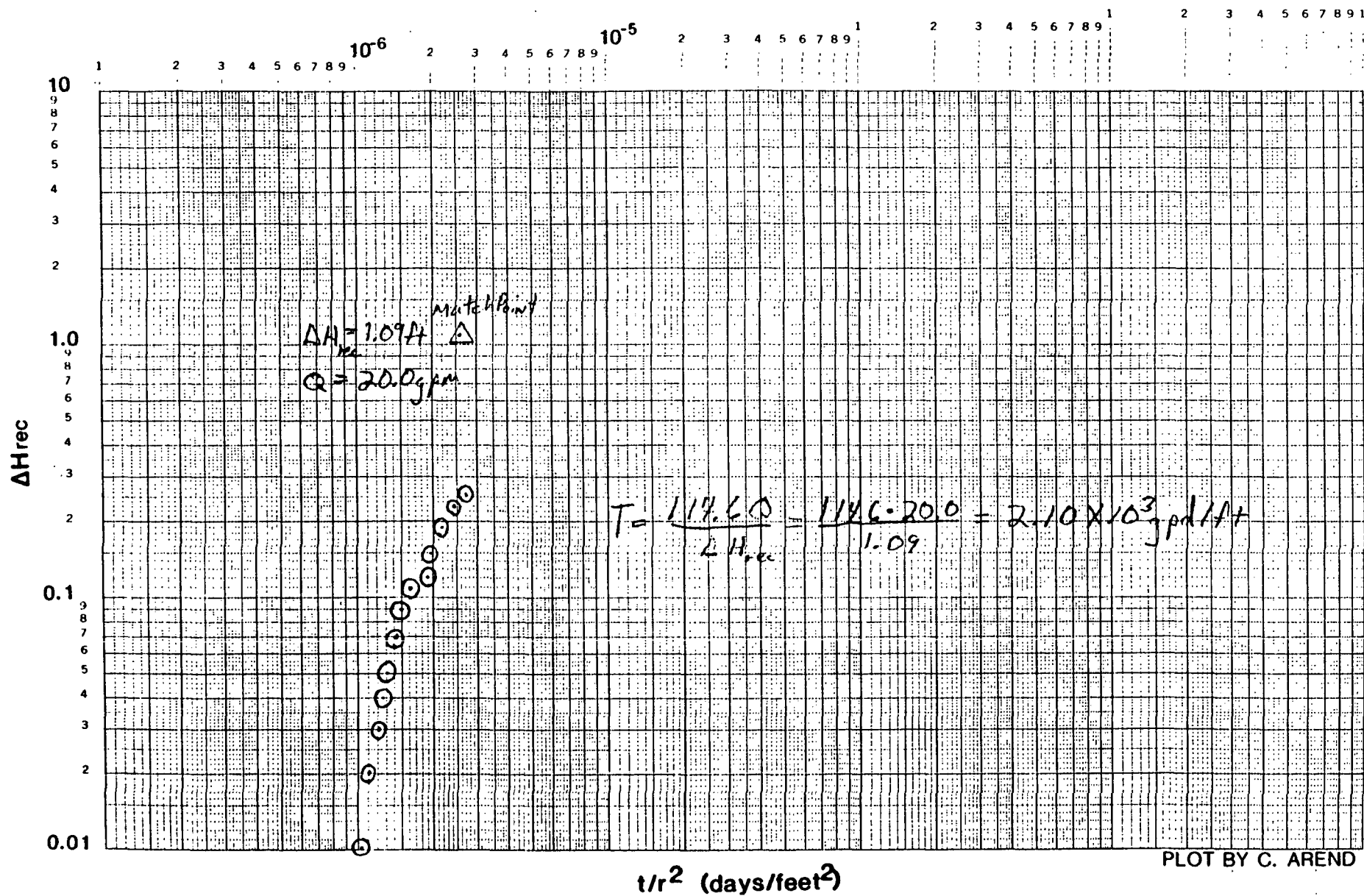
$$K = \frac{2.36 \times 10^3}{15.0} = 1.57 \times 10^2 \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.713 \times 10^{-5} = 7.41 \times 10^{-3} \text{ cm}^2/\text{s}$$

**ERT**

REI 10-1 RUN #1 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF REI-7

9/15/86

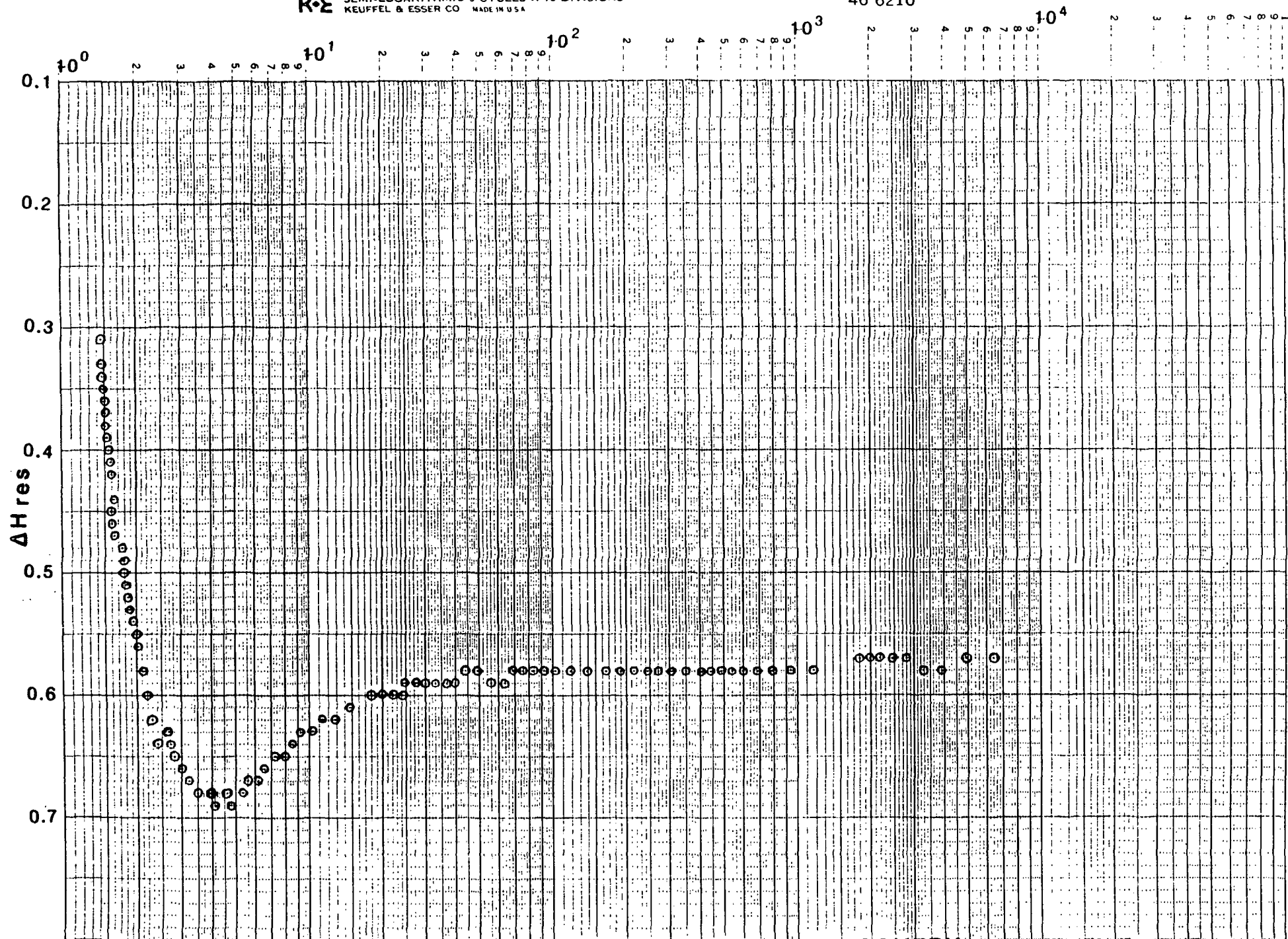


PLOT BY C. AREND

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

$t/t'$

46 6210

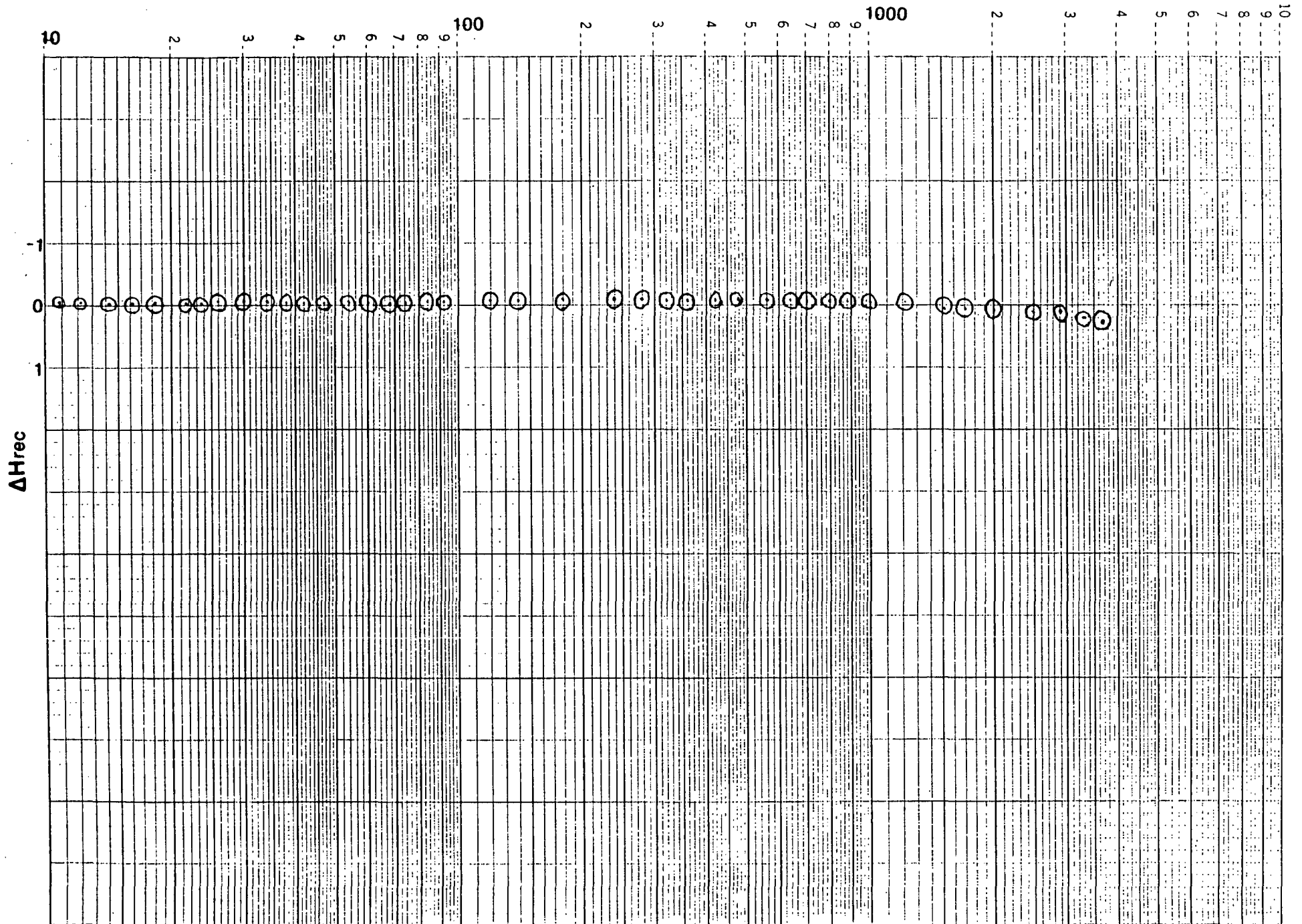


REI 10-1 RUN #1 PUMP TEST - RECOVERY

PLOT BY M. BARRON

t(min)

46 5490

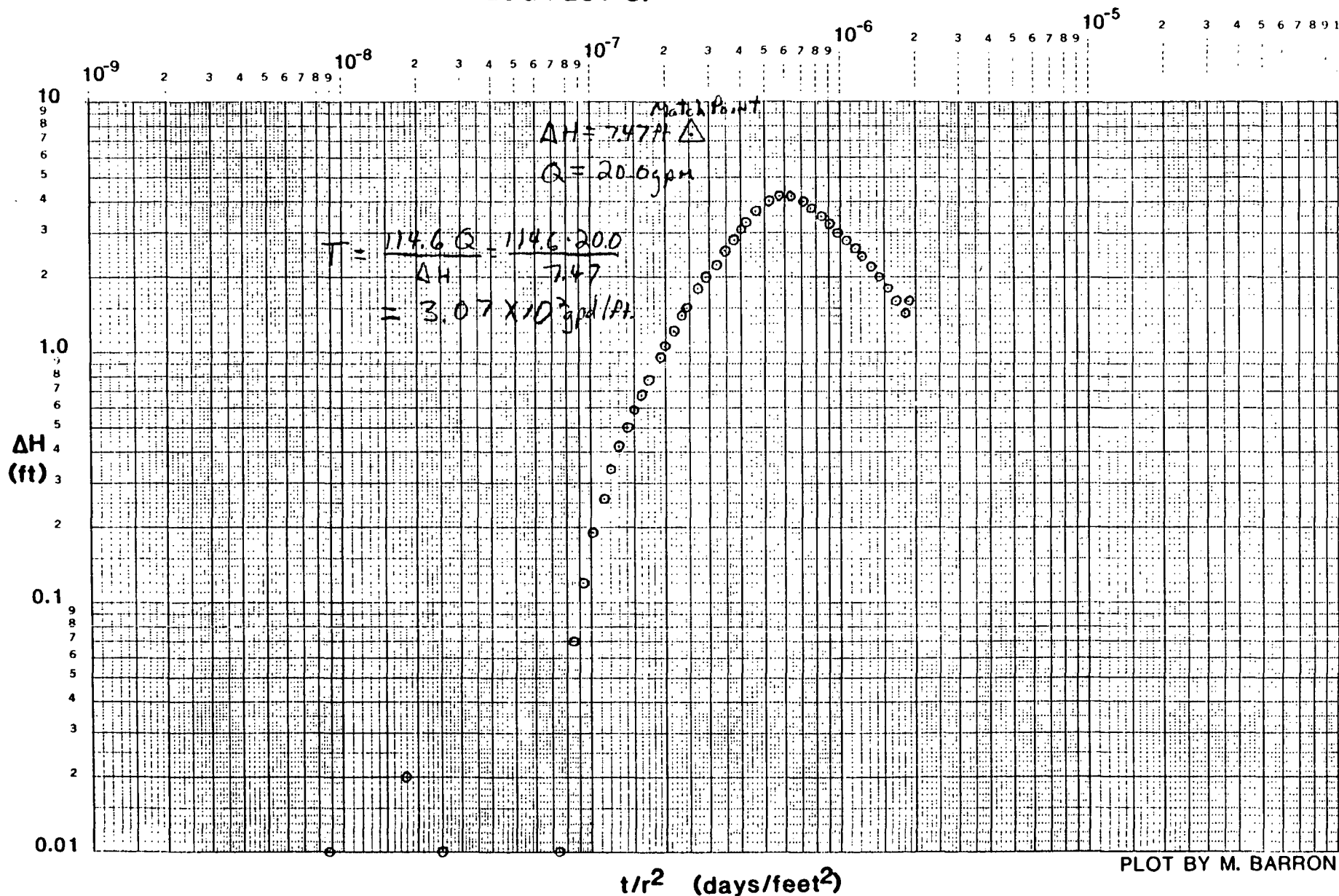


REI 10-1 RUN #1 PUMP TEST - RECOVERY  
SEMI-LOG PLOT OF REI-7

9/15/86

PLOT BY C. AREND

REI 10-1 RUN #1 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI 12-1 9/15/86



PLOT BY M. BARRON

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #1 Calc for REI 12-1

COMPUTED BY: DP DATE: 11-1-80

CHECKED BY: DD DATE: 11-1-80

## Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity } (T) = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$Q = 20.0 \text{ gpm}$$

$$\Delta H = 7.47 \text{ ft}$$

$$T = \frac{(114.6)(20.0)}{7.47} = 3.07 \times 10^2 \text{ cfd/ft}$$

$$\times \text{ Conversion Factor } 1.432 \times 10^{-7} = 4.41 \times 10^{-5} \text{ m}^2/\text{s}$$

## Log-Log solution for Storage - Drawdown

$$\text{Storage } (S) = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 2.60 \times 10^{-7} \text{ days/ft}^2$$

$$T = 3.07 \times 10^2 \text{ cfd/ft}$$

$$S = \frac{(1)(3.07 \times 10^2)(2.60 \times 10^{-7})}{1.87} = 4.23 \times 10^{-5}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

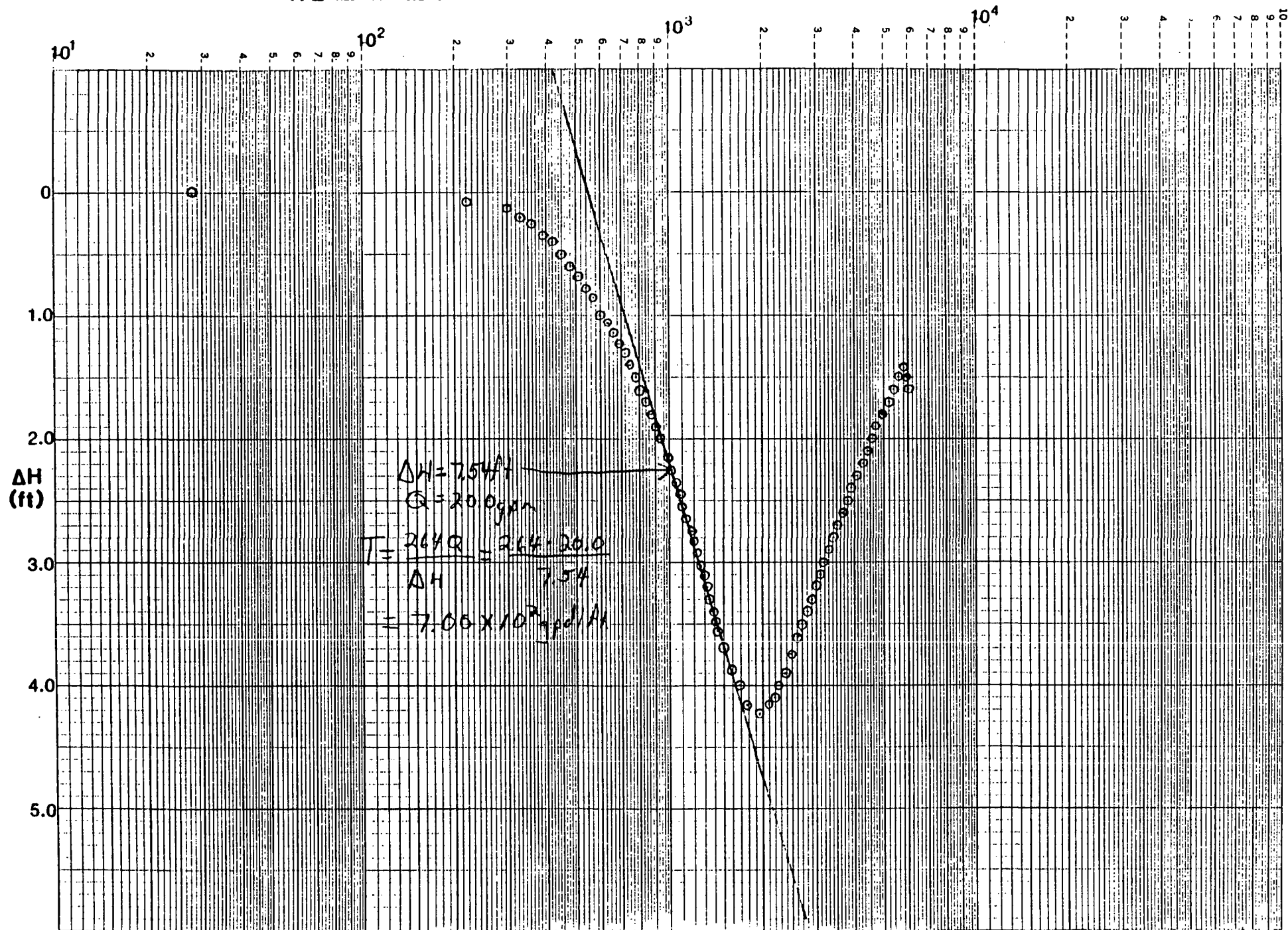
$$T = 3.07 \times 10^2 \text{ cfd/ft}$$

$$b = 36.75 \text{ ft}$$

$$K = \frac{3.07 \times 10^2}{36.75} = 8.35 \times 10^2 \text{ cfd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 3.94 \times 10^{-2} \text{ cm/s}$$

**ERT**





# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 276-14

SUBJECT: PEI 10-1 Pump & Calc for PEI 12-1

COMPUTED BY: DD DATE: 11/19/86

CHECKED BY: DD DATE: 11/19/86

Semi-Log solution for Transmissivity - Drawdown

$$Transmissivity (T) = \frac{264Q}{\Delta h}$$

$$Q = 20.0 \text{ gpm}$$

$$\Delta h = 7.54 \text{ ft}$$

$$T = \frac{(264)(20.0)}{7.54} = 7.00 \times 10^2 \text{ gpd/ft}$$

$$Y \text{ Conversion Factor } 1.432 \times 10^{-7} = 1.01 \times 10^{-4} \text{ m}^2/\text{s}$$

Semi-Log solution for Storativity - Drawdown

$$Storativity (S) = \frac{0.3 T t_0}{r^2}$$

$$r = 1492.112 \text{ ft}$$

$$t_0 = 550 \text{ min} / 1440 = 3.82 \times 10^{-1} \text{ days}$$

$$T = 7.00 \times 10^2 \text{ gpd/ft}$$

$$S = \frac{(0.3)(7.00 \times 10^2)(3.82 \times 10^{-1})}{(1492.112)^2} = 3.60 \times 10^{-5}$$

Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 7.00 \times 10^2 \text{ gpd/ft}$$

$$b = 36.75 \text{ ft}$$

$$K = \frac{7.00 \times 10^2}{36.75} = 1.91 \times 10^1 \text{ gpd/ft}^2$$

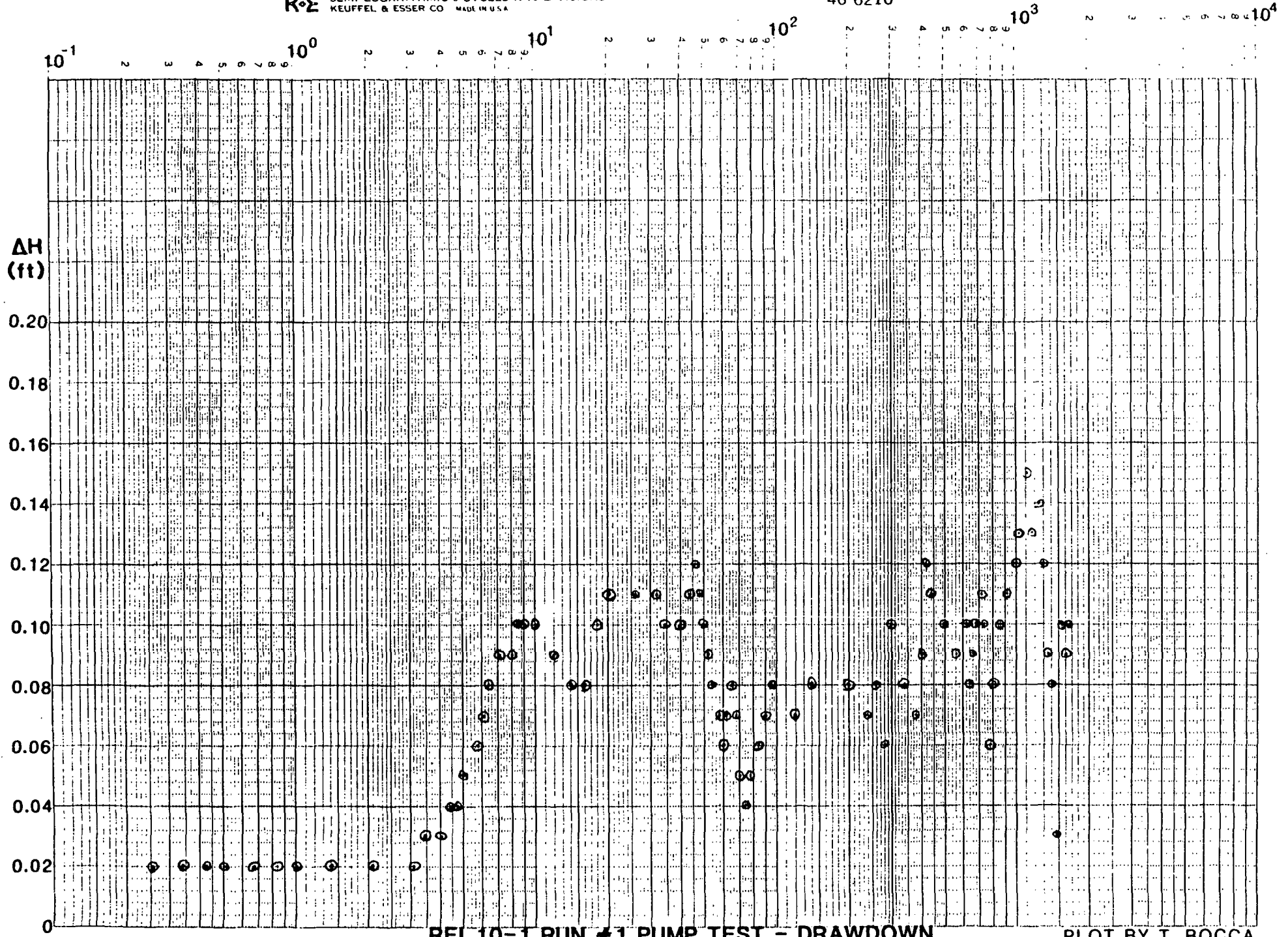
$$X \text{ Conversion Factor } 4.715 \times 10^{-5} = 8.98 \times 10^{-4} \text{ cm/s}$$

**EIRT**

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

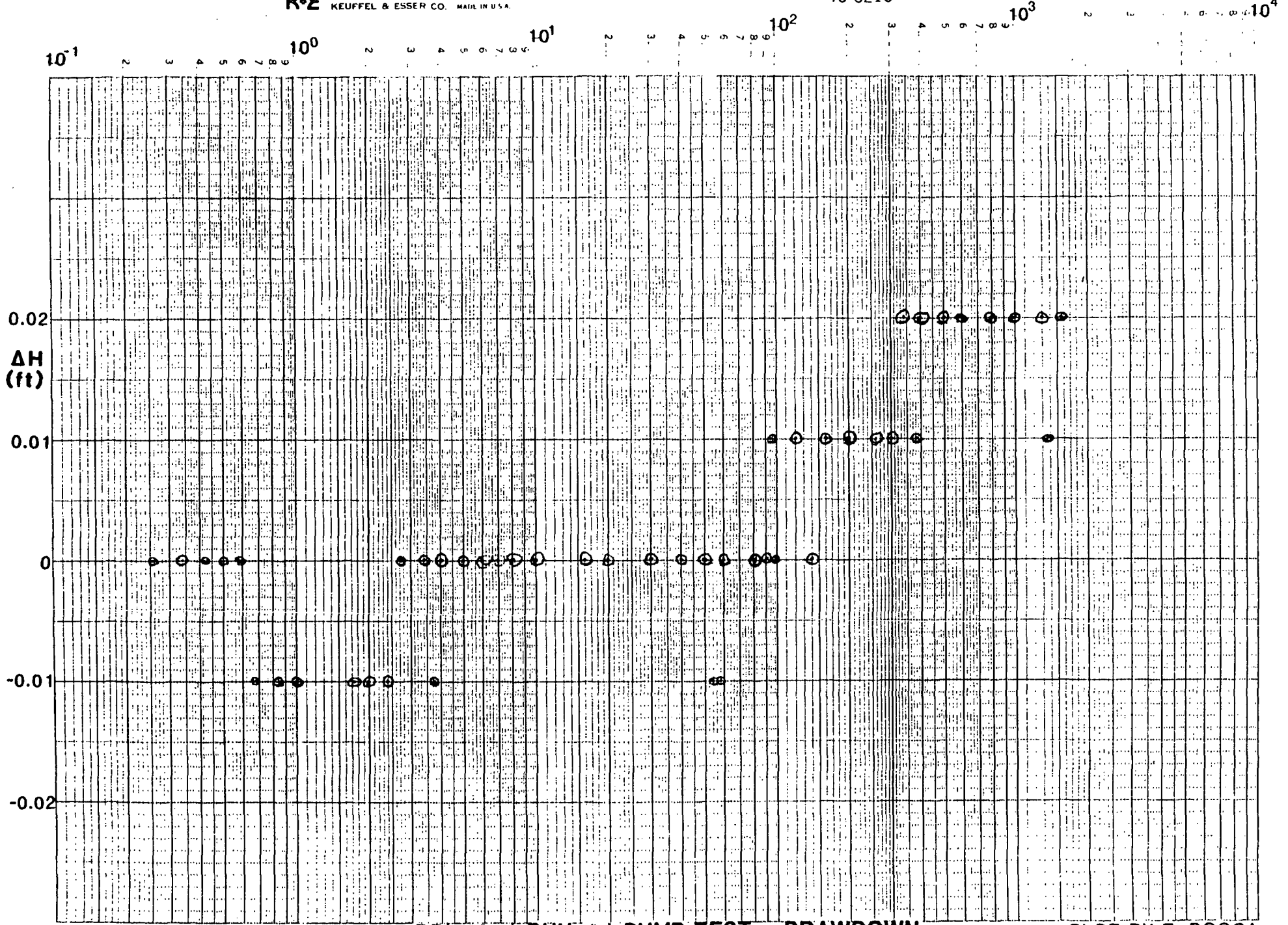
46 6210



K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

46 6210



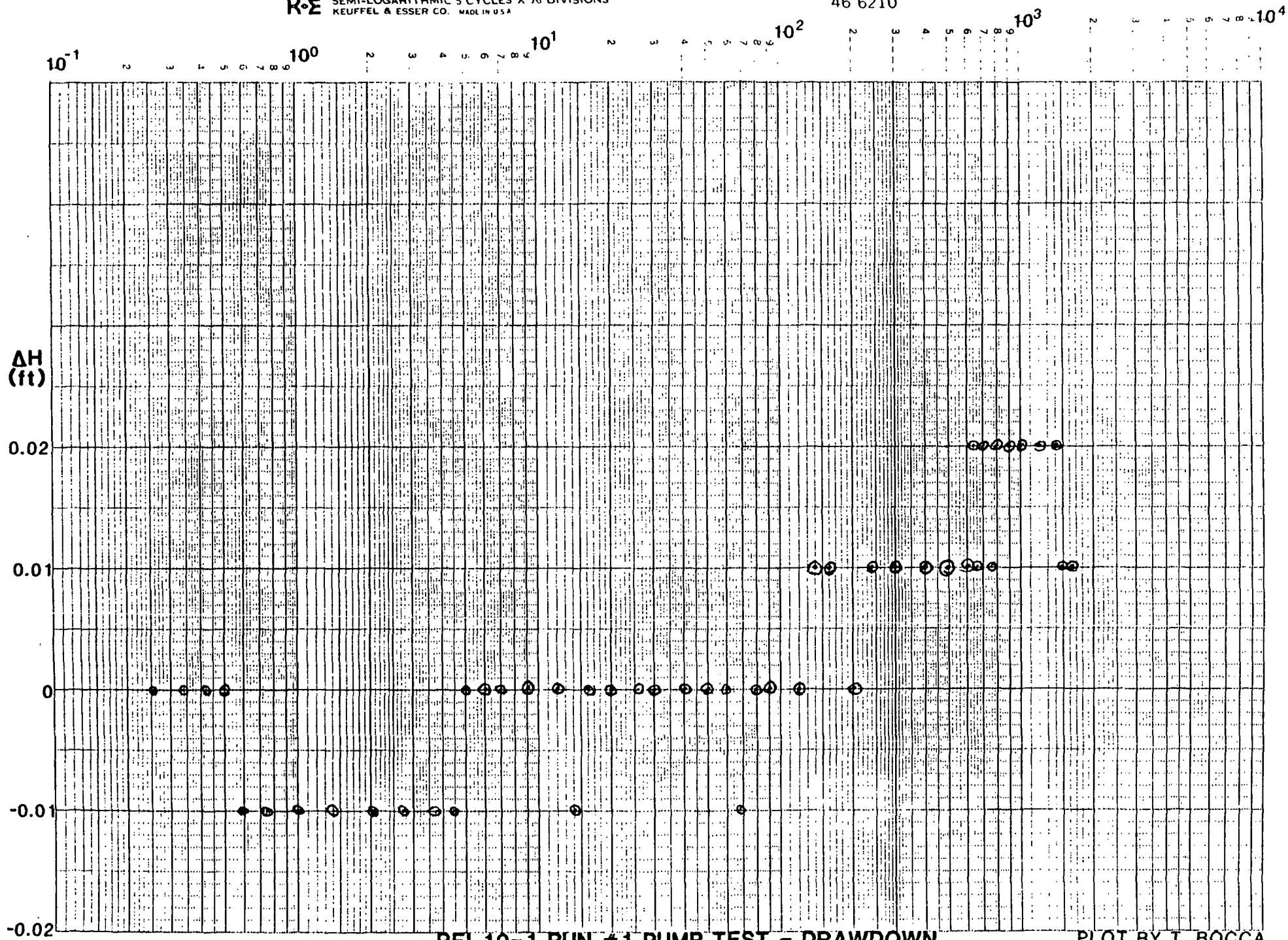
REI 10-1 RUN #1 PUMP TEST - DRAWDOWN

PLOT BY T. BOCCA

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t (min)

46 6210



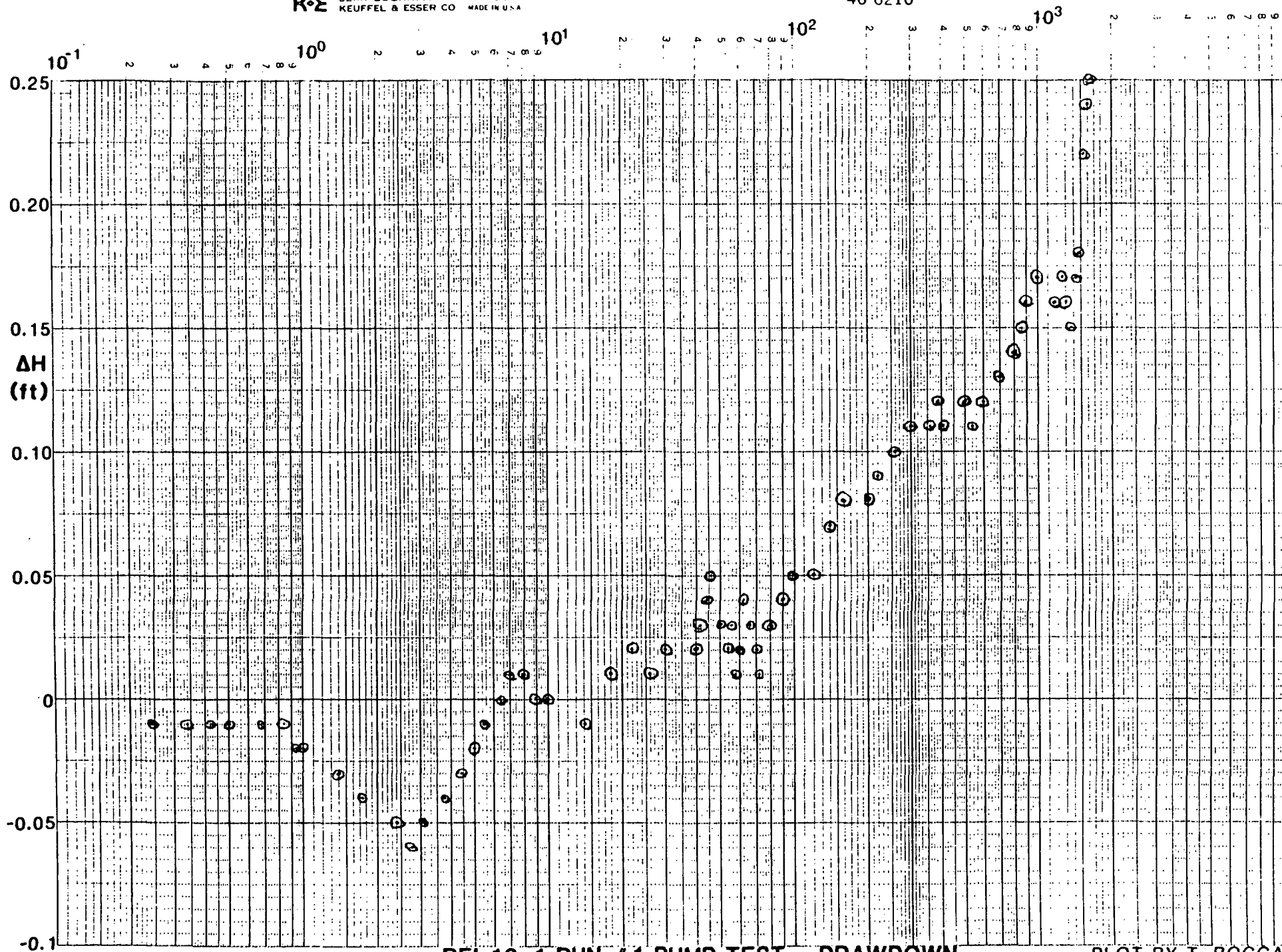
REI 10-1 RUN #1 PUMP TEST - DRAWDOWN

PLOT BY T. BOCCA

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

(min)

46 6210



REI 10-1 RUN #1 PUMP TEST - DRAWDOWN

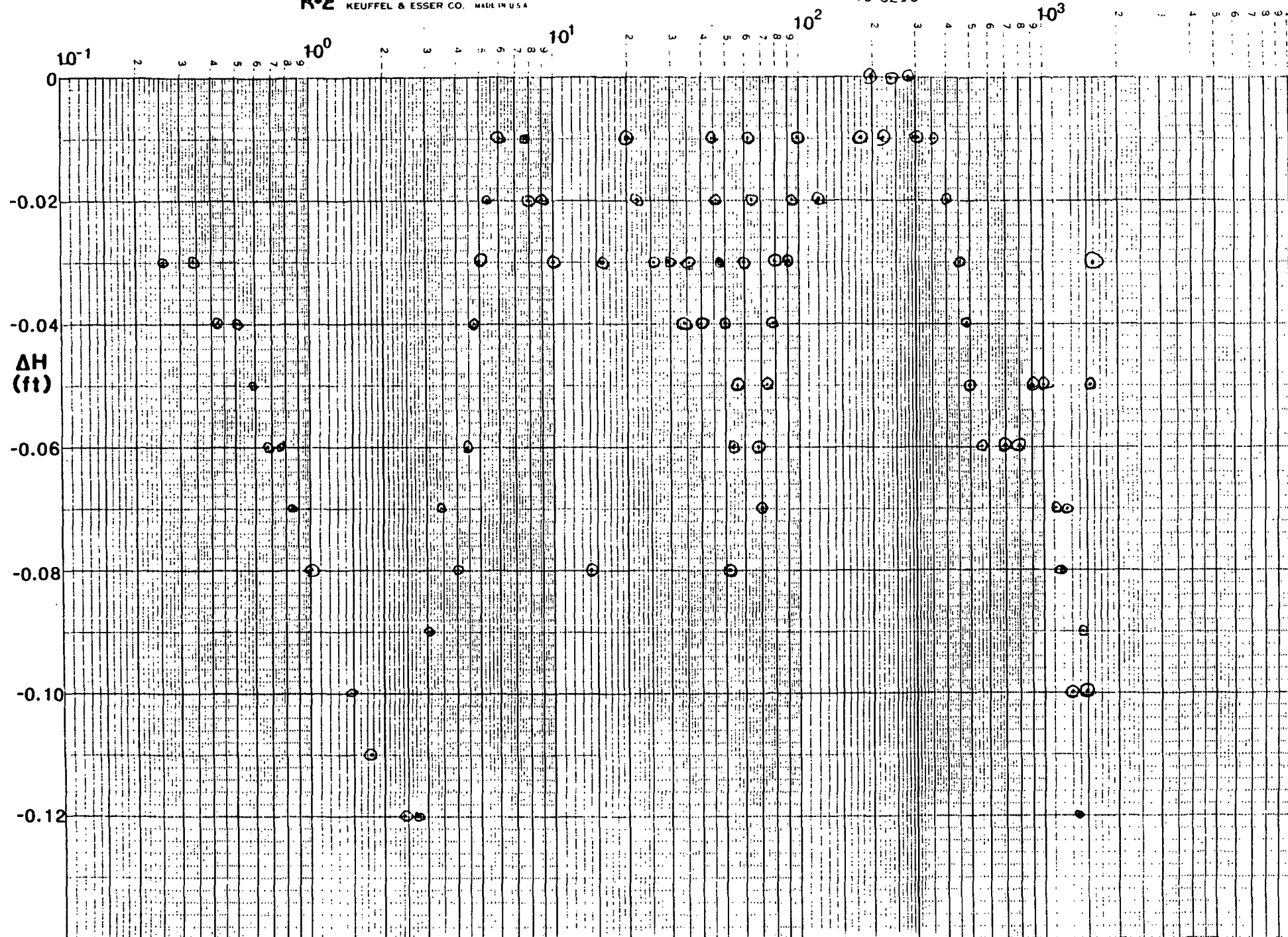
PLOT BY T. BOCCA

9/15/86

K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t (min)

46 6210



REI 10-1 RUN #1 PUMP TEST - DRAWDOWN

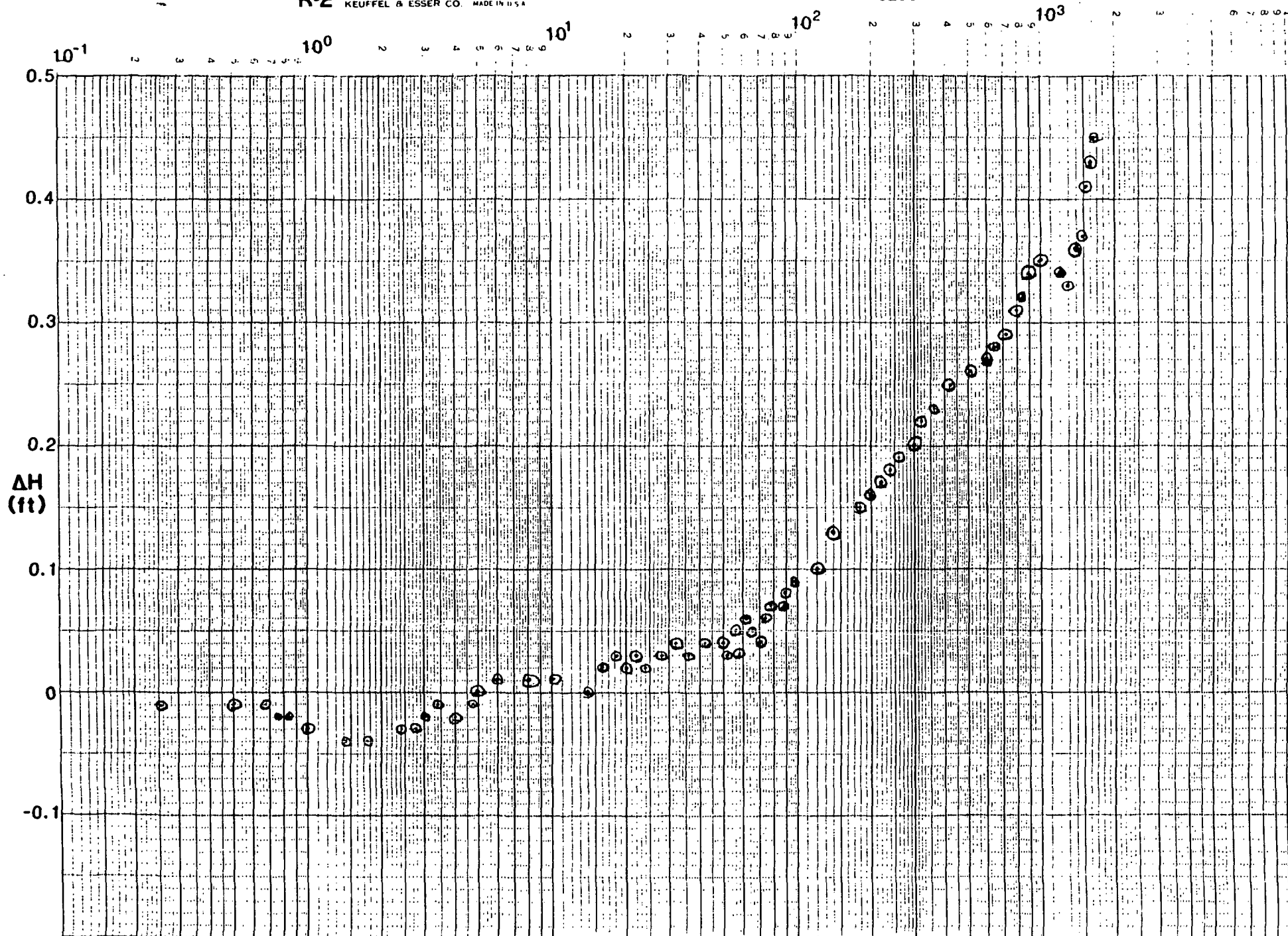
PLOT BY T. BOCCA



K-E SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t (min)

46 6210



REI 10-1 RUN #1 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 10-4

9/15/86

PLOT BY T. BOCCA

Attachment 7

Transmissivity - Well Potential Comparison Chart



# TRANSMISSIVITY

FT <sup>3</sup> /FT/DAY (ft <sup>2</sup> /day)										
10 <sup>8</sup>	10 <sup>7</sup>	10 <sup>6</sup>	10 <sup>5</sup>	10 <sup>4</sup>	10 <sup>3</sup>	10 <sup>2</sup>	10 <sup>1</sup>	1	10 <sup>-1</sup>	10 <sup>-2</sup>
FT <sup>3</sup> /FT/MIN (ft <sup>2</sup> /min)										
10 <sup>4</sup>	10 <sup>3</sup>	10 <sup>2</sup>	10 <sup>1</sup>	1	10 <sup>-1</sup>	10 <sup>-2</sup>	10 <sup>-3</sup>	10 <sup>-4</sup>	10 <sup>-5</sup>	10 <sup>-6</sup>
GAL/FT/DAY (gal/ft/day)										
10 <sup>8</sup>	10 <sup>7</sup>	10 <sup>6</sup>	10 <sup>5</sup>	10 <sup>4</sup>	10 <sup>3</sup>	10 <sup>2</sup>	10 <sup>1</sup>	1	10 <sup>-1</sup>	10 <sup>-2</sup>
METERS <sup>3</sup> /METER/DAY (m <sup>2</sup> /day)										
10 <sup>8</sup>	10 <sup>7</sup>	10 <sup>6</sup>	10 <sup>5</sup>	10 <sup>4</sup>	10 <sup>3</sup>	10 <sup>2</sup>	10 <sup>1</sup>	1	10 <sup>-1</sup>	10 <sup>-2</sup>
SPECIFIC CAPACITY (gal/min/ft)										
10 <sup>3</sup>	10 <sup>4</sup>	10 <sup>5</sup>	10 <sup>6</sup>	10 <sup>7</sup>	10 <sup>8</sup>	10 <sup>9</sup>	10 <sup>10</sup>	10 <sup>11</sup>	10 <sup>12</sup>	10 <sup>13</sup>
WELL POTENTIAL										
Irrigation					Domestic					
UNLIKELY	VERY GOOD	GOOD	FAIR	POOR	GOOD	FAIR	POOR	INFEASIBLE		

NOTES: Transmissivity (T)=KM where

K=Permeability

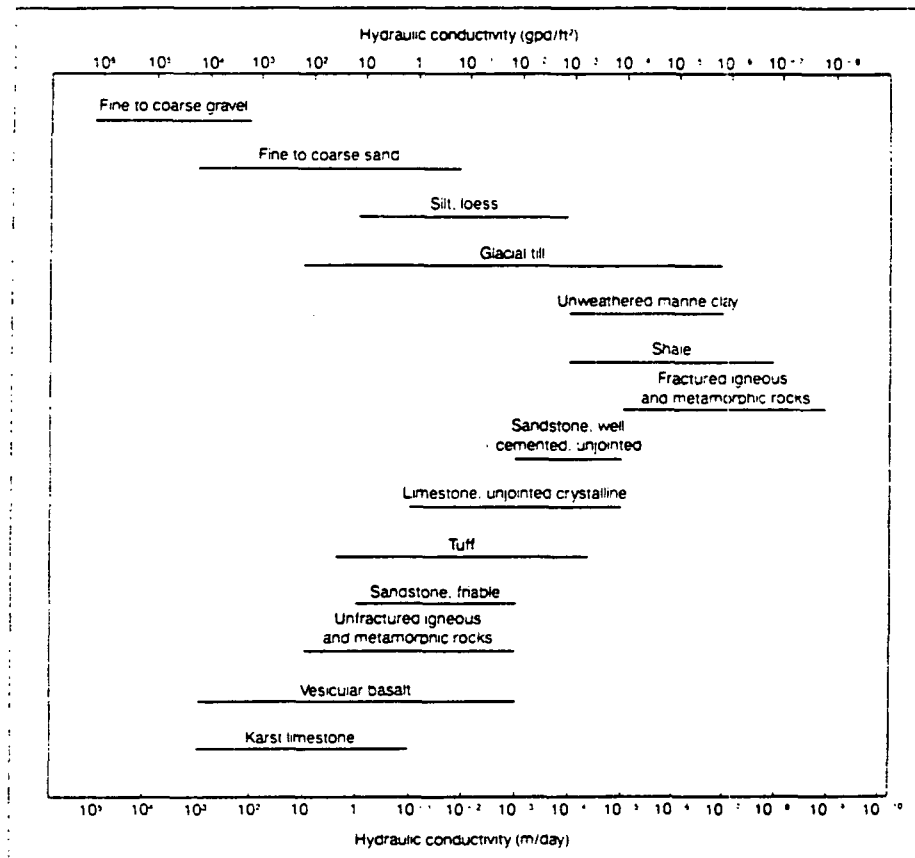
M=Saturated thickness of the aquifer

Specific capacity values based on pumping period of approximately 8-hours but are otherwise generalized.

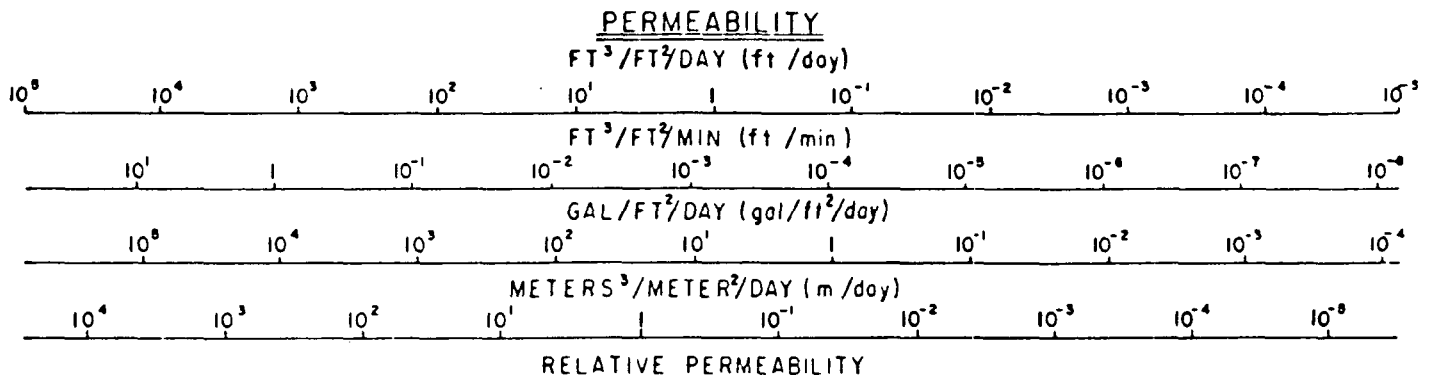
Comparison of transmissivity, specific capacity, and well potential. 103-D-1406.

Attachment 8

Hydraulic Conductivity - Aquifer Material  
Comparison Charts (2)



Typical  $K$  values for consolidated and unconsolidated aquifers. (After Davis, 1969; Dunn and Leopold, 1978; Freeze and Cherry, 1979).



VERY HIGH HIGH MODERATE LOW VERY LOW

REPRESENTATIVE MATERIALS

Clean gravel	—	Clean sand and sand and gravel	—	Fine sand	—	Silt, clay and mixtures of sand, silt and clay	—	Massive clay
Vesicular and scoriaceous basalt and cavernous limestone and dolomite	—	Clean sandstone and fractured igneous and metamorphic rocks	—	Laminated sandstone shale, mudstone	—	Massive igneous and metamorphic rocks		

Comparison of permeability and representative aquifer materials. 103-D-1407.

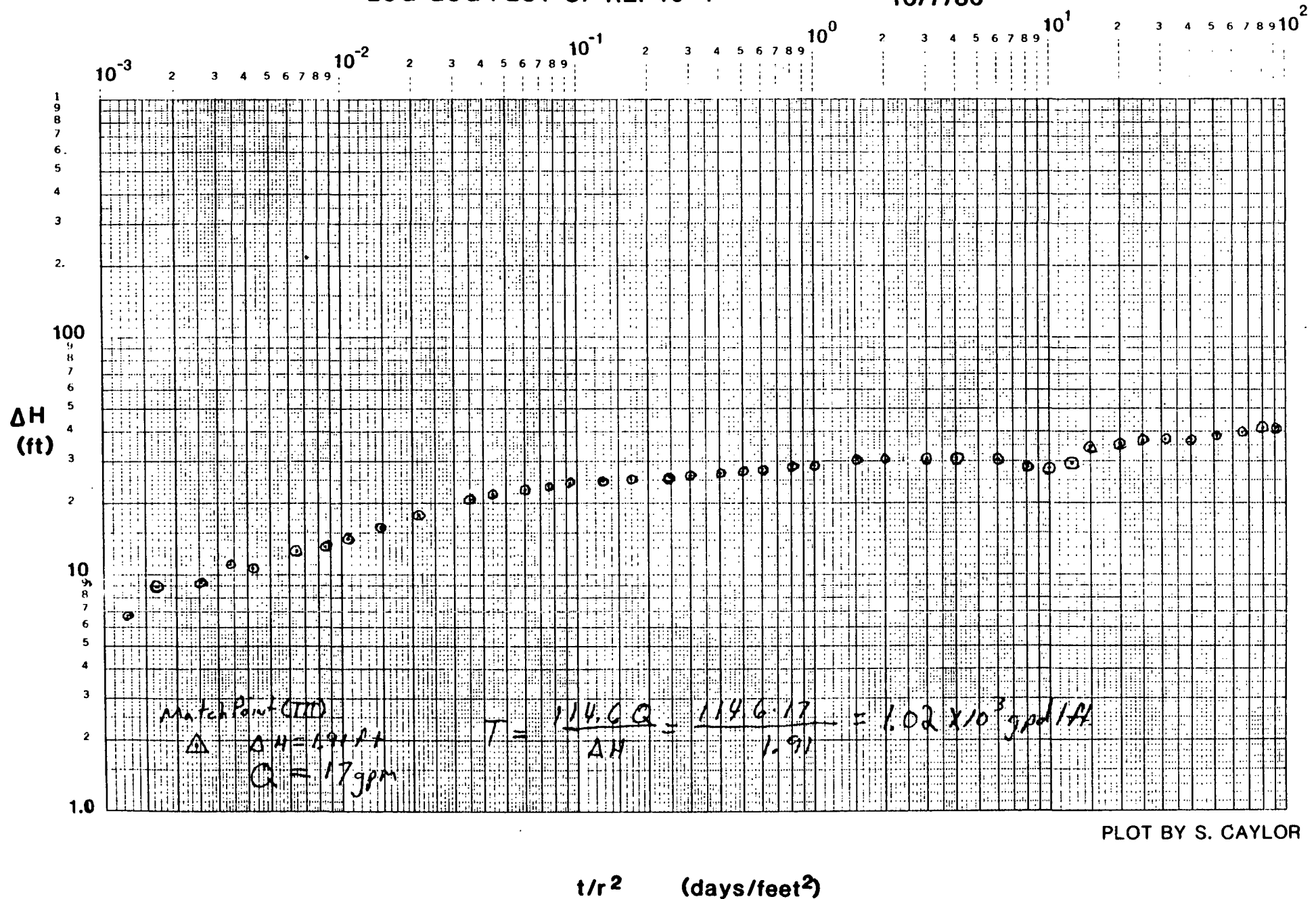
Attachment 9

REI 10-1 Run #2 Pumping Test  
Response Curves and Aquifer  
Characteristics Calculations

REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI 10-1

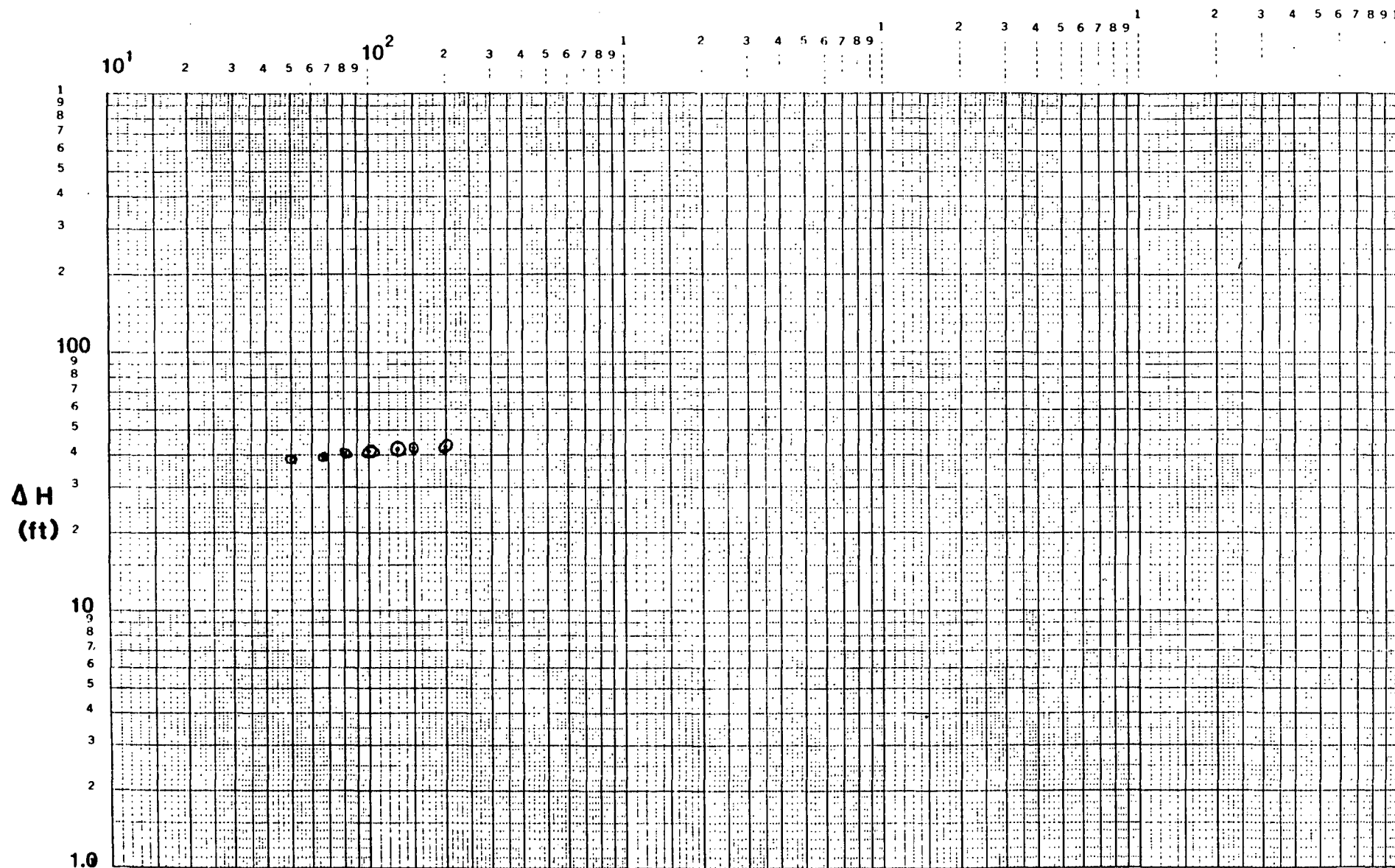
10/7/86

Page 1 of 2



PLOT BY S. CAYLOR

REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI 10-1 10/7/86



$t/r^2$  (days/feet²)

## CALCULATIONS AND COMPUTATIONS

SHEET 1 OF

PROJECT: FRECH LTPJOB NO.: 275-14SUBJECT: REI 10-1 Run #2 Calc. for REI 10-1COMPUTED BY: PCM DATE: 11-13-96CHECKED BY: DEE DATE: 11-14-96

Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$ 

$$\Delta H = 1.91 \text{ ft.}$$

$$Q = 17 \text{ gpm}$$

$$T = \frac{(114.6)(17)}{1.91} = 1.02 \times 10^3 \text{ gpd/ft.}$$

$$\times \text{ Conversion Factor } 1.432 \times 10^{-7} = 1.47 \times 10^{-4} \text{ m}^2/\text{s}$$

Log-Log solution for Storage - Drawdown

$$\text{Storage (S)} = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$ 

$$t/r^2 = 2.40 \times 10^{-7} \text{ days/ft}^2$$

$$T = 1.02 \times 10^3 \text{ gpd/ft.}$$

$$S = \frac{(1)(1.02 \times 10^3)(2.40 \times 10^{-7})}{1.87} = 1.31 \times 10^{-4}$$

Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \text{ where } b \text{ is the screened thickness in feet.}$$

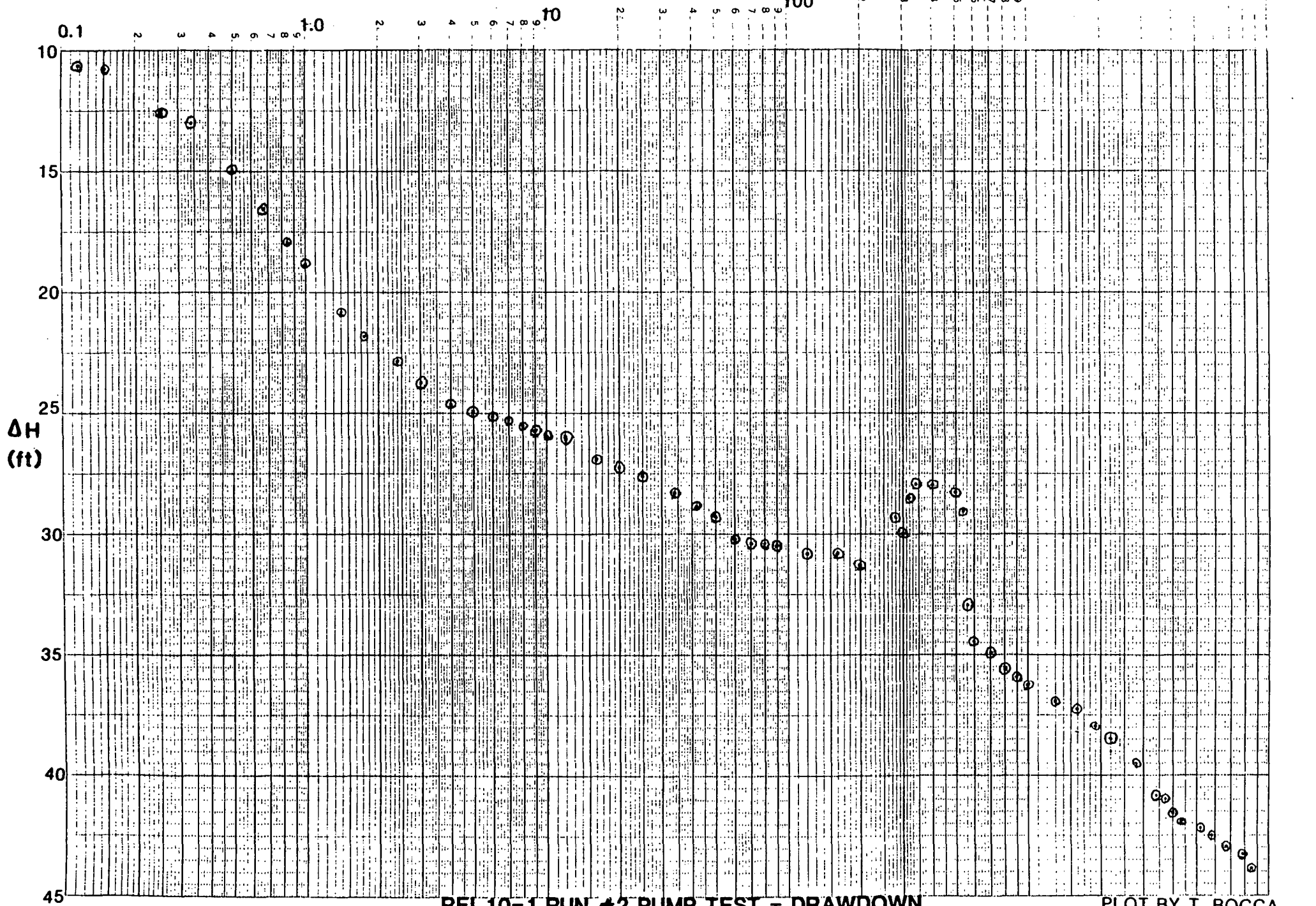
$$T = 1.02 \times 10^3 \text{ gpd/ft.}$$

$$b = 25.30 \text{ ft.}$$

$$K = \frac{1.02 \times 10^3}{25.30} = 4.03 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 1.90 \times 10^{-3} \text{ cm/s}$$



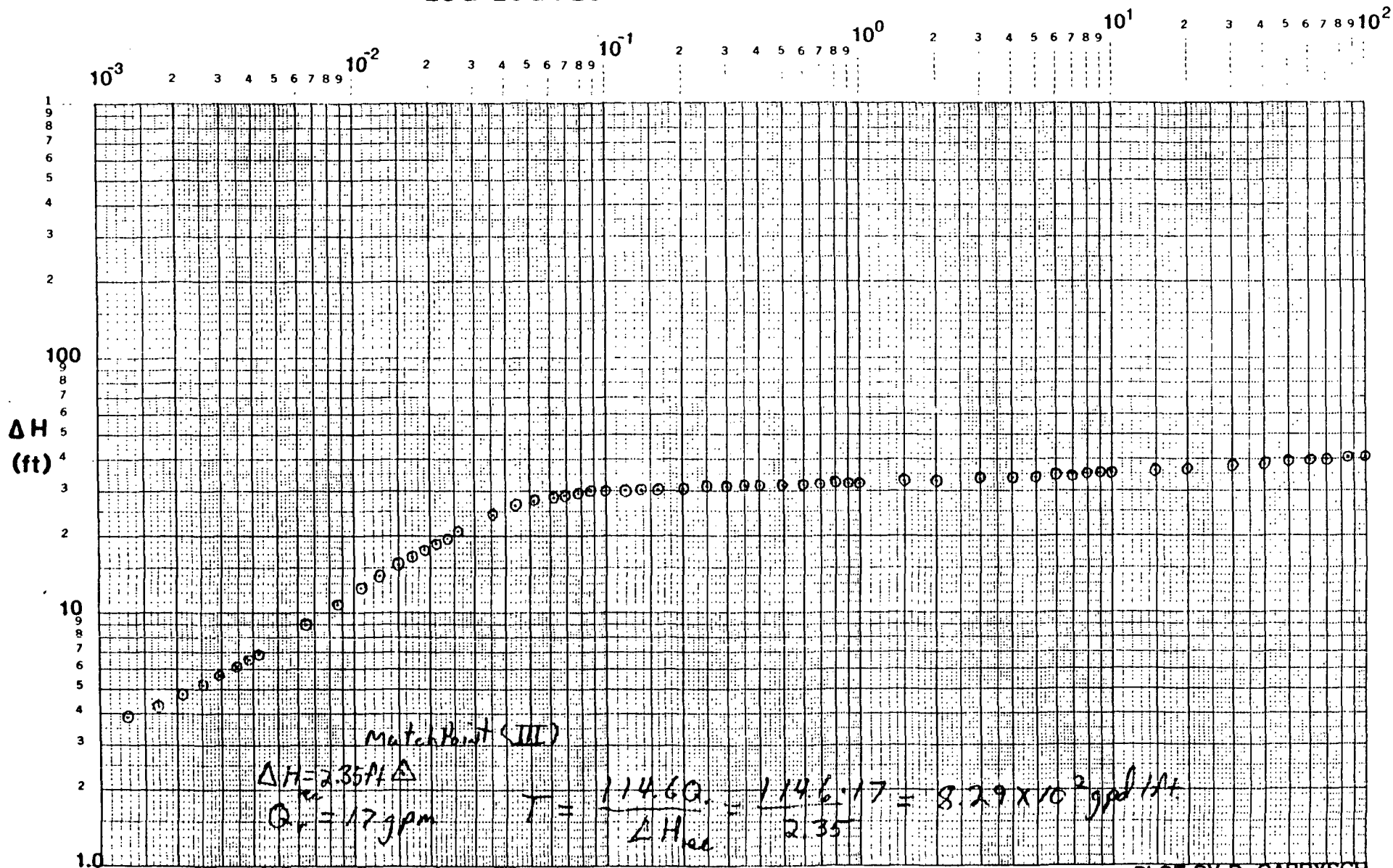


REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 10-1 10/7/86

PLOT BY T. BOCCA

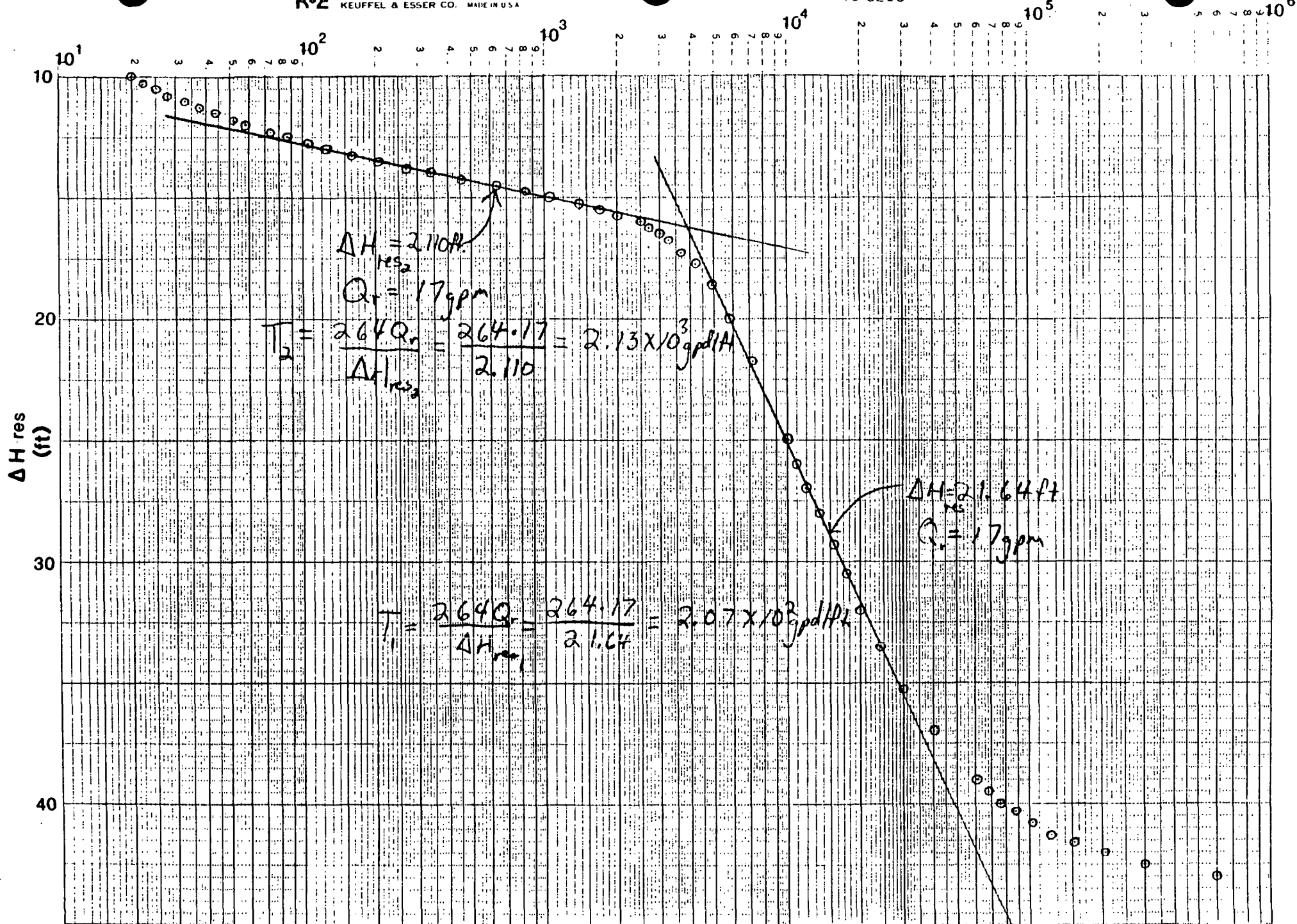
REI 10-1 RUN #2 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF REI 10-1

10/7/86



PLOT BY D. GABRYSCH

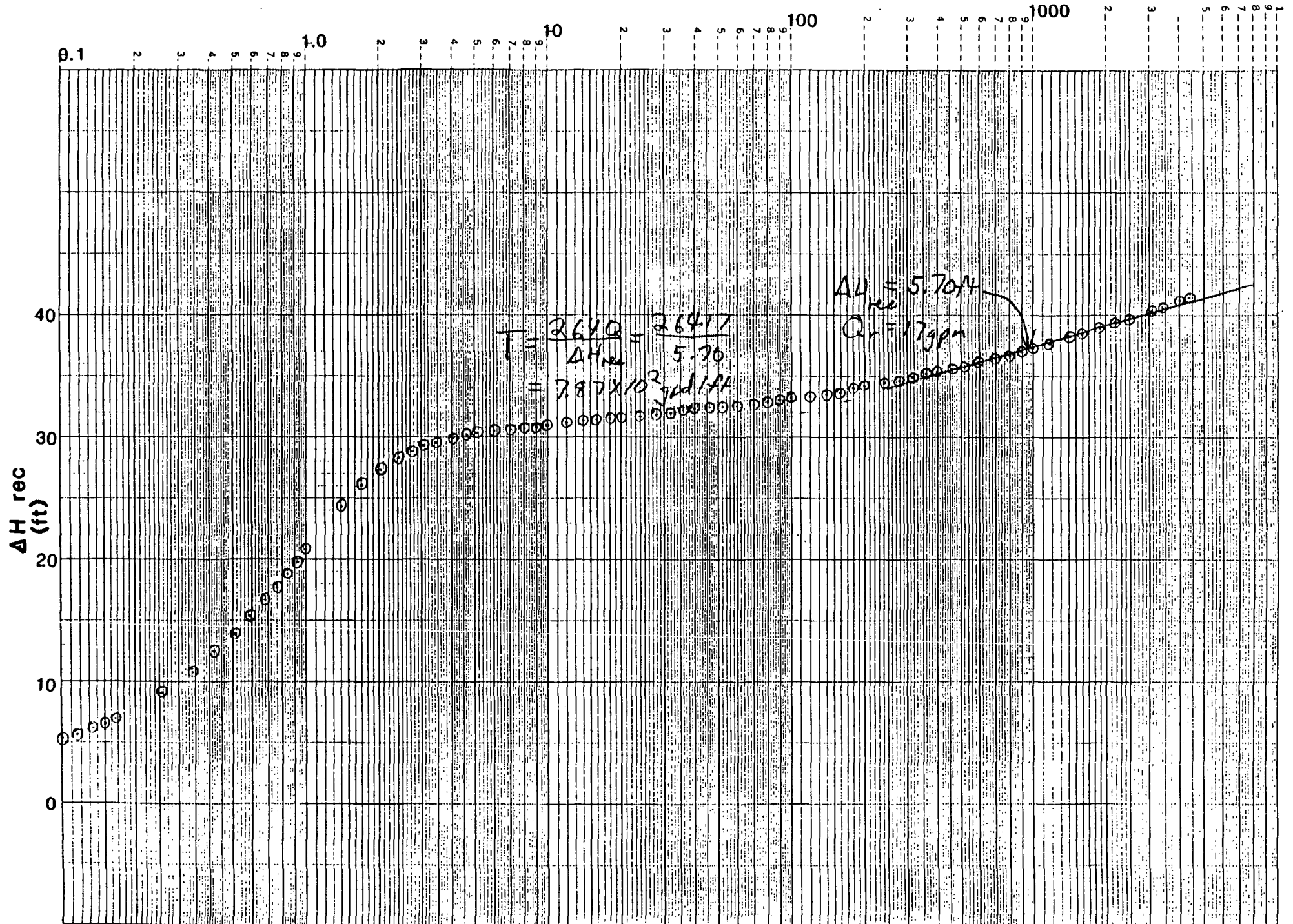
$t/r^2$  (days/feet<sup>2</sup>)



REI 10-1 RUN #2 PUMP TEST - RECOVERY  
SEMI-LOG PLOT OF REI 10-1

10/7/86

PLOT BY M. BARRON



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FEELING LTD.

JOB NO.: 274-14

SUBJECT: REI 10-1 Run #2 Calc for REI 10-1

COMPUTED BY: DRG DATE: 11-17-85

CHECKED BY: DD DATE: 11-19-85

## Log-Log solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$\Delta H = 2.35 \text{ ft}$$

$$Q = 17 \text{ gpm}$$

$$T = \frac{(114.6)(17)}{2.35}$$

$$= 8.29 \times 10^2 \text{ gpd/ft}$$

X Conversion Factor  $1.438 \times 10^{-7}$

$$1.19 \times 10^{-4} \text{ m}^2/\text{s}$$

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 8.29 \times 10^2 \text{ gpd/ft}$$

$$b = 25.30 \text{ ft}$$

$$K = \frac{8.29 \times 10^2}{25.30}$$

$$3.28 \times 10^1 \text{ gpd/ft}^2$$

X Conversion Factor  $4.715 \times 10^{-5}$

$$1.54 \times 10^{-5} \text{ cm/s}$$

## Semi-Log(u) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H_{\text{res}}}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H_{\text{res}_1} = 21.64 \text{ ft}$$

$$T_1 = \frac{(264)(17)}{21.64}$$

$$= 2.07 \times 10^2 \text{ gpd/ft}$$

$$\Delta H_{\text{res}_2} = 2.110 \text{ ft}$$

$$T_2 = \frac{(264)(17)}{2.110}$$

$$= 2.13 \times 10^3 \text{ gpd/ft}$$

X Conversion Factor  $1.438 \times 10^{-7}$

$$2.98 \times 10^{-5} \text{ m}^2/\text{s}$$

$$3.06 \times 10^{-5} \text{ m}^2/\text{s}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc for REI 10-1

COMPUTED BY: DRG DATE: 11-14-85

CHECKED BY: DD DATE: 11-19-85

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T_1 = \boxed{2.07 \times 10^2 \text{ gpd/ft}}$$

$$b = 25.30 \text{ ft}$$

$$K_1 = \frac{2.07 \times 10^2}{25.30} = \boxed{8.18 \times 10^0 \text{ gpd/ft}^2}$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = \boxed{3.86 \times 10^{-4} \text{ cm/s}}$$

$$T_2 = \boxed{2.13 \times 10^3 \text{ gpd/ft}}$$

$$b = 25.30 \text{ ft}$$

$$K_2 = \frac{2.13 \times 10^3}{25.30} = \boxed{8.42 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = \boxed{3.97 \times 10^{-3} \text{ cm/s}}$$

## Semi-Log(L) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H_{\text{rec}}}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H_{\text{rec}} = 5.70 \text{ ft}$$

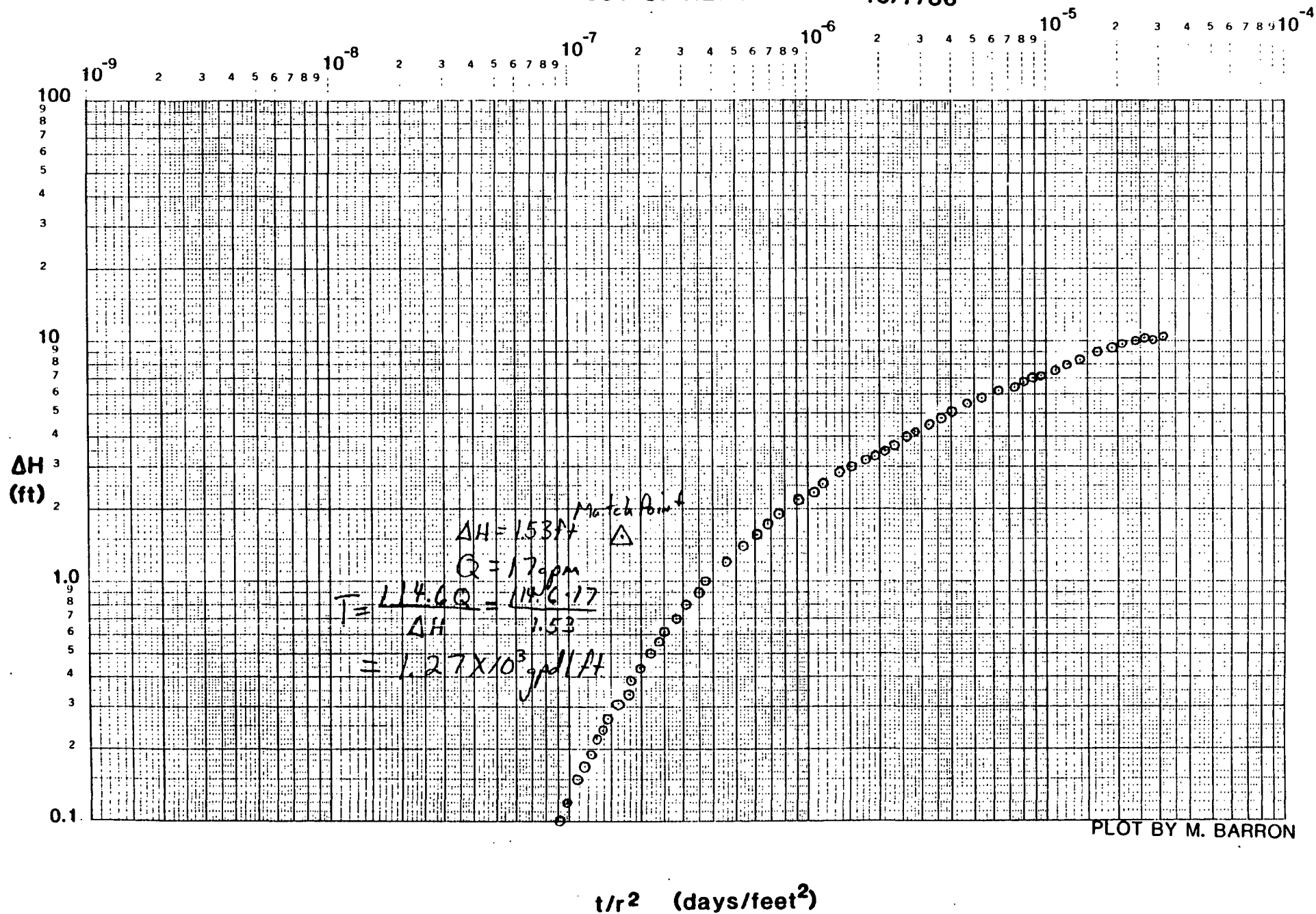
$$T = \frac{(264)(17)}{5.70} = \boxed{7.87 \times 10^2 \text{ gpd/ft}}$$

$$\times \text{Conversion Factor } 1.432 \times 10^{-7} = \boxed{1.13 \times 10^{-4} \text{ m/s}}$$

**ERT**

REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI 11

10/7/86



PLOT BY M. BARRON

# CALCULATIONS AND COMPUTATIONS

SHEET 5 OF 5

PROJECT: FRENCH LTD

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc. for REI 11

COMPUTED BY: DRG DATE: 11-2-73

CHECKED BY: DD DATE: 11-14-73

## Log-Log solution for Transmissivity - Drawdown

$$Transmissivity (T) = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$\Delta H = 1.53 \text{ ft.}$

$Q = 17 \text{ gpm}$

$$T = \frac{(114.6)(17)}{1.53} = 1.27 \times 10^3 \text{ cfd/ft.}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 1.83 \times 10^{-4} \text{ m}^2/\text{s}$$

## Log-Log solution for Storativity - Drawdown

$$Storativity (S) = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 1.68 \times 10^{-7} \text{ days/ft}^2$$

$$T = 1.27 \times 10^3 \text{ cfd/ft.}$$

$$S = \frac{(1)(1.27 \times 10^3)(1.68 \times 10^{-7})}{1.87} = 1.14 \times 10^{-4}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \text{ where } b \text{ is the screened thickness in feet.}$$

$$T = 1.27 \times 10^3 \text{ cfd/ft.}$$

$b = 16.45 \text{ ft}$

$$K = \frac{1.27 \times 10^3}{16.45} = 7.72 \times 10^1 \text{ cfd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 3.64 \times 10^{-3} \text{ cm/s}$$

**REI**

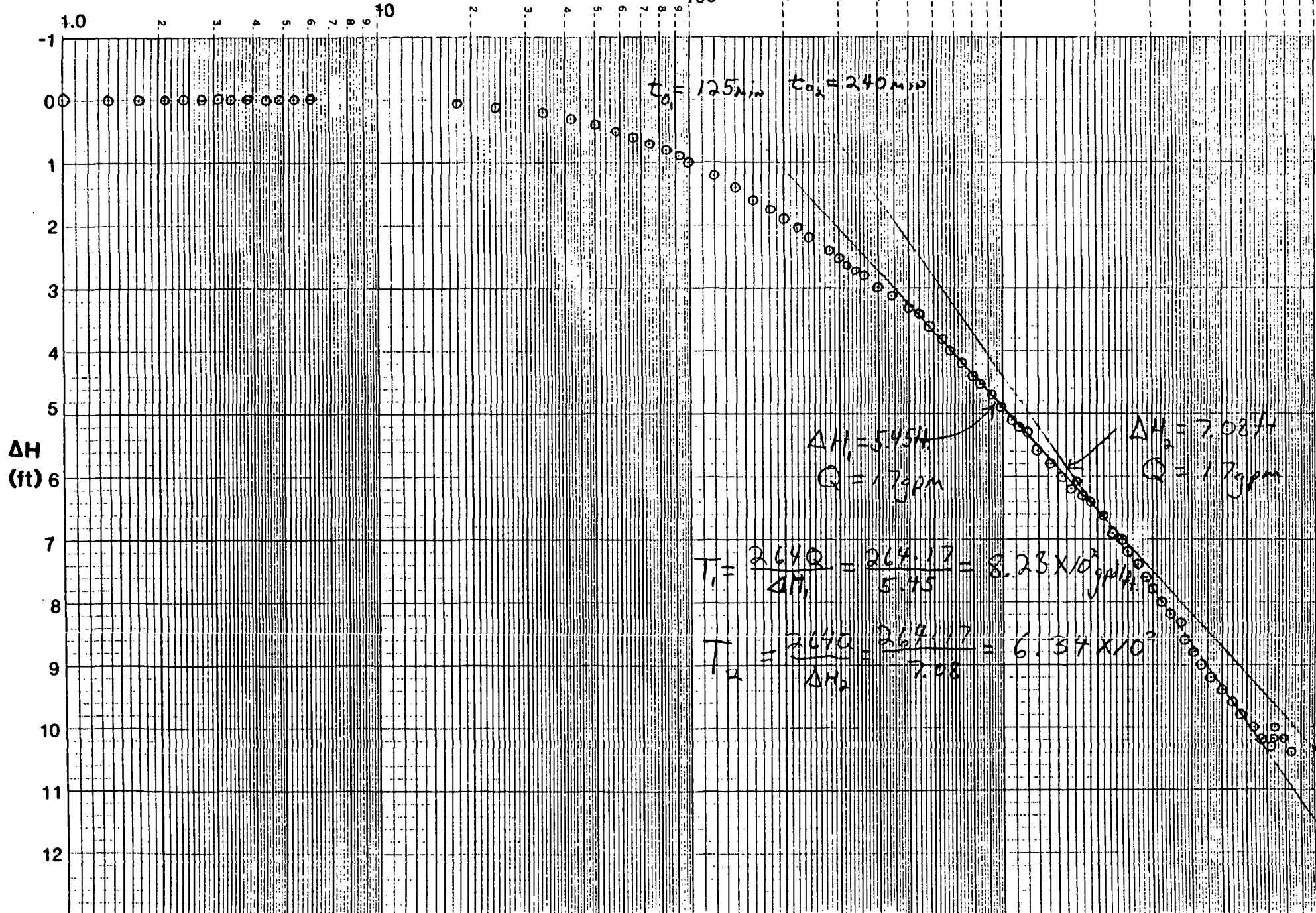


t(min)

46 6010

1000

10000



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc. for REI 11

COMPUTED BY: PCM DATE: 11-13-21

CHECKED BY: DRG DATE: 11-14-21

DD 11-14-21

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H_1 = 5.45 \text{ ft.}$$

$$T_1 = \frac{264(17)}{5.45}$$

$$= 8.24 \times 10^2 \text{ gpd/ft}$$

$$\Delta H_2 = 7.08 \text{ ft.}$$

$$T_2 = \frac{264(17)}{7.08}$$

$$6.34 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.432 \times 10^{-7} =$$

$$1.18 \times 10^{-4} \text{ m}^2/\text{s}$$

$$9.12 \times 10^{-5} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.3 T t_0}{r^2}$$

$$r = 427.782 \text{ ft.}$$

$$t_{01} = 125 \text{ min.} / 1440 = 8.68 \times 10^{-2} \text{ days}$$

$$T_1 = 8.24 \times 10^2 \text{ gpd/ft}$$

$$t_{02} = 240 \text{ min.} / 1440 = 1.67 \times 10^{-1} \text{ days}$$

$$T_2 = 6.34 \times 10^2 \text{ gpd/ft.}$$

$$S_1 = \frac{(0.3)(8.24 \times 10^2)(8.68 \times 10^{-2})}{(427.782)^2} = 1.17 \times 10^{-4}$$

$$S_2 = \frac{(0.3)(6.34 \times 10^2)(1.67 \times 10^{-1})}{(427.782)^2} = 1.74 \times 10^{-4}$$

**REI**

# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc. for REI 11

COMPUTED BY: PCM DATE: 11-15-86

CHECKED BY: DRG DATE: 11-15-86  
DD 11-15-86

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T_1 = \boxed{8.24 \times 10^2 \text{ gpd/ft}}$$

$$b = 16.45 \text{ ft}$$

$$K = \frac{8.24 \times 10^2}{16.45}$$

$$\boxed{5.01 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5}$$

$$\boxed{2.36 \times 10^{-3} \text{ cm/s}}$$

$$T_2 = \boxed{6.34 \times 10^2 \text{ gpd/ft}}$$

$$b = 16.45 \text{ ft}$$

$$K = \frac{6.34 \times 10^2}{16.45}$$

$$\boxed{3.85 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5}$$

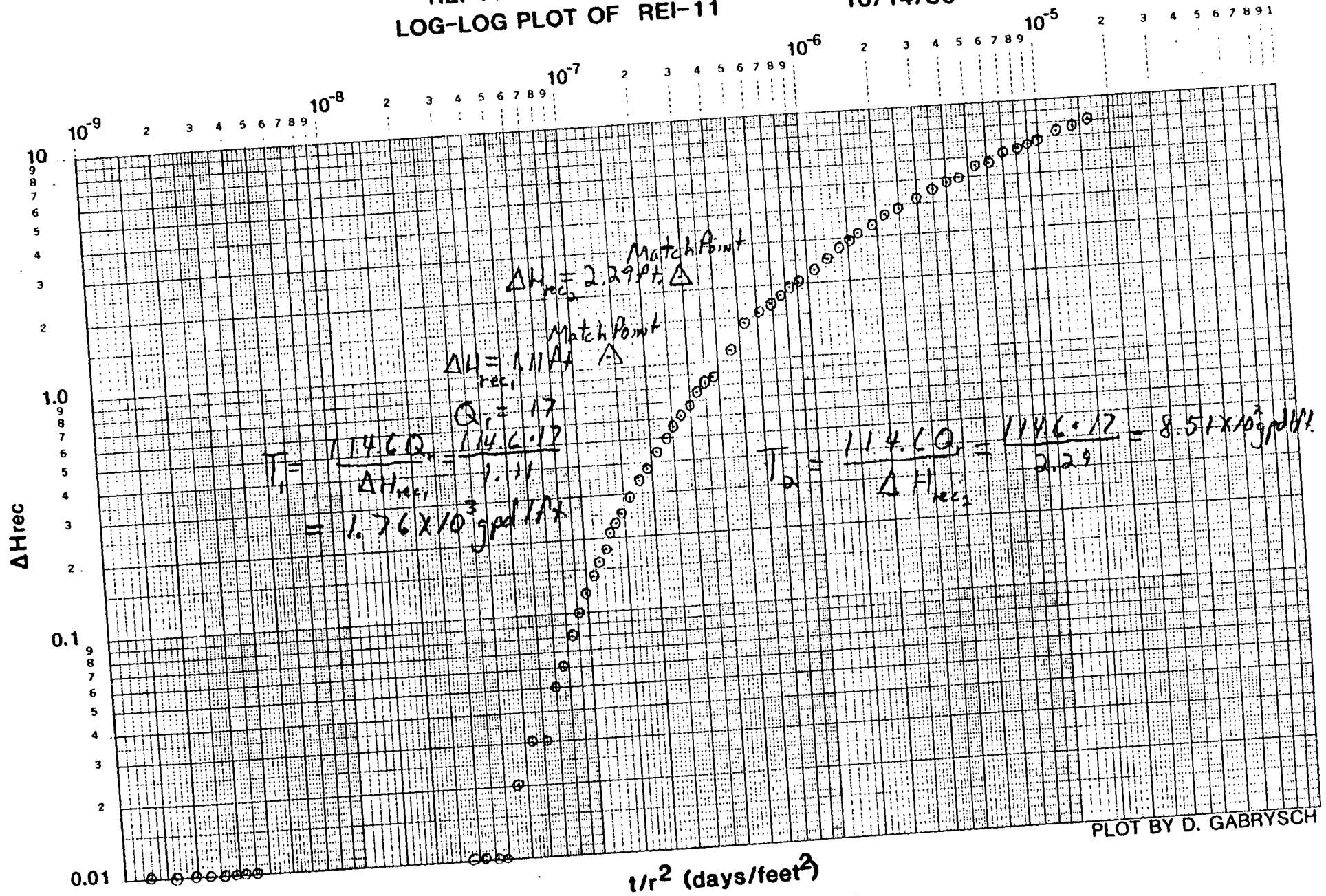
$$\boxed{1.82 \times 10^{-3} \text{ cm/s}}$$

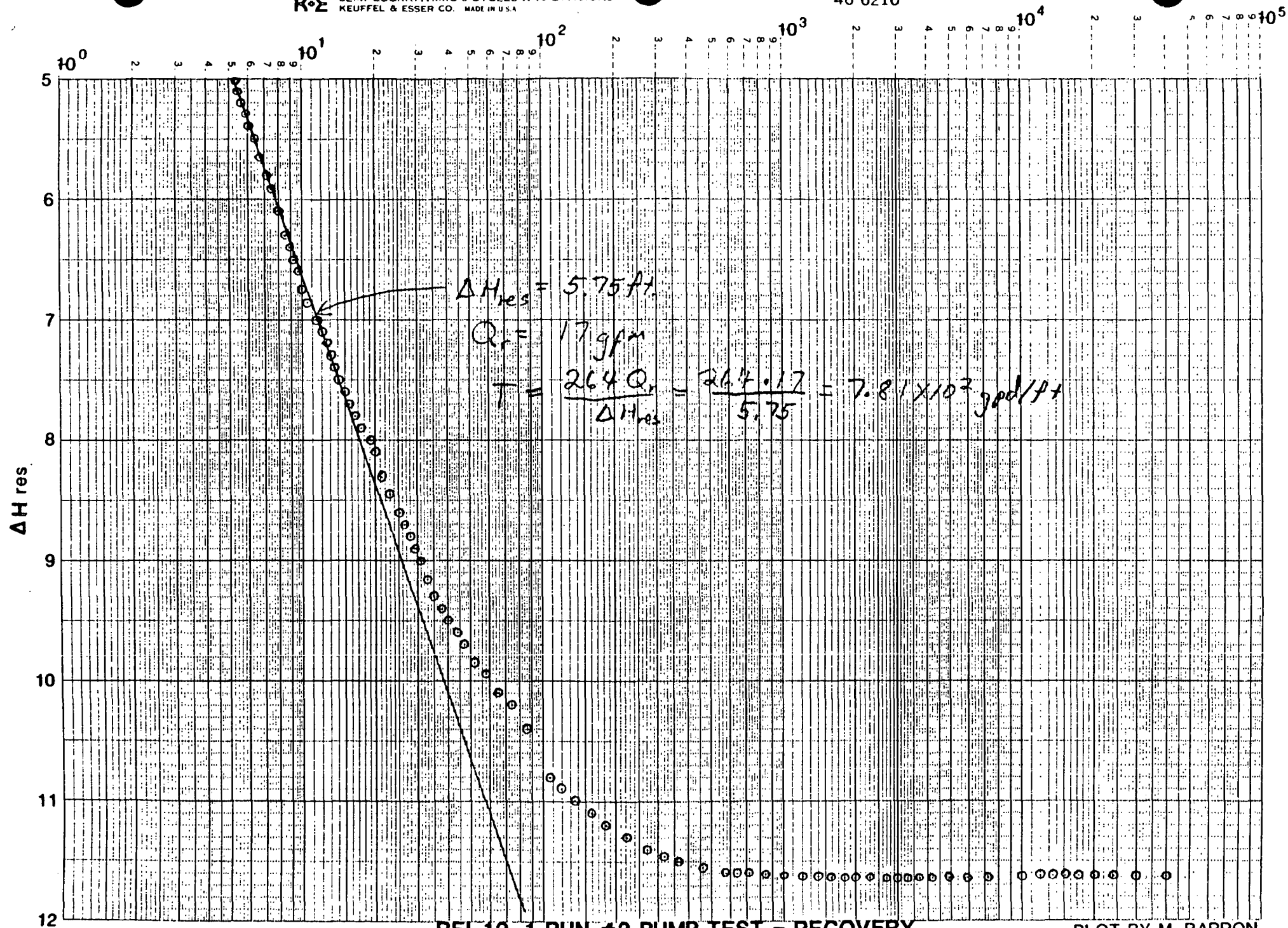
**REI**

K-E LOGARITHMIC 3 x 5 CYCLES  
KEUFFEL & ESSER CO. MADE IN USA

46 7520

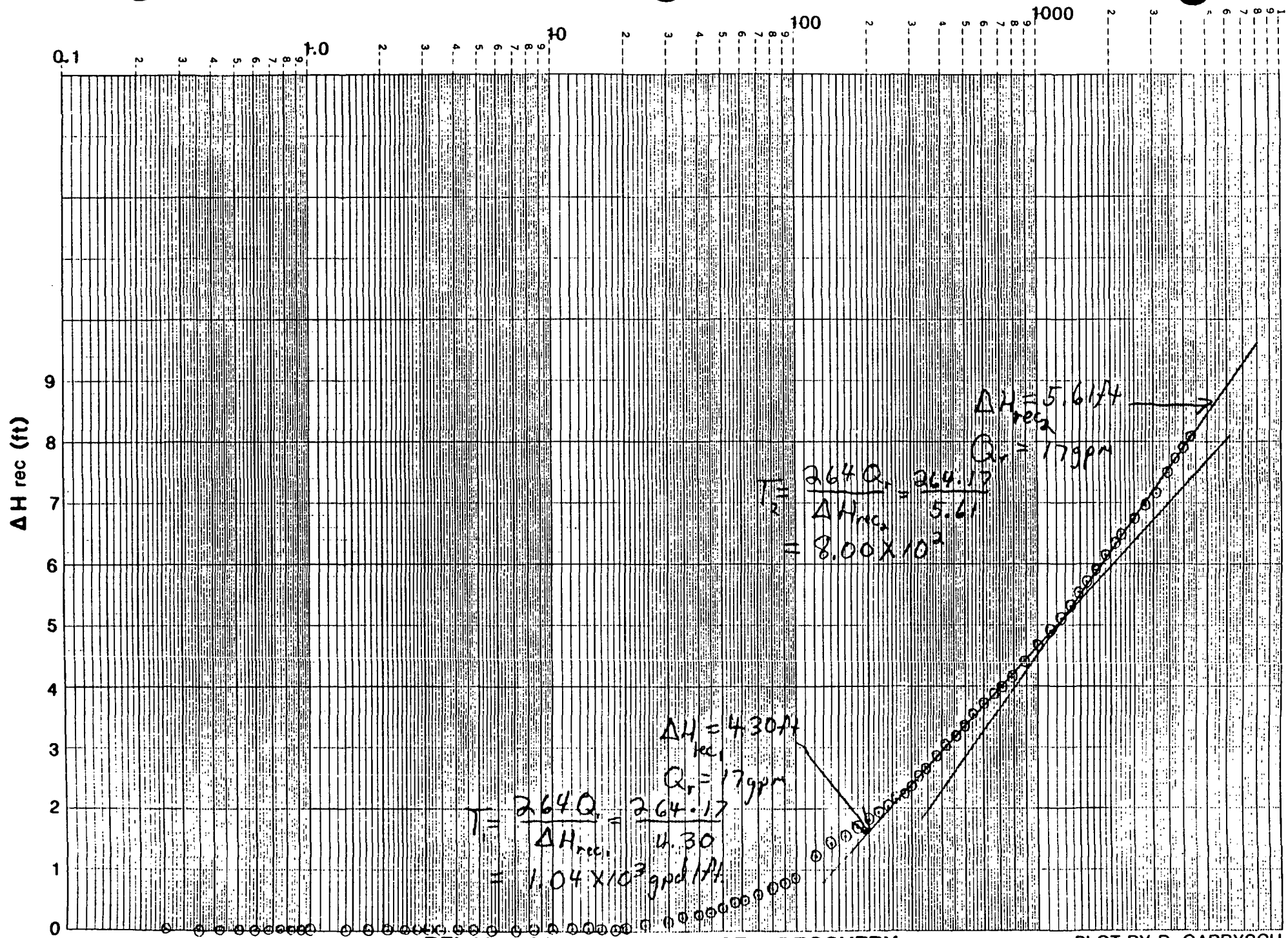
REI 10-1 RUN #2 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF REI-11 10/14/86





REI 10-1 RUN #2 PUMP TEST - RECOVERY  
SEMI-LOG PLOT OF REI-11  
10/7/86

PLOT BY M. BARRON



REI 10-1 RUN #2 PUMP TEST - RECOVERY  
SEMI-LOG PLOT OF REI 11  
10/7/86

PLOT BY D. GABRYSCH

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc. for REI 11

COMPUTED BY: DRG DATE: 11-14-81

CHECKED BY: DD DATE: 11-15-81

## Log-Log solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$Q = 17 \text{ gpm}$$

$$\Delta H_1 = 1.11 \text{ ft}$$

$$\Delta H_2 = 2.29 \text{ ft}$$

$$T_1 = \frac{(114.6)(17)}{1.11}$$

$$T_2 = \frac{(114.6)(17)}{2.29}$$

$$= 1.76 \times 10^3 \text{ gpd/ft}$$

$$= 8.51 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7}$$

$$= 2.52 \times 10^{-4} \text{ m}^2/\text{s}$$

$$= 1.22 \times 10^{-4} \text{ m}^2/\text{s}$$

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T_1 = 1.76 \times 10^3 \text{ gpd/ft}$$

$$b = 16.45 \text{ ft}$$

$$K_1 = \frac{1.76 \times 10^3}{16.45}$$

$$= 1.07 \times 10^2 \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5}$$

$$= 5.04 \times 10^{-3} \text{ cm/s}$$

$$T_2 = 8.51 \times 10^2 \text{ gpd/ft}$$

$$b = 16.45 \text{ ft}$$

$$K = \frac{8.51 \times 10^2}{16.45}$$

$$= 5.17 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5}$$

$$= 2.44 \times 10^{-3} \text{ cm/s}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc for REI 11

COMPUTED BY: DEK DATE: 11/14/88

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Semi-Log(a) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264Q}{\Delta H_{res}}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H_{res} = 5.75 \text{ ft} \quad T = \frac{(264)(17)}{5.75} = 7.81 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7}$$

$$1.12 \times 10^{-4} \text{ m}^2/\text{s}$$

Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 7.81 \times 10^2 \text{ gpd/ft}$$

$$b = 16.45 \text{ ft}$$

$$K = \frac{7.81 \times 10^2}{16.45} = 4.75 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 2.24 \times 10^{-3} \text{ cm/s}$$

Semi-Log(b) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264Q}{\Delta H_{rec}}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H_{rec1} = 4.30 \text{ ft} \quad T_1 = \frac{(264)(17)}{4.30} = 1.04 \times 10^3 \text{ gpd/ft}$$

$$\Delta H_{rec2} = 5.61 \text{ ft} \quad T_2 = \frac{(264)(17)}{5.61} = 8.00 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7} =$$

$$1.50 \times 10^{-4} \text{ m}^2/\text{s}$$

$$1.15 \times 10^{-4} \text{ m}^2/\text{s}$$

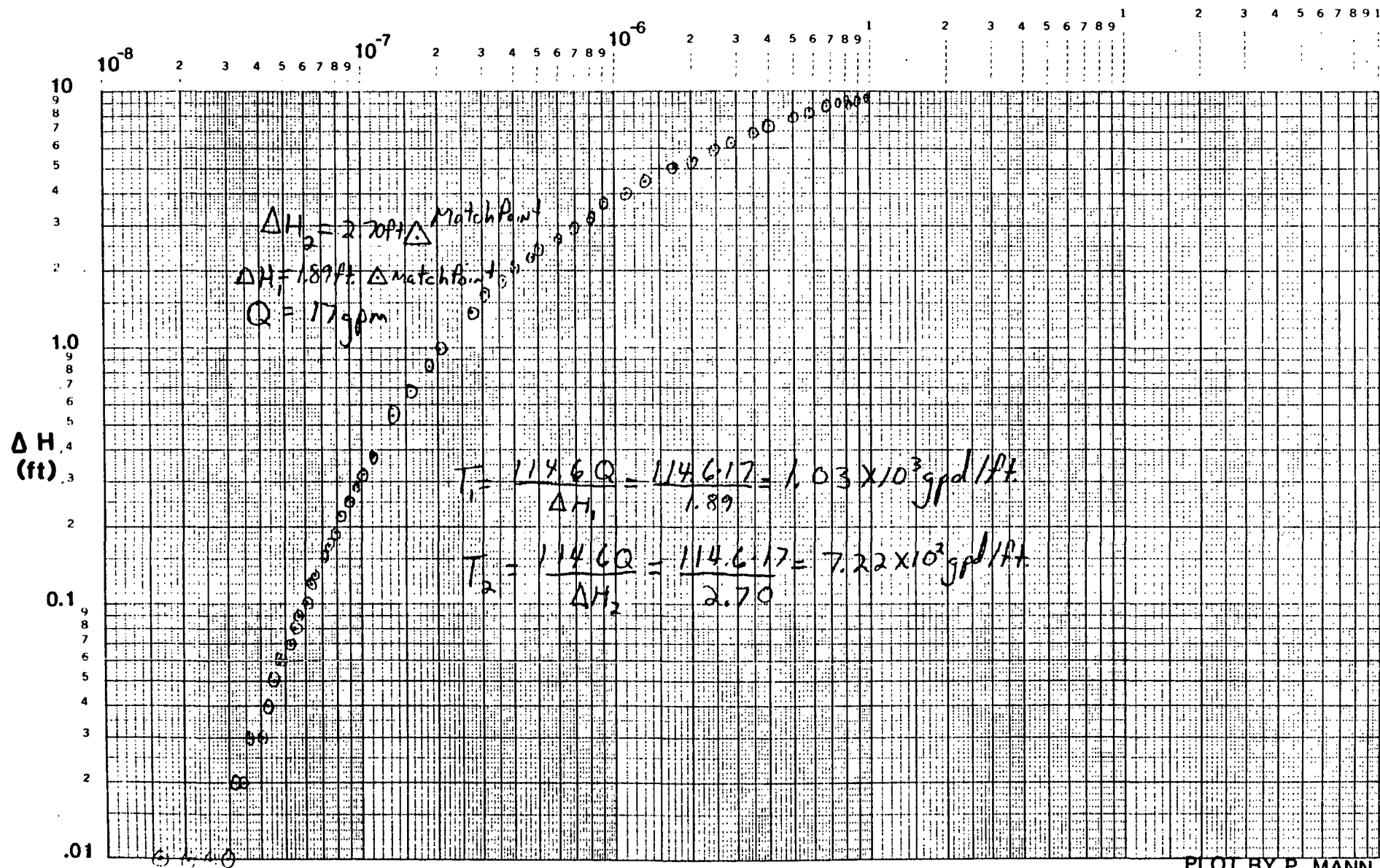
**ERT**



REI 10-1 RUN #2 PUMP TEST - DRAWDOWN

LOG-LOG PLOT OF REI 3-4

10/7/86



PLOT BY P. MANN

$t/r^2$  (days/feet<sup>2</sup>)

# CALCULATIONS AND COMPUTATIONS

SHEET 2 OF

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc for REI 3-4

COMPUTED BY: DEG DATE: 11-13-23

CHECKED BY: AM DATE: 11-14-23

## Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

$$\text{where } W(u) = 1$$

$$Q = 17 \text{ gpm}$$

$$\Delta H_1 = 1.89 \text{ ft.}$$

$$T_1 = \frac{(114.6)(17)}{1.89} =$$

$$1.03 \times 10^3 \text{ cpd/ft.}$$

$$\Delta H_2 = 2.70 \text{ ft.}$$

$$T_2 = \frac{(114.6)(17)}{2.70} =$$

$$7.22 \times 10^2 \text{ cpd/ft.}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} =$$

$$1.48 \times 10^{-4} \text{ m}^2/\text{s}$$

$$1.04 \times 10^{-4} \text{ m}^2/\text{s}$$

## Log-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

$$\text{where } u = 1$$

$$\left( \frac{t}{r^2} \right)_1 = 1.17 \times 10^{-7} \text{ days/ft}^2$$

$$T_1 = 1.03 \times 10^3 \text{ cpd/ft.}$$

$$S_1 = \frac{(1)(1.03 \times 10^3)(1.17 \times 10^{-7})}{1.87} =$$

$$6.44 \times 10^{-5}$$

$$\left( \frac{t}{r^2} \right)_2 = 1.70 \times 10^{-7} \text{ days/ft}^2$$

$$T_2 = 7.22 \times 10^2 \text{ cpd/ft.}$$

$$S_2 = \frac{(1)(7.22 \times 10^2)(1.70 \times 10^{-7})}{1.87} =$$

$$6.56 \times 10^{-5}$$

**REI**

# CALCULATIONS AND COMPUTATIONS

DD 11/19/56

SHEET 3 OF

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc. for REI 3-4

COMPUTED BY: DRG DATE: 11-18-56

CHECKED BY: DD DATE: 11/19/56

Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \text{ where } b \text{ is the screened thickness in feet.}$$

$$T_1 = 1.03 \times 10^3 \text{ cfd/ft.}$$

$$b = 23.0 \text{ ft.}$$

$$K_1 = \frac{1.03 \times 10^3}{23.0} = 4.48 \times 10^1 \text{ cfd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 2.11 \times 10^{-2} \text{ cm/s}$$

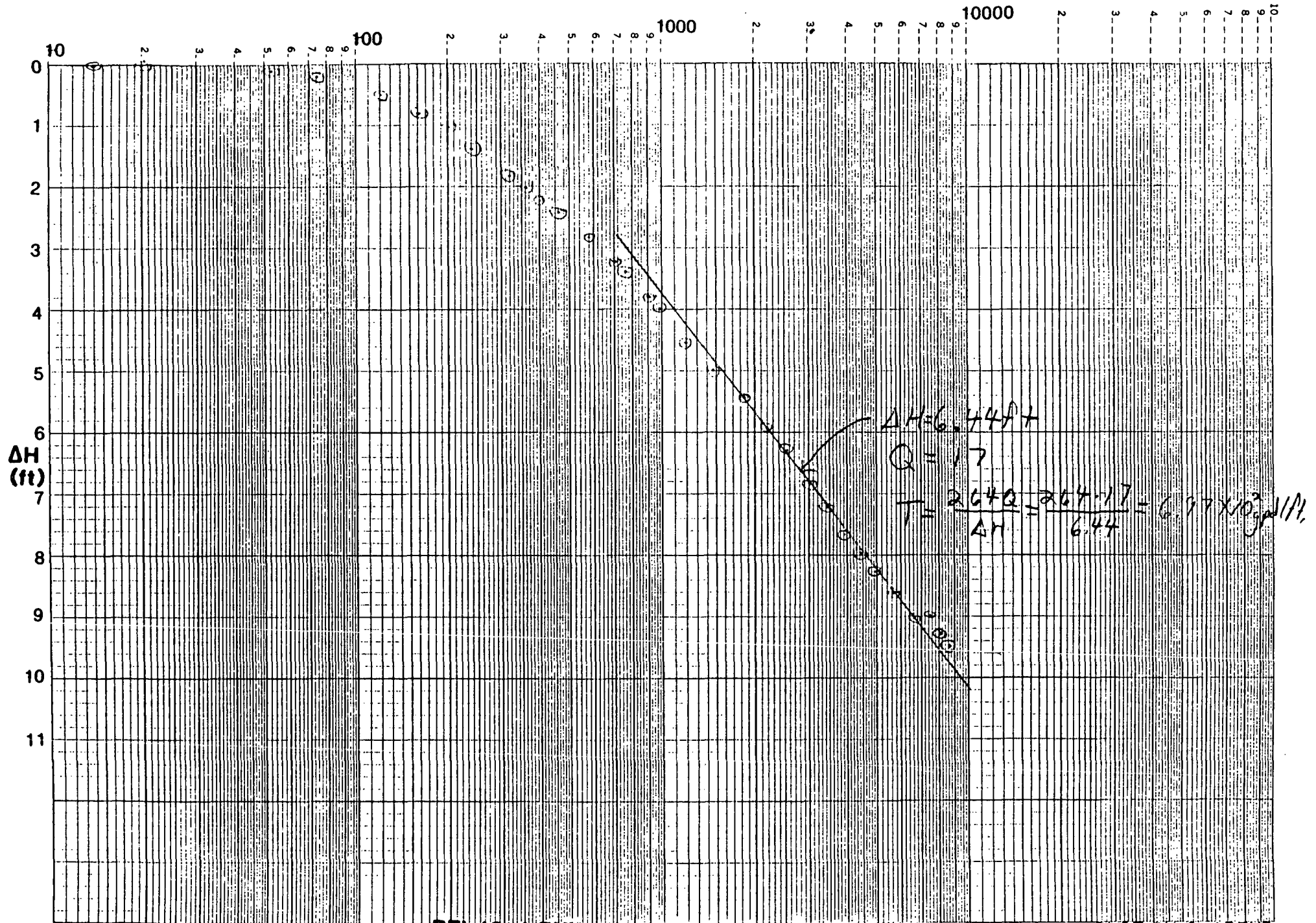
$$T_2 = 7.22 \times 10^2 \text{ cfd/ft.}$$

$$b = 23.0 \text{ ft.}$$

$$K_2 = \frac{7.22 \times 10^2}{23.0} = 3.14 \times 10^1 \text{ cfd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 1.48 \times 10^{-2} \text{ cm/s}$$

**REI**



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc. for REI 3-4

COMPUTED BY: DRG DATE: 11/14/85

CHECKED BY: DT DATE: 11-19-85

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H = 6.44 \text{ ft.}$$

$$T = \frac{264(17)}{6.44} = \boxed{6.97 \times 10^2 \text{ gpd/ft}}$$

$$\times \text{ Conversion Factor } 1.428 \times 10^{-7} = \boxed{1.00 \times 10^{-4} \text{ m}^2/\text{s}}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.3 T t_0}{r^2}$$

$$r = 784.360 \text{ ft.}$$

$$t_0 = 265 \text{ min.} / 1440 = 1.84 \times 10^{-1} \text{ days}$$

$$T = \boxed{6.97 \times 10^2 \text{ gpd/ft.}}$$

$$S = \frac{(0.3)(6.97 \times 10^2)(1.84 \times 10^{-1})}{(784.360)^2} = \boxed{6.26 \times 10^{-5}}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \text{ where } b \text{ is the screened thickness in feet.}$$

$$T = \boxed{6.97 \times 10^2 \text{ gpd/ft.}}$$

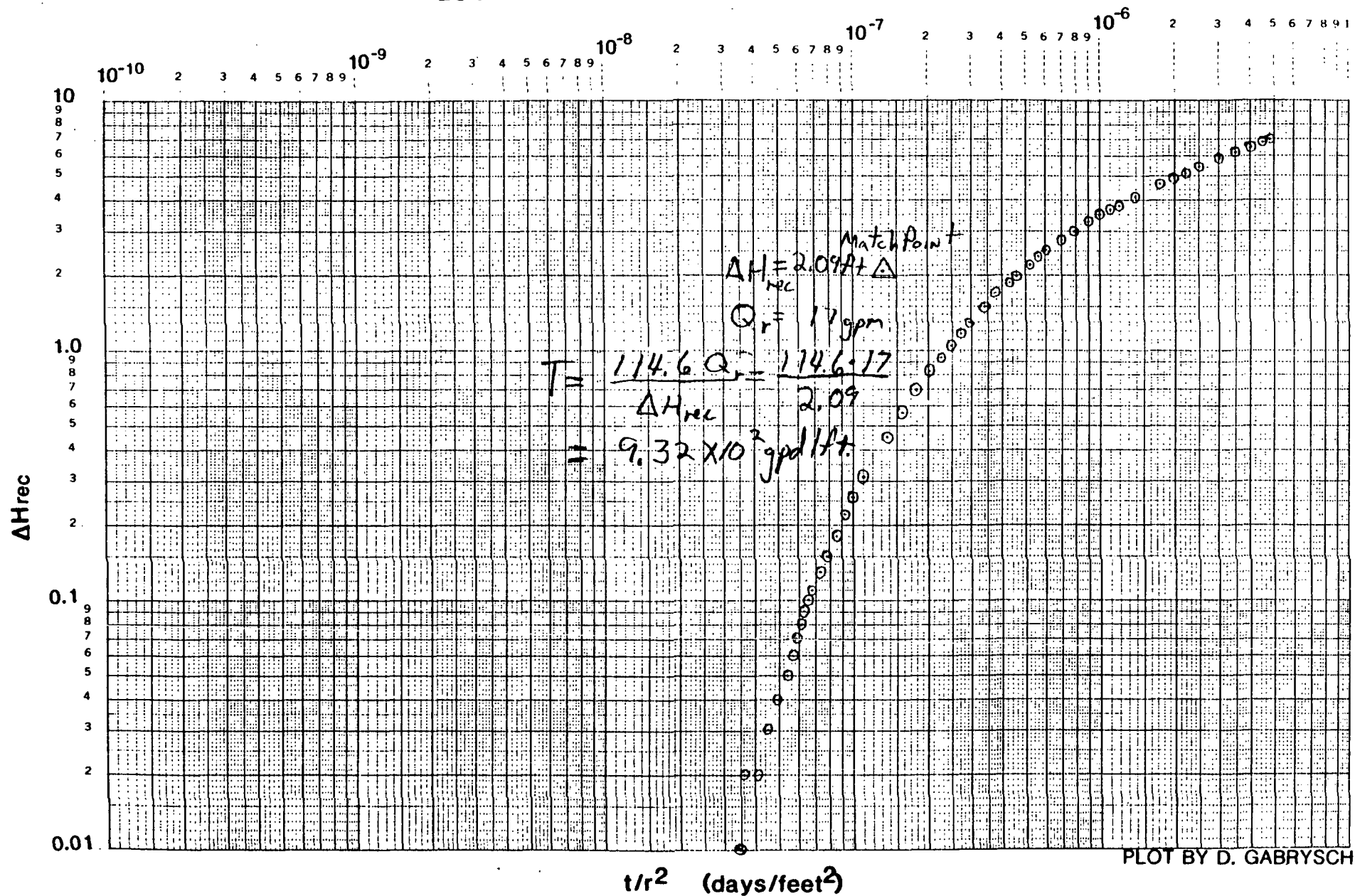
$$b = 23.0 \text{ ft.}$$

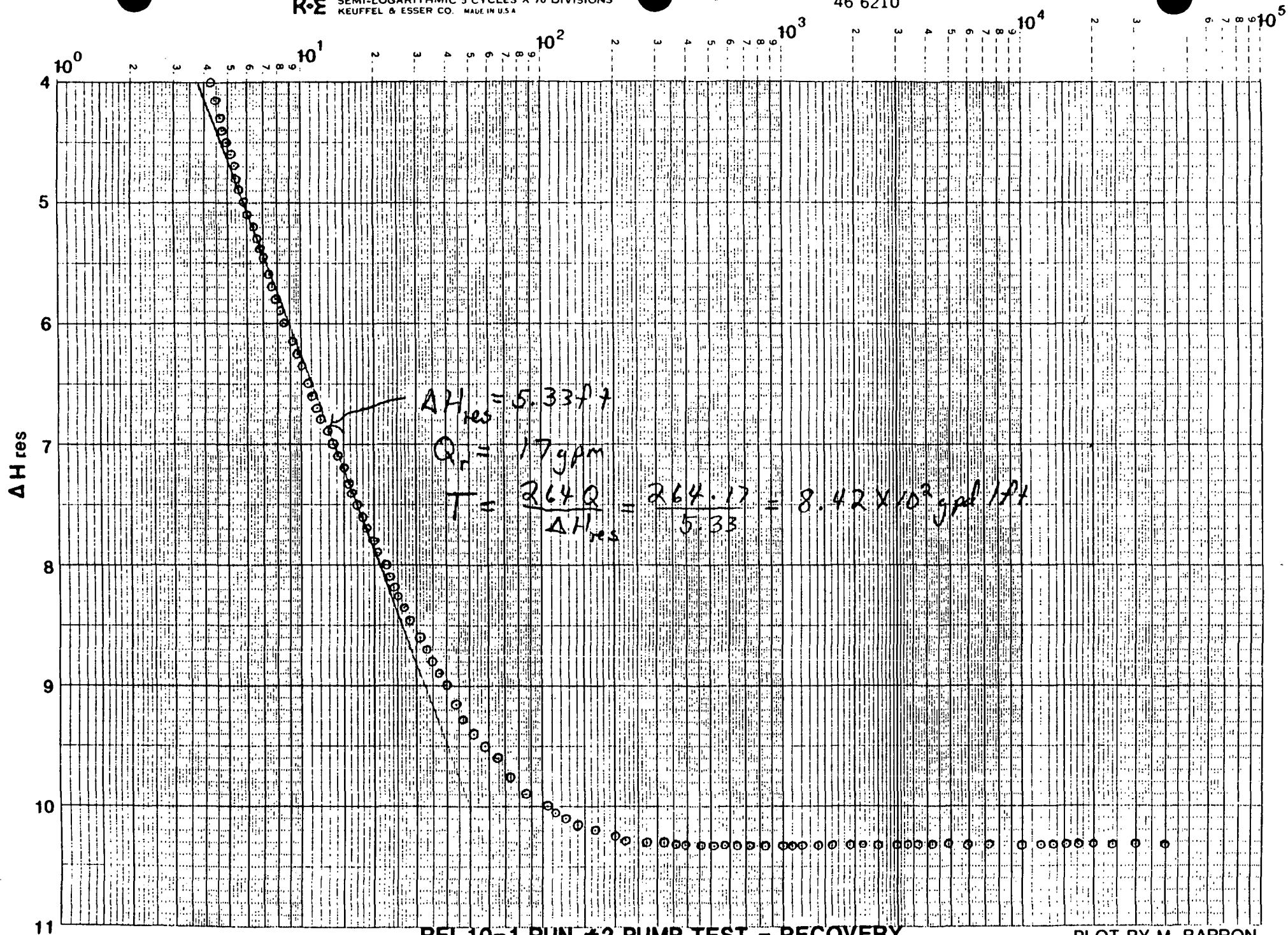
$$K = \frac{6.97 \times 10^2}{23.0} = \boxed{3.03 \times 10^1 \text{ gpd/ft}^2}$$

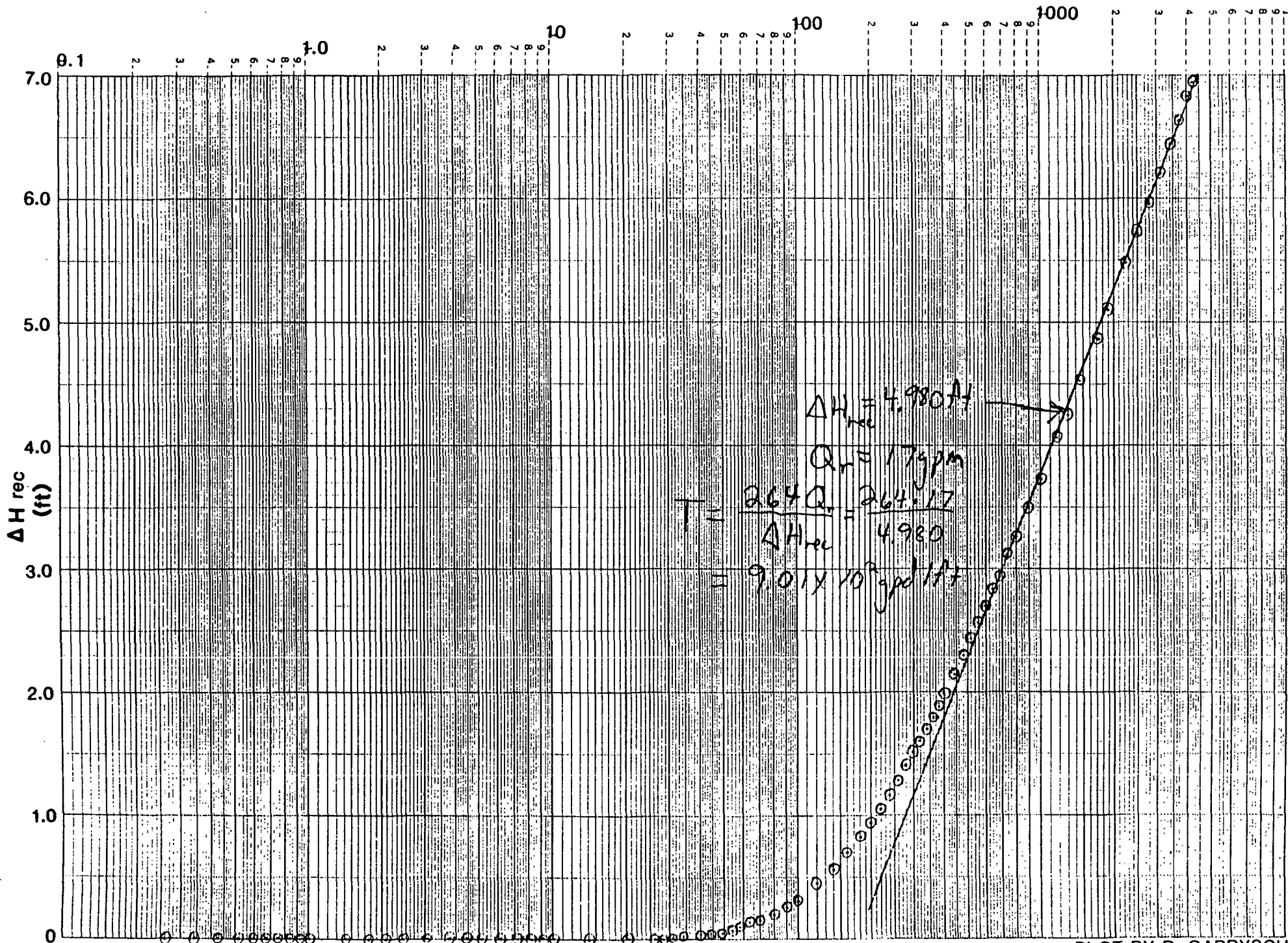
$$\times \text{ Conversion Factor } 4.716 \times 10^{-5} = \boxed{1.43 \times 10^{-3} \text{ cm/s}}$$

**REI**

REI 10-1 RUN #2 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF REI 3-4 10/14/86









# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: EPF 110-1 LTD.

JOB NO.: 275-14

SUBJECT: PEI 10-1 Run #2 Calc for PEI 3-4

COMPUTED BY: DPG DATE: 11-19-86

CHECKED BY: DD DATE: 11-19-86

## Log-Log solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$\Delta H = 2.09 \text{ ft}$$

$$Q = 17 \text{ gpm}$$

$$T = \frac{(114.6)(17)}{2.09}$$

$$= 9.32 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7} = 1.34 \times 10^{-4} \text{ m}^2/\text{s}$$

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 9.32 \times 10^2 \text{ gpd/ft}$$

$$b = 23.0 \text{ ft}$$

$$K = \frac{9.32 \times 10^2}{23.0}$$

$$= 4.05 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-2} = 1.91 \times 10^{-2} \text{ cm/s}$$

## Semi-Log (u) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H_{res}}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H_{res} = 5.33 \text{ ft}$$

$$T = \frac{(264)(17)}{5.33}$$

$$= 8.42 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7} = 1.21 \times 10^{-4} \text{ m}^2/\text{s}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_ OF \_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-1 Run = 2 Calc. for REI 3-4

COMPUTED BY: DLG DATE: 11-19-88

CHECKED BY: DD DATE: 11-19-88

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = \boxed{8.42 \times 10^2 \text{ gpd/ft}}$$

$$b = 23.0 \text{ ft}$$

$$K = \frac{8.42 \times 10^2}{23.0} = \boxed{3.66 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = \boxed{1.73 \times 10^{-3} \text{ cm/s}}$$

## Semi-Log (b) solution for Transmissivity - Recovery

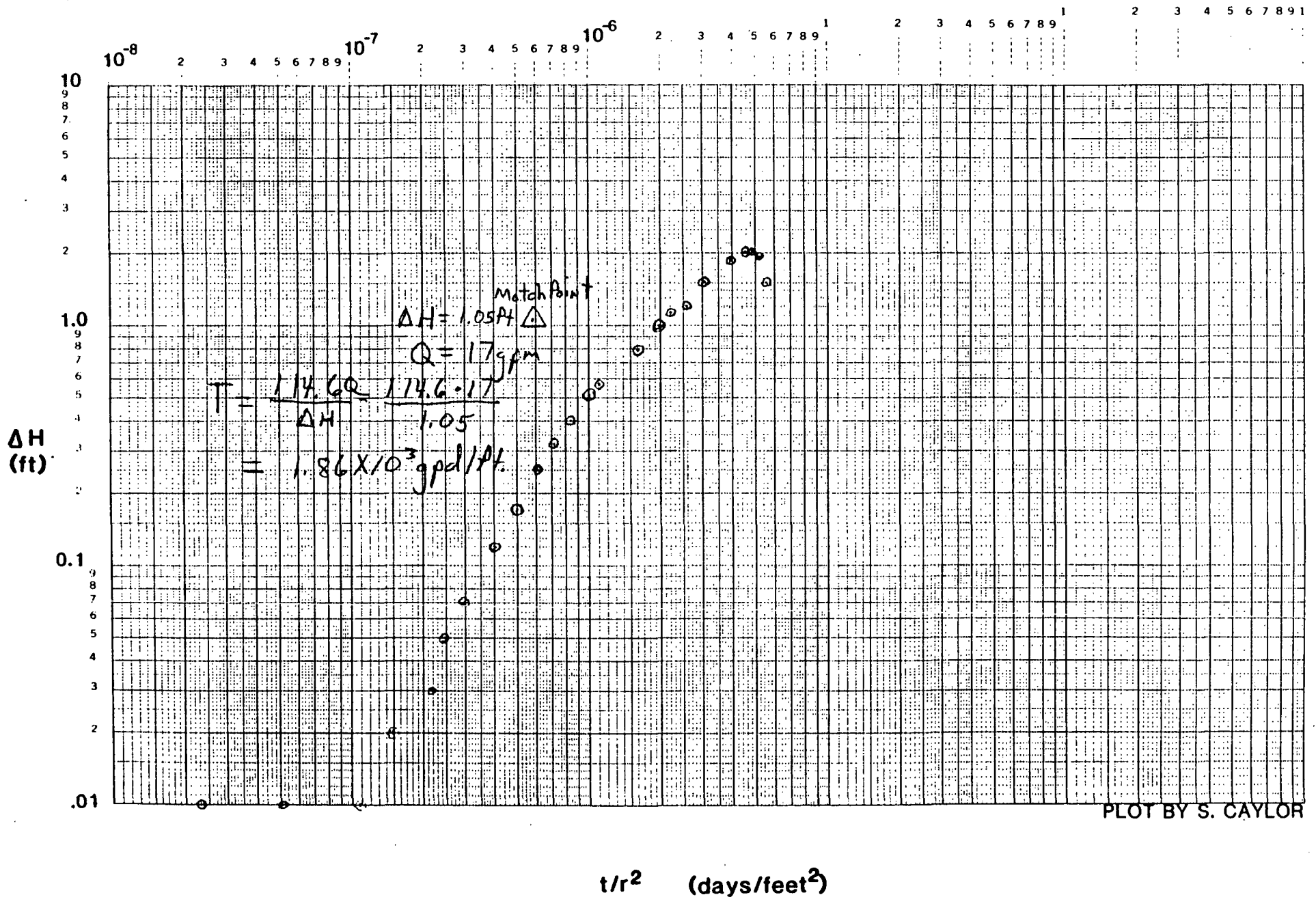
$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H_{rec}}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H_{rec} = 4.920 \text{ ft} \quad T = \frac{(264)(17)}{4.920} = \boxed{9.01 \times 10^2 \text{ gpd/ft}}$$

$$\times \text{ Conversion Factor } 1.432 \times 10^{-7} = \boxed{1.30 \times 10^{-4} \text{ m/s}}$$

REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI 7 10/7/86



# CALCULATIONS AND COMPUTATIONS

SHEET 4 OF       

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-2 Run #2 Calc. for REI 7

COMPUTED BY: DRG DATE: 11-12-20

CHECKED BY: DD DATE: 11-12-20

## Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$\Delta H = 1.05 \text{ ft.}$

$Q = 17 \text{ gpm}$

$$T = \frac{(114.6)(17)}{1.05} =$$

$1.86 \times 10^3 \text{ cfd/ft}$

X Conversion Factor  $1.438 \times 10^{-7} =$

$2.67 \times 10^{-4} \text{ m}^2/\text{s}$

## Log-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$t/r^2 = 5.80 \times 10^{-7} \text{ days/ft}^2$

$T =$   $1.86 \times 10^3 \text{ cfd/ft.}$

$$S = \frac{(1)(1.86 \times 10^3)(5.80 \times 10^{-7})}{1.87} =$$

$5.77 \times 10^{-4}$

## Solutions for Hydraulic Conductivity (K)

$K = \frac{T}{b}$  where  $b$  is the screened thickness in feet.

$T =$   $1.86 \times 10^3 \text{ cfd/ft.}$

$b = 15.0 \text{ ft.}$

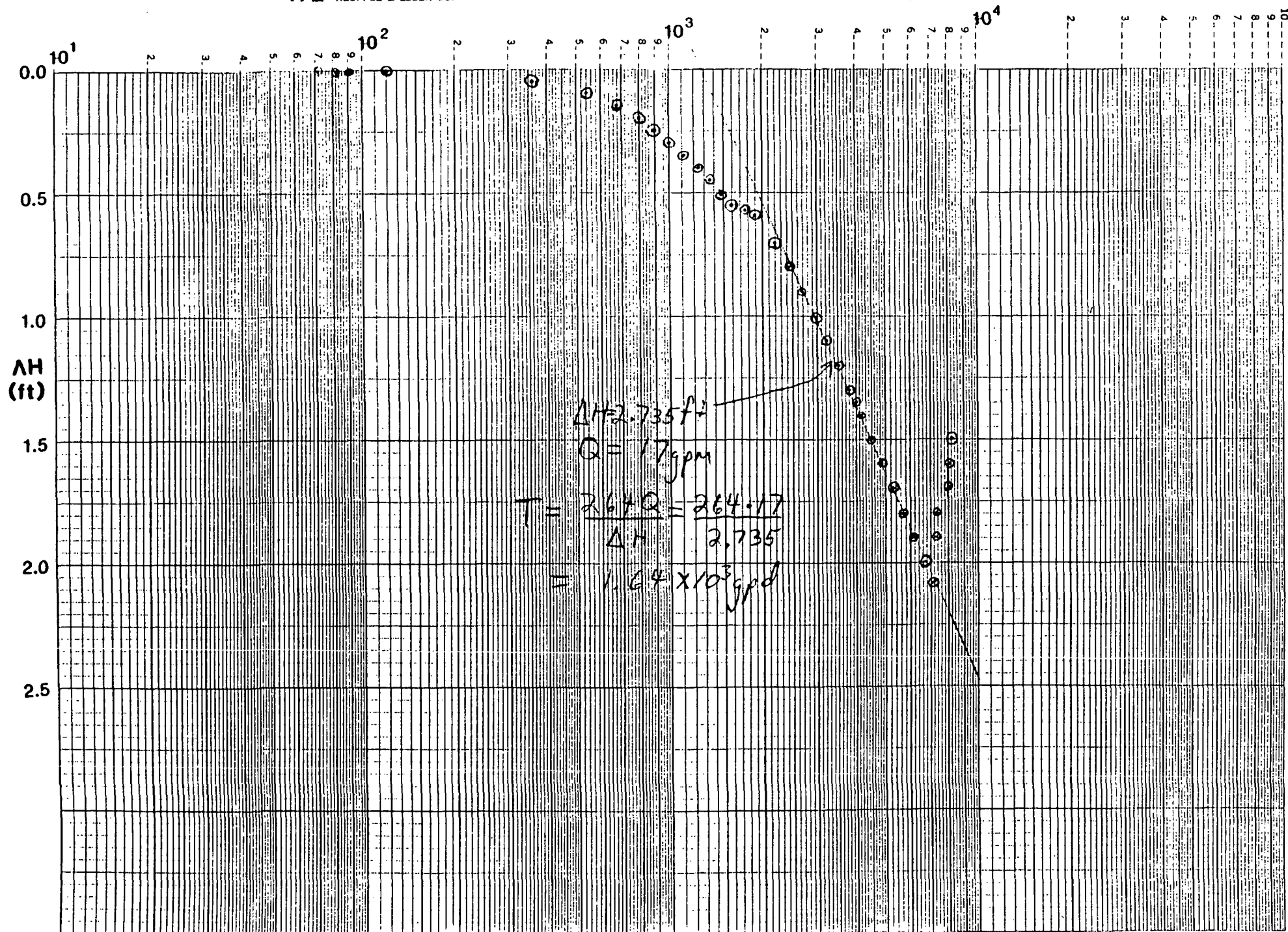
$$K = \frac{1.86 \times 10^3}{15.0} =$$

$1.24 \times 10^2 \text{ cfd/ft}^2$

X Conversion Factor  $4.715 \times 10^{-5} =$

$5.85 \times 10^{-3} \text{ cm/s}$

**REI**



REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI-7  
10/7/86

PLOT BY S. CAYLOR

# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc. for REI 7

COMPUTED BY: DRG DATE: 11/14/86

CHECKED BY: DD DATE: 11-15-86

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H = 2.735 \text{ ft.}$$

$$T = \frac{264(17)}{2.735} = 1.64 \times 10^3 \text{ gpd/ft.}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 2.36 \times 10^{-4} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.3 T t_0}{r^2}$$

$$r = 1012.704 \text{ ft.}$$

$$t_0 = 1275 \text{ min.} / 1440 = 8.85 \times 10^{-1} \text{ days}$$

$$T = 1.64 \times 10^3 \text{ gpd/ft.}$$

$$S = \frac{(0.3)(1.64 \times 10^3)(8.85 \times 10^{-1})}{(1012.704)^2} = 4.25 \times 10^{-4}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 1.64 \times 10^3 \text{ gpd/ft.}$$

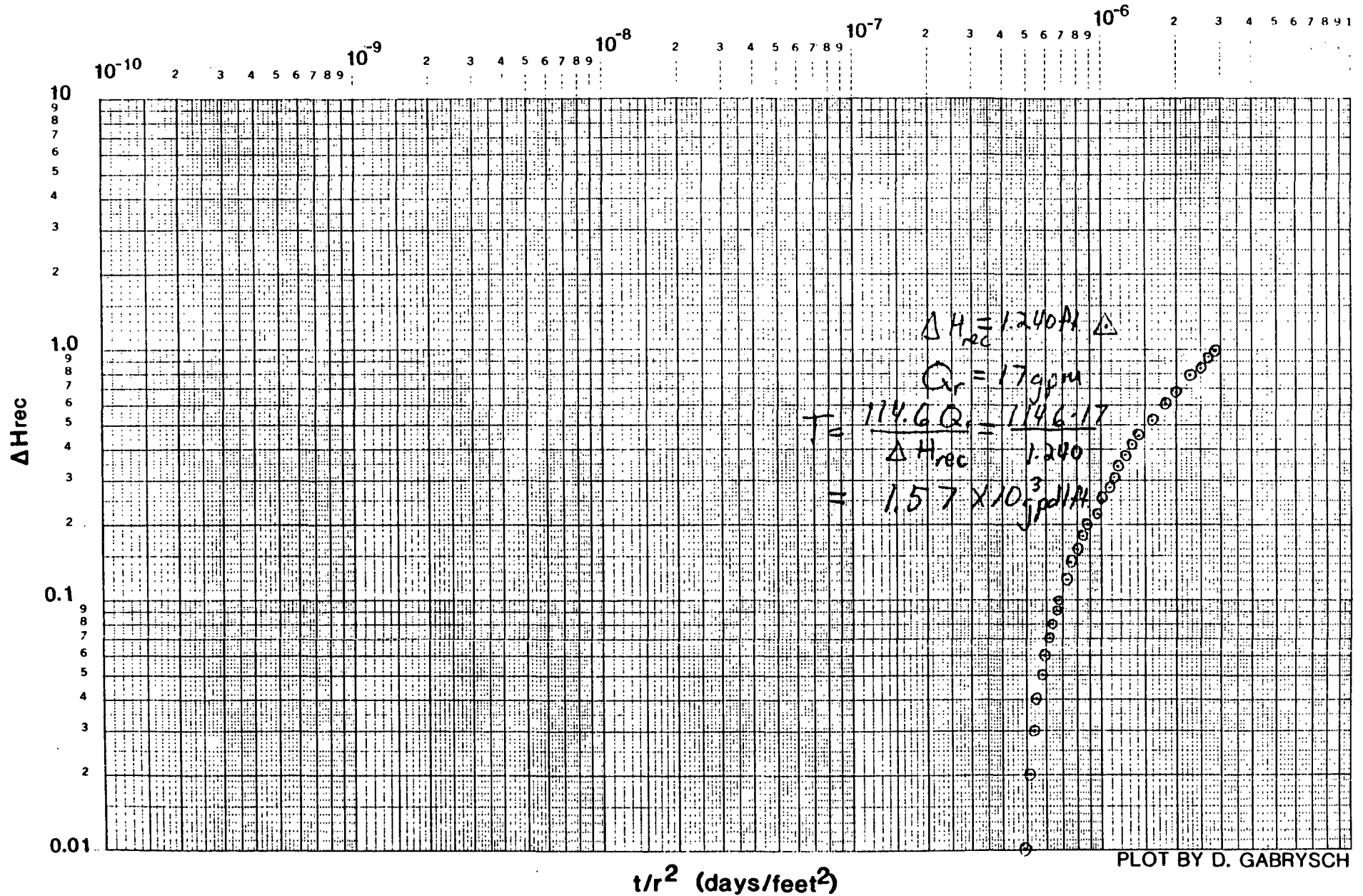
$$b = 15.0 \text{ ft.}$$

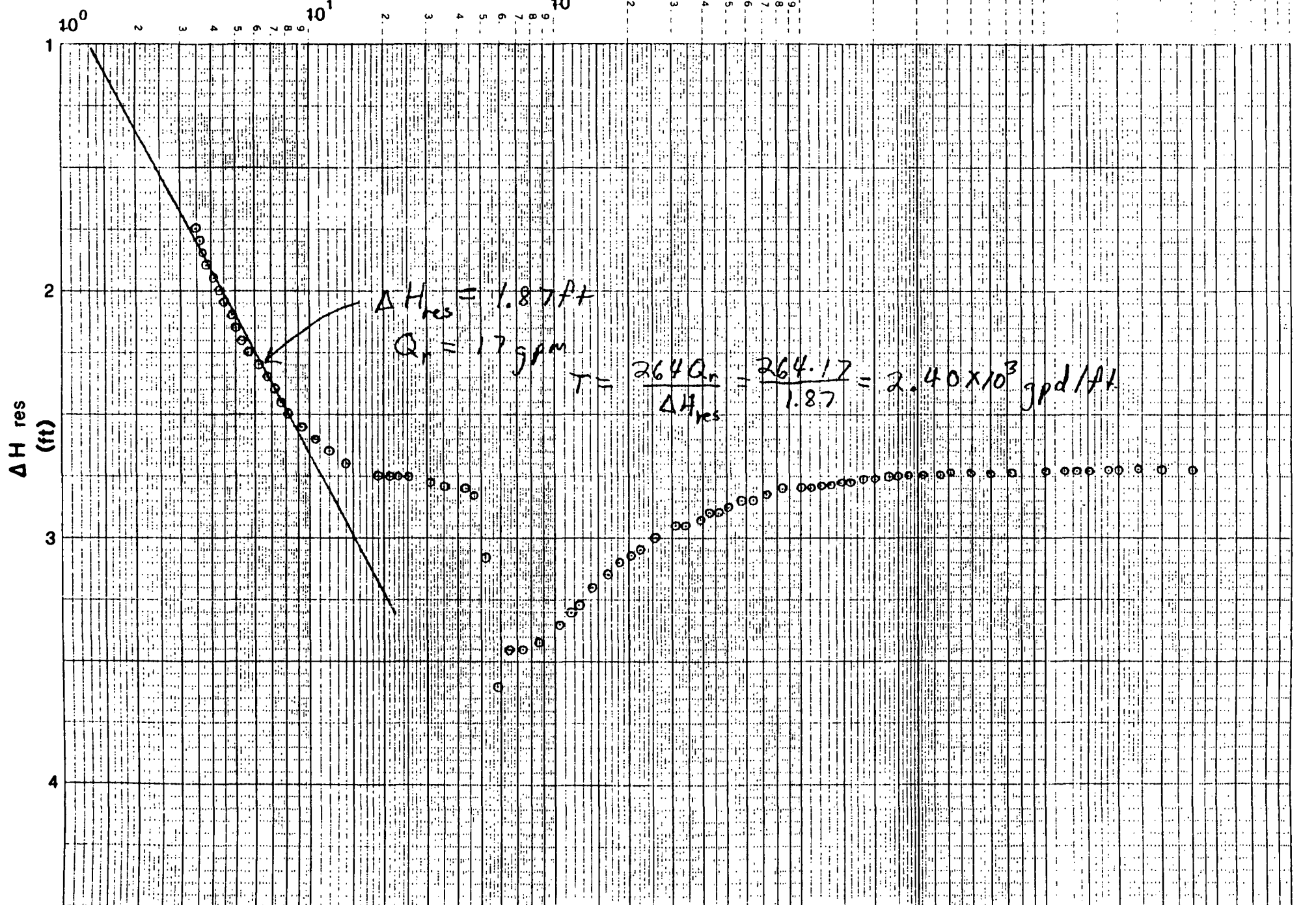
$$K = \frac{1.64 \times 10^3}{15.0} = 1.09 \times 10^2 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 5.16 \times 10^{-3} \text{ cm/s}$$

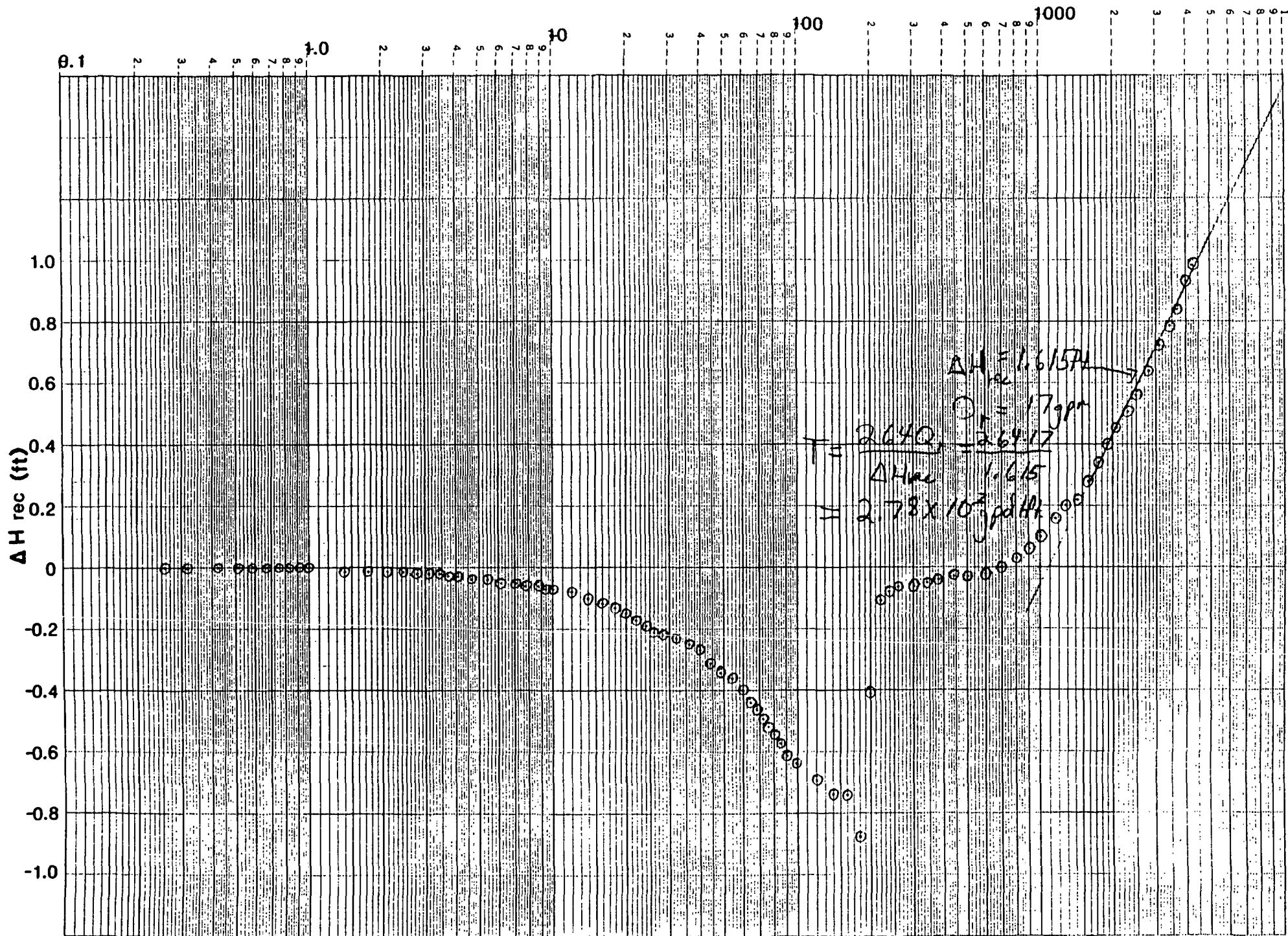
**REI**

REI 10-1 RUN #2 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF REI-7 10/14/86









# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FREIGHT LTD

JOB NO.: 274-14

SUBJECT: REI 10-1 Run #2 Calc for REI 7

COMPUTED BY: DRG DATE: 11-10-88

CHECKED BY: DD DATE: 11-18-88

## Log-Log solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$\Delta H = 1.240 \text{ ft}$$

$$Q = 17 \text{ gpm}$$

$$T = \frac{(114.6)(17)}{1.240}$$

$$= 1.57 \times 10^3 \text{ gpd/ft}$$

X Conversion Factor  $1.438 \times 10^{-7}$

$$= 2.26 \times 10^{-4} \text{ m}^2/\text{s}$$

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 1.57 \times 10^3 \text{ gpd/ft}$$

$$b = 15.0 \text{ ft}$$

$$K = \frac{1.57 \times 10^3}{15.0}$$

$$= 1.05 \times 10^2 \text{ gpd/ft}^2$$

X Conversion Factor  $4.715 \times 10^{-5}$

$$= 4.95 \times 10^{-3} \text{ cm/s}$$

## Semi-Log(a) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H_{res}}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H_{res} = 1.87 \text{ ft}$$

$$T = \frac{(264)(17)}{1.87}$$

$$2.40 \times 10^3 \text{ gpd/ft}$$

X Conversion Factor  $1.432 \times 10^{-7}$

$$= 3.45 \times 10^{-4} \text{ m}^2/\text{s}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 273-14

SUBJECT: REI 17-1 P. 10 #2 Calc for REI 7

COMPUTED BY: DRS DATE: 11-10-86

CHECKED BY: DD DATE: 11-11-86

## Solution for Hydraulic Conductivity - Recovery

$$R = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = \boxed{2.40 \times 10^3 \text{ gpd/ft}}$$

$$b = 15.0 \text{ ft}$$

$$R = \frac{2.40 \times 10^3}{15.0} = \boxed{1.60 \times 10^2 \text{ gpd/ft}^2}$$

$$Y \text{ Conversion Factor } 4.715 \times 10^{-5} = \boxed{7.54 \times 10^{-3} \text{ cm/s}}$$

## Semi-Log (b) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta h_{\text{rec}}}$$

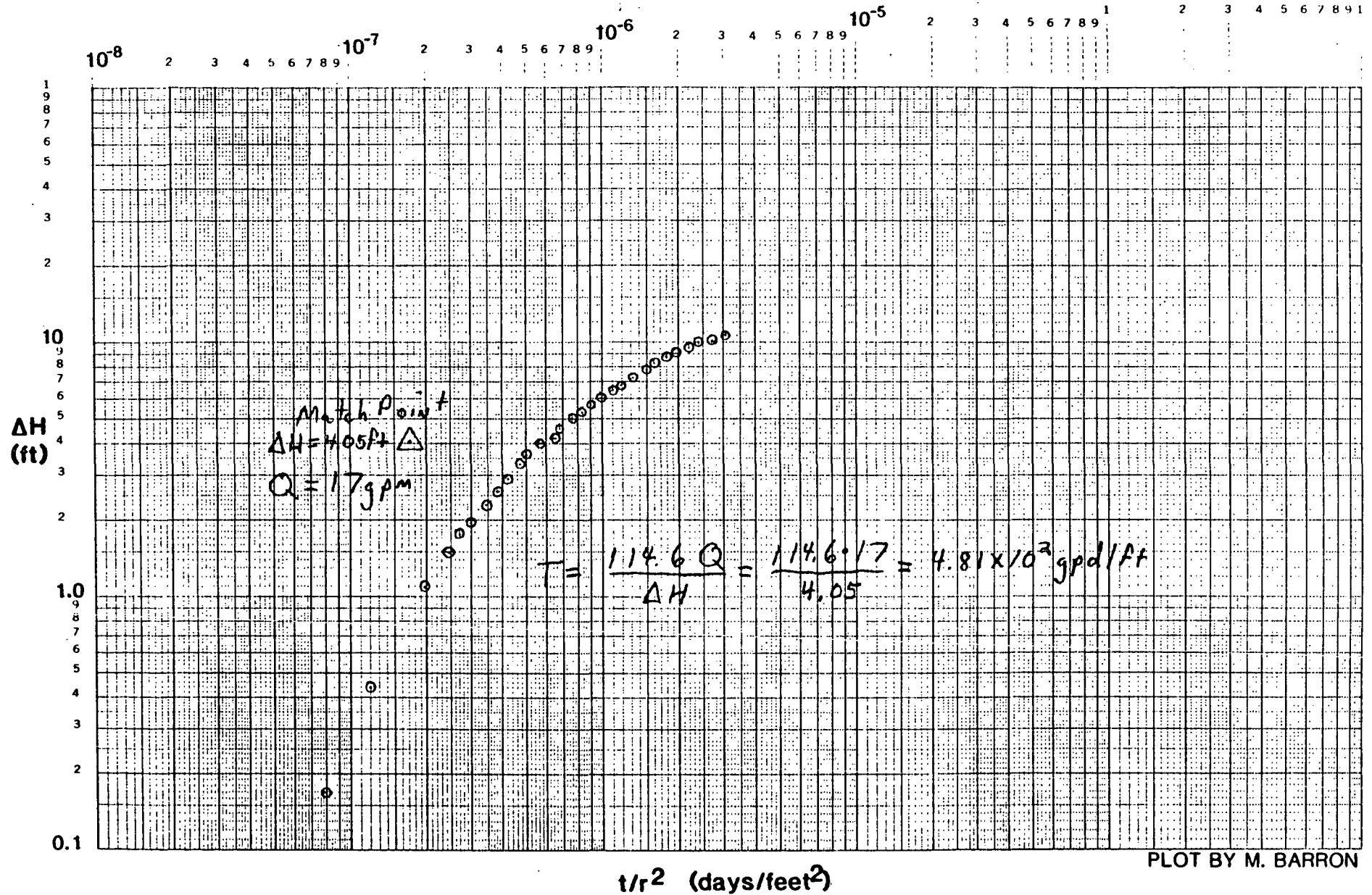
$$Q = 17 \text{ gpm}$$

$$\Delta h_{\text{rec}} = 1.615 \text{ ft} \quad T = \frac{(264)(17)}{1.615} = \boxed{2.78 \times 10^3 \text{ gpd/ft}}$$

$$X \text{ Conversion Factor } 1.432 \times 10^{-2} = \boxed{4.00 \times 10^{-6} \text{ m/s}}$$

**ERT**

REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI 12-1  
10/7/86



# CALCULATIONS AND COMPUTATIONS

SHEET 6 OF       

PROJECT: FRENCH LTD.

JOB NO.: 274-14

SUBJECT: REI 10-1 Run #2 Calc. for REI 12-1

COMPUTED BY: DRG DATE: 11/14/85

CHECKED BY: DB DATE: 11/15/85

## Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$\begin{aligned} \Delta H &= 4.05 \text{ ft.} \\ Q &= 17 \text{ gpm} \end{aligned} \quad T = \frac{(114.6)(17)}{4.05} = \boxed{4.81 \times 10^2 \text{ gpd/ft.}}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = \boxed{6.92 \times 10^{-5} \text{ m}^2/\text{s}}$$

## Log-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 1.73 \times 10^{-7} \text{ days/ft}^2$$

$$T = \boxed{4.81 \times 10^2 \text{ gpd/ft.}}$$

$$S = \frac{(1)(4.81 \times 10^2)(1.73 \times 10^{-7})}{1.87} = \boxed{4.45 \times 10^{-5}}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

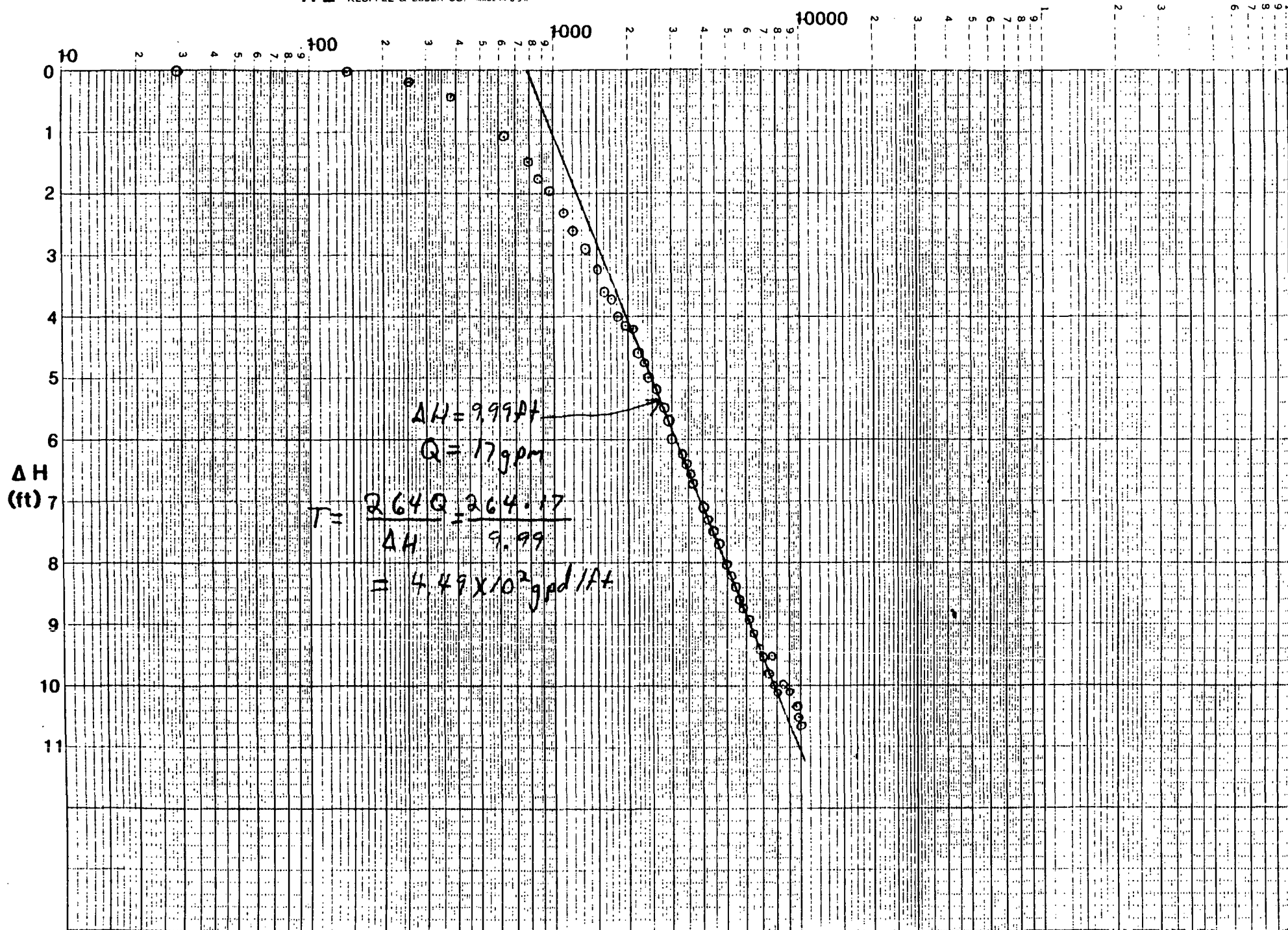
$$T = \boxed{4.81 \times 10^2 \text{ gpd/ft}}$$

$$b = 36.75 \text{ ft.}$$

$$K = \frac{4.81 \times 10^2}{36.75} = \boxed{1.31 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = \boxed{6.17 \times 10^{-4} \text{ cm/s}}$$

**REI**



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 10-1 Run #2 Calc. for REI 12-1

COMPUTED BY: DRG DATE: 11-19-86

CHECKED BY: DD DATE: 11-19-86

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H}$$

$$Q = 17 \text{ gpm}$$

$$\Delta H = 9.99 \text{ ft.}$$

$$T = \frac{264(17)}{9.99}$$

$$4.49 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7}$$

$$6.46 \times 10^{-5} \text{ m/s}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.3 T t_c}{r^2}$$

$$r = 1492.112 \text{ ft}$$

$$t_c = 780 \text{ min} / 1440 = 5.42 \times 10^{-1} \text{ days}$$

$$T = 4.49 \times 10^2 \text{ gpd/ft.}$$

$$S = \frac{(0.3)(4.49 \times 10^2)(5.42 \times 10^{-1})}{(1492.112)^2}$$

$$3.28 \times 10^{-5}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 4.49 \times 10^2 \text{ gpd/ft}$$

$$b = 36.75 \text{ ft}$$

$$K = \frac{4.49 \times 10^2}{36.75}$$

$$= 1.22 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5}$$

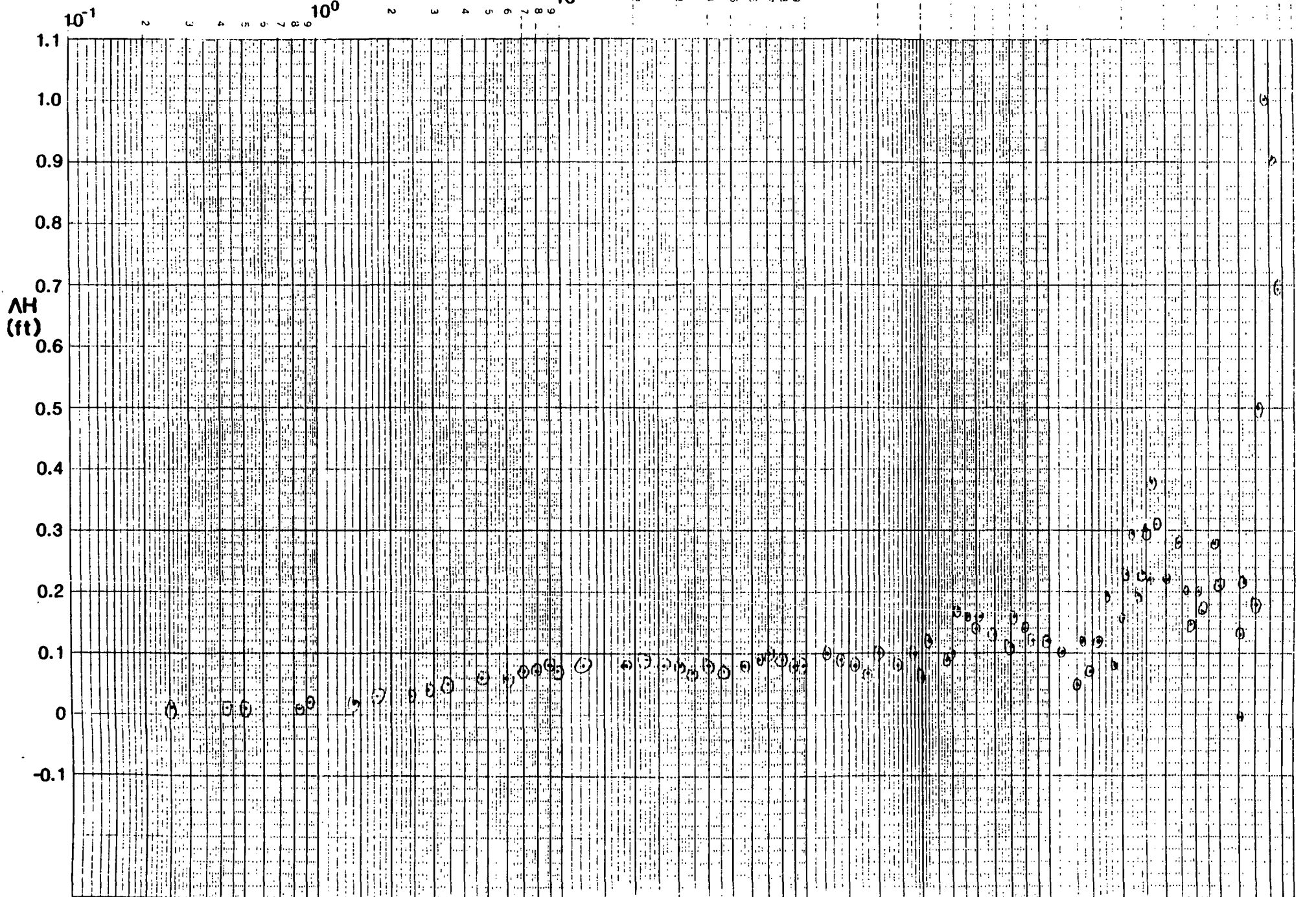
$$= 5.76 \times 10^{-4} \text{ cm/s}$$

**REI**

K·Σ SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

t(min)

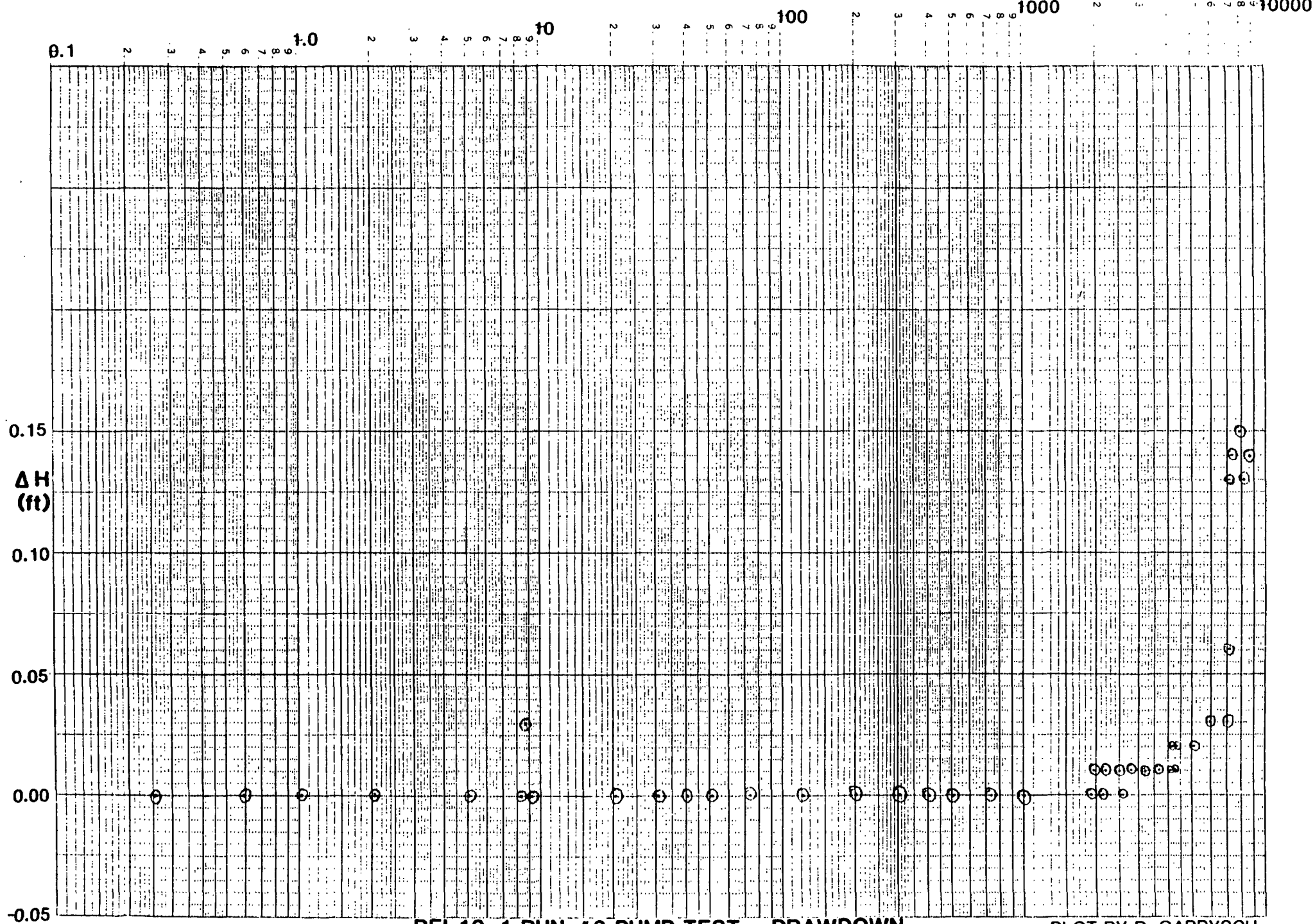
46 6210



REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF P 10-2  
10/7/86

PLOT BY T. BOCCA

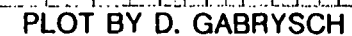


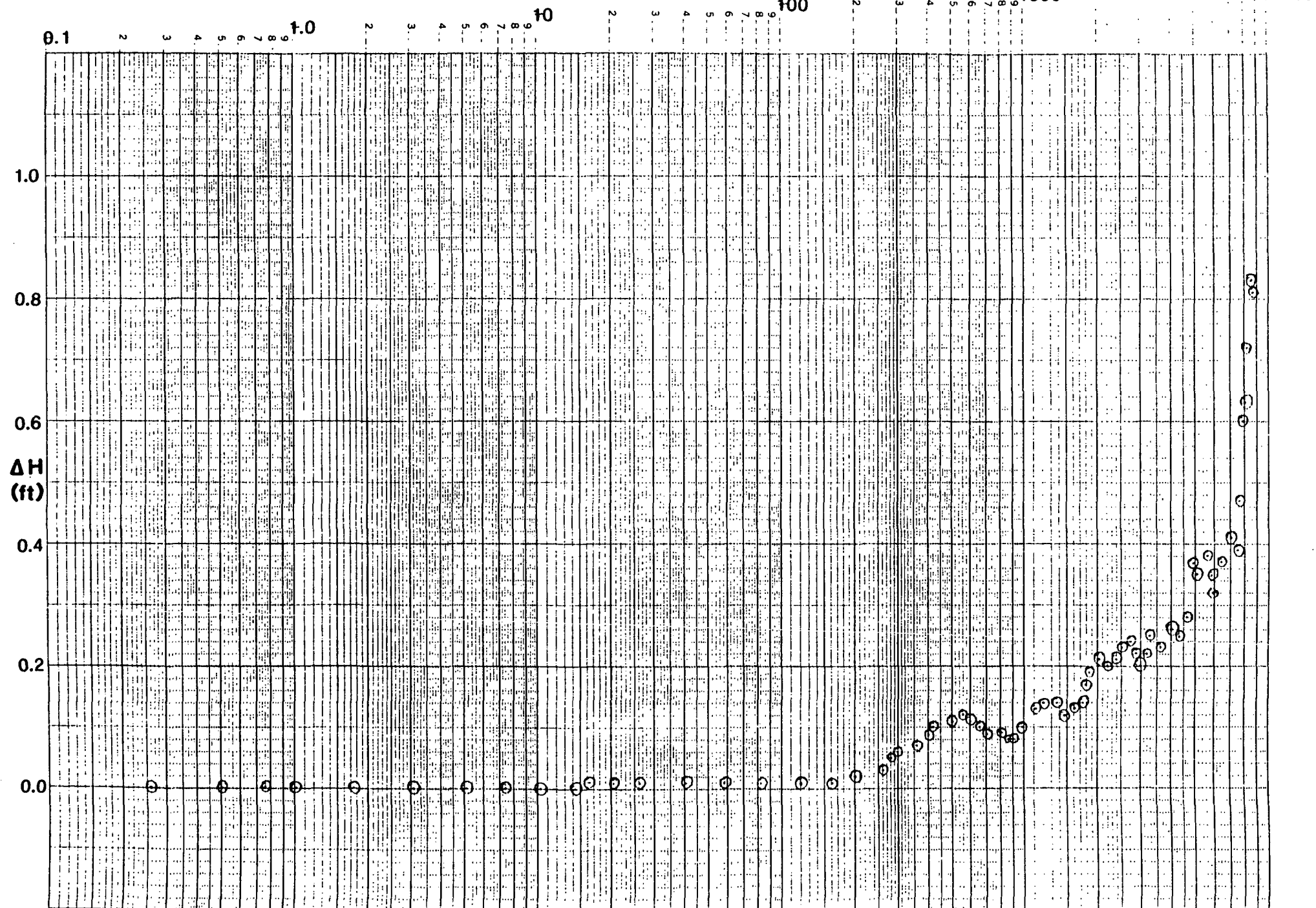


REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF P-10-3

10/7/86

PLOT BY D. GABRYSCH





REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 10-2

10/7/86

PLOT BY D. GABRYSCH

K-Σ SEMI-LOGARITHMIC 5 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.

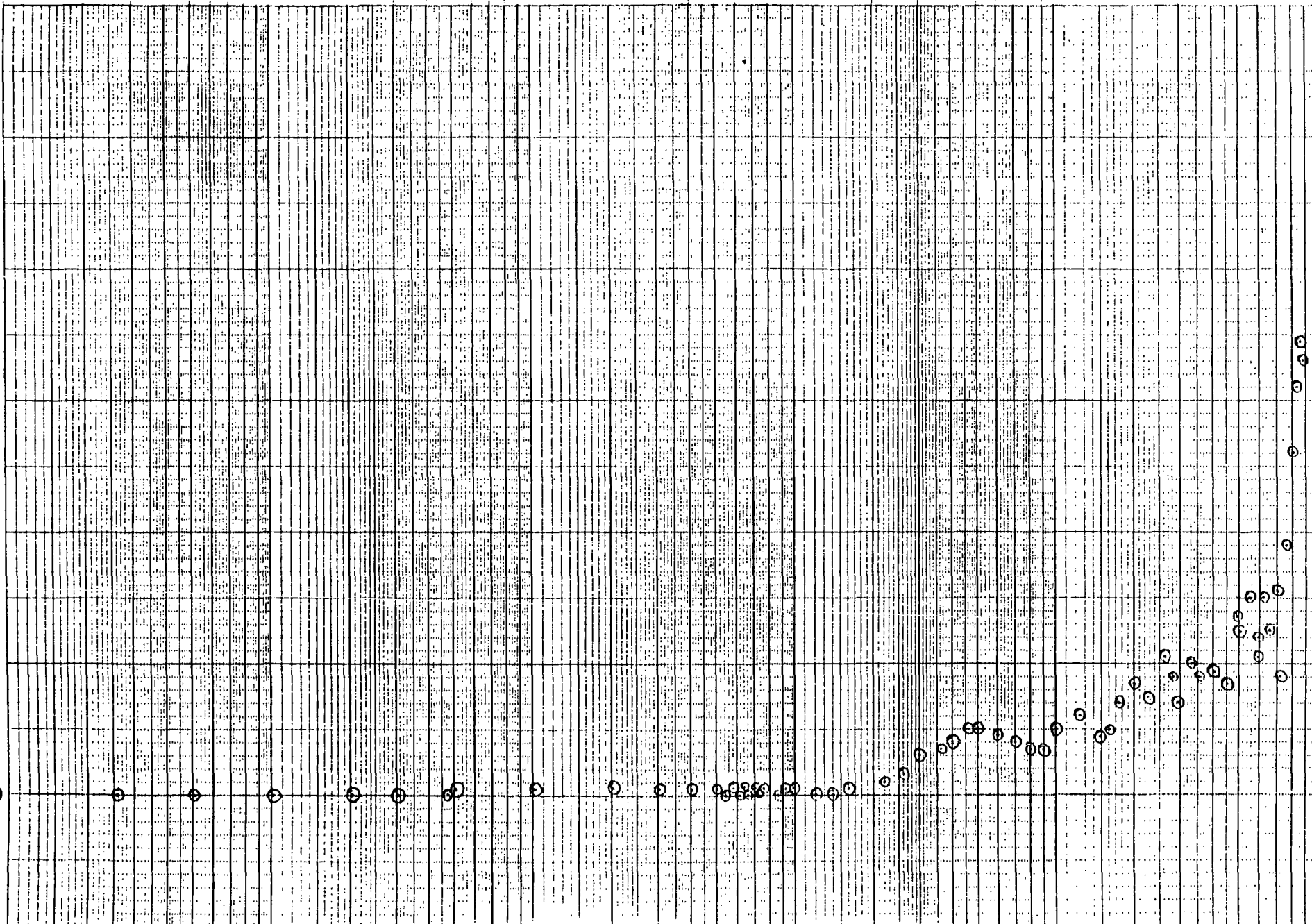
t(min)

46 6210

10<sup>-1</sup> 10<sup>0</sup> 10<sup>1</sup> 10<sup>2</sup> 10<sup>3</sup> 10<sup>4</sup>

Δh  
(ft)

1.0  
0.8  
0.6  
0.4  
0.2  
0.0



REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 10-2  
10/7/86

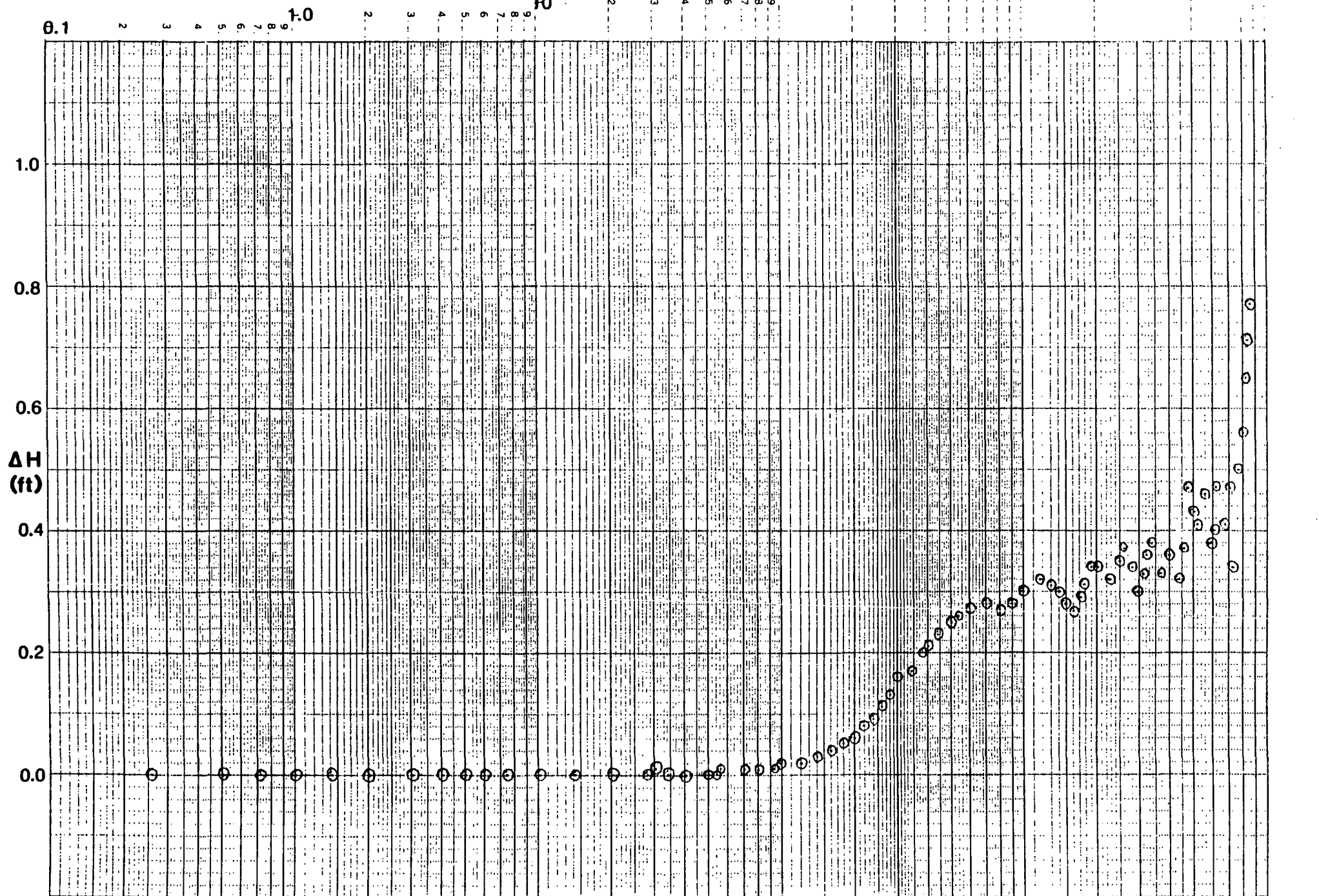
PLOT BY D. GABRYSCH

t(min)

46 6210

1000

10000



REI 10-1 RUN #2 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 10-1

PLOT BY D. GABRYSCH

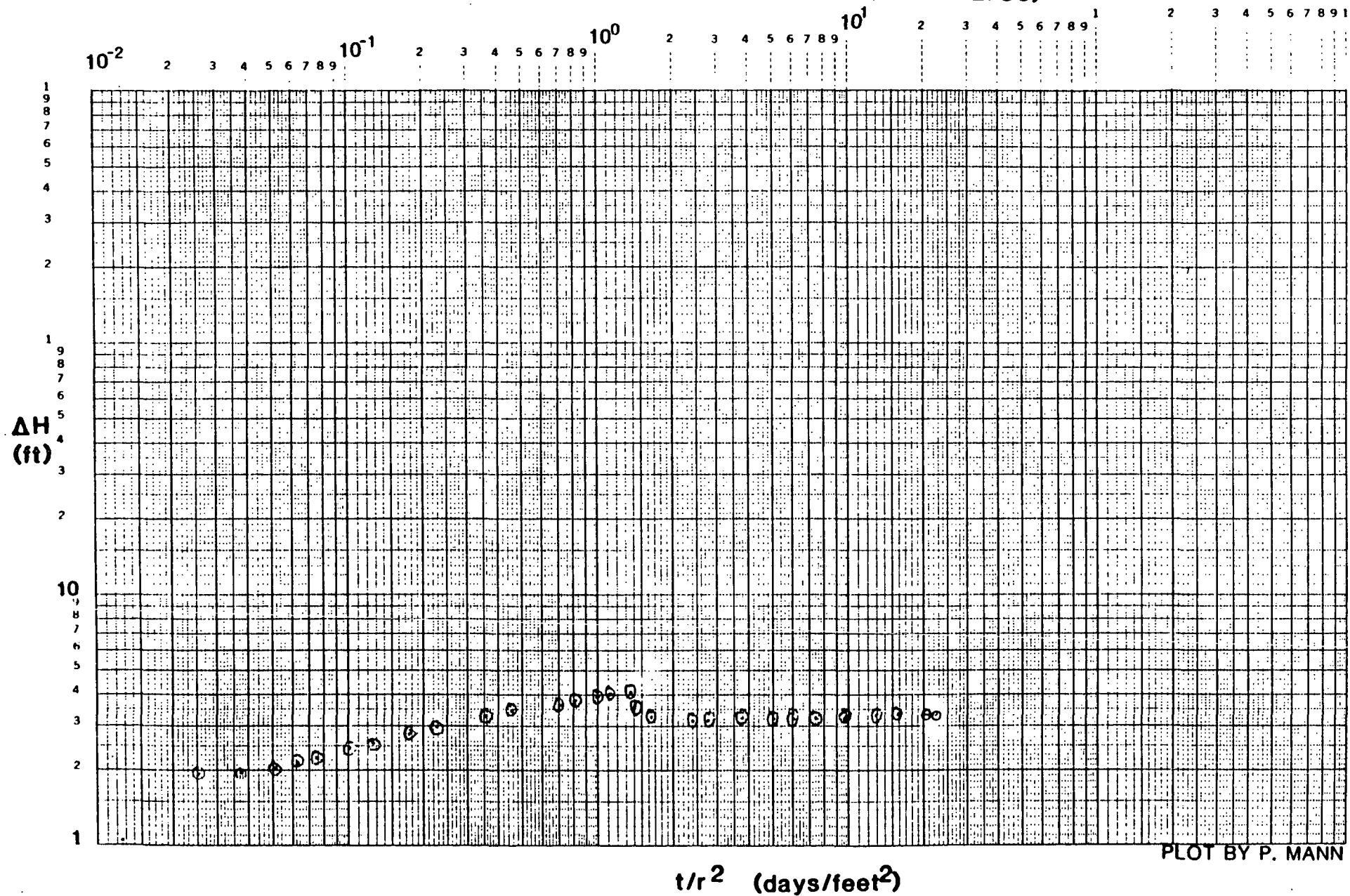
Attachment 10

REI 3-3 Pumping Test  
Response Curves and Aquifer  
Characteristics Calculations

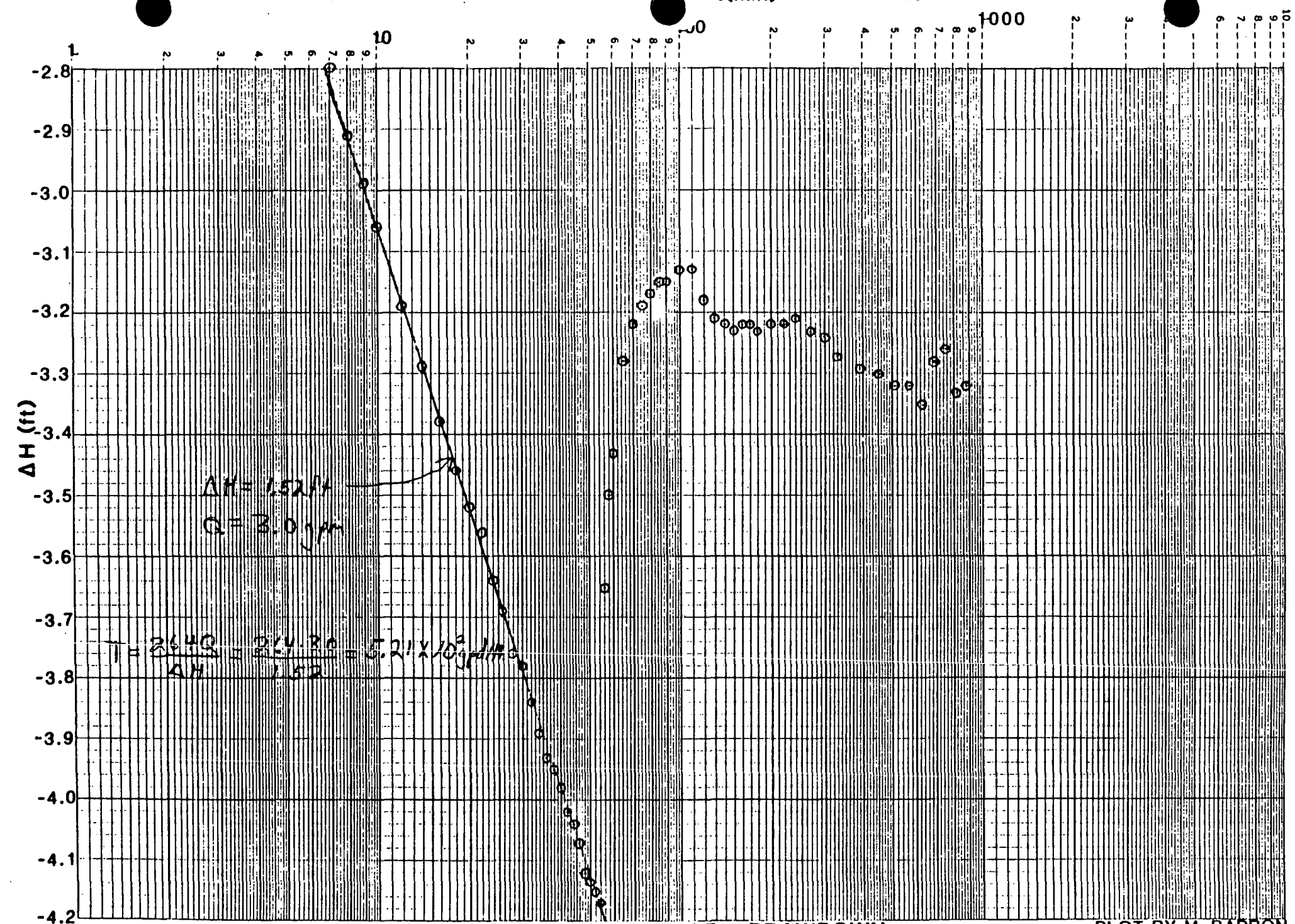


# REI 3-3 PUMP TEST - DRAWDOWN

LOG-LOG PLOT OF REI 3-3 (8/11-12/86)



PLOT BY P. MANN



REI 3-3 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 3-3 (8/11-12/86)

PLOT BY M. BARRON



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 3-3 Calc. for REI 3-3

COMPUTED BY: ERS DATE: 10/10/00

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264Q}{\Delta H}$$

$$Q = 3.0 \text{ gpm}$$

$$\Delta H = 1.52 \text{ ft} \quad T = \frac{(264)(3.0)}{1.52} = 5.21 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.432 \times 10^{-7} = 7.49 \times 10^{-5} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.3Tt_0}{r^2}$$

$$r = 0.166 \text{ ft}$$

$$t_0 = 9.3 \times 10^{-1} \text{ min} / 1440 = 6.46 \times 10^{-4} \text{ days}$$

$$T = 5.21 \times 10^2 \text{ gpd/ft}$$

$$S = \frac{(0.3)(5.21 \times 10^2)(6.46 \times 10^{-4})}{(0.166)^2} = 3.66 \times 10^0$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 5.21 \times 10^2 \text{ gpd/ft}$$

$$b = 14.0 \text{ ft}$$

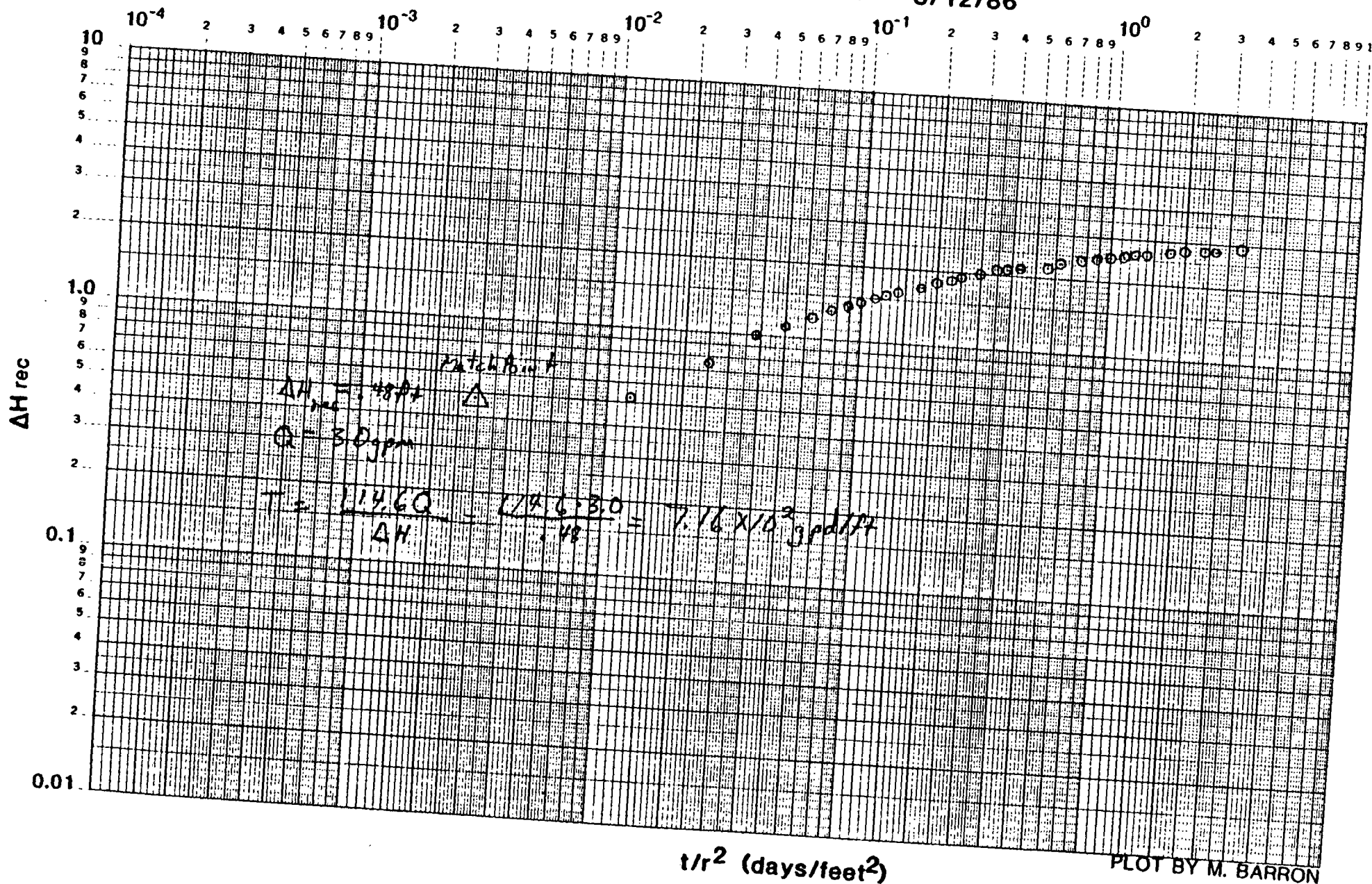
$$K = \frac{5.21 \times 10^2}{14.0} = 3.72 \times 10^1 \text{ gpd/ft}^2$$

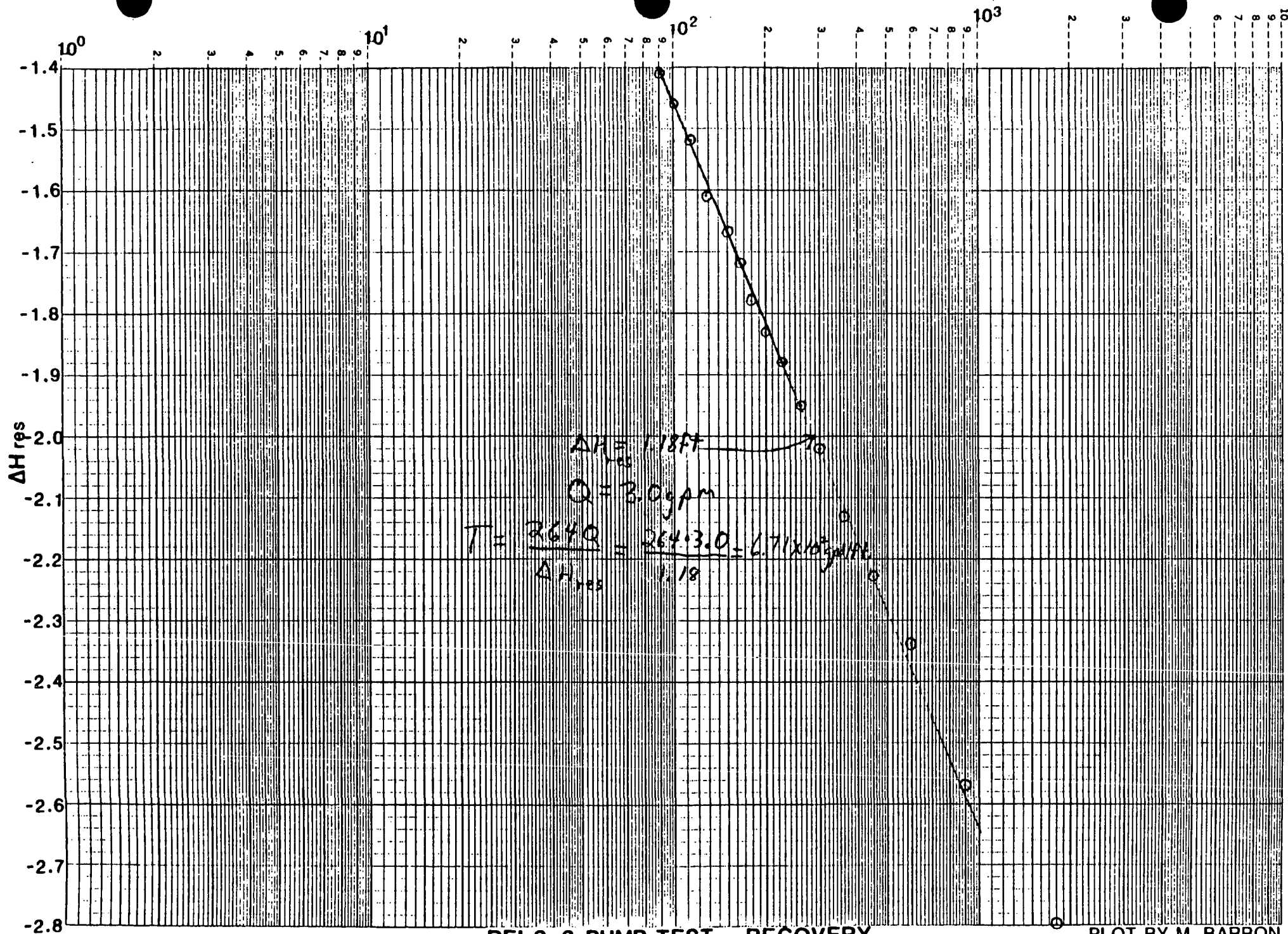
$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 1.75 \times 10^{-5} \text{ cm/s}$$

**ERT**

REI 3-3 PUMP TEST - RECOVERY

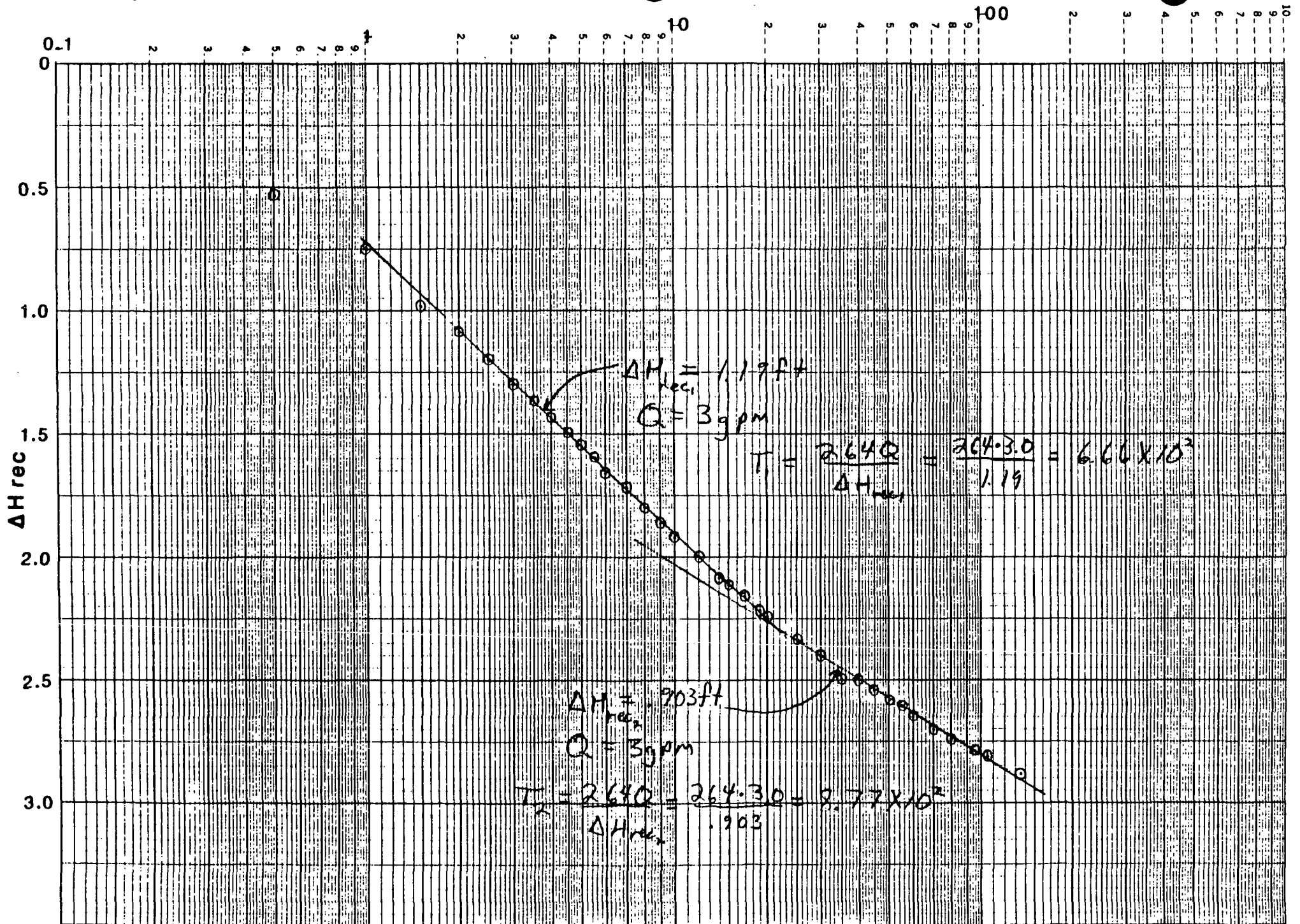
LOG-LOG PLOT OF REI 3-3 8/12/86





REI 3-3 PUMP TEST - RECOVERY  
SEMI-LOG PLOT OF REI 3-3 8/12/86

PLOT BY M. BARRON



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 225-14

SUBJECT: REI 3-3 Calc for REI 3-3

COMPUTED BY: TRK DATE: 11-2-4

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Log-Log solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{114.6QW(u)}{\Delta H}$$

where  $W(u) = 1$

$$Q = 3.0 \text{ gpm}$$

$$\Delta H = 0.48 \text{ ft}$$

$$T = \frac{(114.6)(3.0)}{0.48} = 7.16 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.432 \times 10^{-7} = 1.03 \times 10^{-4} \text{ m}^2/\text{s}$$

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 7.16 \times 10^2 \text{ gpd/ft}$$

$$b = 14.0 \text{ ft}$$

$$K = \frac{7.16 \times 10^2}{14.0} = 5.12 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 2.41 \times 10^{-3} \text{ cm/s}$$

## Semi-Log(a) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264Q}{\Delta H_{res}}$$

$$Q = 3.0 \text{ gpm}$$

$$\Delta H_{res} = 1.18 \text{ ft}$$

$$T = \frac{(264)(3.0)}{1.18} = 6.71 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.432 \times 10^{-7} = 9.65 \times 10^{-5} \text{ m}^2/\text{s}$$

ERT

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 273-14

SUBJECT: REI 3-3 Calc. for REI 3-3

COMPUTED BY: DRS DATE: 11/20/77

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = \boxed{6.71 \times 10^2 \text{ gpd/ft}}$$

$$b = 14.0 \text{ ft}$$

$$K = \frac{6.71 \times 10^2}{14.0} = \boxed{4.79 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = \boxed{2.26 \times 10^{-3} \text{ cm/s}}$$

## Semi-Log (t) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H_{\text{rec}}}$$

$$Q = 3.0 \text{ gpm}$$

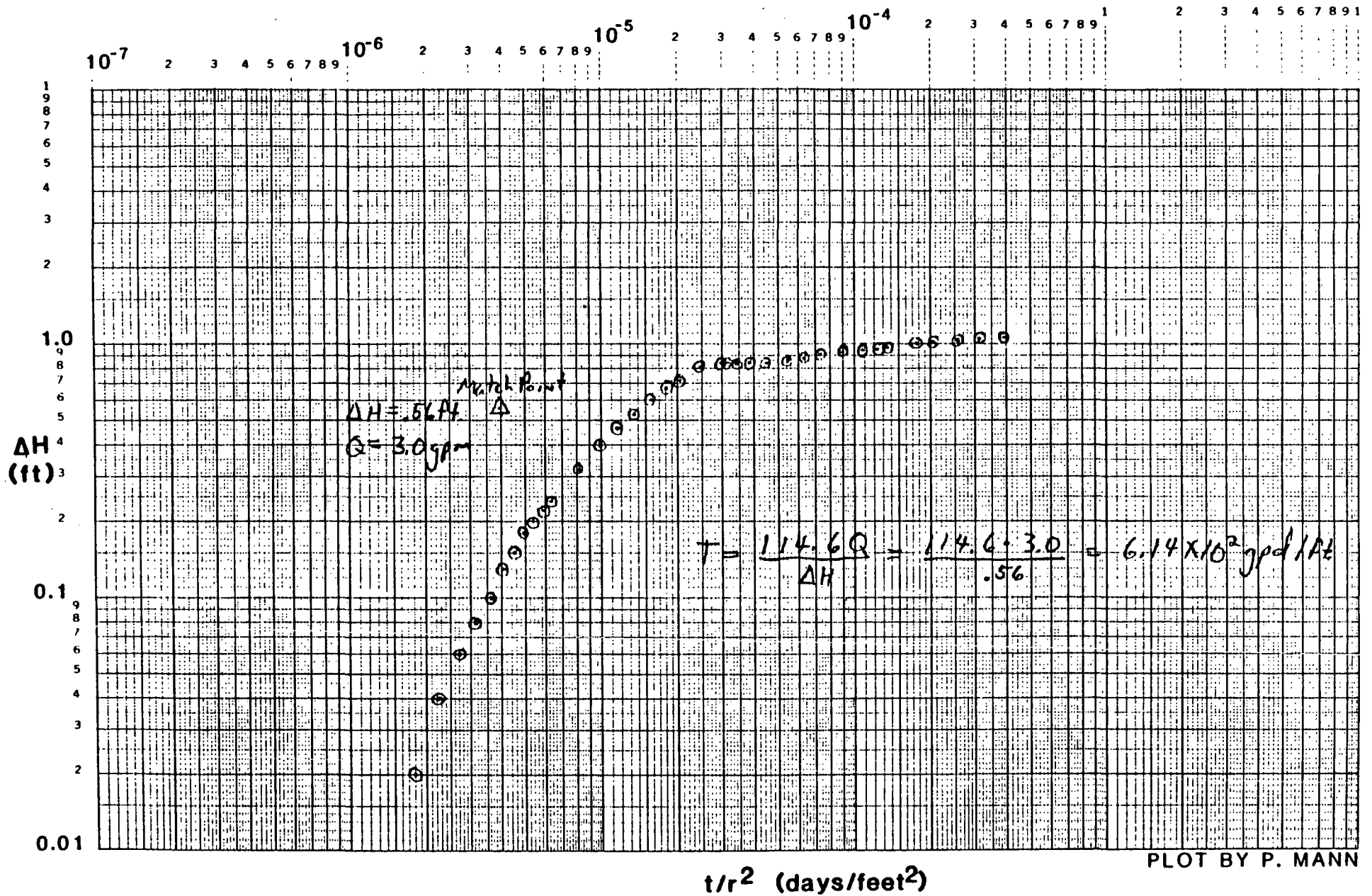
$$\Delta H_{\text{rec}1} = 1.19 \text{ ft} \quad T_1 = \frac{(264)(3.0)}{1.19} = \boxed{6.66 \times 10^2 \text{ gpd/ft}}$$

$$\Delta H_{\text{rec}2} = 0.903 \text{ ft} \quad T_2 = \frac{(264)(3.0)}{0.903} = \boxed{8.77 \times 10^2 \text{ gpd/ft}}$$

$$\times \text{ Conversion Factor } 1.432 \times 10^{-7} = \boxed{9.57 \times 10^{-5} \text{ m}^2/\text{s}}$$

$$\boxed{1.26 \times 10^{-4} \text{ m}^2/\text{s}}$$

REI 3-3 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF REI 3-5 (8/11 - 12/86)



PLOT BY P. MANN

v/b .5-.6.

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 274-14

SUBJECT: REI 3-3 Calc. for REI 3-5

COMPUTED BY: DRG DATE: 11/9/76

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$\Delta H = 0.56 \text{ ft} \quad T = \frac{(114.6)(3.0)}{0.56} = 6.14 \times 10^2 \text{ gpd/ft}$$

$$Q = 3.0 \text{ gpm}$$

$$\times \text{Conversion Factor } 1.432 \times 10^{-7} = 8.83 \times 10^{-5} \text{ m}^2/\text{s}$$

## Log-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 3.95 \times 10^{-6} \text{ days/ft}^2$$

$$T = 6.14 \times 10^2 \text{ gpd/ft}$$

$$S = \frac{(1)(6.14 \times 10^2)(3.95 \times 10^{-6})}{1.87} = 1.30 \times 10^{-3}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 6.14 \times 10^2 \text{ gpd/ft}$$

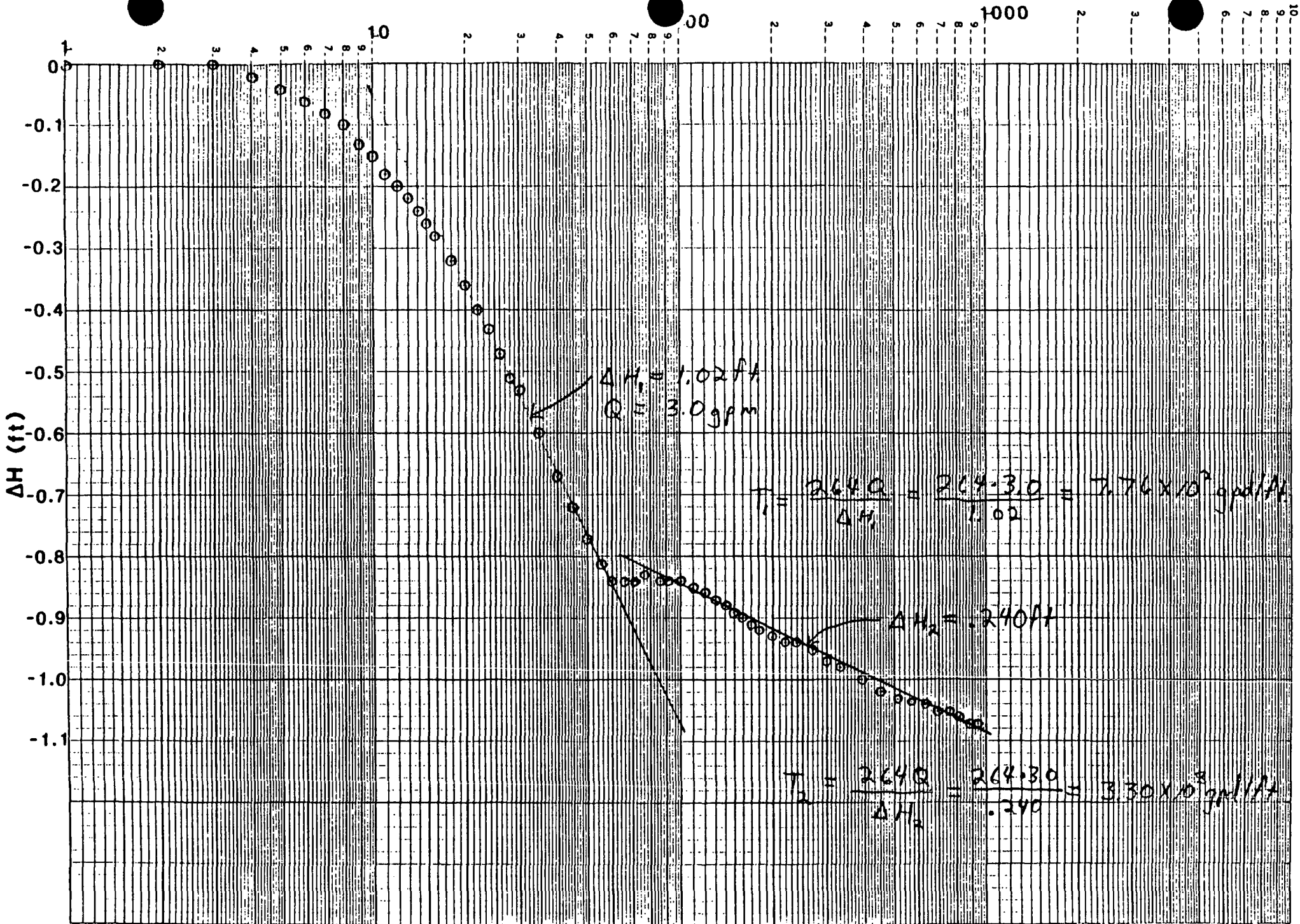
$$b = 15.20 \text{ ft}$$

$$K = \frac{6.14 \times 10^2}{15.20} = 4.04 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 1.90 \times 10^{-3} \text{ cm/s}$$

**ERT**





REI 3-3 PUMP TEST - DRAWDOWN

PLOT BY M. BARRON

SEMI-LOG PLOT OF REI 3-5 (8/11 - 12/86)

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTI

JOB NO.: 271-14

SUBJECT: REI 3-2 Calc for REI 3-5

COMPUTED BY: DBL DATE: 11/1/77

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264Q}{\Delta H}$$

$$Q = 3.0 \text{ gpm}$$

$$\Delta H_1 = 1.02 \text{ ft} \quad T_1 = \frac{(264)(3.0)}{1.02} = 7.76 \times 10^2 \text{ gpd/ft}$$

$$\Delta H_2 = 2.40 \text{ ft} \quad T_2 = \frac{(264)(3.0)}{2.40} = 3.30 \times 10^3 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.432 \times 10^{-7} =$$

$$1.12 \times 10^{-4} \text{ m}^2/\text{s}$$

$$4.75 \times 10^{-4} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.2 T t_0}{r^2}$$

$$r = 39.33 \text{ ft}$$

$$t_{01} = 89 \text{ min} / 1440 = 6.18 \times 10^{-2} \text{ days}$$

$$T_1 = 7.76 \times 10^2 \text{ gpd/ft}$$

$$t_{02} = 3.4 \times 10^{-2} \text{ m}^2 / 1440 = 2.36 \times 10^{-5} \text{ days}$$

$$T_2 = 3.30 \times 10^3 \text{ gpd/ft}$$

$$S_1 = \frac{(0.2)(7.76 \times 10^2)(6.18 \times 10^{-2})}{(39.33)^2}$$

$$9.31 \times 10^{-3}$$

$$S_2 = \frac{(0.2)(3.30 \times 10^3)(2.36 \times 10^{-5})}{(39.33)^2}$$

$$1.51 \times 10^{-5}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 274-14

SUBJECT: REI 3-3 Calc for REI 3-5

COMPUTED BY: DRS DATE: 11/20/14

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{Where } b \text{ is the screened thickness in feet.}$$

$$T_1 = \boxed{7.76 \times 10^2 \text{ gpd/ft}}$$

$$b = 15.20 \text{ ft}$$

$$K_1 = \frac{7.76 \times 10^2}{15.20} = \boxed{5.11 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = \boxed{2.41 \times 10^{-3} \text{ cm}^2/\text{s}}$$

$$T_2 = \boxed{3.30 \times 10^2 \text{ gpd/ft}}$$

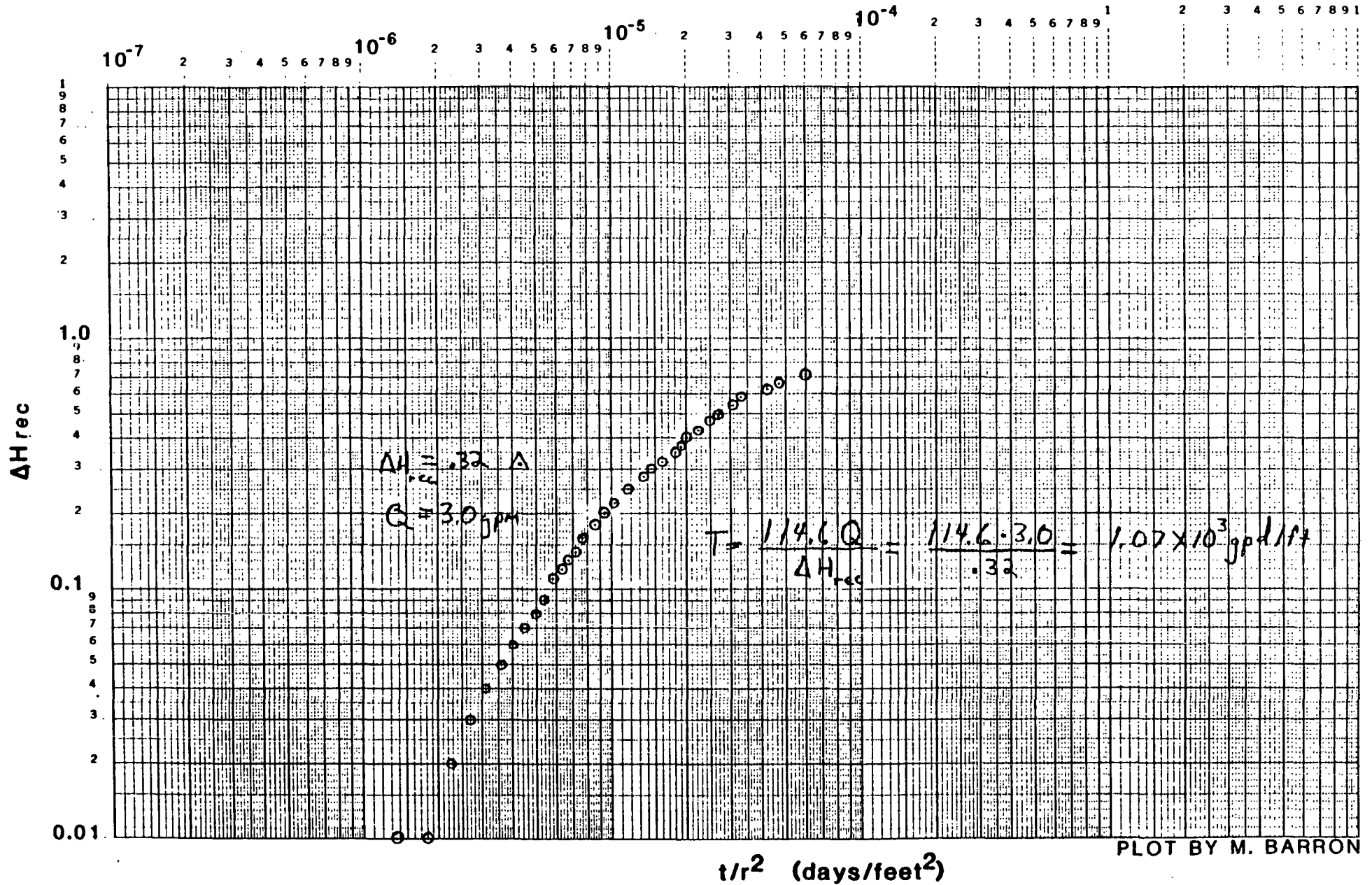
$$b = 15.20 \text{ ft}$$

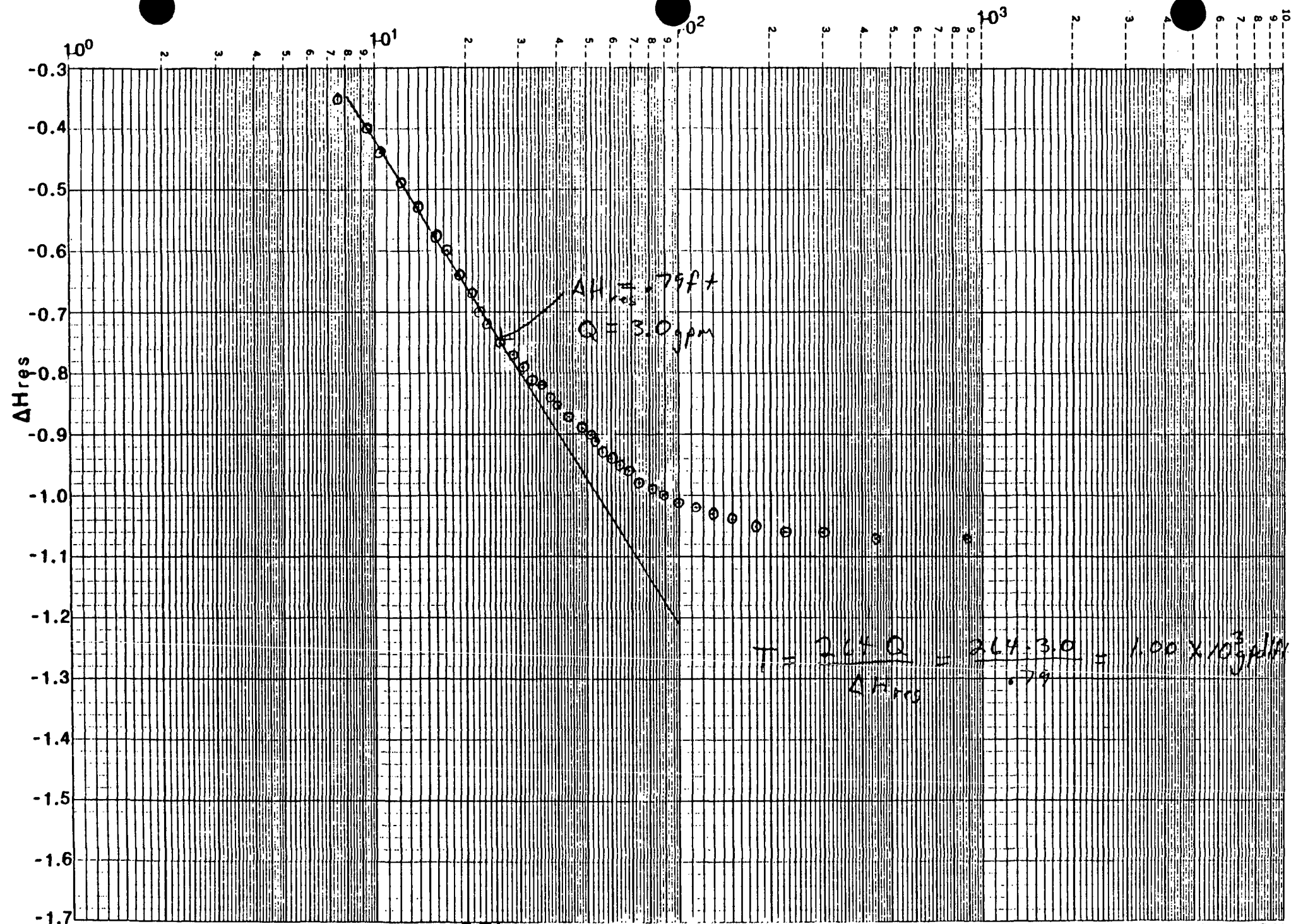
$$K = \frac{3.30 \times 10^2}{15.20} = \boxed{2.17 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = \boxed{1.02 \times 10^{-3} \text{ cm}^2/\text{s}}$$

**ERT**

REI 3-3 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF REI 3-5 8/12/86





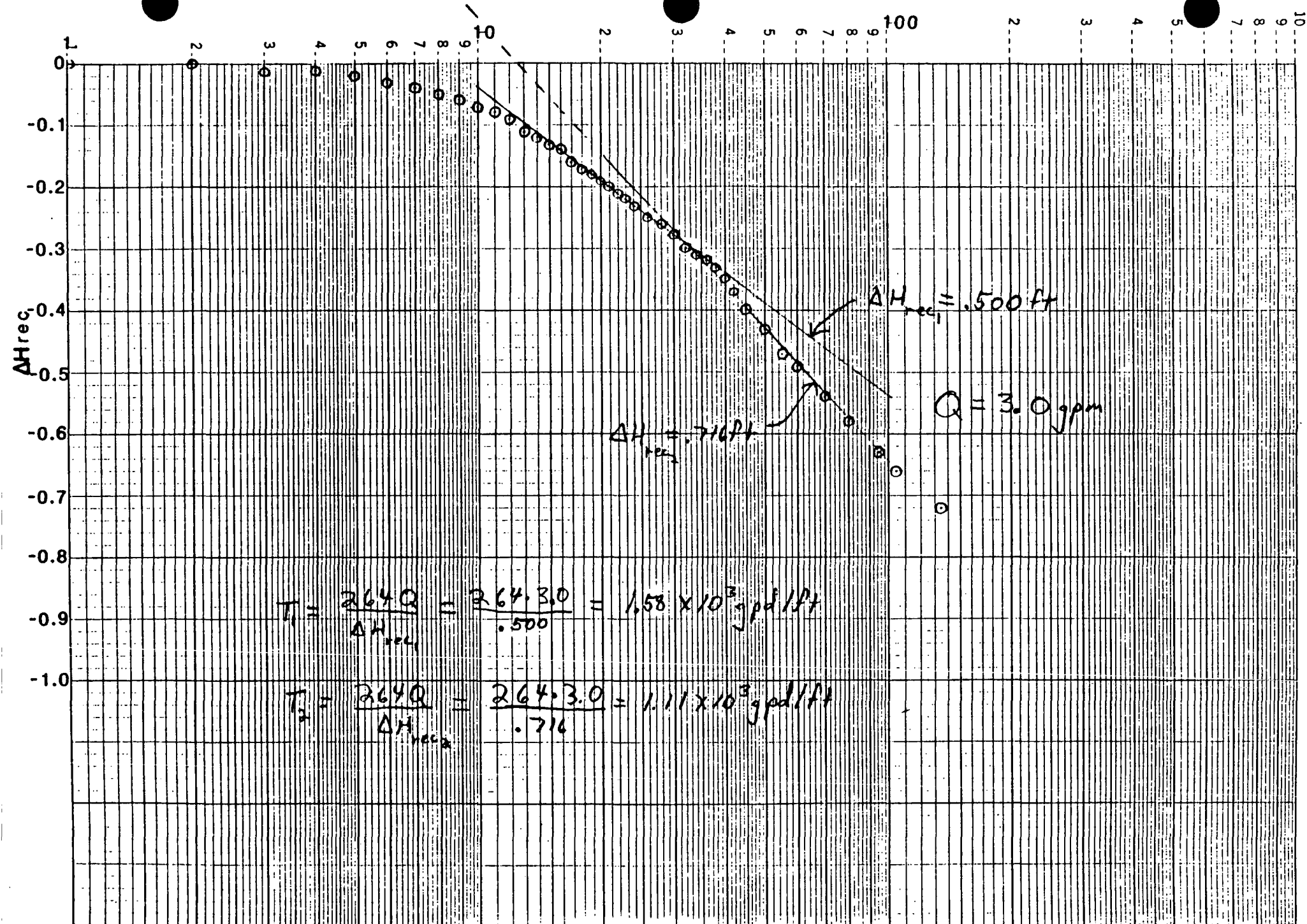
$$T = \frac{2.64 Q}{\Delta H_{res}} = \frac{2.64 \cdot 3.0}{.79} = 1.00 \times 10^3 \text{ gpm}$$

REI 3-3 PUMP TEST - RECOVERY

PLOT BY M. BARRON

SEMI-LOG PLOT OF REI 3-5

8/12/86



REI 3-3 PUMP TEST - RECOVERY

PLOT BY M. BARRON

SEMI-LOG PLOT OF REI 3-5 8/12/86

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 236-14

SUBJECT: FEI 3-2 Calc for FEI 3-6

COMPUTED BY: JD DATE: 12/22

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Log-Log solution for Transmissivity - Recovery

$$Transmissivity (T) = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$Q = 3.0 \text{ gpm}$$

$$\Delta H = 0.32 \text{ ft}$$

$$T = \frac{(114.6)(3.0)}{0.32} = 1.07 \times 10^5 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7} = 1.54 \times 10^{-4} \text{ m/s}$$

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 1.07 \times 10^5 \text{ gpd/ft}$$

$$b = 15.20 \text{ ft}$$

$$K = \frac{1.07 \times 10^5}{15.20} = 7.07 \times 10^3 \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 3.33 \times 10^{-3} \text{ cm/s}$$

## Semi-Log(u) solution for Transmissivity - Recovery

$$Transmissivity (T) = \frac{264 Q}{\Delta H_{res}}$$

$$Q = 3.0 \text{ gpm}$$

$$\Delta H_{res} = 0.79 \text{ ft}$$

$$T = \frac{(264)(3.0)}{0.79} = 1.00 \times 10^5 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.438 \times 10^{-7} = 1.44 \times 10^{-6} \text{ m/s}$$

**ERT**

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 274-14

SUBJECT: REI 3-2 Calc for REI 3-5

COMPUTED BY: DRA DATE: 10/1/77

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = \boxed{1.00 \times 10^5 \text{ gpd/ft}}$$

$$b = 15.20 \text{ ft}$$

$$K = \frac{1.00 \times 10^5}{15.20} = \boxed{6.60 \times 10^4 \text{ gpd/ft}^2}$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = \boxed{3.11 \times 10^{-3} \text{ cm/s}}$$

## Semi-Log (b) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H_{\text{rec}}}$$

$$Q = 3.0 \text{ gpm}$$

$$\Delta H_{\text{rec}1} = 0.500 \text{ ft} \quad T_1 = \frac{(264)(3.0)}{0.500} = \boxed{1.58 \times 10^5 \text{ gpd/ft}^2}$$

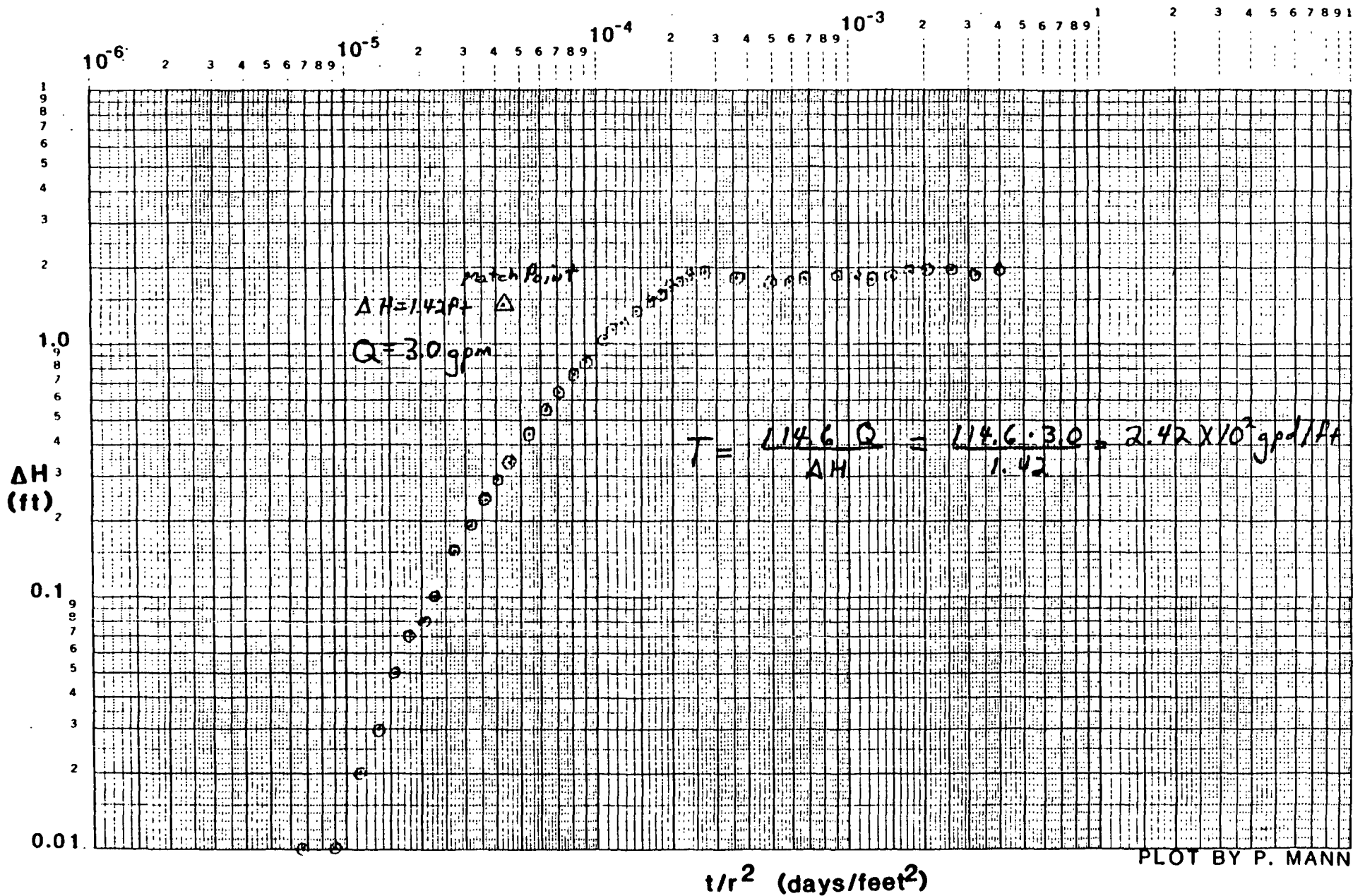
$$\Delta H_{\text{rec}2} = 0.716 \text{ ft} \quad T_2 = \frac{(264)(3.0)}{0.716} = \boxed{1.11 \times 10^5 \text{ gpd/ft}^2}$$

$$\times \text{ Conversion Factor } 1.432 \times 10^{-7} = \boxed{2.27 \times 10^{-4} \text{ m}^2/\text{s}}$$

$$\boxed{1.59 \times 10^{-4} \text{ m}^2/\text{s}}$$



REI 3-3 PUMP TEST - DRAWDOWN  
LOG-LOG PLOT OF P3-3 (8/11 - 12/86)



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_ OF \_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 3-2 Calc. for P3-3

COMPUTED BY: DRS DATE: 11/5/2

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Log-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$$\Delta H = 1.42 \text{ ft}$$

$$Q = 3.0 \text{ gpm}$$

$$T = \frac{(114.6)(3.0)}{1.42} = 2.42 \times 10^2 \text{ gpd/ft}$$

$$\times \text{Conversion Factor } 1.432 \times 10^{-7} = 3.48 \times 10^{-5} \text{ m}^2/\text{s}$$

## Log-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{uT}{1.87} \left( \frac{t}{r^2} \right)$$

where  $u = 1$

$$t/r^2 = 4.3 \times 10^{-5} \text{ days/ft}^2$$

$$T = 2.42 \times 10^2 \text{ gpd/ft}$$

$$S = \frac{(1)(2.42 \times 10^2)(4.3 \times 10^{-5})}{1.87} = 5.57 \times 10^{-3}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 2.42 \times 10^2 \text{ gpd/ft}$$

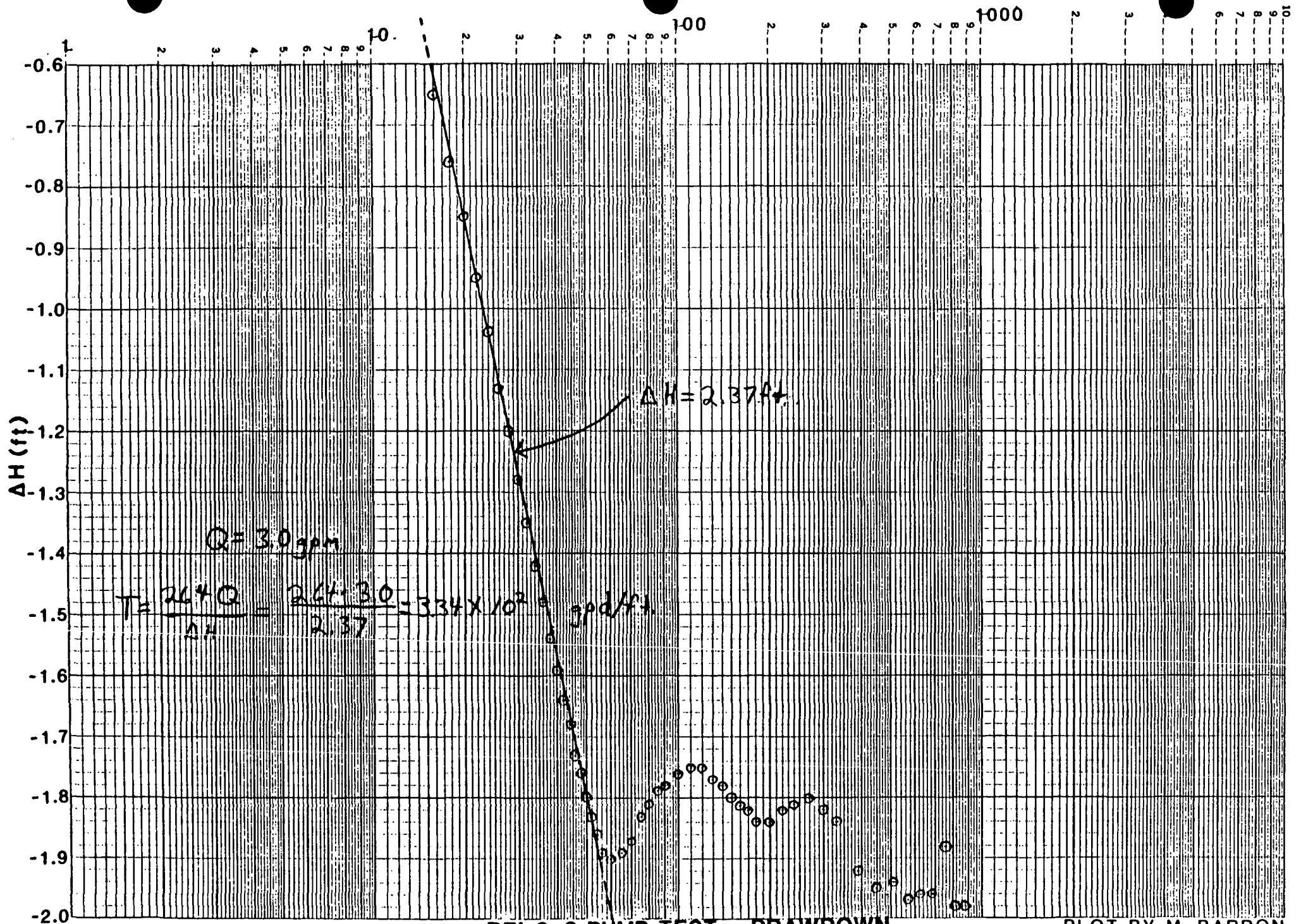
$$b = 14.0 \text{ ft (?) }^*$$

$$K = \frac{2.42 \times 10^2}{14.0} = 1.73 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = 8.15 \times 10^{-4} \text{ cm/s}$$

\* No boring log available. Thickness of screen for P3-3 based on boring log of REI 3-3.

ERT



REI 3-3 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF P3-3 (8/11 - 12/86)

PLOT BY M. BARRON

# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 3-3 Calc for P3-3

COMPUTED BY: DRG DATE: 11-20-77

CHECKED BY:      DATE:     

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity (T)} = \frac{264Q}{\Delta H}$$

$$Q = 3.0 \text{ gpm}$$

$$\Delta H = 2.37 \text{ ft} \quad T = \frac{(264)(3.0)}{2.37} = 3.34 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 4.81 \times 10^{-5} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity (S)} = \frac{0.3 T t_0}{r^2}$$

$$r = 12.42 \text{ ft}$$

$$t_0 = 9.0 \text{ min} / 1440 = 6.25 \times 10^{-3} \text{ days}$$

$$T = 3.34 \times 10^2 \text{ gpd/ft}$$

$$S = \frac{(0.3)(3.34 \times 10^2)(6.25 \times 10^{-3})}{(12.42)^2} = 4.06 \times 10^{-3}$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet}$$

$$T = 3.34 \times 10^2 \text{ gpd/ft}$$

$$b = 14.0 \text{ ft (?) } *$$

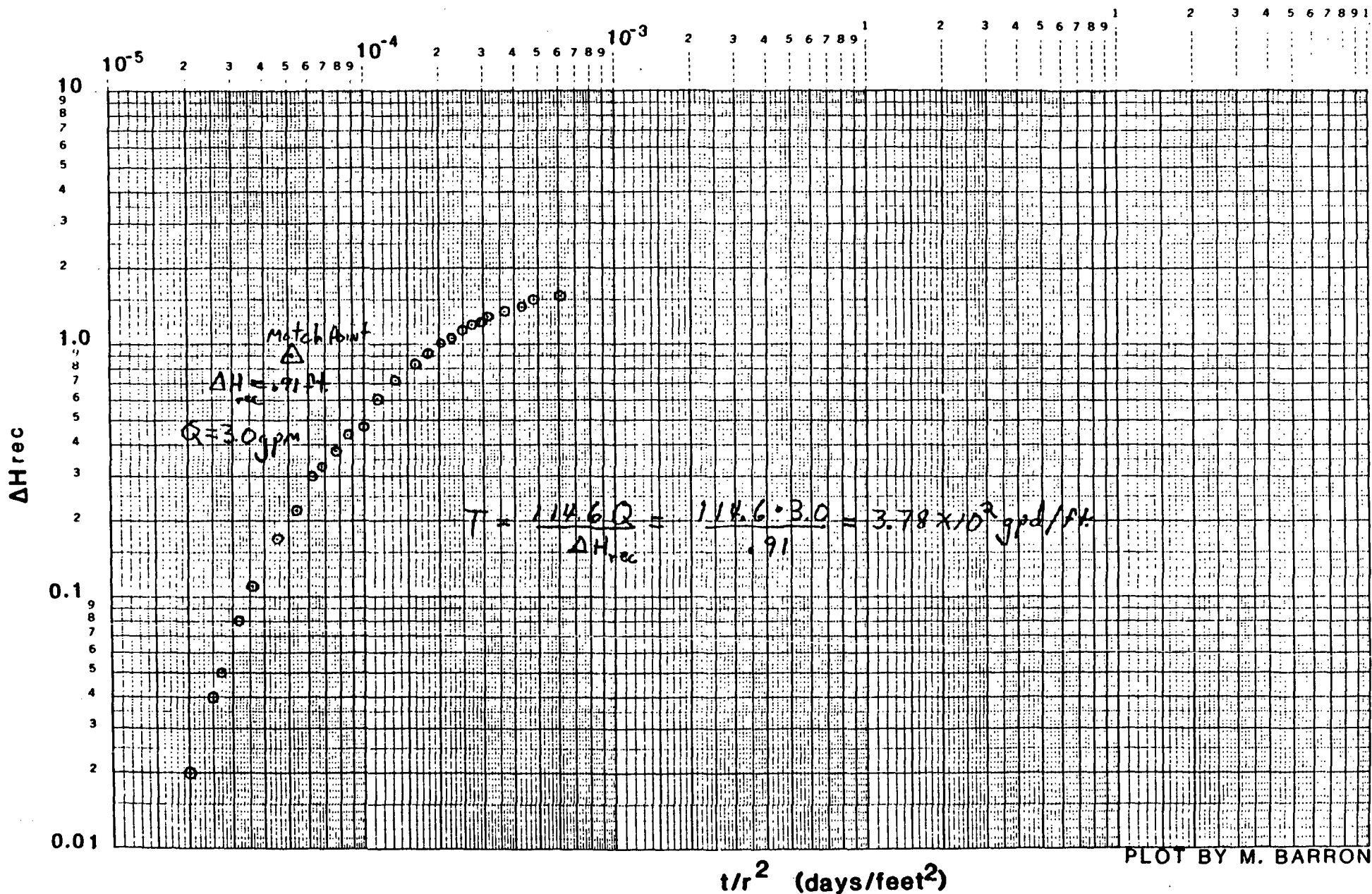
$$K = \frac{3.34 \times 10^2}{14.0} = 2.39 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 1.13 \times 10^{-3} \text{ cm/s}$$

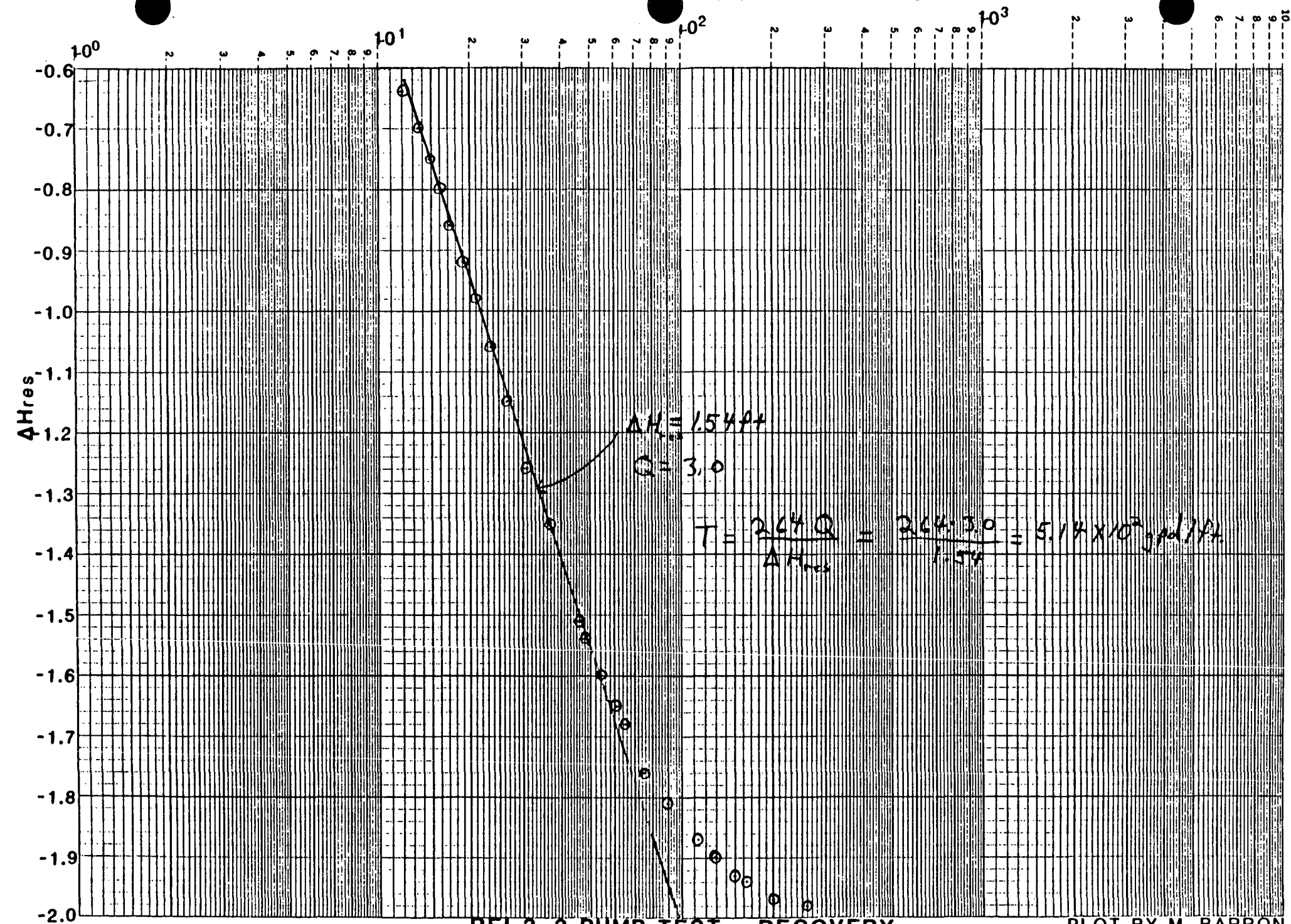
\* No boring log available. Thickness of screen for P3-3 based on boring log of REI 3-3.

**ERT**

REI 3-3 PUMP TEST - RECOVERY  
LOG-LOG PLOT OF P3-3 8/12/86



PLOT BY M. BARRON

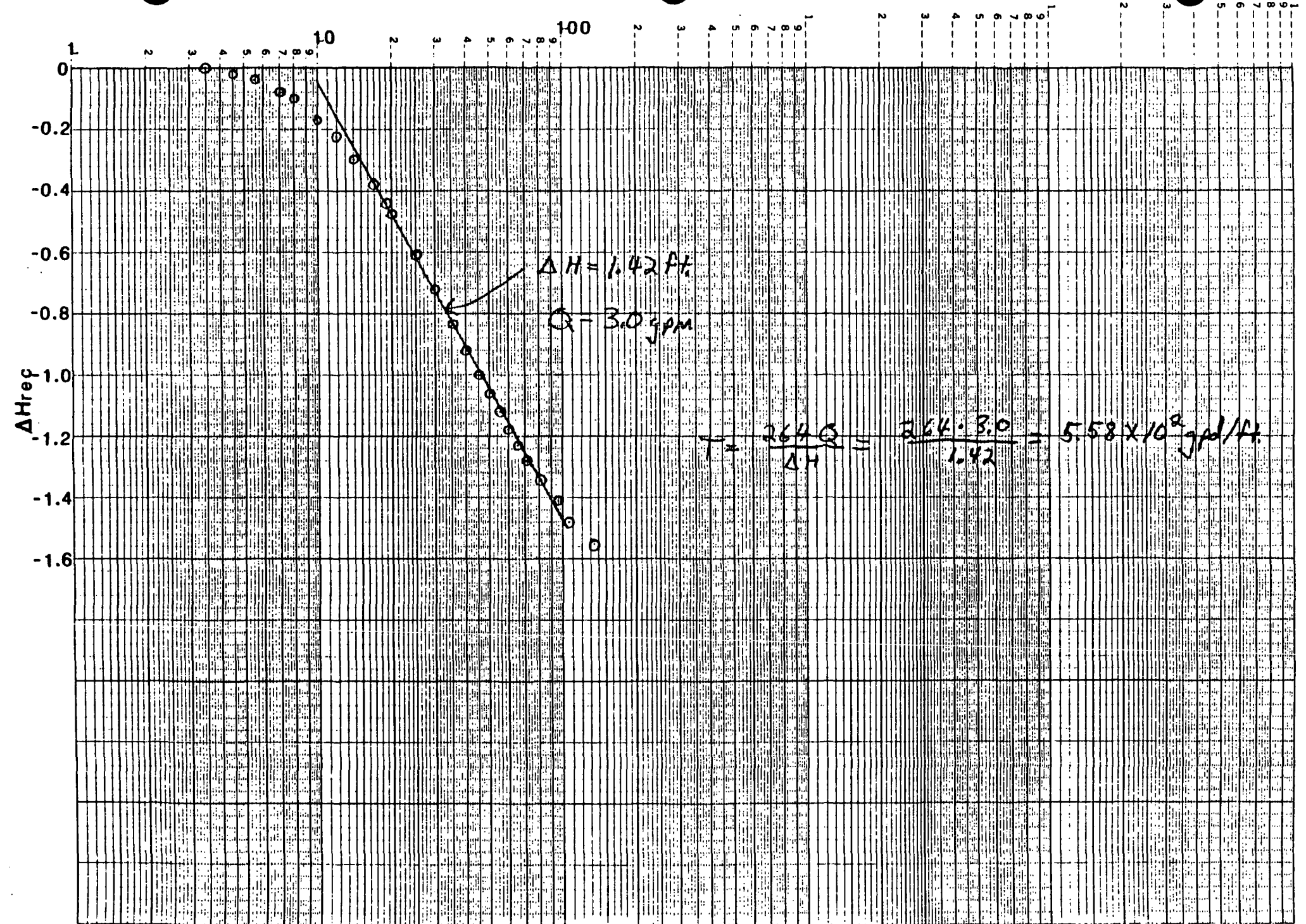


REI 3-3 PUMP TEST - RECOVERY

PLOT BY M. BARRON

SEMI-LOG PLOT OF P3-3

8/12/86



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 275-14

SUBJECT: REI 3-3 Calc for P3-3

COMPUTED BY: DEE DATE: 10-7

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Log-Log solution for Transmissivity - Recovery

$$T = \frac{114.6 Q W(u)}{\Delta H}$$

where  $W(u) = 1$

$Q = 3.0 \text{ gpm}$

$\Delta H = 0.91 \text{ ft}$

$$T = \frac{(114.6)(3.0)}{0.91}$$

$3.78 \times 10^2 \text{ gpd/ft}$

X Conversion Factor  $1.432 \times 10^{-7} = 5.43 \times 10^{-5} \text{ m}^2/\text{s}$

## Solution for Hydraulic Conductivity - Recovery

$K = \frac{T}{b}$  where  $b$  is the screened thickness in feet

$T = 3.78 \times 10^2 \text{ gpd/ft}$

$b = 14.0 \text{ ft (?)}$

$$K = \frac{3.78 \times 10^2}{14.0} = 2.70 \times 10^1 \text{ gpd/ft}^2$$

X Conversion Factor  $4.715 \times 10^{-5} = 1.27 \times 10^{-3} \text{ cm/s}$

## Semi-Log<sub>e</sub>(u) solution for Transmissivity - Recovery

$$T = \frac{264 Q}{\Delta H_{res}}$$

$Q = 3.0 \text{ gpm}$

$\Delta H_{res} = 1.54 \text{ ft}$

$$T = \frac{(264)(3.0)}{1.54}$$

$5.14 \times 10^2 \text{ gpd/ft}$

X Conversion Factor  $1.432 \times 10^{-7} = 7.40 \times 10^{-5} \text{ m}^2/\text{s}$

\* No Loring log available. Thickness of screen for P3-3 based on Loring log of REI 3-3.

ERT



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD

JOB NO.: 275-14

SUBJECT: REI 3-3 Calc for P3-3

COMPUTED BY: DRG DATE: 11/27/74

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Solution for Hydraulic Conductivity - Recovery

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = \boxed{5.14 \times 10^2 \text{ gpd/ft}}$$

$$b = 14.0 \text{ ft (?) }^*$$

$$K = \frac{5.14 \times 10^2}{14.0} = \boxed{3.67 \times 10^1 \text{ gpd/ft}^2}$$

$$\times \text{Conversion Factor } 4.715 \times 10^{-5} = \boxed{1.73 \times 10^{-5} \text{ cm/s}}$$

## Semi-Log(t) solution for Transmissivity - Recovery

$$\text{Transmissivity (T)} = \frac{264 Q}{\Delta H_{rec}}$$

$$Q = 3.0 \text{ gpm}$$

$$\Delta H_{rec} = 1.42 \text{ ft} \quad T = \frac{(264)(3.0)}{1.42} = \boxed{5.58 \times 10^2 \text{ gpd/ft}}$$

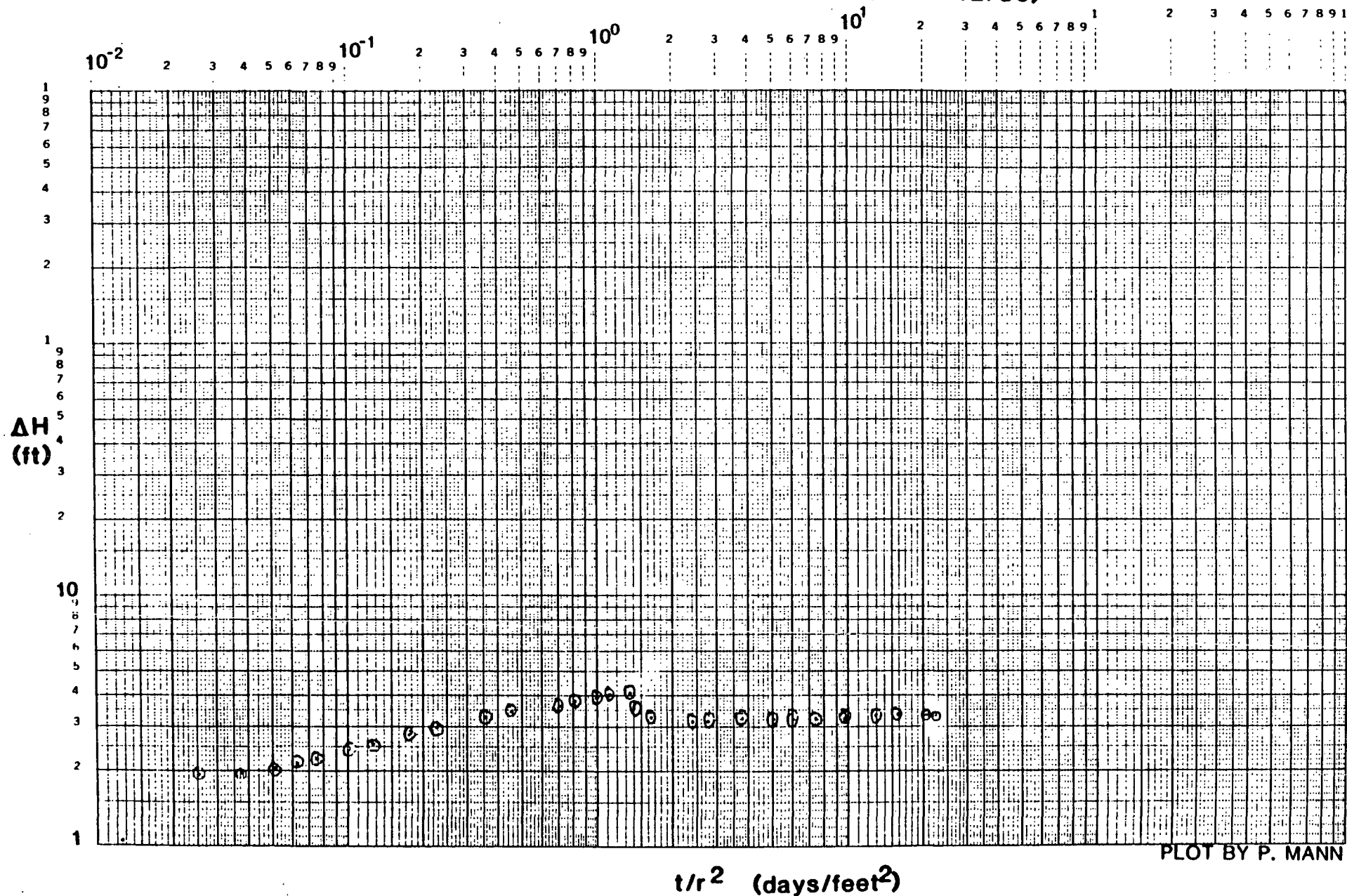
$$\times \text{Conversion Factor } 1.432 \times 10^{-7} = \boxed{8.02 \times 10^{-5} \text{ m}^2/\text{s}}$$

\* No boring log available. Thickness of screen for P3-3 based on boring log of REI 3-3.

**ERT**

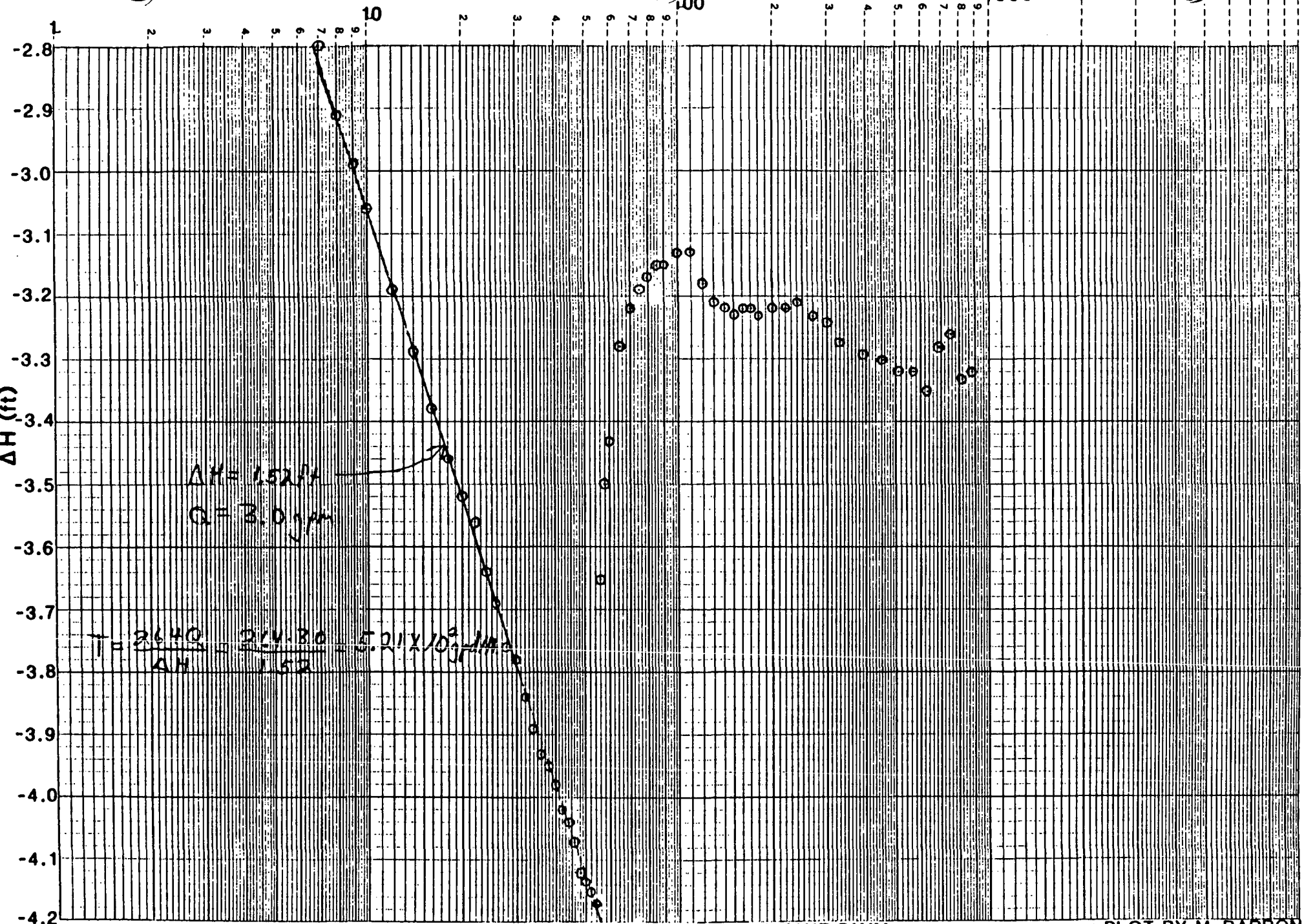
# REI 3-3 PUMP TEST - DRAWDOWN

LOG-LOG PLOT OF REI 3-3 (8/11-12/86)



PLOT BY P. MANN

ΔH (ft)



REI 3-3 PUMP TEST - DRAWDOWN  
SEMI-LOG PLOT OF REI 3-3 (8/11-12/86)

PLOT BY M. BARRON

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: FRENCH LTD.

JOB NO.: 275-14

SUBJECT: REI 3-3 Calc. for REI 3-3

COMPUTED BY: DRS DATE: 10/10/00

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

## Semi-Log solution for Transmissivity - Drawdown

$$\text{Transmissivity } (T) = \frac{264Q}{\Delta H}$$

$$Q = 3.0 \text{ gpm}$$

$$\Delta H = 1.52 \text{ ft} \quad T = \frac{(264)(3.0)}{1.52} = 5.21 \times 10^2 \text{ gpd/ft}$$

$$\times \text{ Conversion Factor } 1.438 \times 10^{-7} = 7.49 \times 10^{-5} \text{ m}^2/\text{s}$$

## Semi-Log solution for Storativity - Drawdown

$$\text{Storativity } (S) = \frac{0.3 T t_0}{r^2}$$

$$r = 0.166 \text{ ft}$$

$$t_0 = 9.3 \times 10^{-1} \text{ min} / 1440 = 6.46 \times 10^{-4} \text{ days}$$

$$T = 5.21 \times 10^2 \text{ gpd/ft}$$

$$S = \frac{(0.3)(5.21 \times 10^2)(6.46 \times 10^{-4})}{(0.166)^2} = 3.66 \times 10^0$$

## Solutions for Hydraulic Conductivity (K)

$$K = \frac{T}{b} \quad \text{where } b \text{ is the screened thickness in feet.}$$

$$T = 5.21 \times 10^2 \text{ gpd/ft}$$

$$b = 14.0 \text{ ft}$$

$$K = \frac{5.21 \times 10^2}{14.0} = 3.72 \times 10^1 \text{ gpd/ft}^2$$

$$\times \text{ Conversion Factor } 4.715 \times 10^{-5} = 1.75 \times 10^{-5} \text{ cm/s}$$

# **1986 FIELD INVESTIGATION AND SUPPLEMENTAL REMEDIAL INVESTIGATION REPORT**

**VOLUME II - APPENDICES**

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**U.S. ENVIRONMENTAL PROTECTION AGENCY  
REGION VI**

**TEXAS WATER COMMISSION**



**DECEMBER, 1986**

**275-14**

***RESOURCE ENGINEERING***

Appendix 1

PCB Extraction and Analytical Procedures

# ETC ENVIRONMENTAL TESTING and CERTIFICATION CORPORATION

July 10, 1986

Mr. Chris Itin  
Resource Engineering  
3000 Richmond Avenue  
Houston, TX 77098

Dear Chris:

Enclosed for your review are the analytical and data reporting requirements ETC will use for the RES27511 project. The method and reporting requirements enclosed have been designed to eliminate as many variables as possible when performing an interlaboratory effort.

Please call us if there is any problem with this protocol presentation.

Sincerely,

*Karen T. Kotz-Gebel*

Karen Kotz-Gebel

KKG/lmd

Enclosure

## Scope of Work

In order to obtain interlaboratory consistency in the analytical protocol ETC has identified several critical areas within the analytical scheme:

- Method of sample homogenization
- Sample extraction method and length of extraction
- Initial sample weight used
- Sample extract clean up
- Holding time.

To minimize analytical variables the above critical areas must be rigidly adhered to as described below under the "Analytical Protocol."

## Analytical Protocol

### I. Pre-Extraction Preparation

#### A. Sample Homogenization

Prior to sample extraction each sample must be homogenized. Due to the variable matrix of the samples some analytical judgement must be used here to determine the best method of homogenization. ETC, after receipt of sample, will give specifications via telephone (to be followed by documentation) as to how each individual sample should be homogenized. ETC envisions that vigorous hand shaking of the sample bottle for one minute prior to taking an aliquot will be sufficient for liquid type samples. Alternately, for those samples containing mostly solids, physical stirring of the entire contents of the sample bottle in a large beaker should be performed with a stainless steel spatula for a set period of time. Whichever method of homogenization is performed, it must be documented and submitted along with the analytical results.

#### B. % Moisture Determination

Each sample must have a % moisture determination performed in conjunction with the extraction procedure. The method for the % moisture determination may be found in the IFB-CLP protocol "Organic Analysis Multi-Media Multi-Concentration." All data will then be reported on a dry weight basis.



## II. Quality Control of Extraction Procedure

### A. QC Requirements

For each 20 samples the following quality control must be performed:

1. One method blank
2. One replicate sample
3. One sample matrix spike.

### B. Spiking Level

The matrix spike will consist of spiking Aroclor 1242<sup>®</sup> at levels equivalent to 20 ppm (mg/kg) in the wet sample.

### C. Holding time of all extractions are within 14 days of sample collection.

## III. Sample Extraction and Clean up (unless otherwise specified by ETC after sample receipt)

### A. Extraction

Extraction will be performed using SW-846 Method #3540 which is a soxhlet extraction procedure. The conditions for this extraction are:

1. Use a 30 gram wet weight sample
2. Extract with 1:1 Acetone/Hexane
3. Extract for 16 hours
4. Concentrate the extract to a final volume of 25 mls.

### B. Silica Gel Clean up

A silica gel clean up column will be used on the extracts. A 5 ml. aliquot of the 25 ml. final volume will be passed through the clean up and then concentrated to a 5 ml. final volume. The effective concentration factor for the procedure will be approximately 1.0 (i.e. Initial weight, dry ÷ final volume). The following is a summary of the clean up procedure. It should be noted that the elution volume may vary depending upon the activity of the silica gel. Before performing the clean up a column recovery study should be performed using Aroclor 1016 and Aroclor 1260.

1. Charge a 20 mm bore chromatography column (equipped with a 250 ml. reservoir and stopcock) with 20 grams of activated silica gel. Place 1/2 inch of  $\text{Na}_2\text{SO}_4$  on top of the silica gel column.
2. Pre-rinse the column with 60 ml of hexane.
3. When the hexane sinks just under the  $\text{Na}_2\text{SO}_4$  layer close the stopcock and add the 5 ml. aliquot of the extract.
4. Open the stopcock and add 200 ml. of hexane as the extract sinks just under the  $\text{Na}_2\text{SO}_4$  layer.
5. Discard the first 100 ml. of eluate.
6. Collect the second 100 ml. of eluate into a receiving vessel for subsequent concentration to 5 ml.
7. Discard any remaining eluate.

#### IV. Gas Chromatography Analysis

The following analytical protocol will be used to analyze the extracts by GC/ECD.

##### A. Primary Column Analysis

1. All 7 Aroclors must be analyzed
2. 3 levels of Aroclor 1242 must be analyzed so that a 3 point calibration curve will be used to calculate the matrix spike % recovery.
3. The level of standards used for quantitation should be such that a detection limit of 1-5 mg/kg is attained.

##### B. Confirmation Column Analysis

1. All primary column hits must be confirmed by second column confirmation with 3 levels of the Aroclor of interest.
2. All analytical results must be calculated using the 3 point calibration curve and all extract concentrations must fall within the calibrations curve.

## Methodology for GC Analysis of Polychlorinated Biphenyls

The method employed in the analysis of your sample for polychlorinated biphenyls is an established EPA method taken from "Test Methods for Evaluating Solid Waste", July 1982.

The method can be summarized as follows: A weighed amount of homogenized sample, approximately 30 grams, is soxhlet extracted for 16 hours with hexane. The extract is dried and concentrated to approximately 25 ml. A 5 ml aliquot of the concentrated extract is transferred to a silica gel column and eluted with hexane. The eluate is concentrated to a final volume of 5 ml and injected into a gas chromatograph equipped with an  $^{63}\text{Ni}$  electron capture detector.

The GC operating parameters were as follows:

### COLUMN

6' x 4 mm glass 1.5% SP-2250 & 1.95% SP-2401  
Supelcoport 100/120 mesh

### CARRIER FLOW

60 ml/min. Argon/Methane

### COLUMN OVEN

220° C

### INJECTOR TEMPERATURE

225° C

### DETECTOR TEMPERATURE

325° C

### DETECTOR

$\text{Ni}^{63}$  Electron Capture Detector

### CONFIRMATION COLUMN

6' x 4 mm glass 3% OV-1  
Supelcoport 100/120 mesh

## Summary of Quality Assurance/Quality Control Procedures (QA/QC)

ETC bases its quality assurance protocols on the following government guidelines:

- "Handbook for Analytical Quality Control in Water and Wastewater Laboratories", EPA-600/4-79-019, March 1979;
- National Enforcement Investigation Center Policies, and Procedures manual; EPA-330/9/79/001-R, October 1979;
- the recommended guidelines for EPA Methods 624 and 625. (Federal Register, December 3, 1979; updated on October 26, 1984);
- "Manual of Analytical Methods for the Analysis of Pesticides in Humans and Environmental Samples," EPA 600/8-80-036, June 1980;
- "Determination of 2,3,7,8-TCDD in Soil and Sediment" EPA, Region VII, Kansas City, September 1983;
- Organic Analysis: Multi-media, Multi Concentration-IFB WA84-A267; and
- Dioxin Analysis: Soil/Sediment Matrix; Multi-Concentration; Selected Ion Monitoring with Jar Extraction Procedure-IFB WA84-A002

However, we have modified our protocols to provide a higher level of QA/QC than the guidelines require. For example, we analyze a higher than required number of quality control samples and we pay especially careful attention to the certification of the "reference standard" compounds we use in analysis. Below are listed the key QA/QC elements for the methods we used.

### Analysis of Volatile Organic Compounds by Gas Chromatography/Mass Spectrometry

- Each batch of 13 samples consists of 9 customer samples (at a maximum), one blank sample, one spiked blank, one spiked sample and one replicate sample. This amounts to a 30% quality control factor.
- Three surrogate compounds are added to each sample in the batch of 13.
- A blind quality control sample is introduced to the laboratory for analysis on a weekly basis.
- Each GC/MS is checked and retuned, if necessary, at the beginning of each day to ensure that its performance on bromofluorobenzene (BFB) meets the EPA criteria.
- A calibration curve for quantitation is prepared using a mixture of Volatile Organic Priority Pollutant "standards" at a minimum of 3 different concentrations and using a mixture of 3 internal standards at a constant concentration.
- The calibration curve is verified with a mixture of priority pollutant standards every day. If the response factors vary greater than 25%, the instrument must be recalibrated.

### Analysis of Organic Compounds Extracted in Acid or Base/Neutral Solutions by Gas Chromatography/Mass Spectrometry

- Each batch of 20 samples consists of 16 customer samples (at a maximum), one blank sample, one spiked blank (for water matrices), one sample spiked with the priority pollutant standard mixture and a duplicate customer sample. This amounts to a 20% quality control factor.

Appendix 2

PCB Analytical Results - ETC

AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9376	RESOURCE ENGINEERING	27514	IPC81-1	860716
ETC Sample No.	Company	Facility	Sample Point	Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	105000.	2040	7170.	8330.	ND	0	-	35200.	19700	113
Aroclor 1254	ND	2040	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2040	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2040	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2040	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2040	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2040	ND	ND	ND	0	-	ND	0	-

\* Identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9377

RESOURCE ENGINEERING

27514

IPCB1-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	73100	1870	7170.	8330.	ND	0	-	35200.	19700	113
Aroclor 1254	ND	1870	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1870	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1870	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1870	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1870	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1870	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.



## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### ***Aroclors (PCB's by GC/ECD)***

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9422

RESOURCE ENGINEERING

27514

IPCBI-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	315000 <sup>a</sup>	2640	17700 <sup>a</sup>	14200 <sup>a</sup>	ND	0	-	ND	19400	85
Aroclor 1254	ND	2640	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2640	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2640	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2640	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2640	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2640	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9423

RESOURCE ENGINEERING

27514

IPC82-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	59500	3440	17700.	14200.	ND	0	-	ND	19400	85
Aroclor 1254	ND	3440	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3440	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3440	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3440	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3440	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3440	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.

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**ETC**ENVIRONMENTAL  
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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9373 RESOURCE ENGINEERING

27514

IPCB2-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	14600	3860	7170 <sup>a</sup>	8330 <sup>a</sup>	ND	0	-	35200 <sup>a</sup>	19700	113
Aroclor 1254	ND	3860	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3860	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3860	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3860	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3860	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3860	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9372 RESOURCE ENGINEERING

27514

IPC82-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
Aroclor 1242	20500	3580	7170.	8330.	ND	0	-	35200.	19700	113
Aroclor 1254	ND	3580	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3580	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3580	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3580	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3580	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3580	ND	ND	ND	0	-	ND	0	-

A identification confirmed by second column analysis.



## Introduction

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Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

**ETC**ENVIRONMENTAL  
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AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9406

RESOURCE ENGINEERING

27514

IPC83-I

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	1500	17700 <sub>a</sub>	14200 <sub>a</sub>	ND	0	-	ND	19400	85
Aroclor 1254	ND	1500	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1500	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1500	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1500	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1500	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1500	ND	ND	ND	0	-	ND	0	-

<sub>a</sub> Identification confirmed by second column analysis.

## Introduction

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### *Aroclors (PCB's by GC/ECD)*

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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9407

RESOURCE ENGINEERING

27514

IPCB3-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	28700	1210	17700 <sup>a</sup>	14200 <sup>a</sup>	ND	0	-	ND	19400	85
Aroclor 1254	ND	1210	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1210	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1210	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1210	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1210	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1210	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

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### **Aroclors (PCB's by GC/ECD)**

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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9401	RESOURCE ENGINEERING	27514	IPC83-3	860716	
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	17800 <sup>a</sup>	1480	17700 <sup>a</sup>	14200 <sup>a</sup>	ND	0	-	ND	19400	85
Aroclor 1254	ND	1480	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1480	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1480	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1480	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1480	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1480	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9400

RESOURCE ENGINEERING

27514

IPC84-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	44900 <sup>a</sup>	2380	17700 <sup>a</sup>	14200 <sup>a</sup>	ND	0	-	ND	19400	85
Aroclor 1254	ND	2380	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2380	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2380	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2380	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2380	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2380	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.



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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9412

RESOURCE ENGINEERING

27514

IPC84-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	72100	2460	17700 <sup>a</sup>	14200 <sup>a</sup>	ND	0	-	ND	19400	85
Aroclor 1254	ND	2460	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2460	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2460	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2460	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2460	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2460	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9413

RESOURCE ENGINEERING

27514

IPC84-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	39400	3320	17700 <sup>a</sup>	14200 <sup>a</sup>	ND	0	-	ND	19400	85
Aroclor 1254	ND	3320	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3320	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3320	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3320	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3320	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3320	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

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TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9387

RESOURCE ENGINEERING

27514

IPC85-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov.	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov.
Aroclor 1242	21700	1860	7170 <sup>a</sup>	8330 <sup>a</sup>	ND	0	-	35200 <sup>a</sup>	19700	113
Aroclor 1254	ND	1860	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1860	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1860	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1860	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1860	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1860	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

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## Results

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### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

## Chain of Custody Data Required for ETC Data Management Summary Reports

M9386	RESOURCE ENGINEERING	27514	IPCB5-2	860716	
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	21700	1920	7170.	8330.	ND	0	-	35200.	19700	113
Aroclor 1254	ND	1920	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1920	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1920	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1920	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1920	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1920	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.



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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9390	RESOURCE ENGINEERING	27514	IPC85-3	860716
ETC Sample No.	Company	Facility	Sample Point	Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	4700	4570	7170 <sup>a</sup>	8330 <sup>a</sup>	ND	0	-	35200 <sup>a</sup>	19700	113
Aroclor 1254	ND	4570	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	4570	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	4570	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	4570	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	4570	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	4570	ND	ND	ND	0	-	ND	0	-

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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9391

RESOURCE ENGINEERING

27514

IPCB5-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	32900	1820	7170 <sup>a</sup>	8330 <sup>a</sup>	ND	0	-	35200 <sup>a</sup>	19700	113
Aroclor 1254	ND	1820	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1820	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1820	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1820	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1820	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1820	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9392 RESOURCE ENGINEERING

27514

IPC86-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	37700	2050	17700 <sup>a</sup>	14200 <sup>a</sup>	ND	0	-	ND	19400	85
Aroclor 1254	ND	2050	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2050	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2050	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2050	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2050	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2050	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

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**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9393

RESOURCE ENGINEERING

27514

IPCB6-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	20600	3680	17700 <sup>a</sup>	14200 <sup>a</sup>	ND	0	-	ND	19400	85
Aroclor 1254	ND	3680	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3680	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3680	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3680	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3680	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3680	ND	ND	ND	0	-	ND	0	-

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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9374 RESOURCE ENGINEERING

27514

IPC87-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	24400	1690	7170 <sup>a</sup>	8330 <sup>a</sup>	ND	0	-	35200 <sup>a</sup>	19700	113
Aroclor 1254	ND	1690	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1690	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1690	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1690	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1690	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1690	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9375

RESOURCE ENGINEERING

27514

IPC87-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	4180	2420	7170 <sup>a</sup>	8330 <sup>a</sup>	ND	0	-	35200 <sup>a</sup>	19700	113
Aroclor 1254	ND	2420	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2420	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2420	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2420	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2420	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2420	ND	ND	ND	0	-	ND	0	-

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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9398	RESOURCE ENGINEERING	27514	IPCB7-3	860716
ETC Sample No.	Company	Facility	Sample Point	Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	16600 <sup>a</sup>	1140	17700 <sup>a</sup>	14200 <sup>a</sup>	ND	0	-	ND	19400	85
Aroclor 1254	ND	1140	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1140	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1140	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1140	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1140	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1140	ND	ND	ND	0	-	ND	0	-

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**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9399

RESOURCE ENGINEERING

27514

IPC88-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	25000	4410	17700	14200	ND	0	-	ND	19400	85
Aroclor 1254	ND	4410	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	4410	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	4410	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	4410	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	4410	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	4410	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.



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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9426

RESOURCE ENGINEERING

27514

IPC88-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	5400	8700.	10200.	ND	0	-	ND	20300	80
Aroclor 1254	ND	5400	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	5400	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	5400	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	5400	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	5400	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	5400	ND	ND	ND	0	-	ND	0	-

R Identification confirmed by second column analysis.

## Summary of Quality Assurance/Quality Control Procedures (QA/QC)

ETC bases its quality assurance protocols on the following government guidelines:

- "Handbook for Analytical Quality Control in Water and Wastewater Laboratories", EPA-600/4-79-019, March 1979;
- National Enforcement Investigation Center Policies, and Procedures manual; EPA-330/9/79/001-R, October 1979;
- the recommended guidelines for EPA Methods 624 and 625. (Federal Register, December 3, 1979; updated on October 26, 1984);
- "Manual of Analytical Methods for the Analysis of Pesticides in Humans and Environmental Samples," EPA 600/8-80-038, June 1980;
- "Determination of 2,3,7,8-TCDD in Soil and Sediment" EPA, Region VII, Kansas City, September 1983;
- Organic Analysis: Multi-media, Multi Concentration-IFB WA84-A267; and
- Dioxin Analysis: Soil/Sediment Matrix; Multi-Concentration; Selected Ion Monitoring with Jar Extraction Procedure-IFB WA84-A002

However, we have modified our protocols to provide a higher level of QA/QC than the guidelines require. For example, we analyze a higher than required number of quality control samples and we pay especially careful attention to the certification of the "reference standard" compounds we use in analysis. Below are listed the key QA/QC elements for the methods we used.

### Analysis of Volatile Organic Compounds by Gas Chromatography/Mass Spectrometry

- Each batch of 13 samples consists of 9 customer samples (at a maximum), one blank sample, one spiked blank, one spiked sample and one replicate sample. This amounts to a 30% quality control factor.
- Three surrogate compounds are added to each sample in the batch of 13.
- A blind quality control sample is introduced to the laboratory for analysis on a weekly basis.
- Each GC/MS is checked and retuned, if necessary, at the beginning of each day to ensure that its performance on bromofluorobenzene (BFB) meets the EPA criteria.
- A calibration curve for quantitation is prepared using a mixture of Volatile Organic Priority Pollutant "standards" at a minimum of 3 different concentrations and using a mixture of 3 internal standards at a constant concentration.
- The calibration curve is verified with a mixture of priority pollutant standards every day. If the response factors vary greater than 25%, the instrument must be recalibrated.

### Analysis of Organic Compounds Extracted in Acid or Base/Neutral Solutions by Gas Chromatography/Mass Spectrometry

- Each batch of 20 samples consists of 16 customer samples (at a maximum), one blank sample, one spiked blank (for water matrices), one sample spiked with the priority pollutant standard mixture and a duplicate customer sample. This amounts to a 20% quality control factor.

**ETC**ENVIRONMENTAL  
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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

MS427 RESOURCE ENGINEERING

27514

IPC88-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	4600	8700 <sub>A</sub>	10200 <sub>A</sub>	ND	0	-	ND	20300	80
Aroclor 1254	ND	4600	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	4600	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	4600	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	4600	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	4600	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	4600	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### **Aroclors (PCB's by GC/ECD)**

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9425

RESOURCE ENGINEERING

27514

IPC89-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	1600	8700 <sup>a</sup>	10200 <sup>a</sup>	ND	0	-	ND	20300	80
Aroclor 1254	ND	1600	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1600	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1600	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1600	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1600	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1600	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

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The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

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### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9424 RESOURCE ENGINEERING

27514

IPCB9-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	1460	8700 <sup>a</sup>	10200 <sup>a</sup>	ND	0	-	ND	20300	80
Aroclor 1254	ND	1460	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1460	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1460	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1460	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1460	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1460	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.



## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### ***Aroclors (PCB's by GC/ECD)***

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9366

RESOURCE ENGINEERING

27514

IPCB9-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	7590	7170 <sup>a</sup>	8330 <sup>a</sup>	ND	0	-	35200 <sup>a</sup>	19700	113
Aroclor 1254	ND	7590	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	7590	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	7590	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	7590	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	7590	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	7590	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### **Aroclors (PCBs by GC/ECD)**

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

AUG 27, 1986

## TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

## Chain of Custody Data Required for ETC Data Management Summary Reports

M9367	RESOURCE ENGINEERING	27514	IPCB10-1	860716
ETC Sample No.	Company	Facility	Sample Point	Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	35800	2740	7170 <sup>a</sup>	8330 <sup>a</sup>	ND	0	-	35200 <sup>a</sup>	19700	113
Aroclor 1254	ND	2740	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2740	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2740	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2740	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2740	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2740	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

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The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

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## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9410

RESOURCE ENGINEERING

27514

IPCB10-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
Aroclor 1242	7570	3730	17700.	14200.	ND	0	-	ND	19400	85
Aroclor 1254	ND	3730	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3730	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3730	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3730	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3730	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3730	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

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### **Aroclors (PCB's by GC/ECD)**

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

## Methodology for GC Analysis of Polychlorinated Biphenyls

The method employed in the analysis of your sample for polychlorinated biphenyls is an established EPA method taken from "Test Methods for Evaluating Solid Waste", July 1982.

The method can be summarized as follows: A weighed amount of homogenized sample, approximately 30 grams, is soxhiet extracted for 16 hours with hexane. The extract is dried and concentrated to approximately 25 ml. A 5 ml aliquot of the concentrated extract is transferred to a silica gel column and eluted with hexane. The eluate is concentrated to a final volume of 5 ml and injected into a gas chromatograph equipped with an  $^{63}\text{Ni}$  electron capture detector.

The GC operating parameters were as follows:

### COLUMN

6' x 4 mm glass 1.5% SP-2250 & 1.95% SP-2401  
Supelcoport 100/120 mesh

### CARRIER FLOW

60 ml/min. Argon/Methane

### COLUMN OVEN

220° C

### INJECTOR TEMPERATURE

225° C

### DETECTOR TEMPERATURE

325° C

### DETECTOR

$\text{Ni}^{63}$  Electron Capture Detector

### CONFIRMATION COLUMN

6' x 4 mm glass 3% OV-1  
Supelcoport 100/120 mesh



**ETC**ENVIRONMENTAL  
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NOV 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N8923

RESOURCE ENGINEERING

27514

IPCB15-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	200000 <sup>a</sup>	1000	144000 <sup>a</sup>	132000 <sup>a</sup>	ND	0	-	30000 <sup>a</sup>	20000	12 <sup>a</sup>
Aroclor 1254	ND	1000	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1000	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1000	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1000	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1000	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1000	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

<sup>b</sup> Spiked samples that contain compounds present at high levels do not provide valid spike recovery data.

## Methodology for GC Analysis of Polychlorinated Biphenyls

The method employed in the analysis of your sample for polychlorinated biphenyls is an established EPA method taken from "Test Methods for Evaluating Solid Waste", July 1982.

The method can be summarized as follows: A weighed amount of homogenized sample, approximately 30 grams, is soxhlet extracted for 16 hours with hexane. The extract is dried and concentrated to approximately 25 ml. A 5 ml aliquot of the concentrated extract is transferred to a silica gel column and eluted with hexane. The eluate is concentrated to a final volume of 5 ml and injected into a gas chromatograph equipped with an  $^{63}\text{Ni}$  electron capture detector.

The GC operating parameters were as follows:

### COLUMN

6' x 4 mm glass 1.5% SP-2250 & 1.95% SP-2401  
Supelcoport 100/120 mesh

### CARRIER FLOW

60 ml/min. Argon/Methane

### COLUMN OVEN

220° C

### INJECTOR TEMPERATURE

225° C

### DETECTOR TEMPERATURE

325° C

### DETECTOR

$\text{Ni}^{63}$  Electron Capture Detector

### CONFIRMATION COLUMN

6' x 4 mm glass 3% OV-1  
Supelcoport 100/120 mesh

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

NOV 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N8926 RESOURCE ENGINEERING

27514

IPC812-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	151000.	4600	144000.	132000.	ND	0	-	30000.	20000	12.
Aroclor 1254	ND	4600	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	4600	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	4600	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	4600	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	4600	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	4600	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.

B Spiked samples that contain compounds present at high levels do not provide valid spike recovery data.

## Methodology for GC Analysis of Polychlorinated Biphenyls

The method employed in the analysis of your sample for polychlorinated biphenyls is an established EPA method taken from "Test Methods for Evaluating Solid Waste", July 1982.

The method can be summarized as follows: A weighed amount of homogenized sample, approximately 30 grams, is soxhlet extracted for 16 hours with hexane. The extract is dried and concentrated to approximately 25 ml. A 5 ml aliquot of the concentrated extract is transferred to a silica gel column and eluted with hexane. The eluate is concentrated to a final volume of 5 ml and injected into a gas chromatograph equipped with an  $^{63}\text{Ni}$  electron capture detector.

The GC operating parameters were as follows:

### COLUMN

6' x 4 mm glass 1.5% SP-2250 & 1.95% SP-2401  
Supelcoport 100/120 mesh

### CARRIER FLOW

60 ml/min. Argon/Methane

### COLUMN OVEN

220° C

### INJECTOR TEMPERATURE

225° C

### DETECTOR TEMPERATURE

325° C

### DETECTOR

$\text{Ni}^{63}$  Electron Capture Detector

### CONFIRMATION COLUMN

6' x 4 mm glass 3% OV-1  
Supelcoport 100/120 mesh

NOV 1, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

N8928 RESOURCE ENGINEERING

27514

IPCB12-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	144000 <sup>a</sup>	3600	144000 <sup>a</sup>	132000 <sup>a</sup>	ND	0	-	30000 <sup>a</sup>	20000	12 <sup>a</sup>
Aroclor 1254	ND	3600	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3600	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3600	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3600	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3600	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3600	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.<sup>b</sup> Spiked samples that contain compounds present at high levels do not provide valid spike recovery data.

## Methodology for GC Analysis of Polychlorinated Biphenyls

The method employed in the analysis of your sample for polychlorinated biphenyls is an established EPA method taken from "Test Methods for Evaluating Solid Waste", July 1982.

The method can be summarized as follows: A weighed amount of homogenized sample, approximately 30 grams, is soxhlet extracted for 16 hours with hexane. The extract is dried and concentrated to approximately 25 ml. A 5 ml aliquot of the concentrated extract is transferred to a silica gel column and eluted with hexane. The eluate is concentrated to a final volume of 5 ml and injected into a gas chromatograph equipped with an  $^{63}\text{Ni}$  electron capture detector.

The GC operating parameters were as follows:

### COLUMN

6' x 4 mm glass 1.5% SP-2250 & 1.95% SP-2401  
Supelcoport 100/120 mesh

### CARRIER FLOW

60 ml/min. Argon/Methane

### COLUMN OVEN

220° C

### INJECTOR TEMPERATURE

225° C

### DETECTOR TEMPERATURE

325° C

### DETECTOR

$\text{Ni}^{63}$  Electron Capture Detector

### CONFIRMATION COLUMN

6' x 4 mm glass 3% OV-1  
Supelcoport 100/120 mesh

NOV 4, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

N8925 RESOURCE ENGINEERING 27514 IPCB12-1 860716

ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	471000 <sup>a</sup>	2800	144000 <sup>a</sup>	132000 <sup>a</sup>	ND	0	-	30000 <sup>a</sup>	20000	12 <sup>a</sup>
Aroclor 1254	ND	2800	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2800	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2800	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2800	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2800	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2800	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.<sup>b</sup> Spiked samples that contain compounds present at high levels do not provide valid spike recovery data.

## Methodology for GC Analysis of Polychlorinated Biphenyls

The method employed in the analysis of your sample for polychlorinated biphenyls is an established EPA method taken from "Test Methods for Evaluating Solid Waste", July 1982.

The method can be summarized as follows: A weighed amount of homogenized sample, approximately 30 grams, is soxhlet extracted for 16 hours with hexane. The extract is dried and concentrated to approximately 25 ml. A 5 ml aliquot of the concentrated extract is transferred to a silica gel column and eluted with hexane. The eluate is concentrated to a final volume of 5 ml and injected into a gas chromatograph equipped with an  $^{63}\text{Ni}$  electron capture detector.

The GC operating parameters were as follows:

### COLUMN

6' x 4 mm glass 1.5% SP-2250 & 1.95% SP-2401  
Supelcoport 100/120 mesh

### CARRIER FLOW

60 ml/min. Argon/Methane

### COLUMN OVEN

220° C

### INJECTOR TEMPERATURE

225° C

### DETECTOR TEMPERATURE

325° C

### DETECTOR

$\text{Ni}^{63}$  Electron Capture Detector

### CONFIRMATION COLUMN

6' x 4 mm glass 3% OV-1  
Supelcoport 100/120 mesh



NOV 1, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**

**Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports									
N8929	RESOURCE ENGINEERING	27514	IPC89-2	860716					
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours			

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	31000	1800	144000	132000	ND	0	-	30000	20000	12
Aroclor 1254	ND	1800	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1800	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1800	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1800	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1800	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1800	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.

B Spiked samples that contain compounds present at high levels do not provide valid spike recovery data.

## Methodology for GC Analysis of Polychlorinated Biphenyls

The method employed in the analysis of your sample for polychlorinated biphenyls is an established EPA method taken from "Test Methods for Evaluating Solid Waste", July 1982.

The method can be summarized as follows: A weighed amount of homogenized sample, approximately 30 grams, is soxhlet extracted for 16 hours with hexane. The extract is dried and concentrated to approximately 25 ml. A 5 ml aliquot of the concentrated extract is transferred to a silica gel column and eluted with hexane. The eluate is concentrated to a final volume of 5 ml and injected into a gas chromatograph equipped with an <sup>63</sup>Ni electron capture detector.

The GC operating parameters were as follows:

### COLUMN

6' x 4 mm glass 1.5% SP-2250 & 1.95% SP-2401  
Supelcoport 100/120 mesh

### CARRIER FLOW

60 ml/min. Argon/Methane

### COLUMN OVEN

220° C

### INJECTOR TEMPERATURE

225° C

### DETECTOR TEMPERATURE

325° C

### DETECTOR

Ni<sup>63</sup> Electron Capture Detector

### CONFIRMATION COLUMN

6' x 4 mm glass 3% OV-1  
Supelcoport 100/120 mesh

NOV 4, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

N8927 RESOURCE ENGINEERING

27514

IPCB1-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	353000.	2740	144000.	132000.	ND	0	-	30000.	20000	12.
Aroclor 1254	ND	2740	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2740	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2740	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2740	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2740	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2740	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.  
 B Spiked samples that contain compounds present at high levels do not provide valid spike recovery data.

## Methodology for GC Analysis of Polychlorinated Biphenyls

The method employed in the analysis of your sample for polychlorinated biphenyls is an established EPA method taken from "Test Methods for Evaluating Solid Waste", July 1982.

The method can be summarized as follows: A weighed amount of homogenized sample, approximately 30 grams, is soxhlet extracted for 16 hours with hexane. The extract is dried and concentrated to approximately 25 ml. A 5 ml aliquot of the concentrated extract is transferred to a silica gel column and eluted with hexane. The eluate is concentrated to a final volume of 5 ml and injected into a gas chromatograph equipped with an  $^{63}\text{Ni}$  electron capture detector.

The GC operating parameters were as follows:

### COLUMN

6' x 4 mm glass 1.5% SP-2250 & 1.95% SP-2401  
Supelcoport 100/120 mesh

### CARRIER FLOW

60 ml/min. Argon/Methane

### COLUMN OVEN

220° C

### INJECTOR TEMPERATURE

225° C

### DETECTOR TEMPERATURE

325° C

### DETECTOR

$\text{Ni}^{63}$  Electron Capture Detector

### CONFIRMATION COLUMN

6' x 4 mm glass 3% OV-1  
Supelcoport 100/120 mesh

NOV 4 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA									
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### Aroclors – GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports						
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours
N8924	RESOURCE ENGINEERING	27514	IPCBI-1	860716		

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	277000 <sup>a</sup>	2100	144000 <sup>a</sup>	132000 <sup>a</sup>	ND	0	-	30000 <sup>a</sup>	20000	12 <sup>a</sup>
Aroclor 1254	ND	2100	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2100	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2100	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2100	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2100	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2100	ND	ND	ND	0	-	ND	0	-
<sup>a</sup> Identification confirmed by second column analysis. <sup>b</sup> Spiked samples that contain compounds present at high levels do not provide valid spike recovery data.										

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9428

RESOURCE ENGINEERING

27514

IPGB22-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	1010	6670.	10800.	ND	0	-	8760.	27400	123
Aroclor 1254	ND	1010	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1010	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1010	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1010	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1010	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1010	ND	ND	ND	0	-	ND	0	-

\* Identification confirmed by second column analysis.

## Introduction

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## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### ***Aroclors (PCB's by GC/ECD)***

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).



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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9429 RESOURCE ENGINEERING 27514 IPCB22-1 860716

ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	2880	1040	6670 <sup>a</sup>	10800 <sup>a</sup>	ND	0	-	8760 <sup>a</sup>	27400	123
Aroclor 1254	ND	1040	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1040	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1040	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1040	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1040	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1040	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

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### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9396

RESOURCE ENGINEERING

27514

IPCB21-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov.	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov.
Aroclor 1242	ND	1300	8700.	10200.	ND	0	-	ND	20300	80
Aroclor 1254	ND	1300	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1300	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1300	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1300	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1300	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1300	ND	ND	ND	0	-	ND	0	-

a Identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

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## Results

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### **Aroclors (PCB's by GC/ECD)**

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).



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TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9395 RESOURCE ENGINEERING 27514 IPCB21-2 860716

ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	1300	8700 <sup>a</sup>	10200 <sup>a</sup>	ND	0	-	ND	20300	80
Aroclor 1254	ND	1300	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1300	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1300	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1300	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1300	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1300	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

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The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

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## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

**ETC**ENVIRONMENTAL  
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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9394 RESOURCE ENGINEERING

27514

IPCB21-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	2200	8700a	10200a	ND	0	-	ND	20300	80
Aroclor 1254	ND	2200	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2200	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2200	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2200	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2200	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2200	ND	ND	ND	0	-	ND	0	-

a Identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

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### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).





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TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9397 RESOURCE ENGINEERING 27514 IPCB20-3 860716

ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	13100	800	8700	10200	ND	0	-	ND	20300	80
Aroclor 1254	ND	800	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	800	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	800	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	800	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	800	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	800	ND	ND	ND	0	-	ND	0	-

A identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

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### **Aroclors (PCB's by GC/ECD)**

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

**ETC**ENVIRONMENTAL  
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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9389 RESOURCE ENGINEERING

27514

IPCB20-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	12300	890	8700 <sup>a</sup>	10200 <sup>a</sup>	ND	0	-	ND	20300	80
Aroclor 1254	ND	890	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	890	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	890	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	890	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	890	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	890	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

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## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as HMDL (Below Method Detection Limit).



ENVIRONMENTAL  
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TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports					
M9388	RESOURCE ENGINEERING	27514	IPCB20-1	860716	
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	10580	1080	8700	10200	ND	0	-	ND	20300	80
Aroclor 1254	ND	1080	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1080	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1080	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1080	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1080	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1080	ND	ND	ND	0	-	ND	0	-

A identification confirmed by second column analysis.

## Introduction

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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9405	RESOURCE ENGINEERING	27514	IPCB19-2	860716
ETC Sample No.	Company	Facility	Sample Point	Date
			Time	Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov.	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov.
Aroclor 1242	38500	2780	6670a	10800a	ND	0	-	8760a	27400	123
Aroclor 1254	ND	2780	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2780	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2780	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2780	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2780	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2780	ND	ND	ND	0	-	ND	0	-

a Identification confirmed by second column analysis.

## Introduction

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### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).



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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9404 RESOURCE ENGINEERING

27514

IPC819-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov.	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov.
Aroclor 1242	8960	2280	6670 <sup>a</sup>	10800 <sup>a</sup>	ND	0	-	8760 <sup>a</sup>	27400	123
Aroclor 1254	ND	2280	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2280	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2280	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2280	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2280	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2280	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

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### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9418 RESOURCE ENGINEERING

27514

IPC818-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concn. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concn. Added ug/kg	% Recov
Aroclor 1242	41600	10600	6670.	10800.	ND	0	-	8760.	27400	123
Aroclor 1254	ND	10600	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	10600	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	10600	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	10600	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	10600	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	10600	ND	ND	ND	0	-	ND	0	-

\* Identification confirmed by second column analysis.

## Introduction

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## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### *Aroclors (PCB's by GC/ECD)*

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as PMDL (Below Method Detection Limit).

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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9419 RESOURCE ENGINEERING

27514

IPCB18-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	34400	17500	6670 <sup>a</sup>	10800 <sup>a</sup>	ND	0	-	8760 <sup>a</sup>	27400	123
Aroclor 1254	ND	17500	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	17500	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	17500	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	17500	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	17500	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	17500	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

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### **Aroclors (PCB's by GC/ECD)**

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9384 RESOURCE ENGINEERING

27514

IPC817-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	1900	8700.	10200.	ND	0	-	ND	20300	80
Aroclor 1254	ND	1900	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1900	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1900	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1900	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1900	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1900	ND	ND	ND	0	-	ND	0	-

R Identification confirmed by second column analysis.

## Introduction

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AUG 29, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9402 RESOURCE ENGINEERING

27514

IPCB17-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	3460	1920	6670.	10800.	ND	0	-	8760.	27400	123
Aroclor 1254	ND	1920	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1920	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1920	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1920	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1920	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1920	ND	ND	ND	0	-	ND	0	-

\* Identification confirmed by second column analysis.

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TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9385 RESOURCE ENGINEERING 27514 IPCB17-1 860716

ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	9450	2300	8700.	10200.	ND	0	-	ND	20300	80
Aroclor 1254	ND	2300	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2300	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2300	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2300	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2300	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2300	ND	ND	ND	0	-	ND	0	-

A identification confirmed by second column analysis.

## Introduction

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TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9381 RESOURCE ENGINEERING

27514

1PCB16-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	8700	2080	8700.	10200.	ND	0	-	ND	20300	80
Aroclor 1254	ND	2080	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2080	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2080	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2080	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2080	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2080	ND	ND	ND	0	-	ND	0	-

\* Identification confirmed by second column analysis.

## Introduction

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**ETC**ENVIRONMENTAL  
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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9380 RESOURCE ENGINEERING 27514 IPCB16-2 860716

ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	3420	2600	8700	10200	ND	0	-	ND	20300	80
Aroclor 1254	ND	2600	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2600	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2600	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2600	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2600	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2600	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

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### *Aroclors (PCB's by GC/ECD)*

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**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9414 RESOURCE ENGINEERING

27514

IPCB16-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	21400	3260	6670.	10800.	ND	0	-	8760.	27400	123
Aroclor 1254	ND	3260	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3260	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3260	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3260	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3260	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3260	ND	ND	ND	0	-	ND	0	-

R Identification confirmed by second column analysis.

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**ETC**ENVIRONMENTAL  
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AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9415

RESOURCE ENGINEERING

27514

IPCB15-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	98600	10300	6670 <sup>a</sup>	10800 <sup>a</sup>	ND	0	-	8760 <sup>a</sup>	27400	123
Aroclor 1254	ND	10300	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	10300	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	10300	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	10300	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	10300	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	10300	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

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**ETC**ENVIRONMENTAL  
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**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9409 RESOURCE ENGINEERING

27514

IPC814-3

860719

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	13500	1780	6670.	10800.	ND	0	-	8760.	27400	123
Aroclor 1254	ND	1780	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	1780	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	1780	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	1780	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	1780	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	1780	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.

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**ETC**ENVIRONMENTAL  
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AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9421

RESOURCE ENGINEERING

27514

IPCBI4-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	40300	28500	6670.	10800.	ND	0	-	8760.	27400	123
Aroclor 1254	ND	28500	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	28500	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	28500	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	28500	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	28500	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	28500	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.

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### ***Aroclors (PCB's by GC/ECD)***

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**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9420 RESOURCE ENGINEERING

27514

IPCB14-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	41400	15000	6670.	10800.	ND	0	-	8760.	27400	123
Aroclor 1254	ND	15000	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	15000	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	15000	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	15000	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	15000	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	15000	ND	ND	ND	0	-	ND	0	-

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AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**

**Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports									
M9408	RESOURCE ENGINEERING	27514	IPCB13-3	860716					
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours			

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	6670	5970	6670	10800	ND	0	-	8760	27400	123
Aroclor 1254	ND	5970	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	5970	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	5970	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	5970	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	5970	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	5970	ND	ND	ND	0	-	ND	0	-

\* Identification confirmed by second column analysis.

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AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**

**Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports									
M9431	RESOURCE ENGINEERING	27514	IPC813-2	860716					
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours			

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	3600	8700.	10200.	ND	0	-	ND	20300	80
Aroclor 1254	ND	3600	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3600	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3600	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3600	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3600	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3600	ND	ND	ND	0	-	ND	0	-

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**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9430 RESOURCE ENGINEERING

27514

IPCB13-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	19300	2120	8700	10200	ND	0	-	ND	20300	80
Aroclor 1254	ND	2120	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2120	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2120	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2120	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2120	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2120	ND	ND	ND	0	-	ND	0	-

R Identification confirmed by second column analysis.

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**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9369

RESOURCE ENGINEERING

27514

IPC812-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	244000 <sup>a</sup>	4770	7170 <sup>a</sup>	8330 <sup>a</sup>	ND	0	-	35200 <sup>a</sup>	19700	113
Aroclor 1254	ND	4770	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	4770	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	4770	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	4770	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	4770	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	4770	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

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AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9368

RESOURCE ENGINEERING

27514

IPCB12-2

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	693000.	3320	7170.	8330.	ND	0	-	35200.	19700	113
Aroclor 1254	ND	3320	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3320	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3320	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3320	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3320	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3320	ND	ND	ND	0	-	ND	0	-

A identification confirmed by second column analysis.

## Introduction

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### ***Aroclors (PCB's by GC/ECD)***

Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9417 RESOURCE ENGINEERING

27514

IPCB12-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	243000.	2010	17700.	14200.	ND	0	-	ND	19400	85
Aroclor 1254	ND	2010	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2010	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2010	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2010	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2010	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2010	ND	ND	ND	0	-	ND	0	-

R Identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

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Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual mixture. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9416 RESOURCE ENGINEERING

27514

IPCB11-3

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	15200	3130	17700	14200	ND	0	-	ND	19400	85
Aroclor 1254	ND	3130	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3130	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3130	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3130	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3130	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3130	ND	ND	ND	0	-	ND	0	-

A identification confirmed by second column analysis.

## Introduction

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ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

Aroclors - GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9379 RESOURCE ENGINEERING 27514 IPCB11-2 860716

ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	ND	4230	7170.	8330.	ND	0	-	35200.	19700	113
Aroclor 1254	ND	4230	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	4230	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	4230	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	4230	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	4230	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	4230	ND	ND	ND	0	-	ND	0	-

A Identification confirmed by second column analysis.

## Introduction

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**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 27, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Aroclors - GC Analysis Data (QR14)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9378

RESOURCE ENGINEERING

27514

IPC811-1

860716

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	7170	2810	7170 <sup>a</sup>	8330 <sup>a</sup>	ND	0	-	35200 <sup>a</sup>	19700	113
Aroclor 1254	ND	2810	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	2810	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	2810	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	2810	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	2810	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	2810	ND	ND	ND	0	-	ND	0	-

<sup>a</sup> Identification confirmed by second column analysis.

## Introduction

This report contains the analytical results on your sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

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Aroclor mixtures analyzed by gas chromatographic methods are reported with a blank, spiked blank, matrix spike and replicate. The method detection limit (MDL) is determined for each individual matrix. When a particular Aroclor mixture is determined to be present at concentrations less than the calculated MDL it is reported as BMDL (Below Method Detection Limit).

AUG 27, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA									
Parameter	Sample A (n=10)			Sample B (n=10)			Sample C (n=10)		
	Mean	Stdev	CV (%)	Mean	Stdev	CV (%)	Mean	Stdev	CV (%)
Parameter 1	12.5	0.5	4.0	15.2	0.8	5.3	18.7	1.2	6.4
Parameter 2	8.3	0.3	3.6	9.1	0.4	4.4	10.5	0.6	5.7
Parameter 3	22.1	1.1	5.0	20.8	0.9	4.3	23.4	1.3	5.6
Parameter 4	5.7	0.2	3.5	6.2	0.3	4.8	7.0	0.4	5.7
Parameter 5	19.4	0.9	4.6	17.9	0.7	3.9	20.1	1.0	5.0
Parameter 6	3.1	0.1	3.2	3.5	0.2	5.7	4.2	0.3	7.1
Parameter 7	14.6	0.7	4.8	13.2	0.6	4.5	15.8	0.8	5.1
Parameter 8	7.8	0.4	5.1	8.5	0.5	5.9	9.2	0.6	6.7
Parameter 9	25.3	1.3	5.1	24.1	1.1	4.6	26.7	1.5	5.6
Parameter 10	4.9	0.2	4.1	5.3	0.3	5.7	6.1	0.4	6.6

### Aroclors – GC Analysis Data (QR14)

Chain of Custody Data Required for ETC Data Management Summary Reports						
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours
M9411	RESOURCE ENGINEERING	27514	IPCB10-3	860716		

Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
	Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
Aroclor 1242	17700 <sup>a</sup>	3130	17700 <sup>a</sup>	14200 <sup>a</sup>	ND	0	-	ND	19400	85
Aroclor 1254	ND	3130	ND	ND	ND	0	-	ND	0	-
Aroclor 1260	ND	3130	ND	ND	ND	0	-	ND	0	-
Aroclor 1248	ND	3130	ND	ND	ND	0	-	ND	0	-
Aroclor 1232	ND	3130	ND	ND	ND	0	-	ND	0	-
Aroclor 1221	ND	3130	ND	ND	ND	0	-	ND	0	-
Aroclor 1016	ND	3130	ND	ND	ND	0	-	ND	0	-
<sup>a</sup> Identification confirmed by second column analysis.										

Appendix 3

PCB Analytical Results - Rocky Mountain

## SAMPLE DESCRIPTION INFORMATION

for

Resource Engineering ERT

<u>RMA Sample No.</u>	<u>Sample Description</u>	<u>Sample Type</u>	<u>Date Sampled</u>	<u>Date Received</u>
61783-01	1-1	Sludge	07/16/86	07/19/86
61783-02	2-2	Sludge	07/16/86	07/19/86
61783-03	3-3	Sludge	07/16/86	07/19/86
61783-04	4-1	Sludge	07/16/86	07/19/86
61783-05	7-2	Sludge	07/16/86	07/19/86
61783-06	9-2	Sludge	07/16/86	07/19/86
61783-07	11-2	Sludge	07/16/86	07/19/86
61783-08	13-2	Sludge	07/16/86	07/19/86
61783-09	17-2	Sludge	07/16/86	07/19/86
61783-10	20-1	Sludge	07/16/86	07/19/86

August 27, 1986

## ANALYTICAL RESULTS

for

Resource Engineering ERT

## PCBs

<u>Parameter</u>	<u>Units</u>	<u>61783-01</u>		<u>61783-02</u>		<u>61783-03</u>		<u>61783-04</u>	
Aroclor 1016	mg/Kg	ND	(3.2)	ND	(1.6)	ND	(0.16)	ND	(3.2)
Aroclor 1221	mg/Kg	ND	(3.2)	ND	(1.6)	ND	(0.16)	ND	(3.2)
Aroclor 1232	mg/Kg	ND	(3.2)	ND	(1.6)	ND	(0.16)	ND	(3.2)
Aroclor 1242	mg/Kg	64	(3.2)	28	(1.6)	3.2	(0.16)	57	(3.2)
Aroclor 1248	mg/Kg	ND	(3.2)	ND	(1.6)	ND	(0.16)	ND	(3.2)
Aroclor 1254	mg/Kg	ND	(20)	ND	(10)	ND	(1)	ND	(20)
Aroclor 1260	mg/Kg	ND	(20)	ND	(10)	ND	(1)	ND	(20)

<u>Parameter</u>	<u>Units</u>	<u>61783-05</u>		<u>61783-06</u>		<u>61783-07</u>		<u>61783-08</u>	
Aroclor 1016	mg/Kg	ND	(0.16)	ND	(1.6)	ND	(0.16)	ND	(1.6)
Aroclor 1221	mg/Kg	ND	(0.16)	ND	(1.6)	ND	(0.16)	ND	(1.6)
Aroclor 1232	mg/Kg	ND	(0.16)	ND	(1.6)	ND	(0.16)	ND	(1.6)
Aroclor 1242	mg/Kg	9.0	(0.16)	34	(1.6)	2.3	(0.16)	32	(1.6)
Aroclor 1248	mg/Kg	ND	(0.16)	ND	(1.6)	ND	(0.16)	ND	(1.6)
Aroclor 1254	mg/Kg	ND	(1)	ND	(10)	ND	(1)	ND	(10)
Aroclor 1260	mg/Kg	ND	(1)	ND	(10)	ND	(1)	ND	(10)

<u>Parameter</u>	<u>Units</u>	<u>61783-09</u>		<u>61783-10</u>	
Aroclor 1016	mg/Kg	ND	(0.16)	ND	(1.6)
Aroclor 1221	mg/Kg	ND	(0.16)	ND	(1.6)
Aroclor 1232	mg/Kg	ND	(0.16)	ND	(1.6)
Aroclor 1242	mg/Kg	2.0	(0.16)	5.1	(1.6)
Aroclor 1248	mg/Kg	ND	(0.16)	ND	(1.6)
Aroclor 1254	mg/Kg	ND	(1)	ND	(10)
Aroclor 1260	mg/Kg	ND	(1)	ND	(10)

ND = Not detected.

Detection limits in parentheses.



Appendix 4

PCB Analytical Results - Radian

REI ERT DATA PACKAGE

Radian Analytical Services, Sacramento

Laboratory I.D.# S6-07-044

This data package consists of the following support documentation:

1. Chain of Custody Record (External)
2. Chain of Custody Record (Internal, also see Ext./Inst. log pages)
3. Homogenization Procedure Summary
4. Extraction Logbook Page
5. Instrument Logbook Page
6. Method Blank, Standard, and Sample Chromatograms  
(Quantitation and Confirmation Columns)

# RESOURCE ENGINEERING - ANALYSIS REQUEST AND CHAIN OF CUSTODY RECORD

PROJECT NO. <b>275-14</b>		PROJECT NAME <b>French Limited</b>					LOCATION <b>Crosby, Texas</b>					
FIELD SAMPLE NUMBER	DATE	TIME	GRAB	COMP.	SAMPLE CONTAINER (SIZE/MAT'L)	SAMPLE TYPE (LIQUID, SLUDGE, ETC.)	PRESERVATIVE	ANALYSIS REQUESTED		COMMENTS AND HOLD STORAGE DATE		
PCB-1-1	7/16/86	PM	✓		500 ml glass jar	Sludge	4°C	PCB OK		None		
PCB-2-2	7/16/86	PM	✓		500 ml glass jar	Sludge	4°C	PCB OK		None		
PCB-3-3	7/16/86	PM	✓		500 ml glass jar	Sludge	4°C	PCB OK		None		
PCB-4-1	7/16/86	PM	✓		500 ml glass jar	Sludge	4°C	PCB OK		None		
PCB-7-2	7/16/86	PM	✓		500 ml glass jar	Sludge	4°C	PCB OK		None		
PCB-9-2	7/16/86	PM	✓		500 ml glass jar	Sludge	4°C	PCB OK		None		
PCB-11-2	7/16/86	PM	✓		500 ml glass jar	Sludge	4°C	PCB OK		None		
PCB-13-2	7/16/86	PM	✓		500 ml glass jar	Sludge	4°C	PCB OK		None		
PCB-17-2	7/16/86	PM	✓		500 ml glass jar	Sludge	4°C	PCB OK		None		
LAB SAMPLE NO.		REMARKS <b>See Enclosed Instructions</b>							SAMPLER SIGNATURE <b>WJ Beck</b>			
RELINQUISHED BY (SIGNATURE) <b>WJ Beck</b>		DATE <b>7/18/86</b>	TIME <b>5 PM</b>	RECEIVED BY (SIGNATURE) <b>W Brown</b>		DATE <b>7/29/86</b>		RELINQUISHED BY (SIGNATURE)		DATE	TIME	RECEIVED BY (SIGNATURE)
RELINQUISHED BY (SIGNATURE)		DATE	TIME	RECEIVED BY (SIGNATURE)		RELINQUISHED BY (SIGNATURE)		DATE	TIME	RECEIVED BY (SIGNATURE)		
RELINQUISHED BY (SIGNATURE)		DATE	TIME	RECEIVED BY (SIGNATURE)		RELINQUISHED BY (SIGNATURE)		DATE	TIME	RECEIVED BY (SIGNATURE)		

# RESOURCE ENGINEERING - ANALYSIS REQUEST AND CHAIN OF CUSTODY RECORD

PROJECT NO. <b>275-14</b>		PROJECT NAME <b>French Limited</b>				LOCATION <b>Crosby, Texas</b>						
FIELD SAMPLE NUMBER	DATE	TIME	GRAB	COMP.	SAMPLE CONTAINER (SIZE/MAT'L)	SAMPLE TYPE (LIQUID SLUDGE, ETC.)	PRESERVATIVE	ANALYSIS REQUESTED	COMMENTS AND HOLD STORAGE DATE			
PCB-20-1	7/16/86	PM	✓		500 ml glass jar	sludge	4°C	PCB OL	None			
LAB SAMPLE NO.		REMARKS <b>See Enclosed Instructions</b>							SAMPLER SIGNATURE <b>W. Beck</b>			
RELINQUISHED BY (SIGNATURE) <b>W. Beck</b>		DATE <b>7/18/86</b>	TIME <b>5 PM</b>	RECEIVED BY (SIGNATURE) <b>W. Brown</b>		DATE <b>7/20/86</b>		RELINQUISHED BY (SIGNATURE)		DATE	TIME	RECEIVED BY (SIGNATURE)
RELINQUISHED BY (SIGNATURE)		DATE	TIME	RECEIVED BY (SIGNATURE)		RELINQUISHED BY (SIGNATURE)		DATE	TIME	RECEIVED BY (SIGNATURE)		
RELINQUISHED BY (SIGNATURE)		DATE	TIME	RECEIVED BY (SIGNATURE)		RELINQUISHED BY (SIGNATURE)		DATE	TIME	RECEIVED BY (SIGNATURE)		

PROJECT NO.

PAGE 1  
 RCVD: 07/20/86 DUE: 08/03/86  
 RAS Sacramento  
 07/21/86 09:17:07  
 (Internal)  
 CHAIN OF CUSTODY  
 ORD # S6-07-044  
 KEEP: 10/02/86 DISP: D

DASH	SAMPLE IDENTIFICATION	STORED	TESTS
01A	PCB-1-1 Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
02A	PCB-2-2 Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
03A	PCB-3-3 Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
04A	PCB-4-1 Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
05A	PCB-7-2 Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
06A	PCB-9-2 Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
07A	PCB-11-2 Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
08A	PCB-13-2 Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
09A	PCB-17-2 Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
10A	PCB-20-1 Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
11A	Matrix Spike Soil	sac:refrig	BOBOPB DRY_WT EX_PCB
12A	Duplicate Analysis	sac:refrig	BOBOPB DRY_WT EX_PCB
13A	Reagent Blank	sac:refrig	BOBOPB DRY_WT EX_PCB

RELEASED BY	DATE
Wanda Brown	7/19/86
WALK-IN PD	7/22/86
Extractions PL	7/24-25/86
extracts refrigerator LC	7/31+8/1/86
concentrations PL	7/31+8/1/86

TRANSFERRED TO	DATE
Walk-in	7/19/86
EXTRACTIONS P.D.	7/22/86
Concentrations PL	7/24-25/86
Silica Gel Cleanup LC	7/31+8/1/86
extracts freezer PL	7/31+8/1/86

RECEIVED BY	DATE
RETURNED TO walk-in P.D.	7/22/86
extracts refrigerator PL	7/24-25/86
concentrations PL	7/31/86+8/1/86

## LABORATORY NARRATIVE LOG

CASE NUMBER: REI-ERT

SAM NUMBER: 5607044

[illegible]

# SOIL EXTRACTION LOG

Client	SAM # 84-	ID Code	Frac #	Ext Type	Ext Date/ Analyst	Sample Vol	(mL) Final Vol	Dry WT	pH	Location (Box #)	Conc Date Analyst
REI-ERT	5607044	PCB 1-1	1A <sup>H</sup>	PCB	7/23 P.D.	29.73g	25.0mL	0.41		8	7/31 PL
		PCB 2-2	2A <sup>H</sup>			30.48g		0.21			8/1 PL
		PCB 3-3	3A <sup>H</sup>			31.27g		0.53			8/1 PL
		PCB 4-1	4A <sup>H</sup>			30.13g		0.37			8/1 PL
		PCB 7-2	5A <sup>H</sup>		↓	30.10g		0.36			7/31 PL
		PCB 9-2	6A <sup>H</sup>		7/24 P.D.	29.41g		0.45			8/1 PL
		PCB 11-2	7A <sup>H</sup>			29.59g		0.20			7/31 PL
		PCB 13-2	8A <sup>H</sup>			30.04g		0.20			7/31 PL
		PCB 17-2	9A <sup>H</sup>			29.52g		0.40			8/1 PL
		PCB 20-1	10A <sup>H</sup>		↓	29.75g		0.40			7/31 PL
		MS OF 2A	11A <sup>H</sup>		P.D. 7/23	30.31g		0.21			8/1 PL
		DUP OF 7A	12A <sup>H</sup>			30.37g		0.20			7/31 PL
		REAGENT BLANK	13A <sup>H</sup>			—		—			8/1 PL
↓	✓	CB0725 PCB 000	14A <sup>H</sup>	✓	✓	—	↓	—	/	↓	8/1 PL

Solvent Type/Volume/Lot #: Hexane / 350 mL / AN991

Surrogate Spike: \_\_\_\_\_

Matrix Spike: 600 mL OF 86-18

Notebook Reference: \_\_\_\_\_

Lab Narrative Attached: No ☐ Yes ☒

Comments: Concentrate in Hexane to 25 mL of this taken thru Silica Gel Cleanup → Final Vol. 5 mLs.)

NOTE: THAT THIS GROUP IS DISTINGUISHED FROM THE Hexane: Acetone FRACTIONS BY THE LETTER 'H'.

TLE REI/ERT PCB<sub>2</sub>

Book No. \_\_\_\_\_

From Page No. _____	Vol.	Sample or	Concentration	Amount	Comments
File #	Inj.	Standard I.D.			
Columns (1-1)(M8)	1.5% SP-2250	1.95% SP-240	(1-2)(SP)	3% SP-2100	6'x2mm I.D. glass
N <sub>2</sub> flows (1-1)(MP)	26 ml/min	(1-2)(SP)	28 ml/min	Temp.	Columns 192°C Isothermal
Injector	20°C	Detectors	300°C (ECD)	Range = 10	Intg. see back
1/2-60906-01	1/2 ul	12623-20AAR <sup>1221</sup> <sub>1254</sub> ②	1000 ng/ml	RY	REI/ERT PCB <sub>2</sub>
02		12623-17AAR <sub>1232</sub> ②	1000 ng/ml		
03		12623-19AAR <sub>1248</sub> ②	500 ng/ml		
04		12623-16BAR <sup>1016</sup> <sub>1260</sub> ③	125 <sup>250</sup> ng/ml		
05		Hexane Rinse			
06		12623-16AAR <sup>1016</sup> <sub>1260</sub> ②	500/1000 ng/ml		
07		Hexane Rinse			
08		12623-16AAR <sup>1016</sup> <sub>1260</sub> ①	2500/5000 ng/ml		
09		Hexane Rinse			
10		12623-18BAR <sub>1242</sub> ③	125 ng/ml		
11		12623-18AAR <sub>1242</sub> ②	500 ng/ml		
12		12623-18AAR <sub>1242</sub> ①	2500 ng/ml		
13		8607044-1A	29.73g → 25.0ml	1:200	
14		8607044-2A	30.48g → 25.0ml	1:20	
15		8607044-3A	31.27g → 25.0ml	1:20	
16		8607044-4A	30.13g → 25.0ml	1:50	
17		8607044-5A	30.10g → 25.0ml	1:40	
18		8607044-6A	29.41g → 25.0ml	1:200	
19		8607044-7A	29.59g → 25.0ml	1:4	
20		8607044-8A	30.04g → 25.0ml	1:40	
21		8607044-9A	29.52g → 25.0ml	1:4	
22		12623-18AAR <sub>1242</sub> ②	500 ng/ml		
23		8607044-10A	29.75g → 25.0ml	1:40	
24		8607044-11A	30.31g → 25.0ml	1:25	
25		8607044-12A	30.37g → 25.0ml	1:4	
26		8607044-13A	→ 25.0ml		
27		CB0724 PCB000	→ 25.0ml		
28		8607044-2A-AH	30.23g → 25.0ml	1:40	
29		8607044-5A-AH	30.45g → 25.0ml	1:20	
30		12623-18AAR <sub>1242</sub> ②	500 ng/ml		
✓ 31	✓	8607044-12A	30.37g → 25.0ml	1:10	✓

To Page No. \_\_\_\_\_

Witnessed &amp; Understood by me,

Date

Invented by

Date

Recorded by



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RAS Sacramento  
09/08/86 11:18:31

REPORT

Work Order # S6-07-044

REPORT Resource Engineering, Inc.  
TO Tom Beck  
3000 Richmond Avenue  
Houston, Texas 77098  
ATTEN Mr. Chris Itin-REI/ERT

PREPARED Radian Analytical Services  
BY 8501 Mo-pac Bl.  
PO Box 9948  
Austin, TX 78751  
ATTEN  
PHONE 512-454-4797

*Lucas Petkovsek*  
CERTIFIED BY

CLIENT REI ERT  
COMPANY Radian Corporation  
FACILITY Resource Engineering, Inc.  
Houston, Texas

WORK ID Crosby, Texas, French Limited  
TAKEN 7/16/86  
TRANS Fed Ex 598437976  
TYPE Soil PCBs  
P.O. # 275-14  
INVOICE under separate cover

All results reported in ug/kg dry weight.  
Fraction -01B(Sample PCB-1-1) analyzed as crude extract(no  
clean-up) as per client request.

Previously Reported on 09/05/86.

CONTACT PETKOVSEK

### SAMPLE IDENTIFICATION

01 PCB-1-1 Soil  
01 PCB-1-1 Soil-Crude Extract  
02 PCB-2-2 Soil  
03 PCB-3-3 Soil  
04 PCB-4-1 Soil  
05 PCB-7-2 Soil  
06 PCB-9-2 Soil  
07 PCB-11-2 Soil  
08 PCB-13-2 Soil  
09 PCB-17-2 Soil  
10 PCB-20-1 Soil  
11 PCB-2-2 Matrix Spike Soil  
12 PCB-11-2 Duplicate Analus.  
13 Reagent Blank

### TEST CODES and NAMES used on this report

8080PB PCBs in soil  
DRY WT Dry weight determination  
EX PCB Extraction for PCB

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Results By Test

Work Order # S6-07-044

TEST CODE	Sample 01	Sample 02	Sample 03	Sample 04	Sample 05
default units	(entered units)	(entered units)	(entered units)	(entered units)	(entered units)
DRY_WT	59	79	47	63	64
% moisture					
EX_PCB	07/21/86	07/21/86	07/21/86	07/21/86	07/21/86
date completed					

TEST CODE	Sample 06	Sample 07	Sample 08	Sample 09	Sample 10
default units	(entered units)	(entered units)	(entered units)	(entered units)	(entered units)
DRY_WT	55	80	80	60	60
% moisture					
EX_PCB	07/21/86	07/21/86	07/21/86	07/21/86	07/21/86
date completed					

TEST CODE	Sample 11	Sample 12	Sample 13
default units	(entered units)	(entered units)	(entered units)
EX_PCB	no data	no data	no data
date completed			

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Results By Test

REPORT

Work Order # S6-07-044

SAMPLE		Test: DRY WT	Test: EX PCB
Sample Id		% moisture	date completed
01		59	07/21/86
PCB-1-1 Soil	02	79	07/21/86
PCB-2-2 Soil	03	47	07/21/86
PCB-3-3 Soil	04	63	07/21/86
PCB-4-1 Soil	05	64	07/21/86
PCB-7-2 Soil	06	55	07/21/86
PCB-9-2 Soil	07	80	07/21/86
PCB-11-2 Soil	08	80	07/21/86
PCB-13-2 Soil	09	60	07/21/86
PCB-17-2 Soil	10	60	07/21/86
PCB-20-1 Soil	11		no data
PCB-2-2 Matrix	12		no data
PCB-11-2 Duplic	13		no data
Reagent Blank			

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RAS Sacramento      REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-1-1 Soil</u>		SAMPLE # <u>01</u> FRACTIONS: <u>A</u>	
Date & Time Collected <u>07/16/86</u>		Category <u></u>	
DRY_WT <u>59</u>	EX_PCB <u>07/21/86</u>		
% moisture	date completed		

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RAS Sacramento REPORT  
Results by Sample

Work Order # 56-07-044

SAMPLE ID PCB-1-1 Soil

FRACTION 01A TEST CODE 8080PB NAME PCBs in soil

Date & Time Collected 07/16/86 Category

ORGANICS ANALYSIS DATA SHEET  
PESTICIDES

ANALYST RY  
INSTRMT 1

EXTRCTD 07/23/86  
INJECTD 08/06/86

FILE # 116080613

VERIFIED SCM

UNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>8200</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>16000</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>16000</u>
53469-21-9	PCB-1242	<u>360000</u>	<u>8200</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>8200</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>16000</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>16000</u>

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 RAS Sacramento REPORT  
 Results by Sample

Work Order # S6-07-044

 SAMPLE ID PCB-1-1 Soil-Crude Extract FRACTION Q1B TEST CODE 8080PB NAME PCBs in soil  
 Date & Time Collected 07/16/86 Category \_\_\_\_\_

 ORGANICS ANALYSIS DATA SHEET  
 PESTICIDES

 ANALYST RY  
 INSTRMT 1

 EXTRCTD 07/23/86  
 INJECTD 08/25/86

 FILE # 116082504

 VERIFIED LFM

 UNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>42000</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>83000</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>83000</u>
53469-21-9	PCB-1242	<u>400000</u>	<u>42000</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>42000</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>83000</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>83000</u>

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RAS Sacramento REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-2-2 Soil</u>		SAMPLE # <u>02</u> FRACTIONS: <u>A</u>	
		Date & Time Collected <u>07/16/86</u>	Category _____
DRY_WT <u>79</u>	EX_PCB <u>07/21/86</u>		
% moisture	date completed		

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Results by Sample

Work Order # S6-07-044

SAMPLE ID PCB-2-2 Soil FRACTION 02A TEST CODE 8080PB NAME PCBs in soil  
Date & Time Collected 07/16/86 Category ORGANICS ANALYSIS DATA SHEET  
PESTICIDESANALYST RY EXTRACTD 07/23/86 FILE # 116080614 VERIFIED SCM  
INSTRMT 1 INJECTD 08/06/86 UNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>1600</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>3200</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>3200</u>
53469-21-9	PCB-1242	<u>38000</u>	<u>1600</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>1600</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>3200</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>3200</u>

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RAS Sacramento      REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-3-3 Soil</u>		SAMPLE # <u>03</u> FRACTIONS: <u>A</u>	
Date & Time Collected <u>07/16/86</u>		Category <u></u>	
DRY_WT <u>47</u>	EX_PCB <u>07/21/86</u>		
% moisture	date completed		

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RAS Sacramento REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID PCB-3-3 Soil FRACTION 03A TEST CODE 8080PB NAME PCBs in soil  
Date & Time Collected 07/16/86 Category

ORGANICS ANALYSIS DATA SHEET  
PESTICIDES

ANALYST RY  
INSTRMT 1

EXTRCTD 07/23/86  
INJECTD 08/06/86

FILE # 116080615

VERIFIED SCM

UNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>600</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>1200</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>1200</u>
53469-21-9	PCB-1242	<u>12000</u>	<u>600</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>600</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>1200</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>1200</u>

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RAS Sacramento      REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-4-1 Soil</u>		SAMPLE # <u>04</u> FRACTIONS: <u>A</u>	
Date & Time Collected <u>07/16/86</u>		Category _____	
DRY_WT <u>63</u>	EX <u>PCB</u>	<u>07/21/86</u>	
% moisture	date completed		

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Results by Sample

Work Order # S6-07-044

SAMPLE ID PCB-4-1 Soil FRACTION Q4A TEST CODE 8080PB NAME PCBs in soil  
Date & Time Collected 07/16/86 Category ORGANICS ANALYSIS DATA SHEET  
PESTICIDESANALYST RY  
INSTRMT 1EXTRCTD 07/23/86  
INJECTD 08/06/86FILE # 116080616VERIFIED SCMUNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>2200</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>4400</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>4400</u>
53469-21-9	PCB-1242	<u>84000</u>	<u>2200</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>2200</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>4400</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>4400</u>

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Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-7-2 Soil</u>		SAMPLE # <u>05</u> FRACTIONS: <u>A</u>	
Date & Time Collected <u>07/16/86</u>		Category _____	
DRY_WT <u>64</u>	EX_PCB <u>07/21/86</u>		
% moisture	date completed		

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Results by Sample

Work Order # S6-07-044

SAMPLE ID PCB-7-2 Soil FRACTION 05A TEST CODE 8080PB NAME PCBs in soil  
Date & Time Collected 07/16/86 Category ORGANICS ANALYSIS DATA SHEET  
PESTICIDESANALYST RY EXTRACTD 07/23/86 FILE # 116080617 VERIFIED SCM  
INSTRMT 1 INJECTD 08/06/86 UNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>1900</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>3800</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>3800</u>
53469-21-9	PCB-1242	<u>28000</u>	<u>1900</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>1900</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>3800</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>3800</u>

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Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-9-2 Soil</u>		SAMPLE # <u>06</u> FRACTIONS: <u>A</u>	
		Date & Time Collected <u>07/16/86</u>	Category <u></u>
DRY WT <u>55</u>	EX PCB <u>07/21/86</u>		
% moisture	date completed		

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Results by Sample

Work Order # S6-07-044

SAMPLE ID PCB-9-2 SoilFRACTION 06A    TEST CODE 8080PB    NAME PCBs in soilDate & Time Collected 07/16/86Category                     ORGANICS ANALYSIS DATA SHEET  
PESTICIDESANALYST          RY  
INSTRMT          1EXTRCTD 07/24/86  
INJECTD 08/06/86FILE # 116080618VERIFIED          SCMUNITS          ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>        </u> ND	<u>        </u> 7600
11104-28-2	PCB-1221	<u>        </u> ND	<u>        </u> 15000
11141-16-5	PCB-1232	<u>        </u> ND	<u>        </u> 15000
53469-21-9	PCB-1242	<u>120000</u>	<u>        </u> 7600
12672-29-6	PCB-1248	<u>        </u> ND	<u>        </u> 7600
11097-69-1	PCB-1254	<u>        </u> ND	<u>        </u> 15000
11096-82-5	PCB-1260	<u>        </u> ND	<u>        </u> 15000

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RAS Sacramento REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-11-2 Soil</u>		SAMPLE # <u>07</u> FRACTIONS: <u>A</u>	
Date & Time Collected <u>07/16/86</u>		Category _____	
DRY_WI <u>80</u>	EX_PCB <u>07/21/86</u>		
% moisture	date completed		

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Results by Sample REPORT

Work Order # S6-07-044

SAMPLE ID PCB-11-2 SoilFRACTION 07A TEST CODE 8080PB NAME PCBs in soilDate & Time Collected 07/16/86Category ORGANICS ANALYSIS DATA SHEET  
PESTICIDESANALYST RY  
INSTRMT 1EXTRCTD 07/24/86  
INJECTD 08/06/86FILE # 116080619VERIFIED SCM  
UNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>340</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>680</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>680</u>
53469-21-9	PCB-1242	<u>3800</u>	<u>340</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>340</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>680</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>680</u>

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RAS Sacramento REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-13-2 Soil</u>		SAMPLE # <u>08</u> FRACTIONS: <u>A</u>	
		Date & Time Collected <u>07/16/86</u>	Category _____
DRY_WT <u>80</u>	EX_PCB <u>07/21/86</u>		
% moisture	date completed		

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Results by Sample

Work Order # S6-07-044

SAMPLE ID PCB-13-2 SoilFRACTION OBA TEST CODE 8080PB NAME PCBs in soilDate & Time Collected 07/16/86Category ORGANICS ANALYSIS DATA SHEET  
PESTICIDESANALYST RY  
INSTRMT 1EXTRCTD 07/24/86  
INJECTD 08/06/86FILE # 116080620VERIFIED SCM  
UNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>3300</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>6600</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>6600</u>
53469-21-9	PCB-1242	<u>48000</u>	<u>3300</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>3300</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>6600</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>6600</u>

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RAS Sacramento REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-17-2 Soil</u>		SAMPLE # <u>09</u> FRACTIONS: <u>A</u>	
Date & Time Collected <u>07/16/86</u>		Category _____	
DRY_WT <u>60</u>	EX_PCB <u>07/21/86</u>		
% moisture	date completed		

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RAS Sacramento

Results by Sample

REPORT

Work Order # S6-07-044

SAMPLE ID PCB-17-2 Soil

FRACTION 09A

TEST CODE 8080PB

NAME PCBs in soil

Date & Time Collected 07/16/86

Category

ORGANICS ANALYSIS DATA SHEET  
PESTICIDES

ANALYST RY  
INSTRMT 1

EXTRCTD 07/24/86  
INJECTD 08/06/86

FILE # 116080621

VERIFIED SCM

UNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>170</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>340</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>340</u>
53469-21-9	PCB-1242	<u>2400</u>	<u>170</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>170</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>340</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>340</u>

NOTES AND DEFINITIONS FOR THIS REPORT.

DET LIMIT = detection limit.

ND = not detected at specified detection limit.

NA = not analyzed.

NS = not spiked.

N/A = not available.

\* = less than 5 times the detection limit.

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RAS Sacramento REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-20-1 Soil</u>		SAMPLE # <u>10</u> FRACTIONS: <u>A</u>	
		Date & Time Collected <u>07/16/86</u>	Category <u></u>
DRY_WT <u>60</u>	EX_PCB <u>07/21/86</u>		
% moisture	date completed		

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Results by Sample

Work Order # S6-07-044

SAMPLE ID PCB-20-1 Soil FRACTION 10A TEST CODE 8080PB NAME PCBs in soil  
Date & Time Collected 07/16/86 Category ORGANICS ANALYSIS DATA SHEET  
PESTICIDESANALYST RY  
INSTRMT 1EXTRCTD 07/24/86  
INJECTD 08/06/86FILE # 116080623VERIFIED SCMUNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>1700</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>3400</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>3400</u>
53469-21-9	PCB-1242	<u>37000</u>	<u>1700</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>1700</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>3400</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>3400</u>

## NOTES AND DEFINITIONS FOR THIS REPORT.

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NS = not spiked.

N/A = not available.

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RAS Sacramento      REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID	PCB-2-2 Matrix Spike Soil	SAMPLE #	11	FRACTIONS:	A
Date & Time Collected		07/16/86		Category	
EX_PCB					

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Results by Sample

Work Order # S6-07-044

SAMPLE ID PCB-2-2 Matrix Spike Soil FRACTION 11A TEST CODE 8080PB NAME PCBs in soil  
Date & Time Collected 07/16/86 Category ORGANICS ANALYSIS DATA SHEET  
PESTICIDESANALYST RY  
INSTRMT 1EXTRCTD 07/23/86  
INJECTD 08/06/86FILE # 116080624VERIFIED SCM  
UNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>2000</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>4000</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>4000</u>
53469-21-9	PCB-1242	<u>13%</u>	<u>2000</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>2000</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>4000</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>4000</u>

## NOTES AND DEFINITIONS FOR THIS REPORT.

DET LIMIT = detection limit.

ND = not detected at specified detection limit.

NA = not analyzed.

NS = not spiked.

N/A = not available.

\* = less than 5 times the detection limit.

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RAS Sacramento      REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID <u>PCB-11-2 Duplicate Analys.</u>	SAMPLE # <u>12</u> FRACTIONS: <u>A</u>
Date & Time Collected <u>07/16/86</u> Category <u>                    </u>	
EX_PCB <u>                    </u>	

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Results by Sample

Work Order # S6-07-044

SAMPLE ID PCB-11-2 Duplicate Analys. FRACTION 12A TEST CODE 8080PB NAME PCBs in soil  
Date & Time Collected 07/16/86 Category \_\_\_\_\_ORGANICS ANALYSIS DATA SHEET  
PESTICIDESANALYST \_\_\_\_\_ RY  
INSTRMT \_\_\_\_\_ 1EXTRCTD 07/23/86  
INJECTD 08/06/86FILE # 116080631VERIFIED \_\_\_\_\_ SCM  
UNITS \_\_\_\_\_ ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	ND	820
11104-28-2	PCB-1221	ND	1600
11141-16-5	PCB-1232	ND	1600
53469-21-9	PCB-1242	68000	820
12672-29-6	PCB-1248	ND	820
11097-69-1	PCB-1254	ND	1600
11096-82-5	PCB-1260	ND	1600

## NOTES AND DEFINITIONS FOR THIS REPORT.

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NA = not analyzed.

NS = not spiked.

N/A = not available.

\* = less than 5 times the detection limit.

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RAS Sacramento      REPORT  
Results by Sample

Work Order # S6-07-044

SAMPLE ID	Reagent Blank	SAMPLE # 13	FRACTIONS: A
Date & Time Collected		not specified	Category
EX_PCB			

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Results by Sample

Work Order # S6-07-044

SAMPLE ID Reagent Blank      FRACTION 13A      TEST CODE 8080PB      NAME PCBs in soil  
Date & Time Collected not specified      Category                     ORGANICS ANALYSIS DATA SHEET  
PESTICIDESANALYST RY  
INSTRMT 1EXTRCTD 07/23/86  
INJECTD 08/06/86FILE # 116080626VERIFIED SCM  
UNITS ug/kg

CAS #	COMPOUND	RESULT	DET LIMIT
12674-11-2	PCB-1016	<u>ND</u>	<u>17</u>
11104-28-2	PCB-1221	<u>ND</u>	<u>33</u>
11141-16-5	PCB-1232	<u>ND</u>	<u>33</u>
53469-21-9	PCB-1242	<u>ND</u>	<u>17</u>
12672-29-6	PCB-1248	<u>ND</u>	<u>17</u>
11097-69-1	PCB-1254	<u>ND</u>	<u>33</u>
11096-82-5	PCB-1260	<u>ND</u>	<u>33</u>

## NOTES AND DEFINITIONS FOR THIS REPORT.

DET LIMIT = detection limit.

ND = not detected at specified detection limit.

NA = not analyzed.

NS = not spiked.

N/A = not available.

\* = less than 5 times the detection limit.

Appendix 5  
Dike Boring Logs



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 2

### LITHOLOGIC LOG AND CONSTRUCTION OF DB-1

Client FRENCH LTD.  
 Project Name French Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-1  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Gulf Coast Coring - Rosenberg, Texas

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/22/86 Date Completed 7/22/86  
 Method Rotary Wash Total Depth 64.0'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HNU (IN dbm)	OVA (IN dbm)	SAMPLED FOR CHEM. ANALYSIS
0	SURFACE ELEVATION								
	TOPSOIL AND CLAYEY SAND, brown and tan, fill(?)	2.0	0-2	ST	.95			<1	
	SILTY SAND TO SAND, fine to coarse grained, brownish tan		2-4	ST	.80				
	below 4.0' wet		4-6	ST	.80				
	below 6.0' dark gray, discolored, odors detected		6-8	SS	1.8				
			8-10	SS	1.6				
			10-12	SS	1.3				
			12-14	SS	1.0				
	14.0 to 14.6' dark oily discoloration		14-16	SS	.60				
			16-18	SS	.70				
			18-20	SS	.60				
		22.0	20-22	SS	.80				
	SAND, fine to very coarse grained and pebbles (fine gravel), gray		22-24	SS	.40				
			24-26	SS	.70				
			26-28	SS	.70				
		29.5	28-30	SS	.60				
	SILTY CLAY, reddish brown and gray, mottled, very firm		30-32	ST	1.3				
		32.8	32-34	ST	1.45				
	CLAYEY SILT, with some very fine grained sand, grayish green, firm		34-36	ST	1.15				
			36-38	ST	1.2				
			38-40	ST	1.4				
	40.0 to 43.1' silty very fine grained sand with some clay, grayish green		40-42	ST	1.3				
	43.1 to 46.0' silty clay, grayish green and tan, mottled, firm		42-44	ST	1.5				
			44-46	SS	1.5				
		48.8	46-48	ST	1.4				
	SILTY CLAY WITH SAND, greenish gray and tan, mottled, very firm		48-50	ST	1.6				
			50-52	ST	1.4				
		53.5	52-54	ST	1.6				
	CLAYEY SAND, very fine grained with silt, greenish gray and tan, mottled, very dense		54-56	ST	1.25				
			56-58	ST	1.2				
	58.0 to 60.0' silty sand, very fine to fine grained, very dense		58-60	ST	1.3				
60	(LOG CONTINUED ON PAGE 2 OF 2)	60.0							

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

Sheet 2 of 2

Client FRENCH LTD.  
 Project Name French Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-1

## CONTINUATION OF DB-1

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HNU (IN ppm)	OVA (IN ppm)	SAMPLED FOR CHEM. ANALYSIS
60	SILTY CLAY, reddish brown and gray, mottled, massive, very firm		60-62	ST	1.6				
		64.0	62-64	ST	1.5				
65	BORING COMPLETED TO 64.0' DEPTH; BOREHOLE WAS GEOPHYSICALLY LOGGED, THEN SEALED WITH CEMENT-BENTONITE GROUT								



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG OF DB-2

Client FRENCH LTD.  
 Project Name French Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-2  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Gulf Coast Coring - Rosenberg, Texas

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/22/86 Date Completed 7/22/86  
 Method Rotary Wash Total Depth 52.0'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HNU (ppm)	OVA (ppm)	SAMPLED FOR CHEMICAL ANALYSIS
0	SURFACE ELEVATION								
	TOPSOIL AND SILTY CLAY, brown and gray, mottled	2.0	0-2	ST	1.1				
	SAND, medium to very coarse grained, brown, loose, moist below 4.0' wet		2-4	ST	.9			<1	
5			4-6	SS	.7			2	
	below 8.0' more grayish color		6-8	SS	.8			2	
		10.0	8-10	SS	.4			12	
10	SILTY SAND TO SAND, very fine to coarse grained, gray to tan 12.0 to 12.3' with dark gray oily stains		10-12	SS	1.0			2	
	14.0 to 14.2' pebbles (fine gravel)		12-14	SS	1.3			50	
15	16.5 to 17.3' some clay lenses with dark oily discoloration		14-16	SS	1.3			1	
			16-18	SS	1.3			3	
20			18-20	SS	.75			2	
			20-22	SS	.7			2	
	24.0 to 26.0' grades to a very coarse sand with some pebbles (fine gravel)		22-24	SS	.6			1	
25			24-26	SS	1.1				
	28.0 to 30.0' no recovery; sand or gravel (?)		26-28	SS	.5			1	
		30.0	28-30	SS	0				
30	SILTY CLAY, reddish brown, firm below 32.0' with pebbles, well rounded		30-32	SS	1.7			3	
			32-34	SS	.8			2	
35		35.15	34-36	SS	1.4			1	
	SANDY SILT TO SILTY SAND, fine grained, gray and tan to greenish gray and tan, mottled		36-38	ST	1.1			<1	
40		40.0	38-40	ST	1.2			<1	
	SILTY SAND TO SAND, very fine to medium grained, greenish gray and tan, mottled, moderately loose, moist to wet		40-42	ST	1.8			2	
45			42-44	ST	1.3			<1	
			44-46	SS	.8			<1	
		48.0	46-48	ST	1.4			<1	
50	SILTY CLAY, reddish brown, very firm		48-50	SS	1.2			<1	
		52.0	50-52	ST	1.5			<1	
55	BORING TERMINATED AT 52.0 FEET; BOREHOLE WAS GEOPHYSICALLY LOGGED, THEN SEALED WITH CEMENT BENTONITE GROUT.								
60									

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG OF DB-3

Client FRENCH LTD.  
 Project Name French Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-3  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Gulf Coast Coring - Rosenberg, Texas

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/23/86 Date Completed 7/23/86  
 Method Rotary Wash Total Depth 50.0'

\* OVA was not working properly; HNU unavailable

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HNU (ppm)	OVA (ppm)	SAMPLED FOR CHEMICAL ANALYSIS
0	SURFACE ELEVATION								
0	TOPSOIL AND SILTY CLAY WITH SAND, dark brown and gray and tan, mottled, moderately firm		0-2	ST	1.4		*	*	
			2-4	ST	1.3				
5	SAND, fine to coarse grained, gray, loose, wet	4.9	4-6	ST	1.1				
	8.0 to 10.0' dark discoloration, light odor detected		6-8	SS	.6				
10			8-10	SS	.6				
			10-12	SS	1.2				
			12-14	SS	1.1				
15	below 14.0' odors detected		14-16	SS	1.0				
			16-18	SS	.5				
20			18-20	SS	.65				
	22.0 to 26.0' with pebbles (fine gravel)		20-22	SS	.9				
25			22-24	SS	1.5				
			24-26	SS	1.1				
	28.0 to 28.6' pebbles (fine gravel) underlain by 0.2' of silty clay	28.6	26-28	SS	.6				
30	SILTY SAND, very fine grained to sandy silt with some thin clay laminae-greenish gray, soft		28-30	SS	.9				
			30-32	SS	.8				
35			32-34	SS	1.5				
			34-36	ST	.9				
			36-38	ST	1.2				
40	38.0 to 38.55' mottled, greenish gray and tan		38-40	ST	1.3				
			40-42	SS	.8				
45			42-44	SS	.7				
		46.3	44-46	ST	.45				
	SILTY CLAY, reddish brown, mottled, massive, very firm		46-48	ST	1.3				
50		50.0	48-50	ST	1.5				
	BORING TERMINATED AT 50.0 FEET; BOREHOLE WAS GEOPHYSICALLY LOGGED, THEN SEALED WITH CEMENT BENTONITE GROUT.								
55									
60									

#### SAMPLER TYPE

SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

#### BORING METHOD

HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG OF DB-4

Client FRENCH LTD.  
 Project Name French Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-4  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Gulf Coast Coring - Rosenberg, Texas

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/23/86 Date Completed 7/23/86  
 Method Rotary Wash Total Depth 58.0'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HNU (ppm)	OVA (ppm)	SAMPLED FOR CHEMICAL ANALYSIS
0	SURFACE ELEVATION								
	TOPSOIL, SANDY CLAY AND SAND (FILL?), dark brown, odor detected		0-2	ST	1.65			2	
		4.0	2-4	ST	1.15			2	
5	SILTY SAND TO SAND, fine to coarse grained, dark brown, discolored, odor detected, moist		4-6	ST	1.1			<1	
		8.0	6-8	SS	.6			<1	
10	SILTY CLAY WITH SAND TO SANDY CLAY, oily, discolored, odors detected		8-10	SS	1.5			100	
		12.0	10-12	SS	1.5			100	
15	SILTY SAND TO SAND, fine to coarse grained, gray, wet below 14.0' fine to very coarse		12-14	SS	.9			100	
			14-16	SS	.9			50	
			16-18	SS	.8			100	
20			18-20	SS	.7			30	
			20-22	SS	.5			14	
	below 24.0' with pebbles (fine grained)		22-24	SS	.8			46	
25			24-26	SS	.6				
		28.0	26-28	SS	1.0			50	
30	SILTY CLAY, reddish brown and gray, mottled, massive, moderately soft to moderately firm		28-30	ST	1.6			10	
		32.8	30-32	ST	1.3			<1	
35	SILTY SAND TO SAND, very fine to fine grained, gray to greenish gray, soft		32-34	ST	1.0			4	
			34-36	SS	.63			3	
			36-38	ST	1.0			32	
40	40.0 to 46.5' silt to sandy silt, loose to dense		38-40	ST	1.6			20	
			40-42	ST	1.3			2	
45			42-44	SS	.4			<1	
	46.5 to 46.9' silty sand, very fine to medium grained		44-46	SS	0				
			46-48	ST	.9			1	
50	50.4 to 51.4' silty clay or clayey silt		48-50	ST	1.65			1	
			50-52	ST	1.4			<1	
		54.7	52-54	ST	1.1			<1	
55	SILTY CLAY, reddish brown and tan, mottled, very firm		54-56	ST	1.6			<1	
		58.0	56-58	ST	1.7			<1	
60	BORING TERMINATED AT 58.0 FEET; BOREHOLE WAS GEOPHYSICALLY LOGGED, THEN SEALED WITH CEMENT BENTONITE GROUT.								

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG OF DB-5

Client FRENCH LTD.  
 Project Name French Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-5  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Gulf Coast Coring - Rosenberg, Texas

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/24/86 Date Completed 7/25/86  
 Method Rotary Wash Total Depth 60.0'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HNU (pdm)	OVA (pdm)	SAMPLED FOR CHEMICAL ANALYSIS
0	SURFACE ELEVATION								
0	SANDY CLAY AND CLAYEY SAND (FILL?), dark gray, odors detected, very stiff		0-2	ST	.8			<1	
			2-4	ST	.85			2	
5	below 4.0' very dark gray, discolored		4-6	ST	1.1			2	
		6.6	6-8	ST	1.5			10	
	SANDY CLAY (FILL?), dark gray	8.7	8-10	ST	1.5			10	
10	SAND, fine to coarse grained (fill?), gray to dark gray, discolored, very strong odors detected		10-12	ST	1.5			300	
			12-14	ST	1.5			160	
15	SILTY SAND TO SAND, fine to coarse grained, gray, wet	14.0	14-16	SS	1.1			60	
			16-18	SS	.8			45	
20	20.0 to 20.45' very coarse sand with pebbles (fine gravel)		18-20	SS	.7			14	
	22.0 to 24.0' very coarse sand with pebbles		20-22	SS	.75			40	
			22-24	SS	1.0			20	
25			24-26	SS	.5			34	
	Note: Upon reaching 26.0' depth, a cable on the rig broke. Returned to operation on 7/25/86 at which time the 24-26 was resampled (?). At 38-40 depth interval it was determined that the intervals were miscounted	28.0	26-28	SS	1.4			10	
30	SILTY CLAY, reddish brown and tan, mottled, massive, moderately firm to firm		* 28-30	SS	1.2			20	
			30-32	ST	1.9			<1	
35	* These are the correct intervals from which these samples were collected for chemical analysis. Prior to correction, these intervals were identified as being 26-28 and 32-34 because of a logging error		32-34	ST	1.3			<1	
			* 34-36	ST	1.8			<1	
			36-38	ST	1.3			<1	
40		40.0	38-40	ST	1.7			<1	
	SANDY SILT TO SILTY SAND, fine grained, greenish gray, dense		40-42	SS	.8			<1	
45			42-44	SS	1.0			<1	
	below 46.0' clayey silt with some fine grained sand		44-46	SS	.7			<1	
			46-48	SS	.35			2	
50			48-50	ST	1.35			<1	
			50-52	ST	1.65			<1	
55			52-54	ST	1.5			<1	
	below 55.6' silty sand	56.0	54-56	ST	1.8			<1	
	SILTY CLAY, reddish brown and tan, mottled, massive, very firm		56-58	ST	1.5			<1	
60	BORING TERMINATED AT 60.0 FEET; BOREHOLE WAS GEOPHYSICALLY LOGGED, THEN SEALED WITH CEMENT BENTONITE GROUT.	60.0	58-60	ST	1.8			2	

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG OF DB-6

Client FRENCH LTD.  
 Project Name French Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-6  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Gulf Coast Coring - Rosenberg, Texas

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/24/85 Date Completed 7/24/86  
 Method Rotary Wash Total Depth 54.0'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HNU (ppm)	OVA (ppm)	SAMPLED FOR CHEMICAL ANALYSIS
0	SURFACE ELEVATION								
0	SANDY CLAY TO SILTY CLAY (FILL?), brown, very firm		0-2	ST	.7				
			2-4	ST	1.2		1.4		
5			4-6	ST	1.0		4		
		8.0	6-8	ST	1.6		4.4		
10	CLAYEY SAND, SANDY CLAY (FILL?), dark gray to black, discolored odors detected 10.0 to 12.0' well compacted; chemically cemented		8-10	ST	1.5		5		
			10-12	ST	1.4		1		
	14.0 to 15.0' oily discoloration	14.0	12-14	ST	1.2		2		
15	SAND, medium to coarse grained, gray, wet		14-16	SS	1.0		4		
			16-18	SS	.6		5		
20	20.0 to 20.2' very coarse sand with pebbles (fine gravel)		18-20	SS	.6				
			20-22	SS	1.2		10		
			22-24	SS	.35		10		
25	below 24.0' very coarse sand with pebbles (fine gravel)		24-26	SS	1.4		2.4		
		28.0	26-28	SS	.7		<1		
30	SILTY CLAY, reddish brown and tan, mottled, massive, moderately firm to firm 31.0 to 33.0' with some fine grained sand		28-30	SS	1.0		1		
			30-32	ST	1.85		5		
			32-34	ST	1.3		1		
35			34-36	ST	.5		<1		
		37.0	36-38	ST	.7		<1		
40	SILTY SAND TO SAND, very fine grained, greenish gray to gray and tan, mottled, loose to dense 40.0 to 41.7' clayey silt, greenish gray and tan		38-40	ST	1.0		1		
			40-42	SS	1.7		<1		
			42-44	ST	.95		<1		
45			44-46	SS	1.4		<1		
			46-48	SS	.6		<1		
50		50.0	48-50	SS	.7		4		
	SILTY CLAY, reddish brown and tan, mottled, very firm, with slickensides		50-52	ST	1.2		2.6		
		54.0	52-54	ST	1.4		<1		
55	BORING TERMINATED AT 54.0 FEET; BOREHOLE WAS GEOPHYSICALLY LOGGED, THEN SEALED WITH CEMENT BENTONITE GROUT.								
60									

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF DB-7

Client FRENCH, LTD.  
 Project Name French, Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-7  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Gulf Coast Coring - Rosenberg, Texas

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/18/86 Date Completed 7/19/86  
 Method Rotary Wash Total Depth 58.0'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HNU (IN ppm)	OVA (IN ppm)	SAMPLED FOR CHEM. ANALYSIS
0	SURFACE ELEVATION								
0	SILTY SAND (FILL?), gray and black; odor detected	2.0	0-2	ST	1.0'		50		
5	SILTY CLAY, gray, massive, moderately firm		2-4	SS	1.0'		<1		
			4-6	ST	1.8'		<1		
			6-8	ST	1.9'		1.0		
10		10.4	8-10	SS	0.3'		<1		
	SILTY SAND, ranging from fine to coarse grained, gray, poorly sorted, graded		10-12	SS	1.4'		<1		
	saturated below 12.0'		12-14	SS	1.7'			1.0	
15			14-16	SS	0.7'		1	6	
			16-18	SS	1.1'		<1	80	
20	18.0' to 22.0' very dark gray, discolored silty sand		18-20	SS	1.3'			100	
			20-22	SS	1.1'		2	200	
			22-24	SS	1.0'			10	
25	24.5' with pebble sized gravel	26.3	24-26	SS	1.0'		3		
	SILTY CLAY, reddish brown and gray, mottled, massive, very firm		26-28	ST	1.5'		3		
30			28-30	ST	1.9'		<1		
			30-32	ST	1.8'		<1		
			32-34	ST	1.7'		<1		
35	below 35.6' increasingly sandy, fine grained with greenish gray color		34-36	ST	1.6'		<1		
		38.0	36-38	ST	1.8'		<1		
40	CLAYEY SAND WITH SILT, very fine grained, greenish gray, moist	41.0	38-40	ST	1.5'		<1		
			40-42	SS	1.2'		<1	2	
	SILTY TO SANDY CLAY, gray, brown and reddish brown, mottled, massive, very firm		42-44	ST	1.35'		<1	2	
45		46.0	44-46	ST	1.2'		<1		
	CLAYEY SAND, very fine to fine grained, gray and brown, mottled, dense, moist		46-48	ST	1.7'		<1		
50			48-50	ST	1.6'		<1		
	below 52.0' reddish brown color observed		50-52	ST	1.5'		<1		
		53.0	52-54	ST	1.65'		<1		
55	CLAY TO SILTY CLAY, reddish brown and gray, mottled, massive, very firm		54-56	ST	1.5'		<1		
		58.0	56-58	ST	1.65'		<1		
60	BORING COMPLETED AT 58.0 FEET; BOREHOLE WAS GEOPHYSICALLY LOGGED, THEN SEALED WITH CEMENT BENTONITE GROUT.								

SAMPLER TYPE: SS - DRIVEN SPLIT SPOON, CA - CONTINUOUS FLIGHT AUGER, ST - PRESSED SHELBY TUBE, RC - ROCK CORE  
 BORING METHOD: HSA - HOLLOW STEM AUGERS, DC - DRIVING CASING, CFA - CONTINUOUS FLIGHT AUGERS, MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF DB-8

Client FRENCH, LTD.  
 Project Name French, Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-8  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Gulf Coast Coring - Rosenberg, Texas

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/20/86 Date Completed 7/20/86  
 Method Rotary Wash Total Depth 56.0'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HHNU (IN ppm)	OVA (IN ppm)	SAMPLED FOR CHEM. ANALYSIS
0	SURFACE ELEVATION								
	SILTY CLAY, brown and black, discolored, oily		0-2	ST	0.9				
		4.0	2-4	ST	1.6				
5	SAND, fine to medium grained, dark gray to gray, wet		4-6	SS	0.7				
			6-8	SS	0.6				
			8-10	SS	0.5				
10	12.6 to 13.5' coarse to very coarse sand with some pebbles		10-12	SS	1.1				
			12-14	SS	1.5				
15	18.0 to 18.4' sandy silt, gray		14-16	SS	1.1				
			16-18	SS	0.5				
20	below 20.0' fine to coarse sand, dark gray color, odor detected		18-20	SS	1.2				
			20-22	SS	0.9				
			22-24	SS	1.2				
25		26.35	24-26	SS	1.3				
	SILTY CLAY, reddish brown and gray, mottled, very firm		26-28	ST	1.1		4		
			28-30	ST	1.65		<1		
30			30-32	ST	1.0				
		34.0	32-34	ST	0.85		<1		
35	CLAY, SILT AND VERY FINE GRAINED SAND, reddish brown and gray, mottled, gray and tan below 36.0'		34-36	SS	0.6				
			36-38	SS	1.2				
40	40.8 to 41.35' clayey silt, gray and tan, mottled		38-40	ST	1.3				
			40-42	ST	1.35				
			42-44	SS	1.4				
45			44-46	SS	1.2				
		48.2	46-48	ST	1.6				
	SILTY CLAY, reddish brown and gray, mottled, massive, very firm		48-50	ST	1.85				
50			50-52	ST	1.2				
			52-54	ST	1.6				
55		56.0	54-56	ST	1.3				
	BORING COMPLETED TO 56.0' DEPTH; THEN SEALED WITH CEMENT-BENTONITE GROUT								
60									

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING





# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF DB-9

Client FRENCH, LTD.  
 Project Name French, Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-9  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Gulf Coast Coring - Rosenberg, Texas

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/21/86 Date Completed 7/21/86  
 Method Rotary Wash Total Depth 56.0'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HNU (IN ppm)	OVA (IN ppm)	SAMPLED FOR CHEM. ANALYSIS
0	SURFACE ELEVATION								
	TOPSOIL AND SILTY SAND, reddish brown to dark gray, fill(?)	2.0	0-2	ST	1.25			2	
	CLAYEY SAND, dark gray, discolored, fill(?)	4.0	2-4	ST	1.3			2	
5	SAND, fine to coarse grained, gray, wet		4-6	SS	.75			< 1	
			6-8	SS	.70			< 1	
10			8-10	SS	1.40			< 1	
			10-12	SS	.90				
			12-14	SS	.75			30	
15			14-16	SS	.75			16	
	18.0 to 20.0' with pebbles		16-18	SS	.65			30	
20	20.0 to 22.0' odor detected; put on respirator		18-20	SS	.75				
	22.0 to 26.0' with pebbles		20-22	SS	.5				
			22-24	SS	.65				
25	26.0 to 28.0' coarse to very coarse gray sand		24-26	SS	1.0			3	
		28.0	26-28	SS	.80				
30	PEBBLES (FINE GRAVEL) WITH SOME SAND		28-30	SS	.50				
		32.4	30-32	SS	.80				
35	SILTY SAND, fine grained, with clay, grayish green to greenish gray, dense		32-34	SS	1.25			2	
			34-36	SS	.50			25	
			36-38	SS	1.0			26	
40			38-40	SS	.85			10	
			40-42	SS	.80			30	
			42-44	SS	.85			35	
45			44-46	SS	.30			< 1	
	-below 46.0' dark brown oily color		46-48	SS	.9			1000	
		48.0	48-50	SS	1.5			40	
50	SILTY CLAY, reddish brown and gray, mottled, massive, very firm		50-52	ST	1.45			< 1	
			52-54	ST	1.55			< 1	
55		56.0	54-56	ST	.90			< 1	
	BORING COMPLETED TO 56.0' DEPTH; THEN SEALED WITH CEMENT BENTONITE GROUT								
60									

#### SAMPLER TYPE

SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

#### BORING METHOD

HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF DB-10

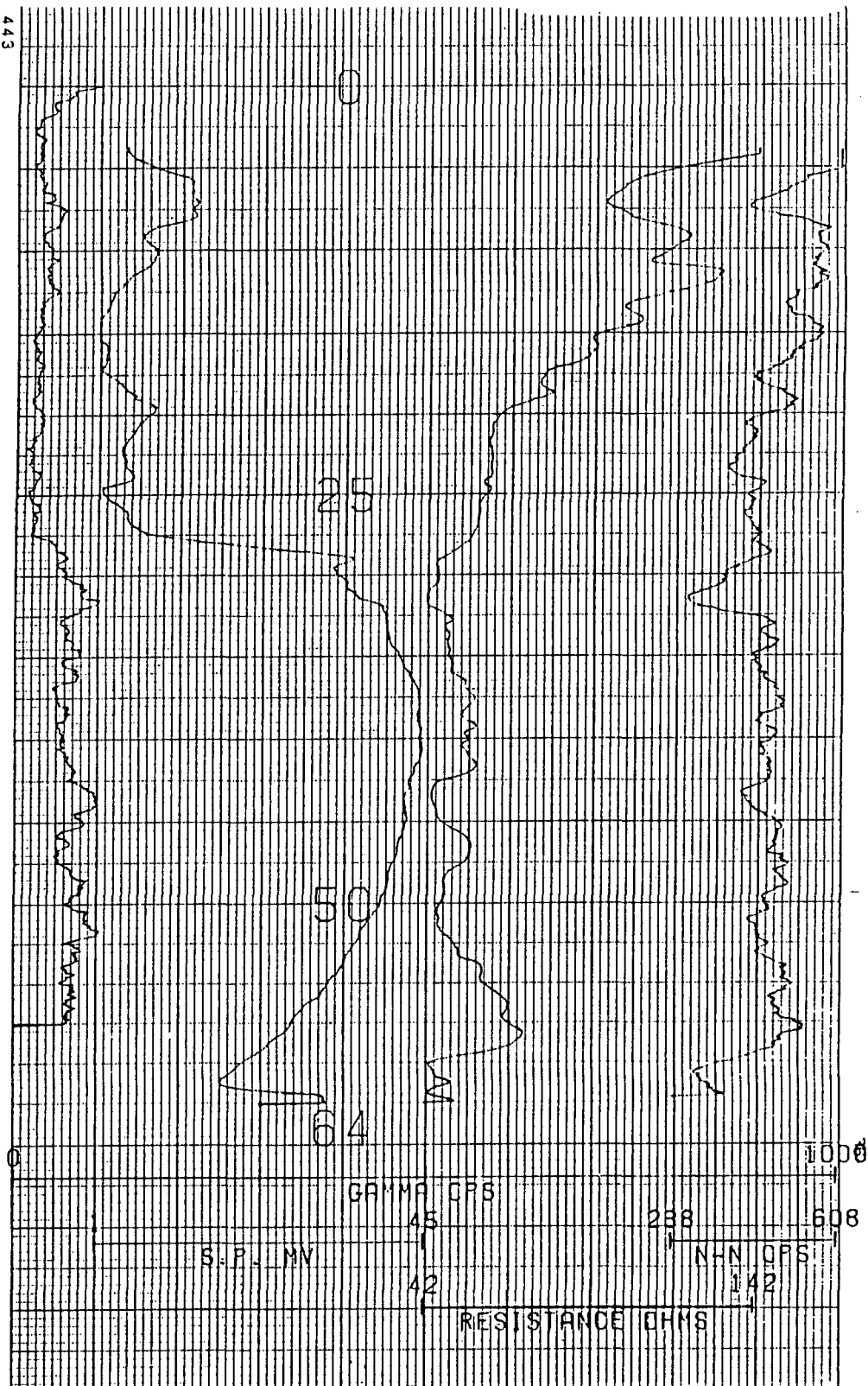
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 Project Name French Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. DB-10  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Gulf Coast Coring - Rosenberg, Texas

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/21/86 Date Completed 7/21/86  
 Method Rotary Wash Total Depth 58.0'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	HNU (IN ppm)	OVA (IN ppm)	SAMPLED FOR CHEM. ANALYSIS
0	SURFACE ELEVATION								
	CLAYEY SILT AND SAND, dark gray and brown		0-2	ST	1.3				
	SAND, FINE TO COARSE GRAINED, dark gray, discolored, moist		2-4	ST	1.0		<1		
5			4-6	SS	1.2		<1		
	below 8.0' wet		6-8	SS	None				
10	10.0 to 16.0' strong odor detected		8-10	SS	.6		<1		
			10-12	SS	.6		4		
			12-14	SS	.8		<1		
15	below 16.0' grayish green color		14-16	SS	1.2		<1		
	18.0' some clay and silt lenses		16-18	SS	.9		<1		
			18-20	SS	.6		<1		
20	below 22.0' some very coarse sand, dark gray oily discoloration		20-22	SS	.4		9		
		24.0	22-24	SS	.5		20		
25	SAND AND PEBBLES (fine gravel)		24-26	SS	.6		6		
		28.0	26-28	SS	.4		1		
	SILTY CLAY, reddish brown, massive, firm	28.5	28-30	SS	1.2		1		
30	SILTY SAND, very fine to fine grained, gray and tan		30-32	SS	.8		10		
			32-34	SS	.4		16		
35	34.0 to 36.0' dense very fine grained sand, tan		34-36	SS	1.3		3		
			36-38	SS	.5		1		
			38-40	SS	.6		<1		
40		42.1	40-42	SS	1.5		<1		
	SILTY CLAY, gray and tan, massive, very firm		42-44	ST	1.6				
45	44.0 to 44.5' clayey silt		44-46	SS	1.2		<1		
			46-48	ST	1.5		<1		
			48-50	ST	1.5		<1		
50	CLAYEY SAND, fine grained, reddish brown and gray, mottled		50-52	ST	1.5		<1		
	below 53.1' medium to coarse grained sand, brownish tan	54.0	52-54	ST	1.4		<1		
55	SILTY CLAY, reddish brown and gray, mottled, firm		54-56	ST	1.6		<1		
		58.0	56-58	ST	1.4		<1		
60	BORING COMPLETED TO 58.0' DEPTH; BOREHOLE WAS GEOPHYSICALLY LOGGED, THEN SEALED WITH CEMENT BENTONITE GROUT								

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**

**DB-1**

**FRENCH LIMITED**

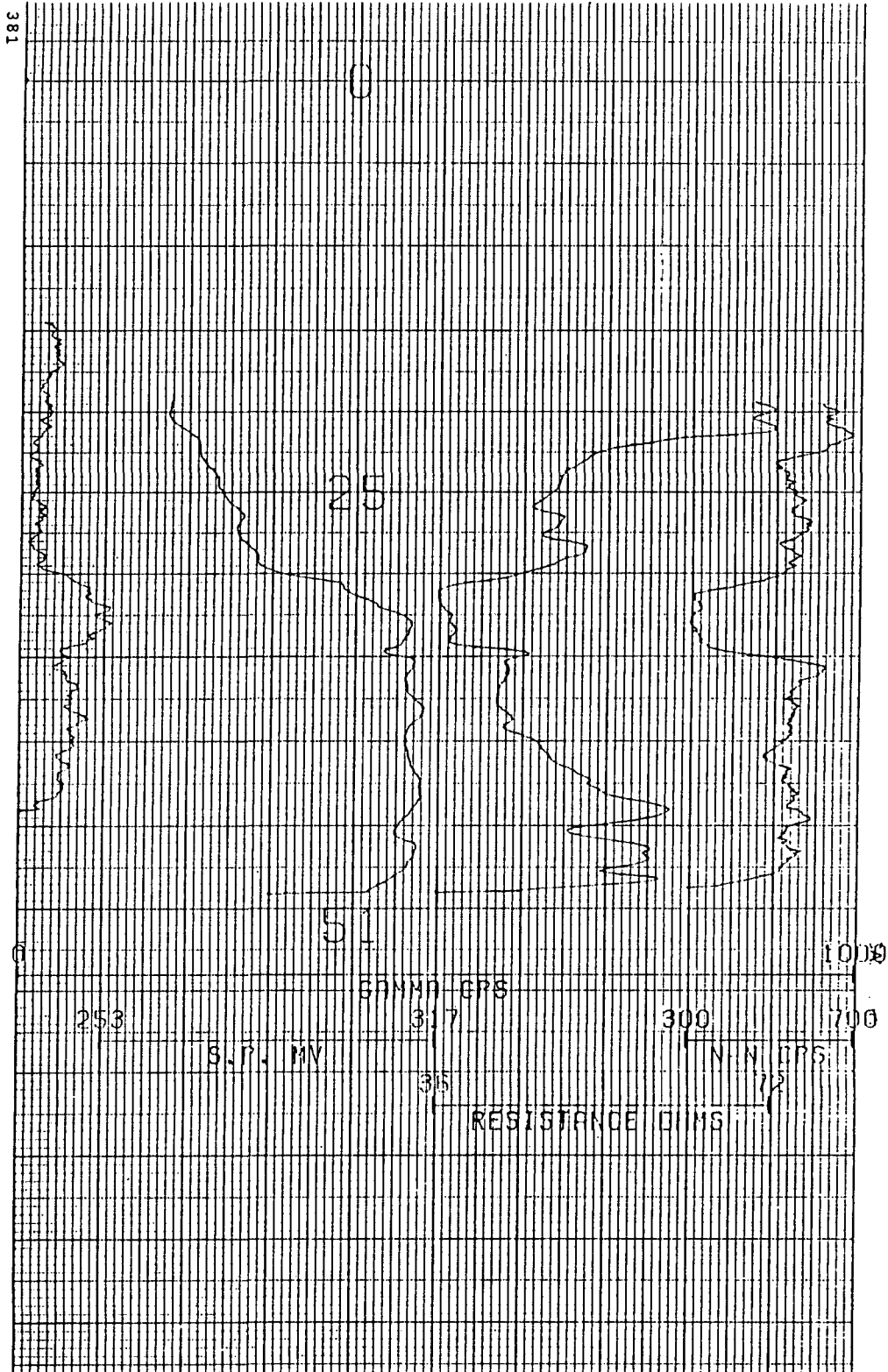
DRAWN BY:

DATE:

11-22-86

PROJECT NO.

275-14



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**

**DB-2**

**FRENCH LIMITED**

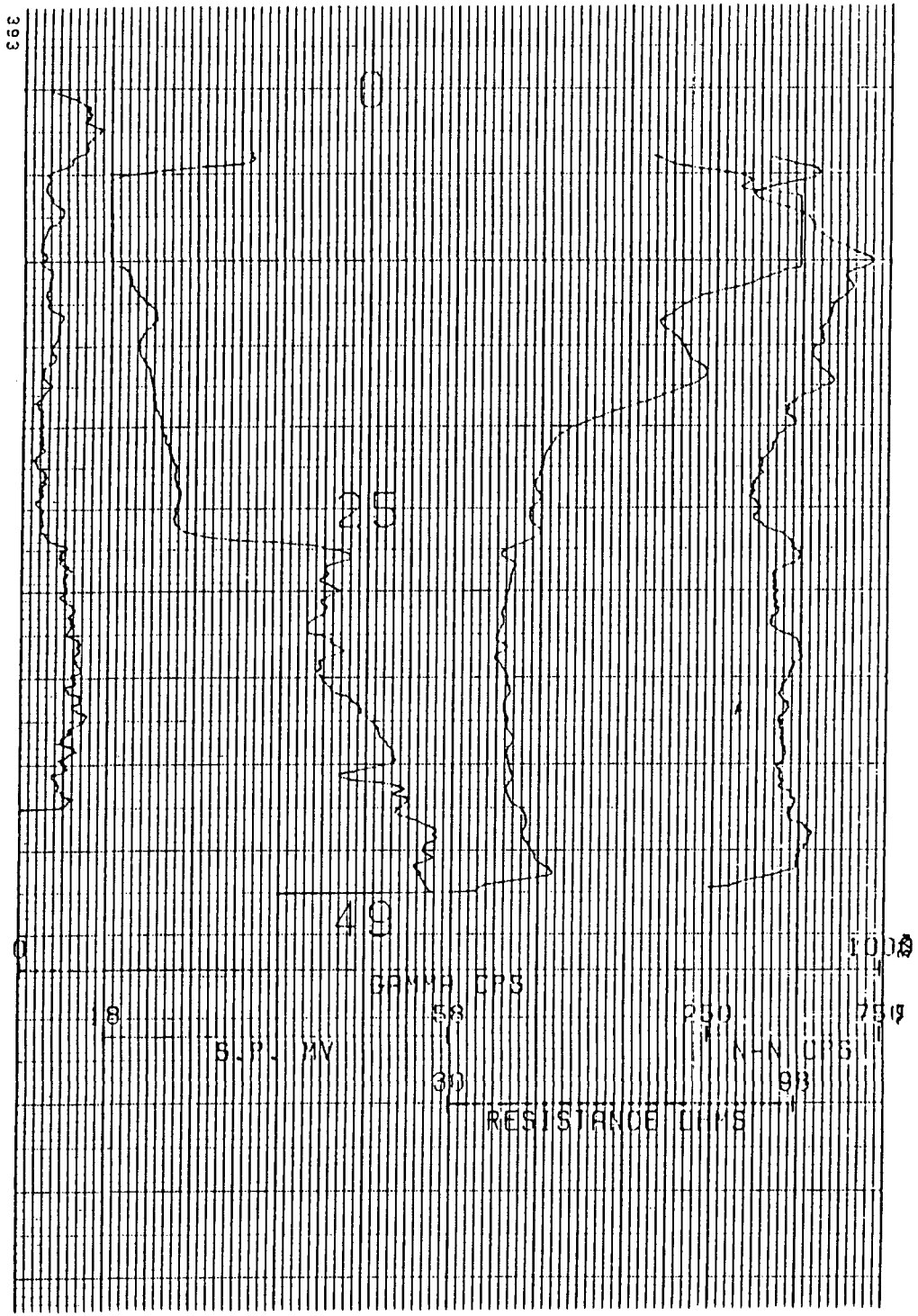
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DATE:

11-22-86

PROJECT NO.

275-14



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**

**DB-3**

**FRENCH LIMITED**

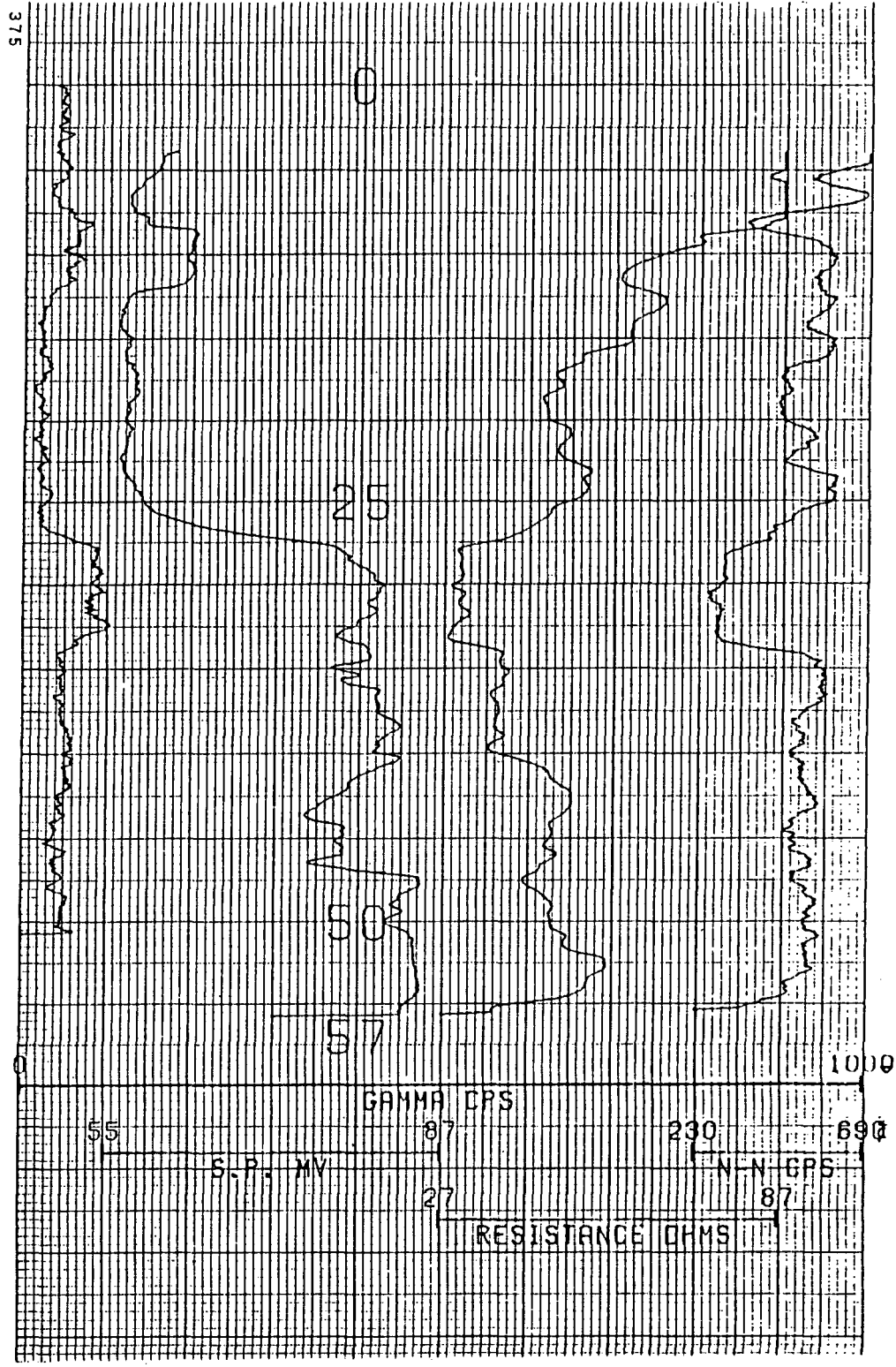
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DATE:

11-22-86

PROJECT NO.

275-14



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**

**DB-4**

**FRENCH LIMITED**

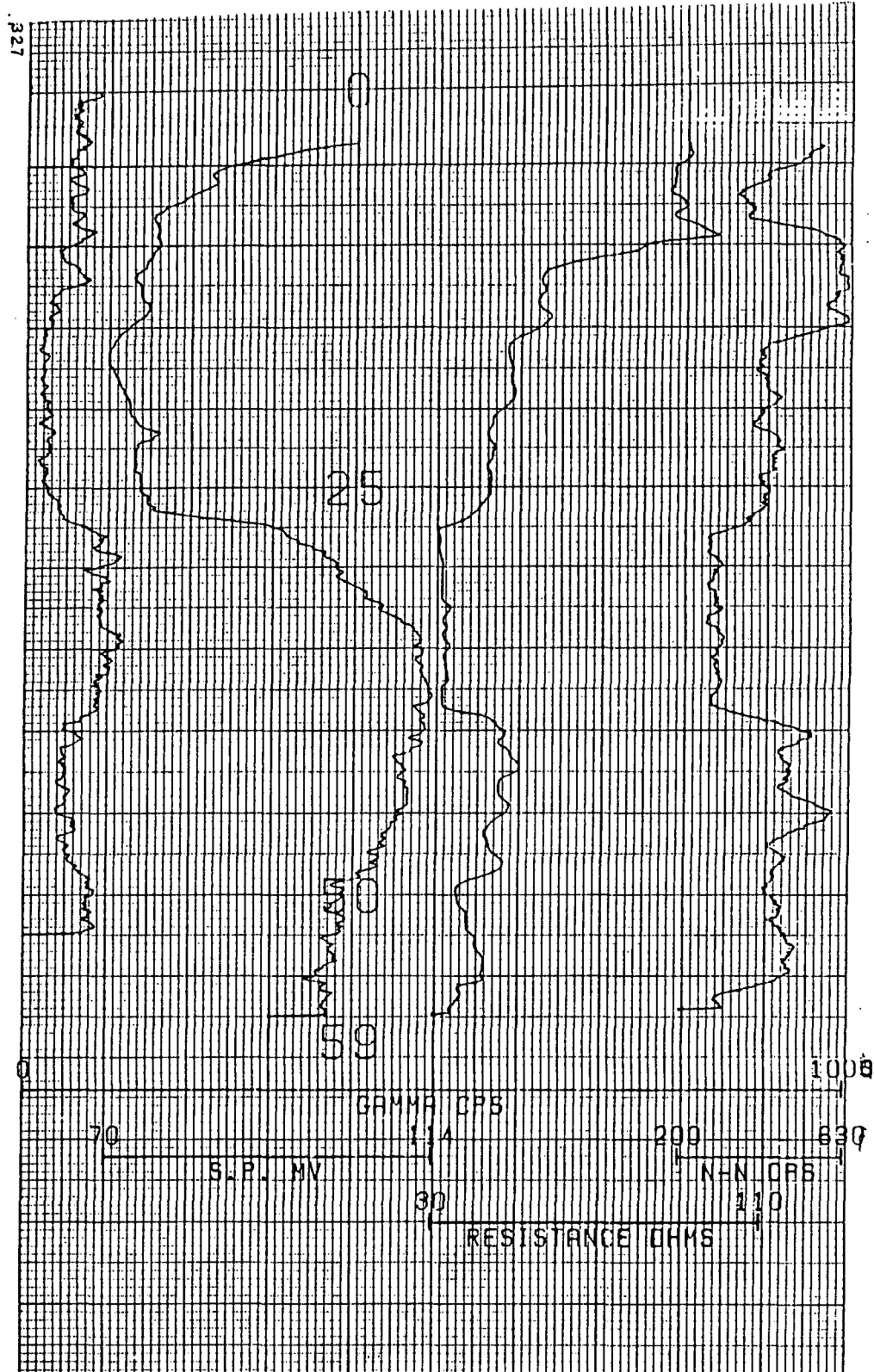
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DATE:

11-22-86

PROJECT NO.

275-14



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**

**DB-5**

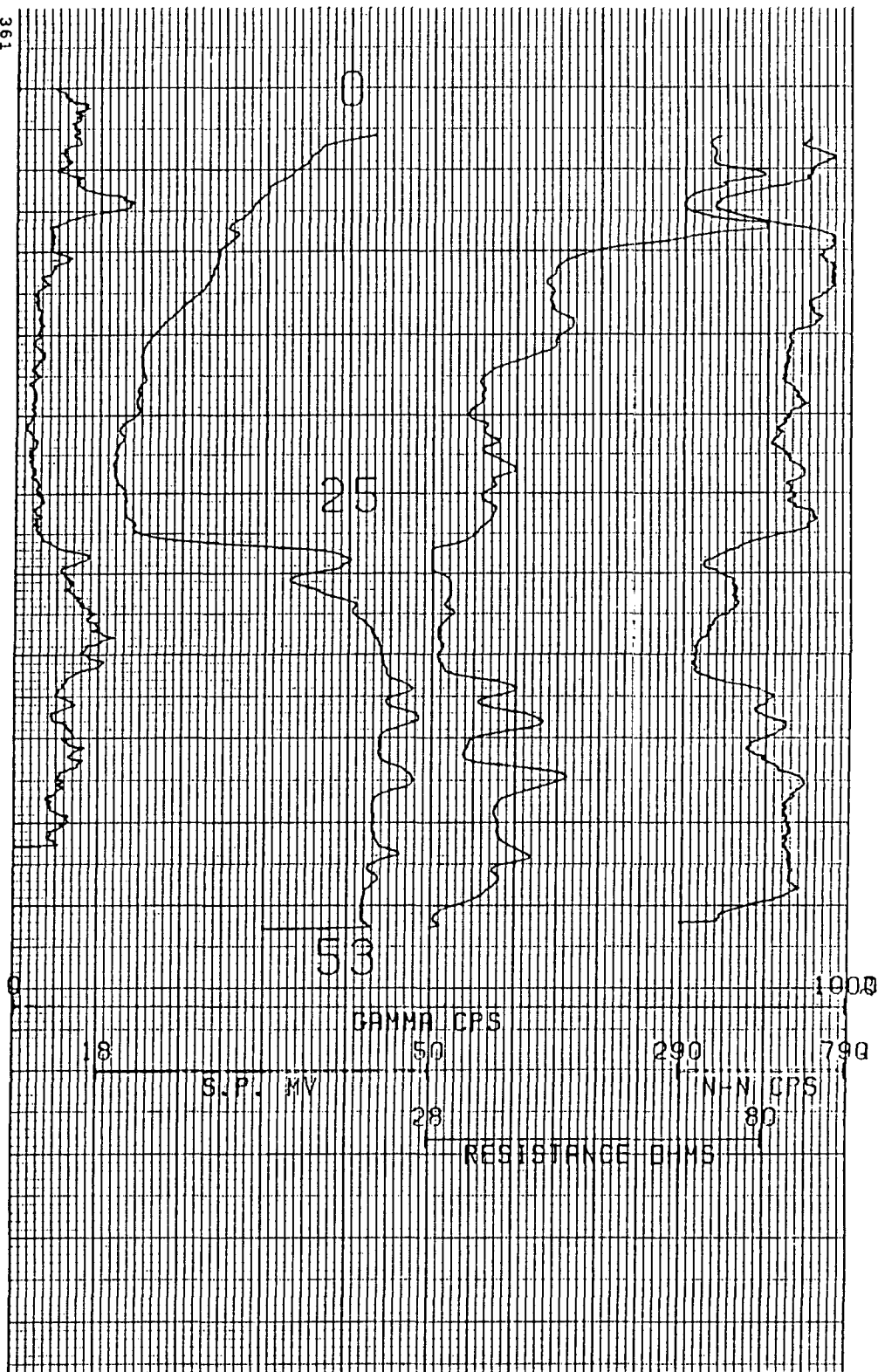
**FRENCH LIMITED**

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DATE: 11-22-86

PROJECT NO. 275-14

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**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**

**DB-6**

**FRENCH LIMITED**

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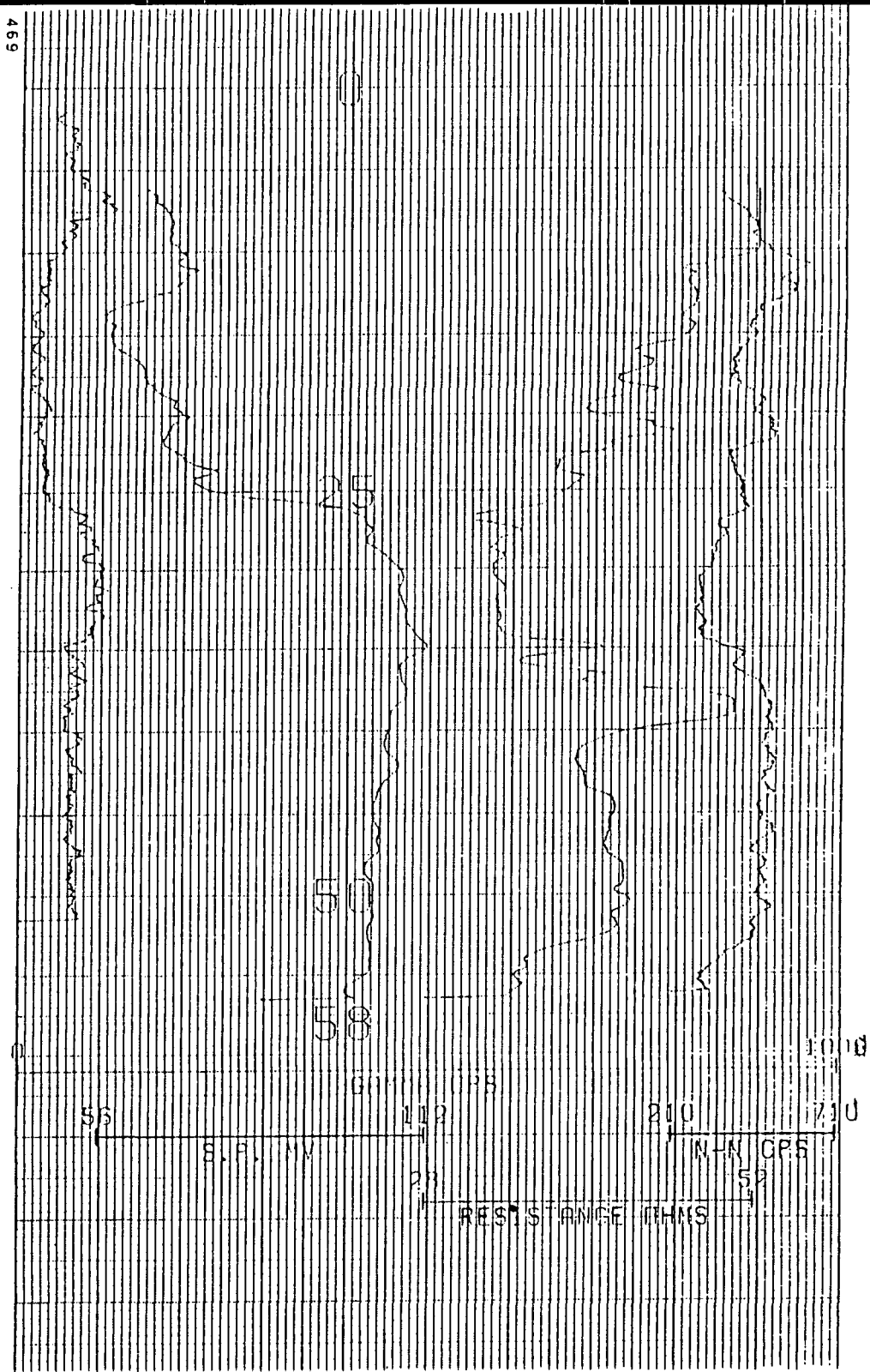
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11-22-86

PROJECT NO.

275-14





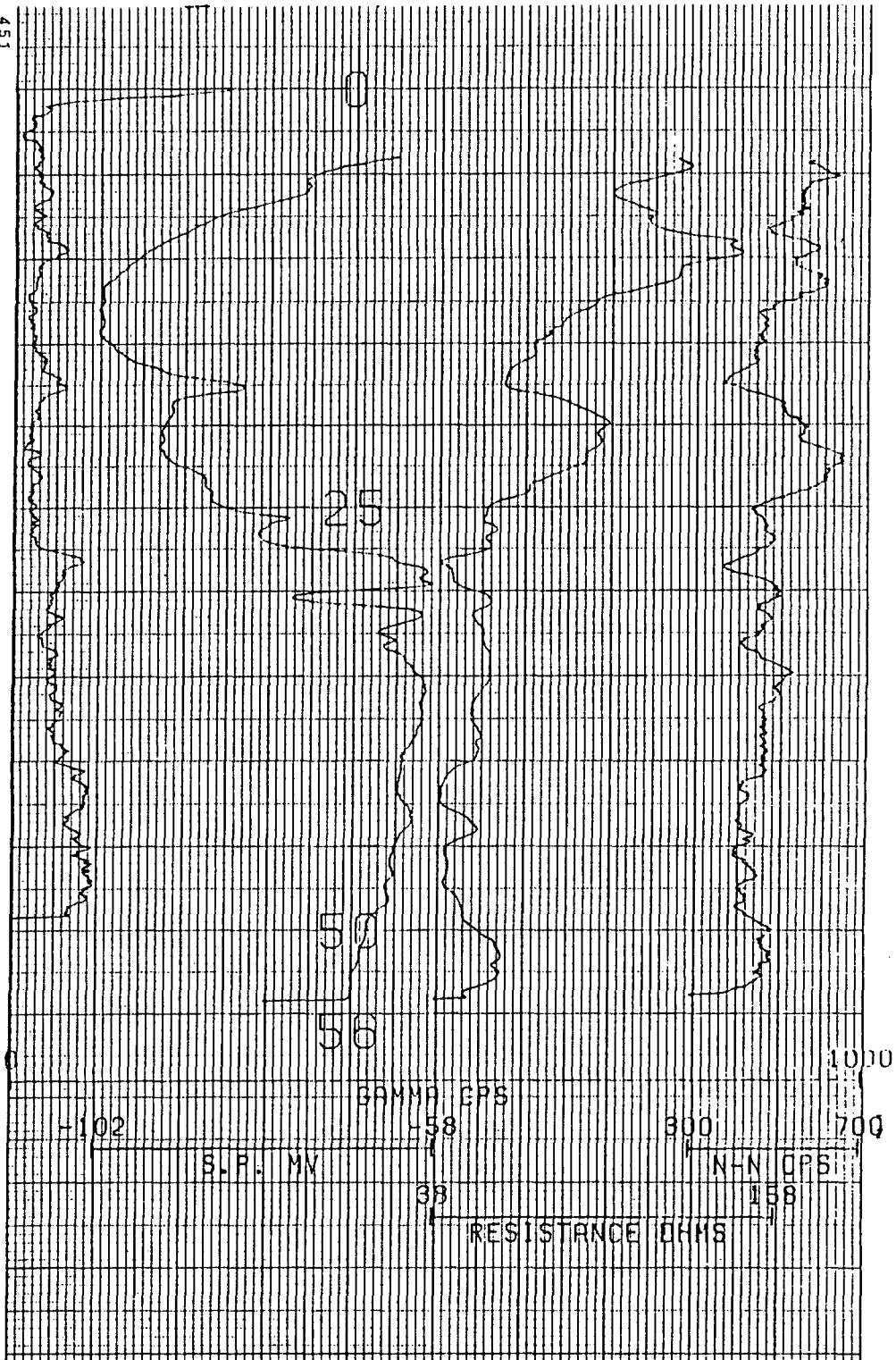
**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG  
DB-7  
FRENCH LIMITED**

DRAWN BY:	DATE: 11-22-86	PROJECT NO. 275-14
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**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**

**DB-10**

**FRENCH LIMITED**

DRAWN BY:

DATE:

11-22-86

PROJECT NO.

275-14

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Appendix 6

Dike Soil PNA Analytical Reports

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0158 RESOURCE ENGINEERING

RES27514

SDB-1-30-32 860722 0130

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	72	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	130	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	72	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	1700	ND	ND	ND	0	-	ND	4040	7.
5B	Benzo(a)anthracene	ND	300	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	95	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	380	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	130	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	200	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	220	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	220	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	ND	380	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	72	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	380	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	72	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	95	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	380	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	72	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	72	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	630	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	380	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	380	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	380	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	220	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	72	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	BMDL	380	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	380	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	84	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	72	ND	ND	ND	0	-	ND	4040	90

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports					
N0158	RESOURCE ENGINEERING	RES27514	SDB-1-30-32	860722	0130
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	72	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	34	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	380	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	61	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	180	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	84	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	61	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	72	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	380	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	380	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	72	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	210	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	72	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	72	ND	ND	ND	0	-	ND	4040	87

A Results variable due to Non-Homogeneous sample matrix.

B Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

<b>N0158</b>	<b>RESOURCE ENGINEERING</b>	<b>RES27514</b>	<b>SDB-1-30-32</b>	<b>86072</b>	<b>0130</b>	<b>0</b>
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	87	23	120
2-Fluorobiphenyl	50	83	30	115
Terphenyl-D14	50	113	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchlorodate	-	-	20..	150..
* IPB EPA Control Limits				
** Advisory Limits Only				

• IPB EPA Control Limits  
 .. Advisory Limits Only

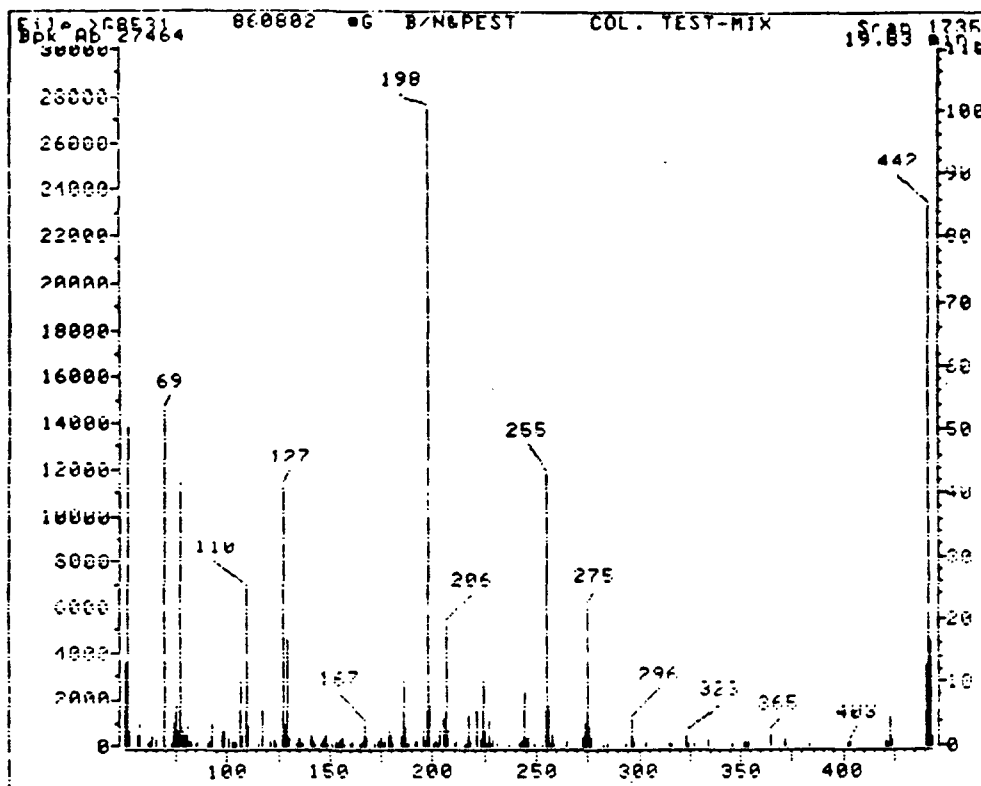


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
69	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.24	.24	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	17-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 15:34

Run No: >G8531

Spectrum No: 1735

Analyst: *Slappach*

Processor: *Tom Kurowski*

GC Batch: *Q85395*

Samples:

*N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 dil)  
N1252-N1253*

*8/8/86*

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0156 RESOURCE ENGINEERING

RES27514

SDB-1-34-36 860722 0135

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	75	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	75	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	1700	ND	ND	ND	0	-	ND	4040	7.
5B	Benzo(a)anthracene	ND	310	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	99	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	400	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	230	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	839	400	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	75	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	75	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	99	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	400	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	650	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	400	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	75	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	ND	400	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	400	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	87	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	75	ND	ND	ND	0	-	ND	4040	90



**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0156 RESOURCE ENGINEERING

RES27514

SDB-1-34-36 860722 0135

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sub>a</sub>	Second ug/kg <sub>a</sub>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	36	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	400	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	63	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	87	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	63	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	75	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	400	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	400	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	75	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	210	ND	ND	ND	0	-	ND	4040	98
45B	Pyrene	ND	75	ND	ND	BMDL	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	87

<sub>a</sub> Results variable due to Non-Homogeneous sample matrix.<sub>b</sub> Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0156	RESOURCE ENGINEERING	RES27514	SDB-1-34-36	86072	0135	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	98	23	120
2-Fluorobiphenyl	50	79	30	115
Terphenyl-D14	50	104	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IPB EPA Control Limits ** Advisory Limits Only				

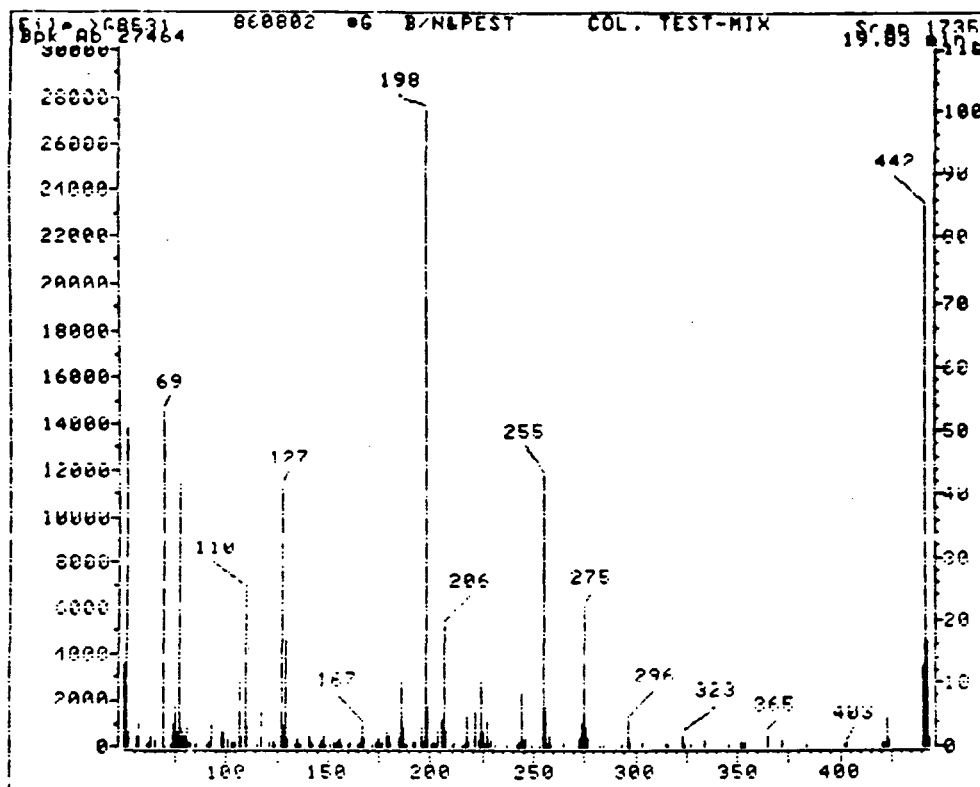


TABLE 2: METHOD PERFORMANCE DATA (UR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Ref.	
51	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.24	.24	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	17-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 16:34

Run No: 86882

Spectrum No: 1735

Analyst: Slapnick

Processor: Tom Kurowski

QC Batch: QB5395

Samples:

N0146-N0152, N0154-N0158,  
 N1250, N1251 (1:10 DIL)  
 N1252-N1253

8/8/86  
 B

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0160

RESOURCE ENGINEERING

RES27514

SDB-1-42-44 860722 0230

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	62	ND	ND	ND	0	-	ND	3290	94
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	ND	3290	96
3B	Anthracene	ND	62	ND	ND	ND	0	-	ND	3290	100
4B	Benidine	ND	1400	ND	ND	ND	0	-	ND	3290	0.
5B	Benzo(a)anthracene	ND	250	ND	ND	ND	0	-	ND	3290	101
6B	Benzo(a)pyrene	ND	81	ND	ND	ND	0	-	ND	3290	100
7B	Benzo(b)fluoranthene	ND	320	ND	ND	ND	0	-	ND	3290	105
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3290	90
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3290	93
11B	bis(2-Chloroethyl) ether	ND	180	ND	ND	ND	0	-	ND	3290	88
12B	bis(2-Chloroisopropyl)ether	ND	180	ND	ND	ND	0	-	ND	3290	70
13B	bis(2-Ethylhexyl)phthalate	BMDL	320	41.2	70.4	BMDL	0	-	ND	3290	105
14B	4-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3290	99
15B	Butyl benzyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	101
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3290	93
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3290	99
18B	Chrysene	ND	81	ND	ND	ND	0	-	ND	3290	91
19B	Dibenzo(a,h)anthracene	ND	320	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	88
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	88
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3290	89
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3290	88
24B	Diethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	104
25B	Dimethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	99
26B	Di-n-butyl phthalate	ND	320	ND	ND	458	0	-	ND	3290	113
27B	2,4-Dinitrotoluene	ND	180	ND	ND	ND	0	-	ND	3290	105
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3290	94
29B	Di-n-octyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	103
30B	1,2-Diphenylhydrazine	ND	320	ND	ND	ND	0	-	ND	3290	102
31B	Fluoranthene	ND	71	ND	ND	ND	0	-	ND	3290	109
32B	Fluorene	ND	62	ND	ND	ND	0	-	ND	3290	98

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0160 RESOURCE ENGINEERING

RES27514

SDB-1-42-44 860722 0230

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	101
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3290	93
35B	Hexachlorocyclopentadiene	ND	320	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	52	ND	ND	ND	0	-	ND	3290	90
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	71	ND	ND	ND	0	-	ND	3290	93
39B	Naphthalene	ND	52	ND	ND	ND	0	-	ND	3290	95
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3290	90
41B	N-Nitrosodimethylamine	ND	320	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	320	ND	ND	ND	0	-	ND	3290	90
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3290	111
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3290	103
45B	Pyrene	ND	62	ND	ND	ND	0	-	ND	3290	113
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	93

A Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0160 RESOURCE ENGINEERING

RES27514

0

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	84	20	140
2-Fluorobiphenyl	50	86	20	140
Terphenyl-D14	50	100	20	150

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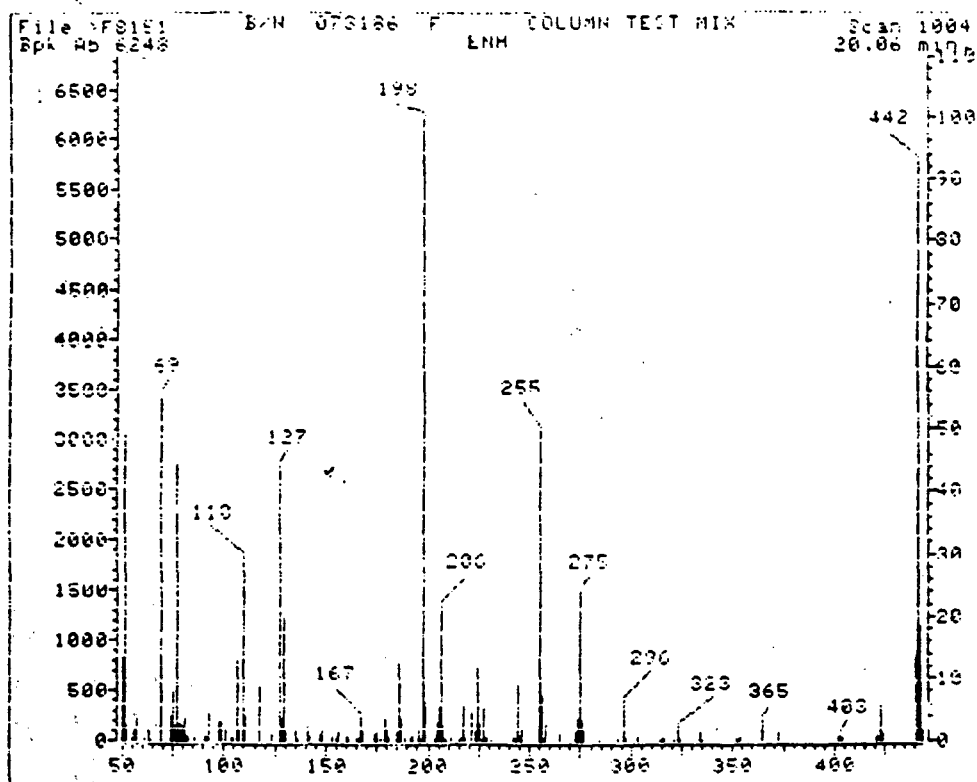


TABLE 2: METHOD PERFORMANCE DATA (CR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	48.74	48.74	UK
68	Less than 2% of mass 69	0.00	0.00	UK
69	(reference only)	55.39	55.39	UK
70	Less than 2% of mass 69	0.00	0.00	UK
127	40-60% of mass 198	43.99	43.99	UK
197	Less than 1% of mass 198	0.00	0.00	UK
198	Base peak, 100% relative abundance	100.00	100.00	UK
199	5-9% of mass 198	6.27	6.27	UK
275	10-30% of mass 198	24.06	24.06	UK
365	Greater than 1% of mass 198	3.36	3.36	UK
441	0-100% of mass 443	13.63	74.94	UK
442	Greater than 40% of mass 198	92.74	92.74	UK
443	17-23% of mass 442	18.19	19.61	UK

Injection Date: 07/31/86

Injection Time: 12:04

Run No: >F8151

Spectrum No: 1004

Analyst: *S. J. M. M.*

Processor: *Meta-Math*

QC Batch: *0135385*

Samples: *Calib. Std. 00159*

*00159, 00160, 00167, 00168, 00170, 00171, 00172*

*B 8/1/86*

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0157 RESOURCE ENGINEERING

RES27514

SDB-1-46-48 860722 0240

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concn. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concn. Added ug/kg	% Recov
1B	Acenaphthene	ND	75	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	75	ND	ND	BMDL	0	-	ND	4040	93
4B	Benidine	ND	1700	ND	ND	ND	0	-	ND	4040	7
5B	Benzo(a)anthracene	ND	310	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	99	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	400	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	230	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	634	400	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	75	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	75	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	99	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	400	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	650	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	ND	400	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	75	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	ND	400	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	400	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	87	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	75	ND	ND	ND	0	-	ND	4040	90



**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0157 RESOURCE ENGINEERING

RES27514

SDB-1-46-48 860722 0240

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	36	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	400	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	63	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	87	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	63	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	75	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	400	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	400	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	75	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	210	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	75	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	87

A Results variable due to Non-Homogeneous sample matrix.

B Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0157	RESOURCE ENGINEERING	RES27514	SDB-1-46-48	86072	0240	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	93	23	120
2-Fluorobiphenyl	50	78	30	115
Terphenyl-D14	50	93	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* 170 EPA Control Limits ** Advisory Limits Only				

© 1986 ETC Control Limits  
 or Recovery Limits Only

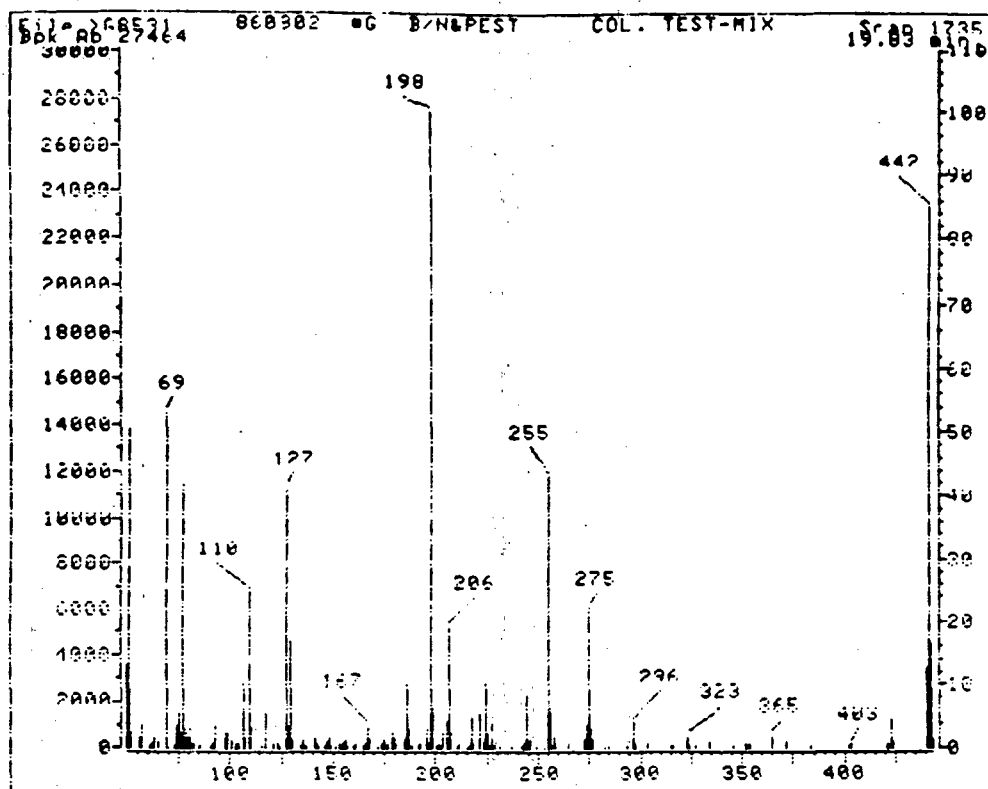


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFIPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.24	.24	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	12-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 15:34

Run No: 68531

Spectrum No: 1735

Analyst: Slapnick

Processor: Tom Kuorikoski

QC Batch: QB5395

Samples:

N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 DIL)  
N1252-N1253

8/8/86

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0155 RESOURCE ENGINEERING

RES27514

SDB-1-58-60 860722 0310

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	76	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	76	ND	ND	BMDL	0	-	ND	4040	93
4B	Benidine	ND	1700	ND	ND	ND	0	-	ND	4040	7.
5B	Benzo(a)anthracene	ND	310	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	99	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	400	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	230	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	BMDL	400	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	76	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	76	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	99	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	400	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	76	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	76	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	660	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	400	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	76	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	ND	400	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	400	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	87	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	76	ND	ND	ND	0	-	ND	4040	90

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0155 RESOURCE ENGINEERING

RES27514

SDB-1-58-60 860722 0310

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	76	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	36	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	400	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	64	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	87	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	64	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	76	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	400	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	400	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	76	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	210	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	76	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	76	ND	ND	ND	0	-	ND	4040	87

<sup>a</sup> Results variable due to Non-Homogenous sample matrix.<sup>b</sup> Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0155	RESOURCE ENGINEERING	RES27514	SDB-1-58-60	86072	0310	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits .	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	95	23	120
2-Fluorobiphenyl	50	92	30	115
Terphenyl-D14	50	96	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFS EPA Control Limits ** Advisory Limits Only				

\* IFB EPA Control Limits  
 .. Advisory Limits Only

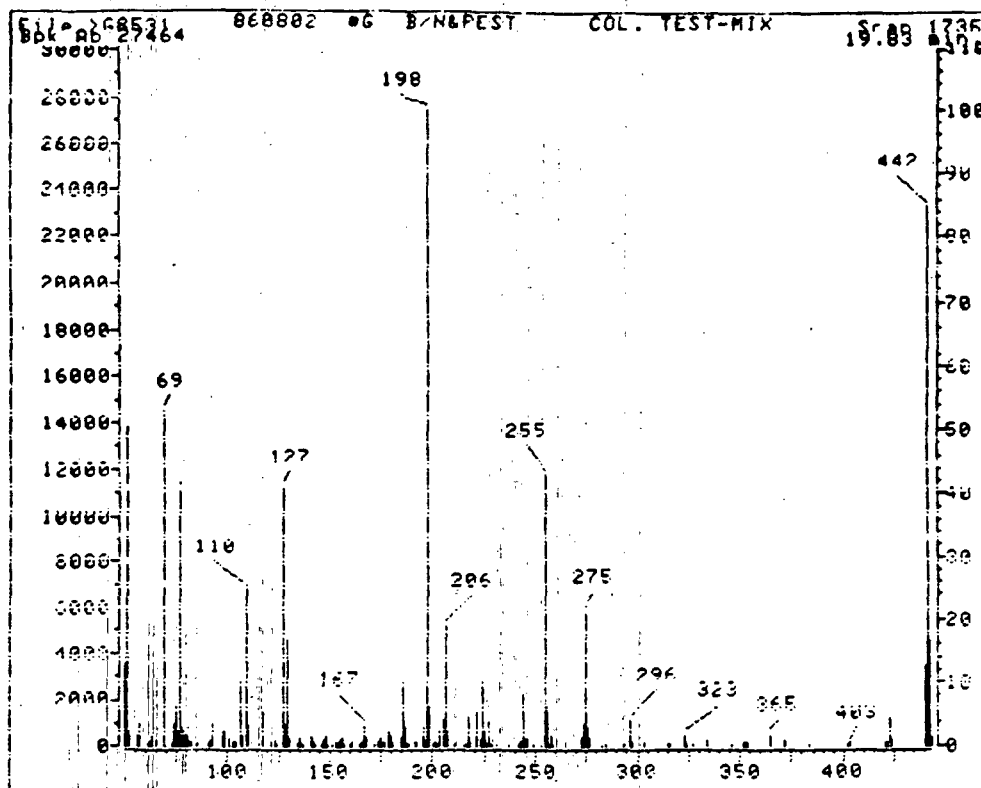


TABLE 2: METHOD PERFORMANCE DATA (DR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

Ion Abundance Criteria		% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.24	.24	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	17-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 15:34

Run No: 68531

Spectrum No: 1735

Analyst: *Stappach*

Processor: *Tom Luoma*

GC Batch: *Q85395*

Samples:

*N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 Dil)  
N1252-N1253*

*8/8/86*

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0159 RESOURCE ENGINEERING

RES27514 SDB-1-62-64 860722 0325

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	62	ND	ND	ND	0	-	ND	3290	94
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	ND	3290	96
3B	Anthracene	ND	62	ND	ND	ND	0	-	ND	3290	100
4B	Benzidine	ND	1400	ND	ND	ND	0	-	ND	3290	0.
5B	Benzo(a)anthracene	ND	250	ND	ND	ND	0	-	ND	3290	101
6B	Benzo(a)pyrene	ND	82	ND	ND	ND	0	-	ND	3290	100
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3290	105
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3290	90
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3290	93
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3290	88
12B	bis(2-Chloroisopropyl) ether	ND	190	ND	ND	ND	0	-	ND	3290	70
13B	bis(2-Ethylhexyl)phthalate	ND	330	41.2	70.4	BMDL	0	-	ND	3290	105
14B	4-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3290	99
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3290	101
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3290	93
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3290	99
18B	Chrysene	ND	82	ND	ND	ND	0	-	ND	3290	91
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	88
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	88
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3290	89
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3290	88
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3290	104
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3290	99
26B	Di-n-butyl phthalate	ND	330	ND	ND	458	0	-	ND	3290	113
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3290	105
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3290	94
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3290	103
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3290	102
31B	Fluoranthene	ND	72	ND	ND	ND	0	-	ND	3290	109
32B	Fluorene	ND	62	ND	ND	ND	0	-	ND	3290	98



AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0159 RESOURCE ENGINEERING

RES27514

SDB-1-62-64 860722 0325

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	101
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3290	93
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	52	ND	ND	ND	0	-	ND	3290	90
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	72	ND	ND	ND	0	-	ND	3290	93
39B	Naphthalene	ND	52	ND	ND	ND	0	-	ND	3290	95
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3290	90
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3290	90
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3290	111
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3290	103
45B	Pyrene	ND	62	ND	ND	ND	0	-	ND	3290	113
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	93

A Recovery normally variable using established methodology.

August 5, 1986

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil- GC/MS Data (QR20)**

*Chain of Custody Data Required for ETC Data Management Summary Reports*

N0159

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Amount Added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	86	20	140
2-Fluorobiphenyl	50	97	20	140
Terphenyl-D14	50	96	20	150
* FB EPA Control Limits.				

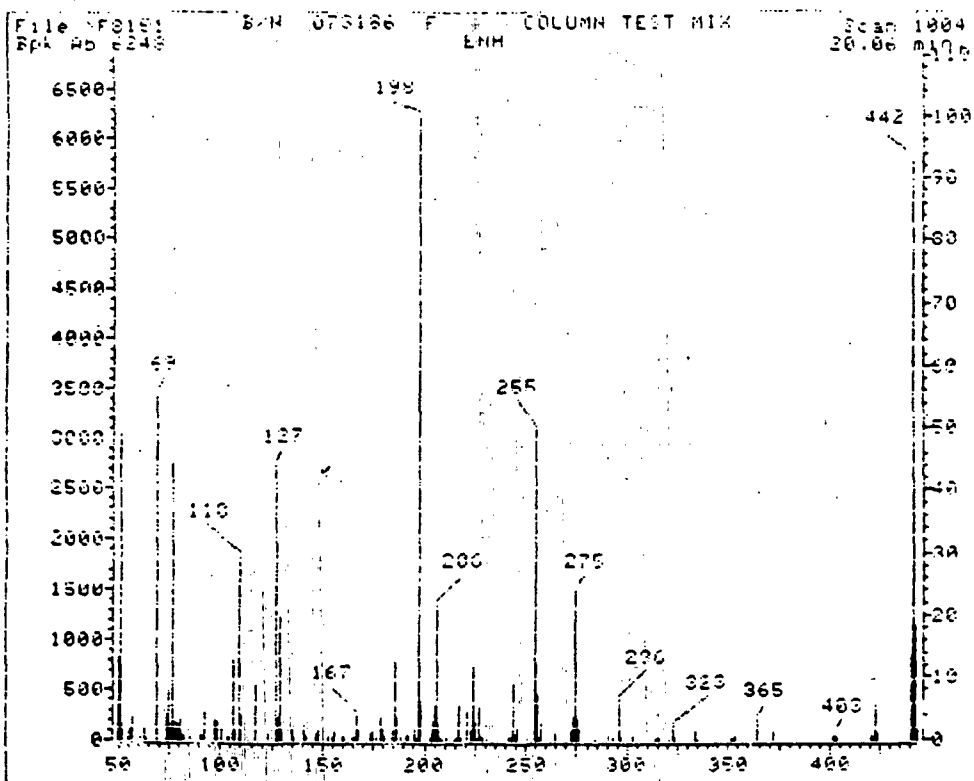


TABLE 2: METHOD PERFORMANCE DATA (UK23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	48.74	48.74	UK
68	Less than 2% of mass 69	0.00	0.00	UK
69	(reference only)	55.39	55.39	UK
70	Less than 2% of mass 69	0.00	0.00	UK
127	40-60% of mass 198	43.99	43.99	UK
197	Less than 1% of mass 198	0.00	0.00	UK
198	Base peak, 100% relative abundance	100.00	100.00	UK
199	5-9% of mass 198	6.27	6.27	UK
275	10-30% of mass 198	24.06	24.06	UK
365	Greater than 1% of mass 198	3.36	3.36	UK
441	0-100% of mass 443	13.63	74.94	UK
442	Greater than 40% of mass 198	92.74	92.74	UK
443	1/-25% of mass 442	18.19	19.61	UK

Injection Date: 07/31/86

Injection Time: 12:04

Run No: >F8151

Spectrum No: 1004

Analyst: SVANUM

Processor: Maria Muthuzi

QC Batch: 035385 MM

Samples: Celilo-Stok 00159  
N0159, N0160, N0167, U016  
N0170, N0171, N242

*B* 8/1/86

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0149

RESOURCE ENGINEERING

RES27514

SDB-2-30-32 860722 2045

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	100	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	190	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	100	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	2400	ND	ND	ND	0	-	ND	4040	7.
5B	Benzo(a)anthracene	ND	420	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	130	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	540	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	220	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	190	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	280	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	310	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	310	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	BMDL	540	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	100	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	540	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	100	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	230	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	130	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	540	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	100	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	100	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	240	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	890	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	540	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	540	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	540	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	310	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	100	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	ND	540	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	540	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	120	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	100	ND	ND	ND	0	-	ND	4040	90

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0149 RESOURCE ENGINEERING

RES27514 SDB-2-30-32 860722 2045

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	100	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	48	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	540	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	86	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	250	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	120	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	BMDL	86	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	100	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	540	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	540	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	100	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	290	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	100	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	100	ND	ND	ND	0	-	ND	4040	87

<sup>a</sup> Results variable due to Non-Homogeneous sample matrix.<sup>b</sup> Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0149	RESOURCE ENGINEERING	RES27514	SDB-2-30-32	86072	2045	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	105	23	120
2-Fluorobiphenyl	50	94	30	115
Terphenyl-D14	50	97	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFR EPA Control Limits				
** Advisory Limits Only				

• IFB EPA Control Limits  
 .. Advisory Limits Only

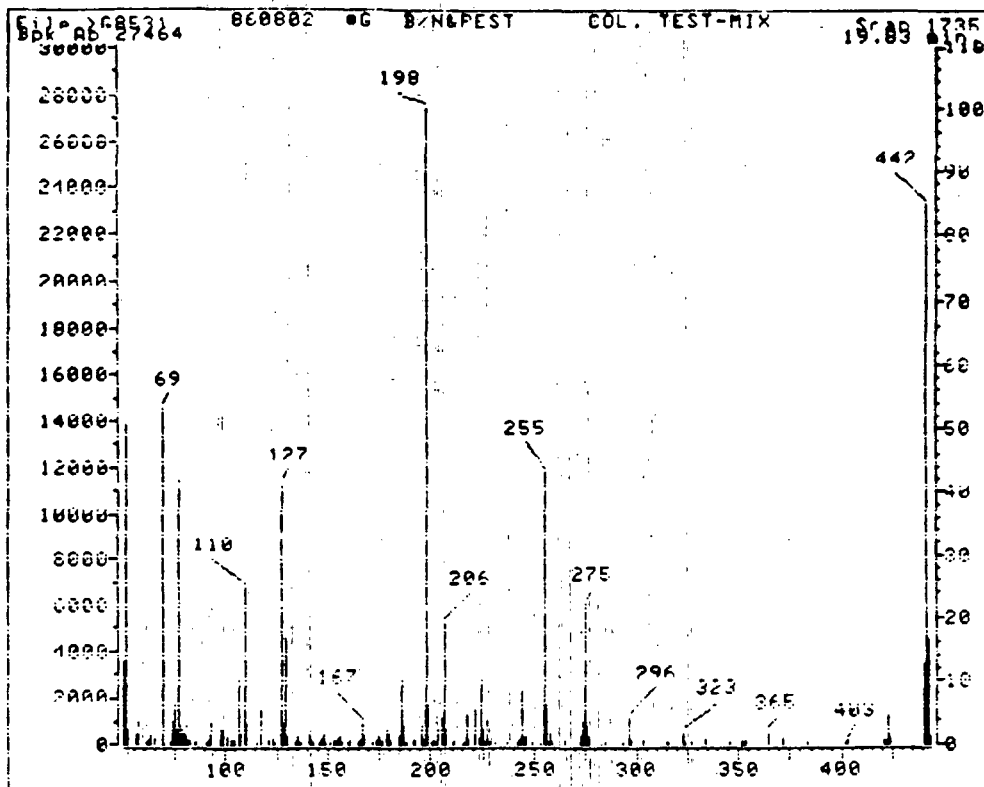


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.24	.24	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	12-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 19:34

Run No: 860801

Spectrum No: 1735

Analyst: Slapnick

Processor: Tom Kurowski

QC Batch: Q85395

Samples:

N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 Dil)  
N1252-N1253

8/8/86

AUG 8, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N0151 RESOURCE ENGINEERING

RES27514

SDB-2-36-38 860722 2100

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concn Added ug/kg	% Recov	Unspiked Sample ug/kg	Concn Added ug/kg	% Recov
1B	Acenaphthene	ND	71	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	130	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	71	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	1600	ND	ND	ND	0	-	ND	4040	7.
5B	Benzo(a)anthracene	ND	290	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	93	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	370	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	150	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	130	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	200	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	210	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	210	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	525	370	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	71	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	370	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	71	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	93	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	370	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	71	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	71	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	160	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	610	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	370	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	370	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	ND	370	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	210	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	71	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	BMDL	370	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	370	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	82	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	71	ND	ND	ND	0	-	ND	4040	90



AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0151 RESOURCE ENGINEERING

RES27514

SDB-2-36-38 860722 2100

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	71	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	34	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	370	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	60	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	170	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	82	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	60	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	71	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	370	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	370	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	71	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	200	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	71	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	71	ND	ND	ND	0	-	ND	4040	87

A Results variable due to Non-Homogeneous sample matrix.

B Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0151	RESOURCE ENGINEERING	RES27514	SDB-2-36-38	86072	2100	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	101	23	120
2-Fluorobiphenyl	50	84	30	115
Terphenyl-D14	50	99	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits				
** Advisory Limits Only				

• 198 EPA Control Limits  
 \*\* Advisory Limits Only

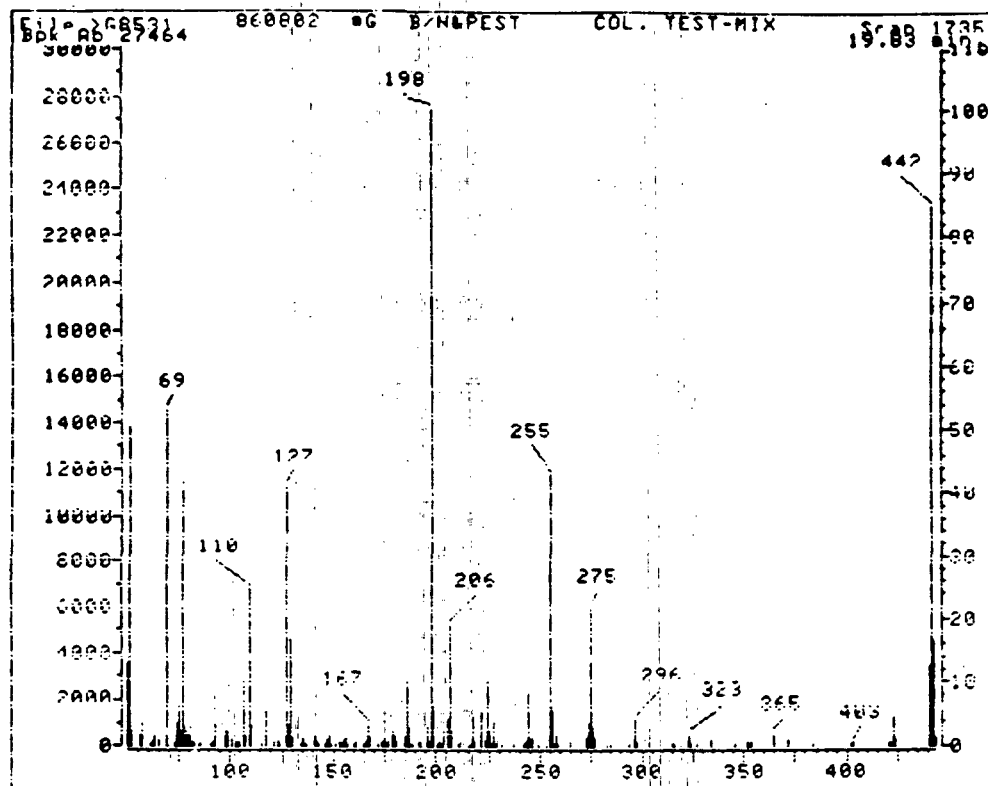


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.24	.24	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	17-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 15:34

Run No: 8531

Spectrum No: 1735

Analyst: Slapnick

Processor: Tom Kuorikoski

QC Batch: QB5395

Samples: N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 DIL)  
N1252-N1253

8/8/86

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0152 RESOURCE ENGINEERING

RES27514

SDB-2-40-42 860722 2105

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	74	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	74	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	1700	ND	ND	ND	0	-	ND	4040	7
5B	Benzo(a)anthracene	ND	300	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	97	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	390	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	220	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	220	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	ND	390	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	74	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	74	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	97	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	390	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	640	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	ND	390	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	220	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	74	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	ND	390	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	390	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	85	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	74	ND	ND	ND	0	-	ND	4040	90

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0152 RESOURCE ENGINEERING

RES27514 SDB-2-40-42 860722 2105

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov.	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov.
33B	Hexachlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	35	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	390	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	62	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	180	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	85	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	62	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	74	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	390	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	390	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	74	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	210	ND	ND	ND	0	-	ND	4040	98
45B	Pyrene	ND	74	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	87

a Results variable due to non-homogenous sample matrix.

b Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0152	RESOURCE ENGINEERING	RES27514	SDB-2-40-42	86072	2105	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	101	23	120
2-Fluorobiphenyl	50	84	30	115
Terphenyl-D14	50	112	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloredate	-	-	20..	150..
* IFB EPR Control Limits				
.. Advisory Limits Only				

\* IFB EPR Control Limits  
 \*\* Advisory Limits Only

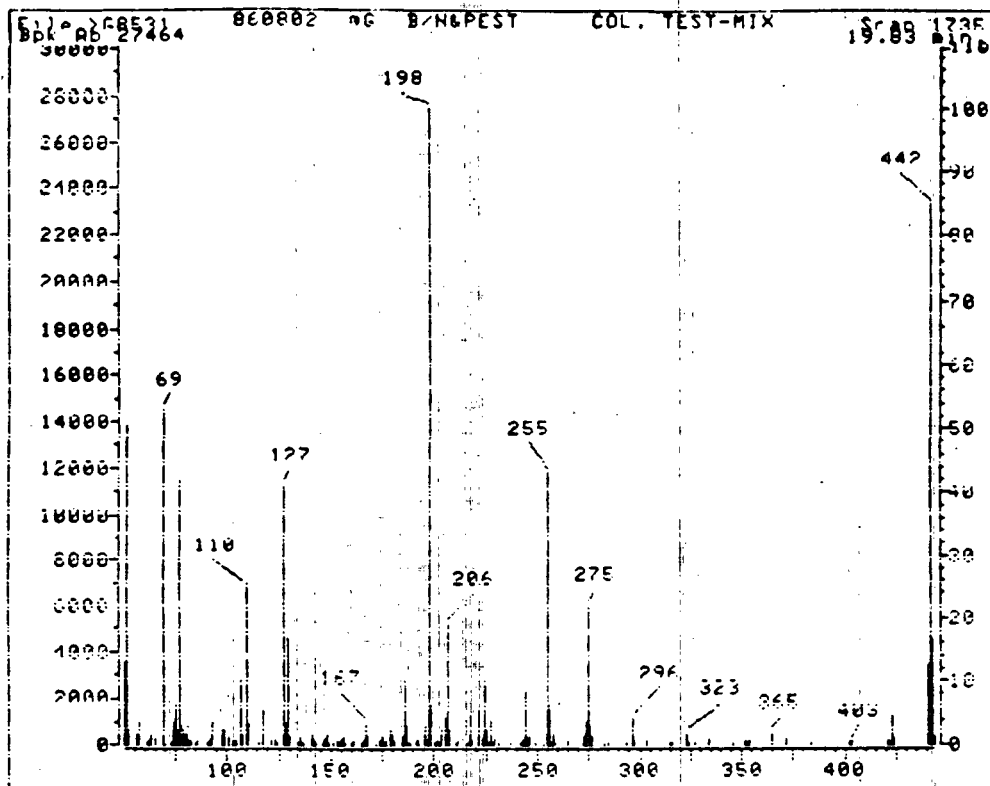


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFIPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.24	.24	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	12-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 15:34

Run No: 268531

Spectrum No: 1735

Analyst: *Snappuch*

Processor: *Tom Luoma*

QC Batch: *QB5395*

Samples: N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 dil)  
N1252-N1253

*8/8/86*

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0150

RESOURCE ENGINEERING

RES27514

SDB-2-46-48 860722 2120

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	74	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	74	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	1700	ND	ND	ND	0	-	ND	4040	7
5B	Benzo(a)anthracene	ND	300	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	98	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	390	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	220	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	220	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	BMDL	390	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	74	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	74	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	98	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	390	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	640	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	390	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	220	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	74	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	ND	390	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	390	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	86	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	74	ND	ND	ND	0	-	ND	4040	90



**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0150 RESOURCE ENGINEERING

RES27514 SDB-2-46-48 860722 2120

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	35	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	390	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	63	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	180	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	86	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	63	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	74	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	390	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	390	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	74	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	210	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	74	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	87

A Results variable due to Non-Homogenous sample matrix.

B Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

NO150	RESOURCE ENGINEERING	RES27514	SDB-2-46-48	86072	2120	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	99	23	120
2-Fluorobiphenyl	50	87	30	115
Terphenyl-D14	50	93	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFS EPA Control Limits				
** Advisory Limits Only				

\* IFB EPA Control Limits

\*\* Advisory Limits Only

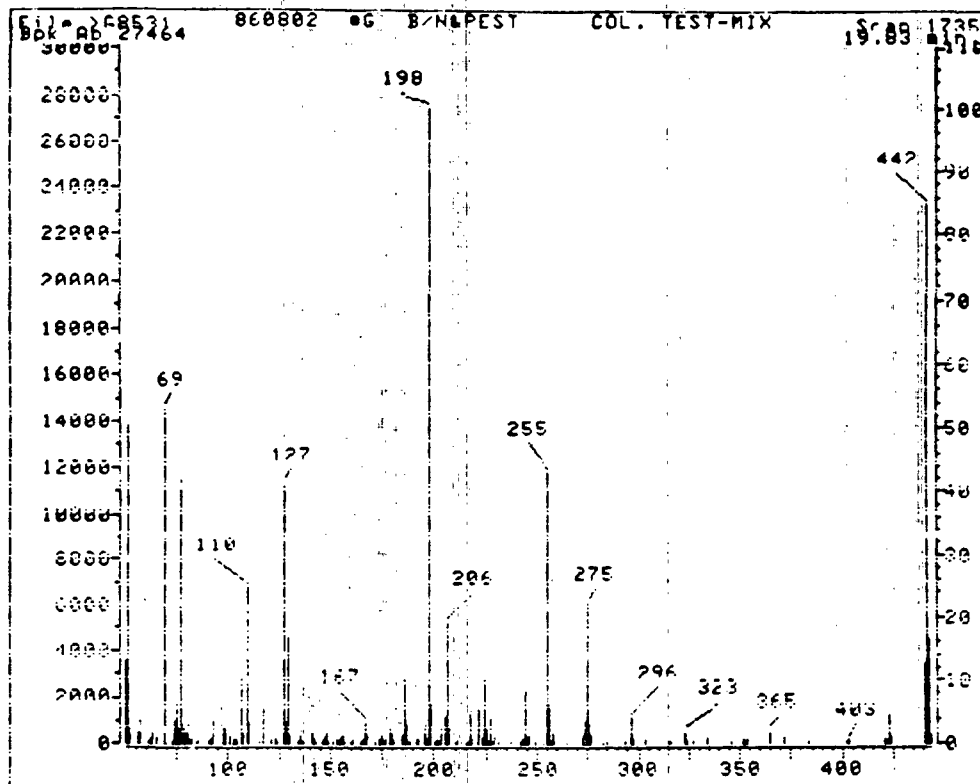


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.74	.74	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	12-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 15:34

Run No: 868551

Spectrum No: 1735

Analyst: Slapnick

Processor: Tom Kowalski

QC Batch: QB5395

Samples:

N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 DIL)  
N1252-N1253

8/8/86

AUG 8, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N0154 RESOURCE ENGINEERING

RES27514

SDB-2-50-52 860722 2125

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
	1B Acenaphthene	ND	76	ND	ND	ND	0	-	ND	4040	92
	2B Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4040	89
	3B Anthracene	ND	76	ND	ND	BMDL	0	-	ND	4040	93
	4B Benzidine	ND	1800	ND	ND	ND	0	-	ND	4040	7
	5B Benzo(a)anthracene	ND	310	ND	ND	ND	0	-	ND	4040	91
	6B Benzo(a)pyrene	ND	100	ND	ND	ND	0	-	ND	4040	89
	7B Benzo(b)fluoranthene	ND	400	ND	ND	ND	0	-	ND	4040	79
	8B Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
	9B Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4040	102
	10B bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4040	101
	11B bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	4040	93
	12B bis(2-Chloroisopropyl)ether	ND	230	ND	ND	ND	0	-	ND	4040	97
	13B bis(2-Ethylhexyl)phthalate	BMDL	400	60.8	ND	BMDL	0	-	159	4040	81
	14B 4-Bromophenyl phenyl ether	ND	76	ND	ND	ND	0	-	ND	4040	92
	15B Butyl benzyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	93
	16B 2-Chloronaphthalene	ND	76	ND	ND	ND	0	-	ND	4040	93
	17B 4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4040	88
	18B Chrysene	ND	100	ND	ND	ND	0	-	ND	4040	83
	19B Dibenzo(a,h)anthracene	ND	400	ND	ND	ND	0	-	ND	0	-
	20B 1,2-Dichlorobenzene	ND	76	ND	ND	ND	0	-	ND	4040	90
	21B 1,3-Dichlorobenzene	ND	76	ND	ND	ND	0	-	ND	4040	88
	22B 1,4-Dichlorobenzene	ND	180	ND	ND	ND	0	-	ND	4040	87
	23B 3,3'-Dichlorobenzidine	ND	660	ND	ND	ND	0	-	ND	4040	56
	24B Diethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	95
	25B Dimethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4040	96
	26B Di-n-butyl phthalate	ND	400	29.2	61.6	BMDL	0	-	151	4040	97
	27B 2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	4040	98
	28B 2,6-Dinitrotoluene	ND	76	ND	ND	ND	0	-	ND	4040	99
	29B Di-n-octyl phthalate	BMDL	400	43.7	ND	ND	0	-	ND	4040	83
	30B 1,2-Diphenylhydrazine	ND	400	ND	ND	ND	0	-	ND	4040	91
	31B Fluoranthene	ND	89	ND	ND	ND	0	-	ND	4040	90
	32B Fluorene	ND	76	ND	ND	ND	0	-	ND	4040	90

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0154 RESOURCE ENGINEERING

RES27514

SDB-2-50-52 860722 2125

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	76	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	36	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	400	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	64	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	89	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	64	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	76	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	400	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	400	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	76	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	220	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	76	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	76	ND	ND	ND	0	-	ND	4040	87

A Requires variable due to non-homogeneous sample matrix.

B Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

<b>N0154</b>	<b>RESOURCE ENGINEERING</b>	<b>RES27514</b>	<b>SDB-2-50-52 86072</b>	<b>2125</b>	<b>0</b>
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	92	23	120
2-Fluorobiphenyl	50	81	30	115
Terphenyl-D14	50	101	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IPB EPA Control Limits ** Advisory Limits Only				

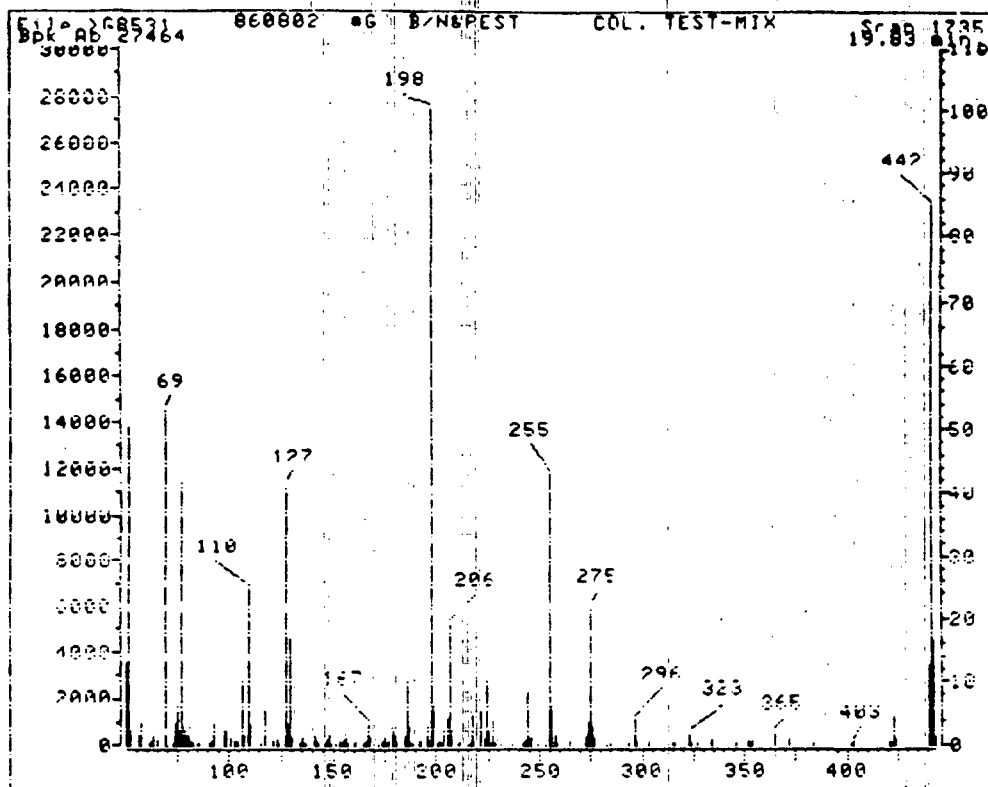


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.49	50.49	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.74	.74	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	17-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 15:34

Run No: 068531

Spectrum No: 1735

Analyst: *Slapnick*

Processor: *Tom Kuorn*

QC Batch: *QB5395*

Samples:

*N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 dil)  
N1252-N1253*

*B 8/8/86*

## Introduction

This report contains the analytical results on your soil sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### *Priority Pollutants*

The priority pollutant compounds and elements are listed with their NPDES (National Pollution Discharge Elimination System) numbers, and the Method Detection Limit (MDL) published in the Federal Register. When a compound or element is present below its published MDL it is reported as BMDL (Below Method Detection Limit). When a compound or element is not present at any detectable concentrations it is reported as ND (Not Detected). MDL's for non-aqueous matrices are based on USEPA published MDL's but are adjusted as per sample weight. Matrix spike and replicate analyses, where included, were performed on samples randomly chosen within each quality assurance batch and are therefore not necessarily spikes and replicates of this report's sample. Surrogate compound recovery data and instrument calibration data are included in the Method Performance Data Tables.



AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0170 RESOURCE ENGINEERING

RES27514

SDB-3-30-32 860723 0050

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	62	ND	ND	ND	0	-	ND	3290	94
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	ND	3290	96
3B	Anthracene	ND	62	ND	ND	ND	0	-	ND	3290	100
4B	Benzidine	ND	1400	ND	ND	ND	0	-	ND	3290	0.
5B	Benzo(a)anthracene	ND	250	ND	ND	ND	0	-	ND	3290	101
6B	Benzo(a)pyrene	ND	81	ND	ND	ND	0	-	ND	3290	100
7B	Benzo(b)fluoranthene	ND	320	ND	ND	ND	0	-	ND	3290	105
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3290	90
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3290	93
11B	bis(2-Chloroethyl) ether	ND	180	ND	ND	ND	0	-	ND	3290	88
12B	bis(2-Chloroisopropyl)ether	ND	180	ND	ND	ND	0	-	ND	3290	70
13B	bis(2-Ethylhexyl)phthalate	BMDL	320	41.2	70.4	BMDL	0	-	ND	3290	105
14B	4-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3290	99
15B	Butyl benzyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	101
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3290	93
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3290	99
18B	Chrysene	ND	81	ND	ND	ND	0	-	ND	3290	91
19B	Dibenzo(a,h)anthracene	ND	320	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	88
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	88
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3290	89
23B	3,3'-Dichlorobenzidine	ND	530	ND	ND	ND	0	-	ND	3290	88
24B	Diethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	104
25B	Dimethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	99
26B	Di-n-butyl phthalate	ND	320	ND	ND	458	0	-	ND	3290	113
27B	2,4-Dinitrotoluene	ND	180	ND	ND	ND	0	-	ND	3290	105
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3290	94
29B	Di-n-octyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	103
30B	1,2-Diphenylhydrazine	ND	320	ND	ND	ND	0	-	ND	3290	102
31B	Fluoranthene	ND	71	ND	ND	ND	0	-	ND	3290	109
32B	Fluorene	ND	62	ND	ND	ND	0	-	ND	3290	98

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0170 RESOURCE ENGINEERING

RES27514

SDB-3-30-32 860723 0050

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	101
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3290	93
35B	Hexachlorocyclopentadiene	ND	320	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	52	ND	ND	ND	0	-	ND	3290	90
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	71	ND	ND	ND	0	-	ND	3290	93
39B	Naphthalene	ND	52	ND	ND	ND	0	-	ND	3290	95
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3290	90
41B	N-Nitrosodimethylamine	ND	320	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	320	ND	ND	ND	0	-	ND	3290	90
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3290	111
44B	Phenanthrene	ND	170	ND	ND	ND	0	-	ND	3290	103
45B	Pyrene	ND	62	ND	ND	ND	0	-	ND	3290	113
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	93

a Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0170	RESOURCE ENGINEERING	RES27514	0
ETC Sample No.	Company	Facility	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	73	20	140
2-Fluorobiphenyl	50	85	20	140
Terphenyl-D14	50	94	20	150

© 1992 EPA Control Limits

AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**

**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0168 RESOURCE ENGINEERING

RES27514 SDB-3-44-46 860723 0140

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	60	ND	ND	ND	0	-	ND	3290	94
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	ND	3290	96
3B	Anthracene	ND	60	ND	ND	ND	0	-	ND	3290	100
4B	Benzidine	ND	1400	ND	ND	ND	0	-	ND	3290	0.
5B	Benzo(a)anthracene	ND	250	ND	ND	ND	0	-	ND	3290	101
6B	Benzo(a)pyrene	ND	80	ND	ND	ND	0	-	ND	3290	100
7B	Benzo(b)fluoranthene	ND	320	ND	ND	ND	0	-	ND	3290	105
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3290	90
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3290	93
11B	bis(2-Chloroethyl) ether	ND	180	ND	ND	ND	0	-	ND	3290	88
12B	bis(2-Chloroisopropyl)ether	ND	180	ND	ND	ND	0	-	ND	3290	70
13B	bis(2-Ethylhexyl)phthalate	ND	320	41.2	70.4	BMDL	0	-	ND	3290	105
14B	4-Bromophenyl phenyl ether	ND	60	ND	ND	ND	0	-	ND	3290	99
15B	Butyl benzyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	101
16B	2-Chloronaphthalene	ND	60	ND	ND	ND	0	-	ND	3290	93
17B	4-Chlorophenyl phenyl ether	ND	130	ND	ND	ND	0	-	ND	3290	99
18B	Chrysene	ND	80	ND	ND	ND	0	-	ND	3290	91
19B	Dibenzo(a,h)anthracene	ND	320	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	60	ND	ND	ND	0	-	ND	3290	88
21B	1,3-Dichlorobenzene	ND	60	ND	ND	ND	0	-	ND	3290	88
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3290	89
23B	3,3'-Dichlorobenzidine	ND	520	ND	ND	ND	0	-	ND	3290	88
24B	Diethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	104
25B	Dimethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	99
26B	Di-n-butyl phthalate	ND	320	ND	ND	458	0	-	ND	3290	113
27B	2,4-Dinitrotoluene	ND	180	ND	ND	ND	0	-	ND	3290	105
28B	2,6-Dinitrotoluene	ND	60	ND	ND	ND	0	-	ND	3290	94
29B	Di-n-octyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	103
30B	1,2-Diphenylhydrazine	ND	320	ND	ND	ND	0	-	ND	3290	102
31B	Fluoranthene	ND	70	ND	ND	ND	0	-	ND	3290	109
32B	Fluorene	ND	60	ND	ND	ND	0	-	ND	3290	98

AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0168 RESOURCE ENGINEERING

RES27514

SDB-3-44-46 860723 0140

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	60	ND	ND	ND	0	-	ND	3290	101
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3290	93
35B	Hexachlorocyclopentadiene	ND	320	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	51	ND	ND	ND	0	-	ND	3290	90
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	70	ND	ND	ND	0	-	ND	3290	93
39B	Naphthalene	ND	51	ND	ND	ND	0	-	ND	3290	95
40B	Nitrobenzene	ND	60	ND	ND	ND	0	-	ND	3290	90
41B	N-Nitrosodimethylamine	ND	320	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	320	ND	ND	ND	0	-	ND	3290	90
43B	N-Nitrosodiphenylamine	ND	60	ND	ND	ND	0	-	ND	3290	111
44B	Phenanthrene	ND	170	ND	ND	ND	0	-	ND	3290	103
45B	Pyrene	ND	60	ND	ND	ND	0	-	ND	3290	113
46B	1,2,4-Trichlorobenzene	ND	60	ND	ND	ND	0	-	ND	3290	93

% Recovery normally variable using established methodology.

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 1, 1986

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0168

RESOURCE ENGINEERING

RES27514

0

ETC Sample No:

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Amount added	% Recovery	Control Limits %	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	59	20	140
2-Fluorobiphenyl	50	65	20	140
Terphenyl-D14	50	95	20	150

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## Introduction

This report contains the analytical results on your soil sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### *Priority Pollutants*

The priority pollutant compounds and elements are listed with their NPDES (National Pollution Discharge Elimination System) numbers, and the Method Detection Limit (MDL) published in the Federal Register. When a compound or element is present below its published MDL it is reported as BMDL (Below Method Detection Limit). When a compound or element is not present at any detectable concentrations it is reported as ND (Not Detected). MDL's for non-aqueous matrices are based on USEPA published MDL's but are adjusted as per sample weight. Matrix spike and replicate analyses, where included, were performed on samples randomly chosen within each quality assurance batch and are therefore not necessarily spikes and replicates of this report's sample. Surrogate compound recovery data and instrument calibration data are included in the Method Performance Data Tables.

AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0171 RESOURCE ENGINEERING

RES27514

SDB-3-46-48 860723 0145

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concn. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concn. Added ug/kg	% Recov
1B	Acenaphthene	ND	62	ND	ND	ND	0	-	ND	3290	94
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	ND	3290	96
3B	Anthracene	ND	62	ND	ND	ND	0	-	ND	3290	100
4B	Benidine	ND	1400	ND	ND	ND	0	-	ND	3290	0.
5B	Benzo(a)anthracene	ND	250	ND	ND	ND	0	-	ND	3290	101
6B	Benzo(a)pyrene	ND	81	ND	ND	ND	0	-	ND	3290	100
7B	Benzo(b)fluoranthene	ND	320	ND	ND	ND	0	-	ND	3290	105
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3290	90
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3290	93
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3290	88
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3290	70
13B	bis(2-Ethylhexyl)phthalate	ND	320	41.2	70.4	ND	0	-	ND	3290	105
14B	4-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3290	99
15B	Butyl benzyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	101
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3290	93
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3290	99
18B	Chrysene	ND	81	ND	ND	ND	0	-	ND	3290	91
19B	Dibenzo(a,h)anthracene	ND	320	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	88
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	88
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3290	89
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3290	88
24B	Diethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	104
25B	Dimethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	99
26B	Di-n-butyl phthalate	ND	320	ND	ND	458	0	-	ND	3290	113
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3290	105
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3290	94
29B	Di-n-octyl phthalate	ND	320	ND	ND	ND	0	-	ND	3290	103
30B	1,2-Diphenylhydrazine	ND	320	ND	ND	ND	0	-	ND	3290	102
31B	Fluoranthene	ND	71	ND	ND	ND	0	-	ND	3290	109
32B	Fluorene	ND	62	ND	ND	ND	0	-	ND	3290	98



**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0171 RESOURCE ENGINEERING

RES27514

SDB-3-46-48 860723 0145

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	101
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3290	93
35B	Hexachlorocyclopentadiene	ND	320	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	52	ND	ND	ND	0	-	ND	3290	90
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	71	ND	ND	ND	0	-	ND	3290	93
39B	Naphthalene	ND	52	ND	ND	ND	0	-	ND	3290	95
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3290	90
41B	N-Nitrosodimethylamine	ND	320	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	320	ND	ND	ND	0	-	ND	3290	90
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3290	111
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3290	103
45B	Pyrene	ND	62	ND	ND	ND	0	-	ND	3290	113
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3290	93

A Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports					
N0171	RESOURCE ENGINEERING	RES27514			0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	79	20	140
2-Fluorobiphenyl	50	90	20	140
Terphenyl-D14	50	106	20	150

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## Introduction

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### *Priority Pollutants*

The priority pollutant compounds and elements are listed with their NPDES (National Pollution Discharge Elimination System) numbers, and the Method Detection Limit (MDL) published in the Federal Register. When a compound or element is present below its published MDL it is reported as BMDL (Below Method Detection Limit). When a compound or element is not present at any detectable concentrations it is reported as ND (Not Detected). MDL's for non-aqueous matrices are based on USEPA published MDL's but are adjusted as per sample weight. Matrix spike and replicate analyses, where included, were performed on samples randomly chosen within each quality assurance batch and are therefore not necessarily spikes and replicates of this report's sample. Surrogate compound recovery data and instrument calibration data are included in the Method Performance Data Tables.

AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0167 RESOURCE ENGINEERING

RES27514

SDB-3-48-50 860723 0150

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3290	94
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3290	96
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3290	100
4B	Benidine	ND	1500	ND	ND	ND	0	-	ND	3290	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3290	101
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3290	100
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3290	105
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3290	90
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3290	93
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3290	88
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3290	70
13B	bis(2-Ethylhexyl)phthalate	ND	330	41.2	70.4	BMDL	0	-	ND	3290	105
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3290	99
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3290	101
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3290	93
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3290	99
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3290	91
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3290	88
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3290	88
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3290	89
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3290	88
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3290	104
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3290	99
26B	Di-n-butyl phthalate	ND	330	ND	ND	458	0	-	ND	3290	113
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3290	105
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3290	94
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3290	103
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3290	102
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3290	109
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3290	98

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 5, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0167 RESOURCE ENGINEERING

RES27514

SDB-3-48-50 860723 0150

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3290	101
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3290	93
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3290	90
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3290	93
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3290	95
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3290	90
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3290	90
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3290	111
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3290	103
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3290	113
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3290	93

a Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports					
N0167	RESOURCE ENGINEERING	RES27514			0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	83	20	140
2-Fluorobiphenyl	50	88	20	140
Terphenyl-D14	50	105	20	150

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0181 RESOURCE ENGINEERING

RES27514

SDB-4-28-30 860723 2050

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	61	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	61	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	1400	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	250	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	80	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	320	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	180	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	180	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	320	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	61	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	61	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	130	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	80	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	320	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	61	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	61	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	530	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	180	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	61	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	320	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	70	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	61	ND	ND	ND	0	-	ND	3280	91

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0181 RESOURCE ENGINEERING RES27514 SDB-4-28-30 860723 2050  
ETC Sample No. Company Facility Sample Point Date Time Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	61	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	320	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	51	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	70	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	51	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	61	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	320	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	320	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	61	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	170	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	61	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	61	ND	ND	ND	0	-	ND	3280	90

\* Recovery normally variable using established methodology.

† Recovery annually verified.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0181	RESOURCE ENGINEERING	RES27514	SDB-4-28-30	86072	2050	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Flange Height

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	41	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	76	23	120
2-Fluorobiphenyl	50	90	30	115
Terphenyl-D14	50	58	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* 1980 EPA Control Limits				
** Subsequent Limits Only				

1. 170 EPA Control Limits

2. Recovery Limits Only

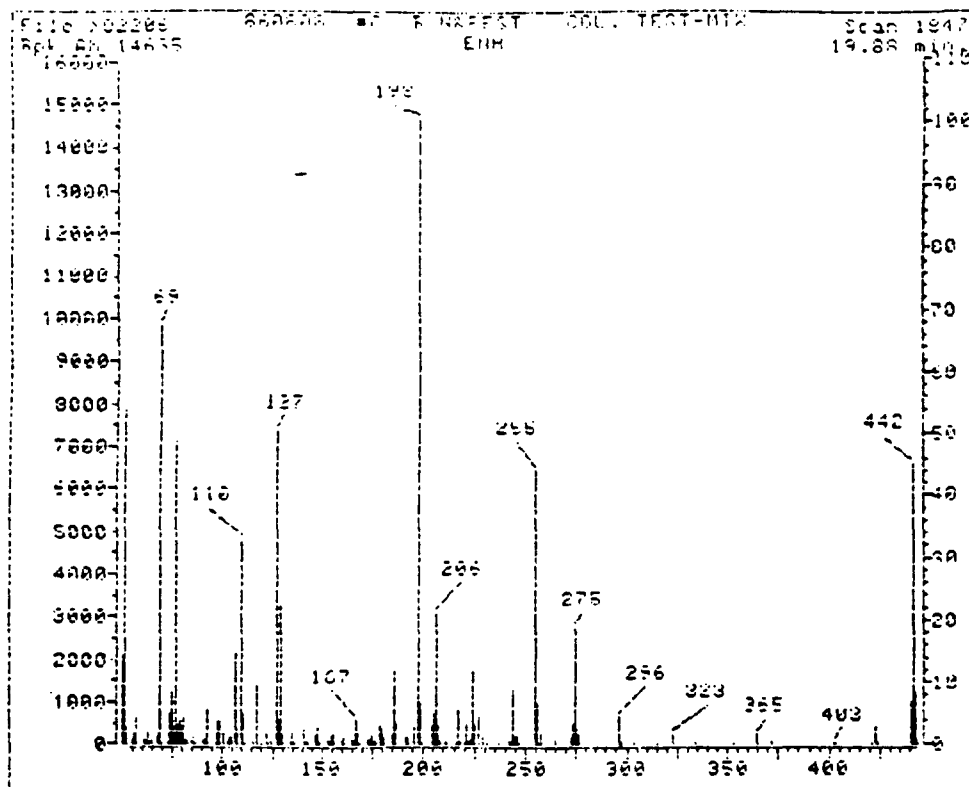


TABLE 2: METHOD PERFORMANCE DATA (CR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) For Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	53.67	53.67	OK
69	Less than 2% of mass 69	1.18	1.76	OK
69	(reference only)	67.08	67.08	OK
70	Less than 2% of mass 69	.12	.18	OK
127	40-60% of mass 198	50.42	50.42	OK
197	Less than 1% of mass 198	.14	.14	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.52	6.52	OK
275	10-30% of mass 198	18.68	18.68	OK
266	Greater than 1% of mass 198	1.61	1.61	OK
441	0-100% of mass 442	6.71	78.75	OK
442	Greater than 40% of mass 198	44.76	44.76	OK
443	17-23% of mass 442	8.52	19.03	OK

Injection Date: 08/08/86

Injection Time: 14:18

Run No: 002206

Spectrum No: 1847

Analyst: *[Signature]*

Processor: *Sharon M. [Signature]*

QC Batch: 08.5420

Samples: 00161-00165  
00179-00190

*[Handwritten initials]*  
5/13/86

AUG 13, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N0184 RESOURCE ENGINEERING

RES27514

SDB-4-34-36 860723 2100

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	1500	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	180	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	550	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3280	91

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0184 RESOURCE ENGINEERING

RES27514

SDB-4-34-36 860723 2100

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	90

a Recovery normally variable using established methodology.

b Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0184	RESOURCE ENGINEERING	RES27514	SDB-4-34-36	86072	2100	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	89	23	120
2-Fluorobiphenyl	50	103	30	115
Terphenyl-D14	50	104	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFS EPA Control Limits ** Recovery Limits Only				

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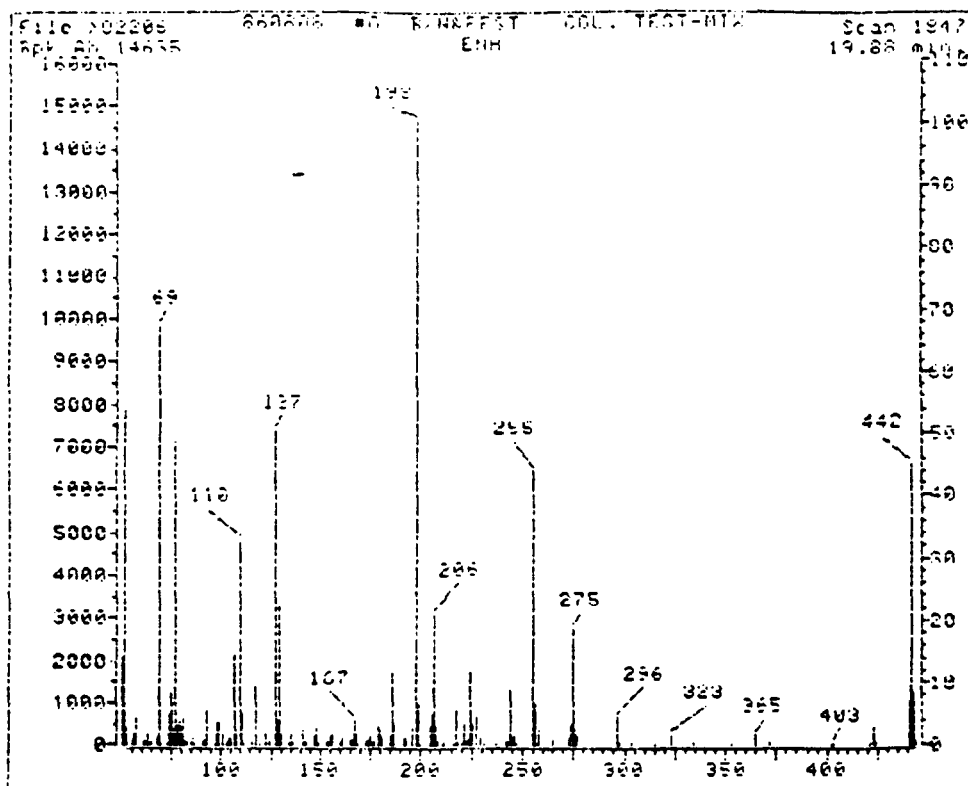


TABLE 2: METHOD PERFORMANCE DATA (GR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
69	30-60% of mass 198	53.67	53.67	OK
70	Less than 1% of mass 69	1.18	1.76	OK
69	(reference only)	62.08	62.08	OK
70	Less than 1% of mass 69	.12	.18	OK
127	40-60% of mass 198	50.42	50.42	OK
197	Less than 1% of mass 198	.14	.14	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.52	6.52	OK
275	10-30% of mass 198	18.68	18.68	OK
365	Greater than 1% of mass 198	1.61	1.61	OK
441	0-100% of mass 443	6.71	78.75	OK
442	Greater than 40% of mass 198	44.76	44.76	OK
443	17-23% of mass 442	8.52	19.03	OK

Injection Date: 08/08/86

Injection Time: 14:18

Run No: 002206

Spectrum No: 1847

Analyst: *V. White*

Processor: *Sharon Marklock*

QC Batch: *08.5420*

Samples: *N0161-N0165*  
*N0179-N0190*

*VS*  
*8/13/86*

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0183 RESOURCE ENGINEERING

RES27514 SDB-4-38-40 860723 2110

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3280	82
4B	Benidine	ND	1500	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	180	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	550	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3280	91

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0183 RESOURCE ENGINEERING

RES27514 SDB-4-38-40 860723 2110

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	BMDL	73	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	90

A Recovery normally variable using established methodology.

B Recovery annually verified.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0183	RESOURCE ENGINEERING	RES27514	SDB-4-38-40	86072	2110	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	90	23	120
2-Fluorobiphenyl	50	98	30	115
Terphenyl-D14	50	72	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* 100 ppm Control Limits ** Advisory Limits Only				

1. 100-100 Percent Limits

2. Recovery Limits Only

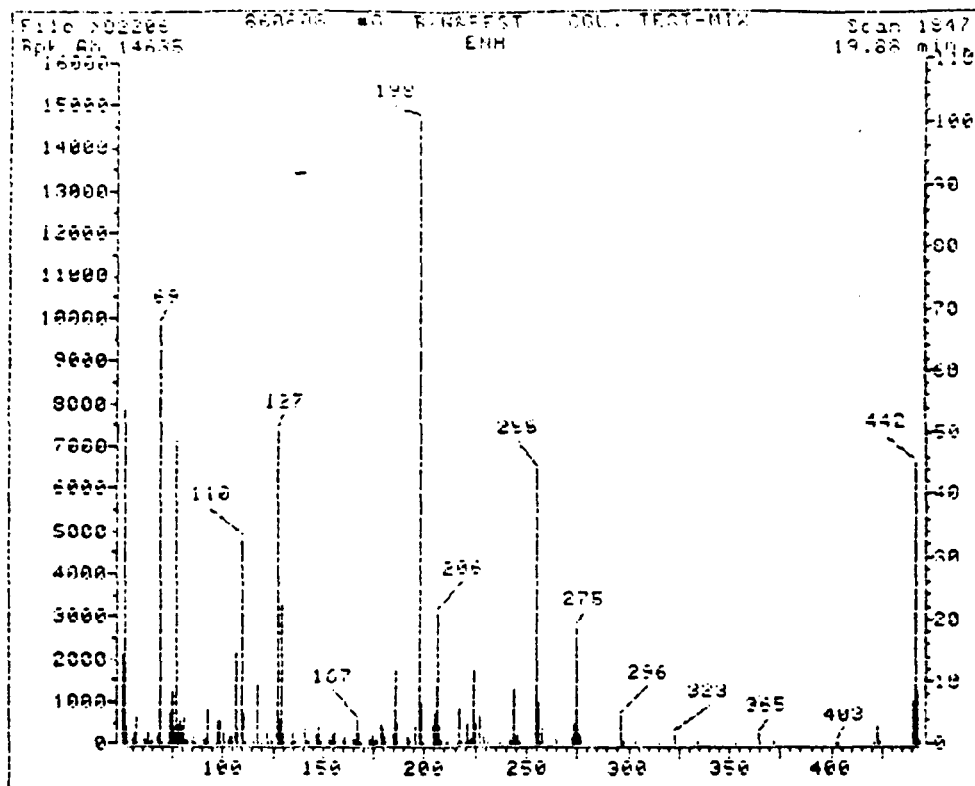


TABLE 2: METHOD PERFORMANCE DATA (CR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	53.67	53.67	OK
69	Less than 2% of mass 69	1.18	1.18	OK
69	(reference only)	67.08	67.08	OK
70	Less than 2% of mass 69	.12	.18	OK
127	40-60% of mass 198	50.42	50.42	OK
197	Less than 1% of mass 198	.14	.14	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.52	6.52	OK
275	10-30% of mass 198	18.68	18.68	OK
365	Greater than 1% of mass 198	1.61	1.61	OK
441	0-100% of mass 443	6.71	78.75	OK
442	Greater than 40% of mass 198	44.76	44.76	OK
443	17-23% of mass 442	8.52	19.03	OK

Injection Date: 08/08/86

Injection Time: 14:18

Run No: >02206

Spectrum No: 1847

Analyst: *K. J. Smith*

Processor: *Sharon Marlock*

GC Batch: *08.5420*

Samples: *N0160 - N0165*

*N0179 - N0190*

*VS 8/13/86*

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0179 RESOURCE ENGINEERING

RES27514

SDB-4-46-48 860723 2205

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	1500	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3280	91

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0179 RESOURCE ENGINEERING

RES27514

SDB-4-46-48 860723 2205

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	90

A Recovery normal: variable using established methodology.

B Recovery unusual: verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0179	RESOURCE ENGINEERING	RES27514	SDB-4-46-48	86072	2205	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	79	23	120
2-Fluorobiphenyl	50	105	30	115
Terphenyl-D14	50	76	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..

1. 175 PPM Control Limits  
 2. 150 PPM Control Limits

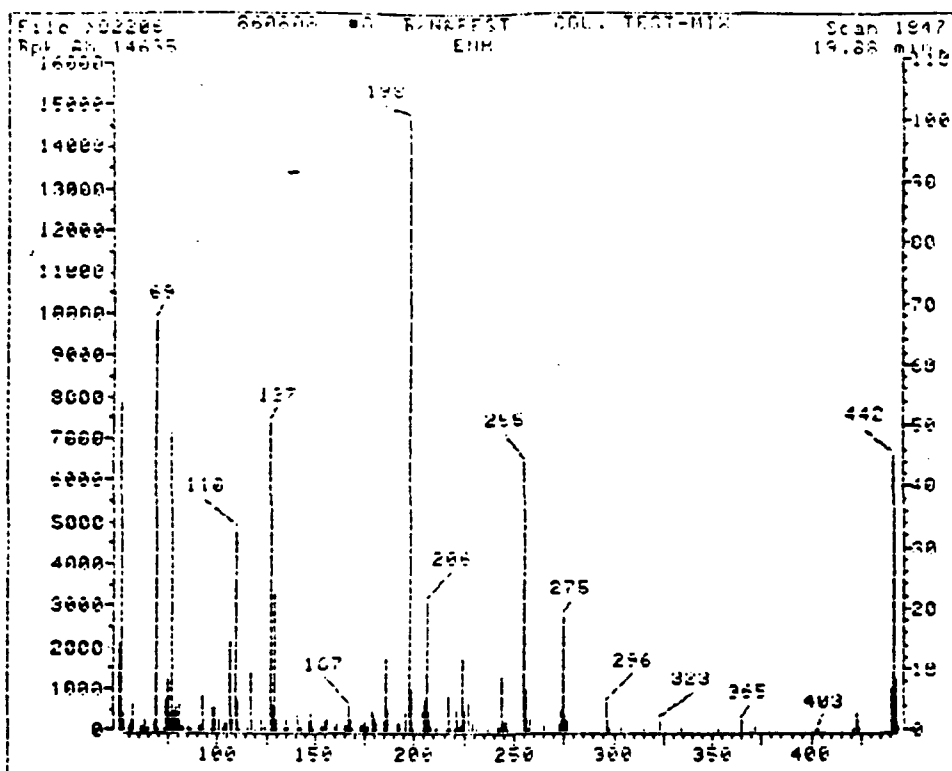


TABLE 2: METHOD PERFORMANCE DATA (GR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	53.67	53.67	OK
77	Less than 1% of mass 69	1.18	1.76	OK
69	(reference only)	67.08	67.08	OK
78	Less than 1% of mass 69	.12	.18	OK
127	40-60% of mass 198	50.42	50.42	OK
197	Less than 1% of mass 198	.14	.14	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.52	6.52	OK
275	10-30% of mass 198	18.68	18.68	OK
365	Greater than 1% of mass 198	1.61	1.61	OK
441	0-100% of mass 443	6.71	78.75	OK
442	Greater than 40% of mass 198	44.76	44.76	OK
443	17-23% of mass 442	8.52	19.03	OK

Injection Date: 08/08/86

Injection Time: 14:18

Run No: 002206

Spectrum No: 1847

Analyst: *[Signature]*

Processor: *Sharon Maxwell*

QC Batch: *085420*

Samples: *N0161 - N0165*  
*N0179 - N0190*

*VS*  
*8/13/86*

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0182 RESOURCE ENGINEERING

RES27514

SDB-4-50-52 860723 2215

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	72	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	90

a Recovery normally variable using established methodology.

b Recovery manually verified.

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0182 RESOURCE ENGINEERING

RES27514

SDB-4-50-52 860723 2215

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	1400	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	82	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	82	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	72	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3280	91



~~Charles Marshall~~  
08.5720  
N0161 - N0165  
N0179 - N0190

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0182	RESOURCE ENGINEERING	RES27514	SDB-4-50-52	86072	2215	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	89	23	120
2-Fluorobiphenyl	50	101	30	115
Terphenyl-D14	50	79	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
9 IPB EPA Control Limits 10 Reference Limits Only				

0-175 EPC Control Limits  
 50 Spenture Limiting Only

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0180 RESOURCE ENGINEERING

RES27514

SDB-4-56-58 860723 2235

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	61	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	320	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	51	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	71	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	51	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	61	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	320	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	320	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	61	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	170	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	61	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	61	ND	ND	ND	0	-	ND	3280	90

a Recovery normally variable using established methodology.

b Recovery manually verified.

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

**NO180 RESOURCE ENGINEERING**
**RES27514**
**SDB-4-56-58 860723 2235**

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	61	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	61	ND	ND	ND	0	-	ND	3280	82
4B	Benizidine	ND	1400	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	250	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	80	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	320	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	180	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	180	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	320	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	61	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	61	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	130	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	80	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	320	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	61	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	61	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	530	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	180	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	61	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	320	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	71	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	61	ND	ND	ND	0	-	ND	3280	91

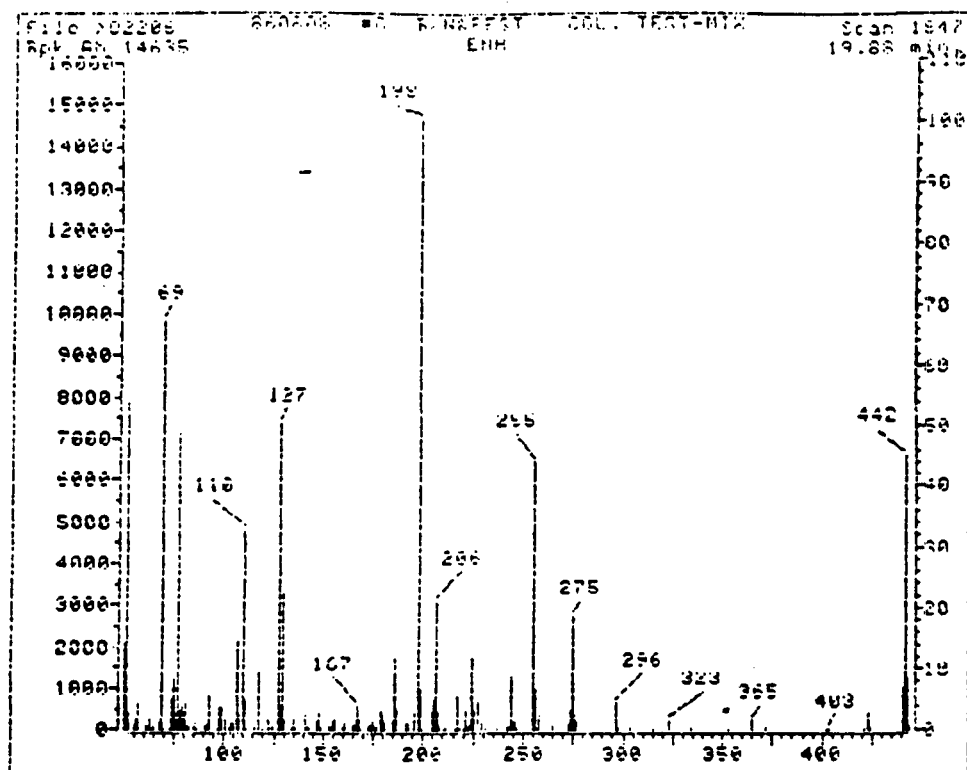


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	53.67	53.67	Ok
69	Less than 1% of mass 69	1.18	1.76	Ok
69	(reference only)	67.08	67.08	Ok
70	Less than 1% of mass 69	.12	.18	Ok
127	40-60% of mass 198	50.42	50.42	Ok
197	Less than 1% of mass 198	.14	.14	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.52	6.52	Ok
275	10-30% of mass 198	18.68	18.68	Ok
365	Greater than 1% of mass 198	1.61	1.61	Ok
441	0-100% of mass 443	6.71	78.75	Ok
442	Greater than 40% of mass 198	44.76	44.76	Ok
443	17-23% of mass 442	8.52	19.03	Ok

Injection Date: 08/08/86

Injection Time: 14:18

Run No: 202206

Spectrum No: 1847

Analyst: V. J. Naffat

Processor: Sharon Manlove

QC Batch: 08.5720

Samples: N0161-N0165  
N0179-N0190

*Handwritten:* 8/13/86

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0180	RESOURCE ENGINEERING	RES27514	SDB-4-56-58	86072	2235	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	79	23	120
2-Fluorobiphenyl	50	109	30	115
Terphenyl-D14	50	79	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFS EPA Control Limits ** Advisory Limits Only				

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AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0186 RESOURCE ENGINEERING RES27514 SDB-5-10-12 860724 1950  
ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	310	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	150	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	1600	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	260	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	760	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	360	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	1590	260	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	310	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	1600	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	1600	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	310	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	870	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	310	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	310	ND	ND	ND	0	-	ND	3280	90

a Large (fine) volume of extract resulted in elevated MDLs.  
 b Recovery normally variable using established methodology.  
 c Recovery manually verified.

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0186

RESOURCE ENGINEERING

RES27514

SDB-5-10-12 860724 1950

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	310	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	570	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	310	ND	ND	ND	0	-	ND	3280	82
4B	Benizidine	ND	7100	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	1300	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	400	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	1600	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	660	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	570	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	860	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	920	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	920	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	1600	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	310	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	1600	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	310	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	680	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	400	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	1600	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	310	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	310	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	710	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	2700	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	1600	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	1600	ND	ND	ND	0	-	ND	3280	92
26B	Di-n-butyl phthalate	ND	1600	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	920	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	310	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	1600	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	1600	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	360	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	310	ND	ND	ND	0	-	ND	3280	91



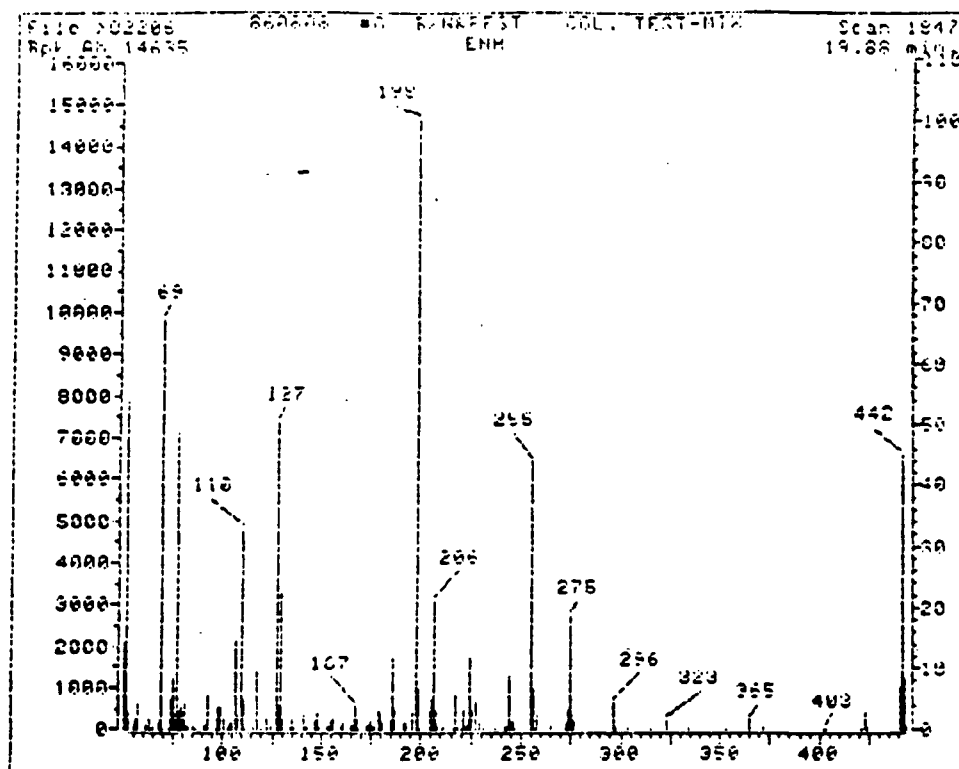


TABLE 2: METHOD PERFORMANCE DATA (DR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	53.67	53.67	Ok
69	Less than 2% of mass 69	1.18	1.76	Ok
69	(reference only)	67.08	67.08	Ok
70	Less than 2% of mass 69	.12	.18	Ok
127	40-60% of mass 198	50.42	50.42	Ok
197	Less than 1% of mass 198	.14	.14	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.52	6.52	Ok
275	10-30% of mass 198	18.68	18.68	Ok
265	Greater than 1% of mass 198	1.61	1.61	Ok
441	0-100% of mass 443	6.71	78.75	Ok
442	Greater than 40% of mass 198	44.76	44.76	Ok
443	17-23% of mass 442	8.52	19.03	Ok

Injection Date: 08/08/86

Injection Time: 14:18

Run No: >U2206

Spectrum No: 1847

Analyst: *[Signature]*

Processor: *Sharon Maslock*

QC Batch: *08.5420*

Samples: *NO1161-NO1165*  
*NO1179-NO1190*

*VJ*  
*8/13/86*

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports					
N0186	RESOURCE ENGINEERING	RES27514	SDB-5-10-12	86072	1950 0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	80	23	120
2-Fluorobiphenyl	50	103	30	115
Terphenyl-D14	50	77	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* 97% 99% General Limits				
** Advisory Limits Only				

\* IFB EPA Federal Limits  
\*\* Advisory Limits Only

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0190 RESOURCE ENGINEERING

RES27514

SDB-5-26-28 860725 0530

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3280	82
4B	Benizidine	ND	1500	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	180	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	550	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3280	91

## Introduction

This report contains the analytical results on your soil sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### *Priority Pollutants*

The priority pollutant compounds and elements are listed with their NPDES (National Pollution Discharge Elimination System) numbers, and the Method Detection Limit (MDL) published in the Federal Register. When a compound or element is present below its published MDL it is reported as BMDL (Below Method Detection Limit). When a compound or element is not present at any detectable concentrations it is reported as ND (Not Detected). MDL's for non-aqueous matrices are based on USEPA published MDL's but are adjusted as per sample weight. Matrix spike and replicate analyses, where included, were performed on samples randomly chosen within each quality assurance batch and are therefore not necessarily spikes and replicates of this report's sample. Surrogate compound recovery data and instrument calibration data are included in the Method Performance Data Tables.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0190	RESOURCE ENGINEERING	RES27514	SDB-S-26-28	86072	0530	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	79	23	120
2-Fluorobiphenyl	50	97	30	115
Terphenyl-D14	50	73	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloredate	-	-	20..	150..
© 1982 EPO Chemical Limited All Rights Reserved				

1. IFB EPC Control Limits  
 2. Recovery Limits Only

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0190 RESOURCE ENGINEERING

RES27514

SDB-5-26-28 860725 0530

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	90

A Recovery manually verified using established methodology.

B Recovery manually verified.

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

NO187 RESOURCE ENGINEERING RES27514 SDB-5-32-34 860725 0545  
ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	90

8 Recovery normally variable using established methodology.

9 Recovery manually verified.

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

NO187 RESOURCE ENGINEERING RES27514 SDB-5-32-34 860725 0545  
ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	1500	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	180	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	550	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3280	91



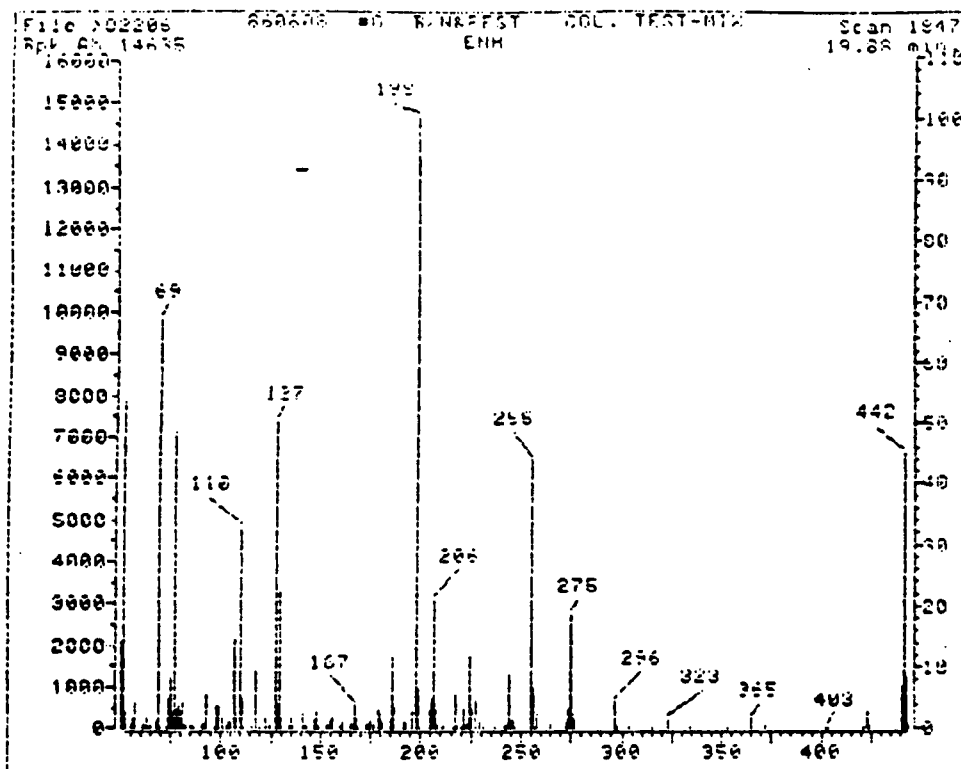


TABLE 2: METHOD PERFORMANCE DATA (CR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
69	30-60% of mass 198	53.67	53.67	OK
70	Less than 1% of mass 69	1.18	1.26	OK
69	(reference only)	67.08	67.08	OK
70	Less than 1% of mass 69	.12	.18	OK
127	40-60% of mass 198	50.42	50.42	OK
197	Less than 1% of mass 198	.14	.14	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.52	6.52	OK
275	10-30% of mass 198	18.68	18.68	OK
355	Greater than 1% of mass 198	1.61	1.61	OK
441	0-100% of mass 443	6.71	78.75	OK
442	Greater than 40% of mass 198	44.76	44.76	OK
443	17-23% of mass 442	8.52	19.03	OK

Injection Date: 08/08/86

Injection Time: 14:18

Run No: 002206

Spectrum No: 1847

Analyst: *[Signature]*

Processor: *[Signature]*

GC Batch: 08.5420

Samples: 00161-00165  
00179-00190

*[Handwritten signature]*  
8/13/86

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0187	RESOURCE ENGINEERING	RES27514	SDB-5-32-34	86072	0545	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	82	23	120
2-Fluorobiphenyl	50	99	30	115
Terphenyl-D14	50	78	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
9 EPA EPA Control Limits 99 Advanced Limit Only				

9-170 EPA Control Limits  
 99 Recovery Limit Only

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports					
NO189	RESOURCE ENGINEERING	RES27514	SDB-5-40-42	860725	0555
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	62	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	62	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	1400	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	82	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	62
14B	3-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	82	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	72	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	62	ND	ND	ND	0	-	ND	3280	91

## Introduction

This report contains the analytical results on your soil sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

The results obtained from your sample are presented in tabular format immediately following this introduction. Quality assurance data is tabulated along with the appropriate sample results for verification. Depending on the analyses ordered, the quality assurance data may include results from blank, spiked blank, spiked sample (i.e. matrix spike) and replicate sample as well as results from surrogate compound analyses. Quality assurance data for verification of proper instrument performance is also included where appropriate. The report appendices include the chain of custody record for your sample and, where appropriate, the gas chromatograms and mass spectra.

The procedures used in the analysis of the sample are described in this report's methodology section. All analytical procedures within our laboratory are performed within a strictly enforced Quality Assurance Protocol. A description of this Protocol is included in the report.

## Results

Sample results, and associated quality assurance data, are always tabulated in one or more of this report's Quantitative Results Tables. The format of each table varies with the class of analysis.

### *Priority Pollutants*

The priority pollutant compounds and elements are listed with their NPDES (National Pollution Discharge Elimination System) numbers, and the Method Detection Limit (MDL) published in the Federal Register. When a compound or element is present below its published MDL it is reported as BMDL (Below Method Detection Limit). When a compound or element is not present at any detectable concentrations it is reported as ND (Not Detected). MDL's for non-aqueous matrices are based on USEPA published MDL's but are adjusted as per sample weight. Matrix spike and replicate analyses, where included, were performed on samples randomly chosen within each quality assurance batch and are therefore not necessarily spikes and replicates of this report's sample. Surrogate compound recovery data and instrument calibration data are included in the Method Performance Data Tables.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports						
N0189	RESOURCE ENGINEERING	RES27514	SDB-5-40-42	86072	0555	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	75	23	120
2-Fluorobiphenyl	50	86	30	115
Terphenyl-D14	50	65	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits				
** Advisory Limits Only				

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0189 RESOURCE ENGINEERING

RES27514 SDB-5-40-42 860725 0555

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	52	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	72	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	52	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	62	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	90

A Recovery normally variable using established methodology.

B Recovery usually verified.

## Introduction

This report contains the analytical results on your soil sample. It is designed to include comprehensive data from the entire analytical process in order to satisfy the needs of various levels of review.

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## Results

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The priority pollutant compounds and elements are listed with their NPDES (National Pollution Discharge Elimination System) numbers, and the Method Detection Limit (MDL) published in the Federal Register. When a compound or element is present below its published MDL it is reported as BMDL (Below Method Detection Limit). When a compound or element is not present at any detectable concentrations it is reported as ND (Not Detected). MDL's for non-aqueous matrices are based on USEPA published MDL's but are adjusted as per sample weight. Matrix spike and replicate analyses, where included, were performed on samples randomly chosen within each quality assurance batch and are therefore not necessarily spikes and replicates of this report's sample. Surrogate compound recovery data and instrument calibration data are included in the Method Performance Data Tables.

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

NO188 RESOURCE ENGINEERING RES27514 SDB-5-48-50 860725 0610  
 ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	1500	ND	ND	ND	0	-	ND	3280	0 <sub>a</sub>
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	180	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	550	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92 <sub>a</sub>
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3280	91



AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0188 RESOURCE ENGINEERING

RES27514

SDB-5-48-50 860725 0610

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	90

A Recovery normally variable using established methodology.

B Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0188	RESOURCE ENGINEERING	RES27514	SDB-5-48-50	86072	0610	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	81	23	120
2-Fluorobiphenyl	50	93	30	115
Terphenyl-D14	50	78	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits				
** Advisory Limits Only				

\* IFB EPA Control Limits

\*\* Advisory Limits Only



AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0185 RESOURCE ENGINEERING

RES27514

SDB-5-58-60 860725 0640

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	90

A Recovery normally variable using established methodology.

B Recovery manually verified.

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0185 RESOURCE ENGINEERING

RES27514

SDB-5-58-60 860725 0640

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	1500	ND	ND	ND	0	-	ND	3280	0 <sub>a</sub>
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	180	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	550	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92 <sub>a</sub>
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3280	91

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0185	RESOURCE ENGINEERING	RES27514	SDB-5-58-60	86072	0640	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits .	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	92	23	120
2-Fluorobiphenyl	50	107	30	115
Terphenyl-D14	50	93	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchlorodate	-	-	20..	150..
* IFB EPA Control Limits				
** Advisory Limits Only				

\* IFB EPR Control Limits

\*\* Advisory Limits Only

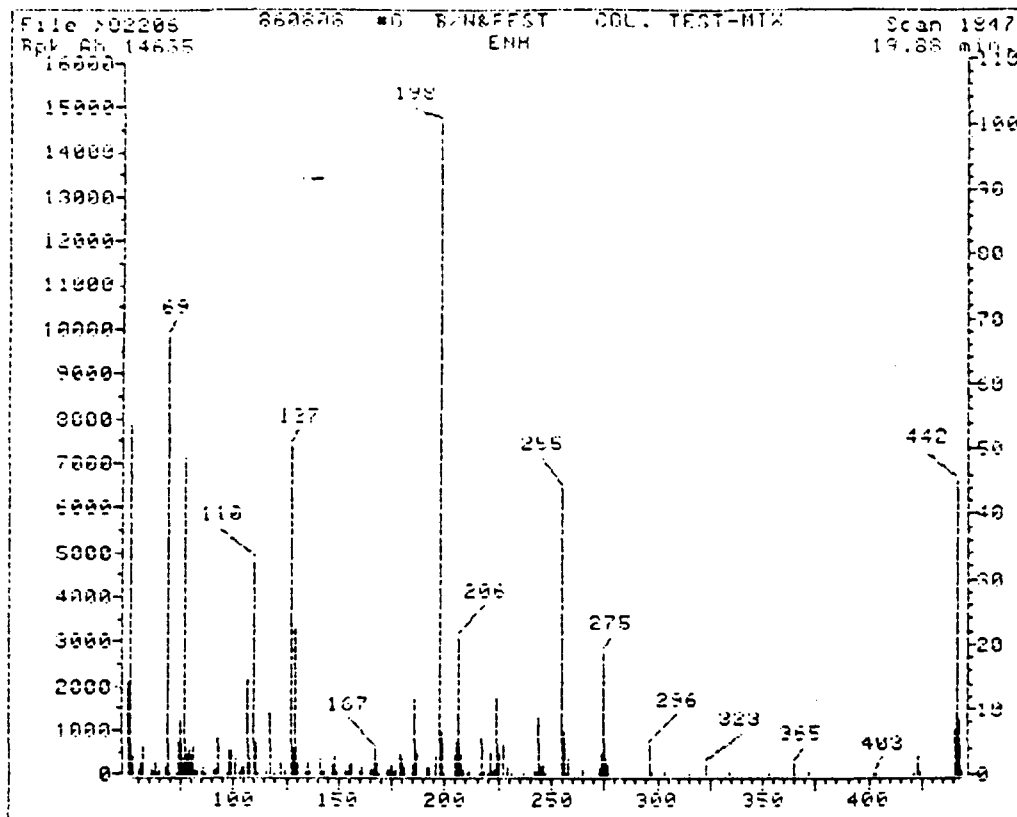


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	53.67	53.67	OK
69	Less than 2% of mass 69	1.18	1.76	OK
69	(reference only)	67.08	67.08	OK
70	Less than 2% of mass 69	.12	.18	OK
127	40-60% of mass 198	50.42	50.42	OK
197	Less than 1% of mass 198	.14	.14	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.52	6.52	OK
275	10-30% of mass 198	18.68	18.68	OK
365	Greater than 1% of mass 198	1.61	1.61	OK
441	0-100% of mass 443	6.71	78.75	OK
442	Greater than 40% of mass 198	44.76	44.76	OK
443	17-23% of mass 442	8.52	19.03	OK

Injection Date: 08/08/86

Injection Time: 14:18

Run No: 702206

Spectrum No: 1847

Analyst: *K. White*

Processor: *Sharon Moulton*

QC Batch: *085420*

Samples: *N0161-N0165*  
*N0179-N0190*

*VJ*  
*8/13/86*

## TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0162 RESOURCE ENGINEERING

RES27514

SDB-6-12-14 860724 0230

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	320	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	580	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	320	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	7300	ND	ND	ND	0	-	ND	3280	0
5B	Benzo(a)anthracene	ND	1300	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	420	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	1700	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	680	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	580	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	880	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	950	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	950	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	1700	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	320	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	1700	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	320	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	700	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	420	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	1700	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	320	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	320	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	730	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	2700	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	1700	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	1700	ND	ND	ND	0	-	ND	3280	92
26B	Di-n-butyl phthalate	ND	1700	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	950	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	320	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	1700	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	1700	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	370	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	320	ND	ND	ND	0	-	ND	3280	91

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0162 RESOURCE ENGINEERING

RES27514

SDB-6-12-14 860724 0230

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg <sup>a</sup>	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	320	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	150	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	1700	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	270	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	780	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	370	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	270	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	320	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	1700	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	1700	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	320	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	900	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	320	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	320	ND	ND	ND	0	-	ND	3280	90

<sup>a</sup> Large final volume of extract resulted in elevated MDLs.<sup>b</sup> Recovery normally variable using established methodology.<sup>c</sup> Recovery manually verified.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery – Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0162

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Amount Added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	86	23	120
2-Fluorobiphenyl	50	109	30	115
Terphenyl-D14	50	91	18	137
PESTICIDE/PCB FRACTION (GC/MS)				
Dibutylchloroendate	-	-	20**	150**
* IFB EPA Control Limits. ** Advisory Limits Only.				

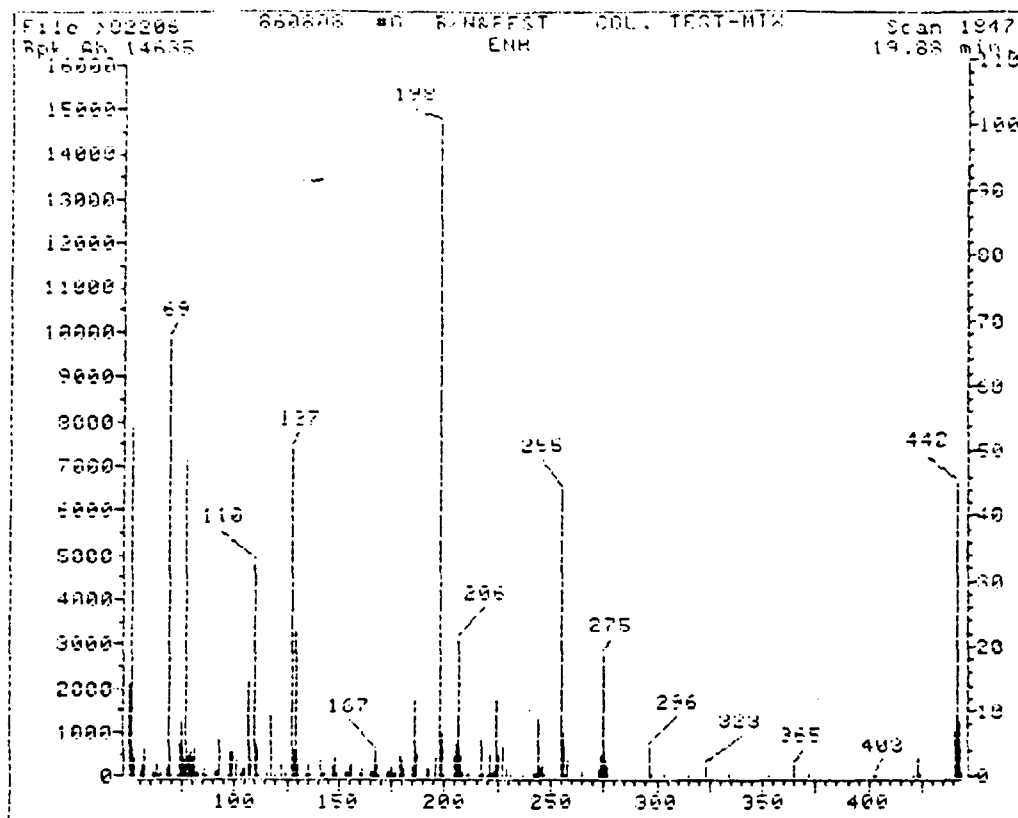


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	53.67	53.67	OK
69	Less than 2% of mass 69	1.18	1.76	OK
69	(reference only)	67.08	67.08	OK
70	Less than 2% of mass 69	.12	.18	OK
127	40-60% of mass 198	50.42	50.42	OK
192	Less than 1% of mass 198	.14	.14	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.52	6.52	OK
275	10-30% of mass 198	18.68	18.68	OK
365	Greater than 1% of mass 198	1.61	1.61	OK
441	0-100% of mass 443	6.71	78.75	OK
442	Greater than 40% of mass 198	44.76	44.76	OK
443	17-23% of mass 442	8.52	19.03	OK

Injection Date: 08/08/86

Injection Time: 14:18

Run No: >U2206

Spectrum No: 1847

Analyst: *[Signature]*

Processor: *Sharon Maylock*

QC Batch: *08.5420*

Samples: *NO161-NO165*  
*NO179-NO190*

*VS*  
*5/13/86*

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0161

RESOURCE ENGINEERING

RES27514

SDB-6-28-30 860724 0305

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concn. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concn. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3280	82
4B	Benztidine	ND	1500	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	180	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	550	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3280	91

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0161 RESOURCE ENGINEERING

RES27514

SDB-6-28-30 860724 0305

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	67.4	53	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	90

A Recovery normally variable using established methodology.

B Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0161	RESOURCE ENGINEERING	RES27514	SDB-6-28-30	86072	0305	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added	% Recovery	Control Limits ,	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	85	23	120
2-Fluorobiphenyl	50	112	30	115
Terphenyl-D14	50	86	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits				
** Advisory Limits Only				

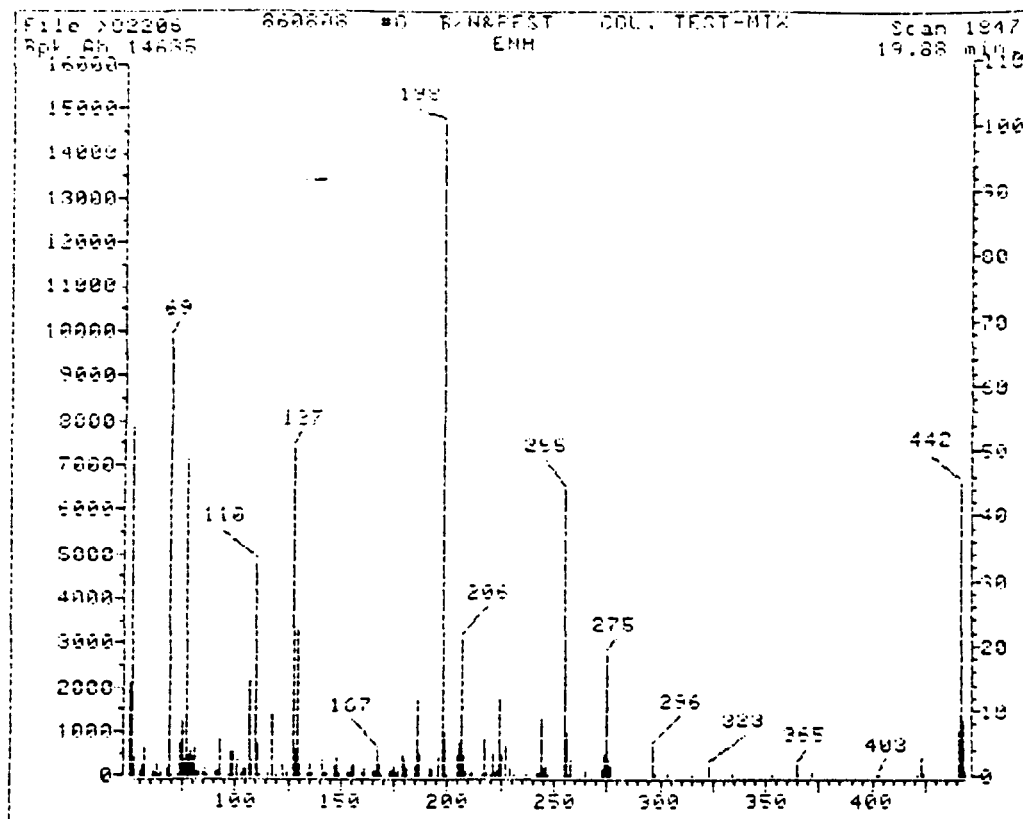


TABLE 2: METHOD PERFORMANCE DATA (GR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
69	30-60% of mass 198	93.67	93.67	OK
78	Less than 1% of mass 69	1.18	1.76	OK
69	(reference only)	67.08	67.08	OK
78	Less than 1% of mass 69	.12	.18	OK
127	40-60% of mass 198	50.42	50.42	OK
197	Less than 1% of mass 198	.14	.14	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.52	6.52	OK
275	10-30% of mass 198	18.68	18.68	OK
365	Greater than 1% of mass 198	1.61	1.61	OK
441	0-100% of mass 443	6.71	78.75	OK
442	Greater than 40% of mass 198	44.76	44.76	OK
443	17-23% of mass 442	8.52	19.03	OK

Injection Date: 08/08/86

Injection Time: 14:18

Run No: >02206

Spectrum No: 1847

Analyst: *[Signature]*

Processor: *Sharon Maxwell*

QC Batch: *085420*

Samples: *N0161-N0165*  
*N0179-N0190*

*VS*  
*8/13/86*



**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0164 RESOURCE ENGINEERING RES27514 SDB-6-38-40 860724 0350  
ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	62	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	62	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	1400	ND	ND	ND	0	-	ND	3280	0.
5B	Benzo(a)anthracene	ND	250	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	81	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	320	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	320	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	81	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	320	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	92.
26B	Di-n-butyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	320	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	320	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	71	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	62	ND	ND	ND	0	-	ND	3280	91

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0164

RESOURCE ENGINEERING

RES27514

SDB-6-38-40 860724 0350

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	320	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	52	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	71	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	52	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	320	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	320	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	62	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	90

A Recovery normally variable using established methodology.

B Recovery manually verified.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0164	RESOURCE ENGINEERING	RES27514	SDB-6-38-40	86072	0350	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	90	23	120
2-Fluorobiphenyl	50	101	30	115
Terphenyl-D14	50	76	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits				
** Advisory Limits Only				

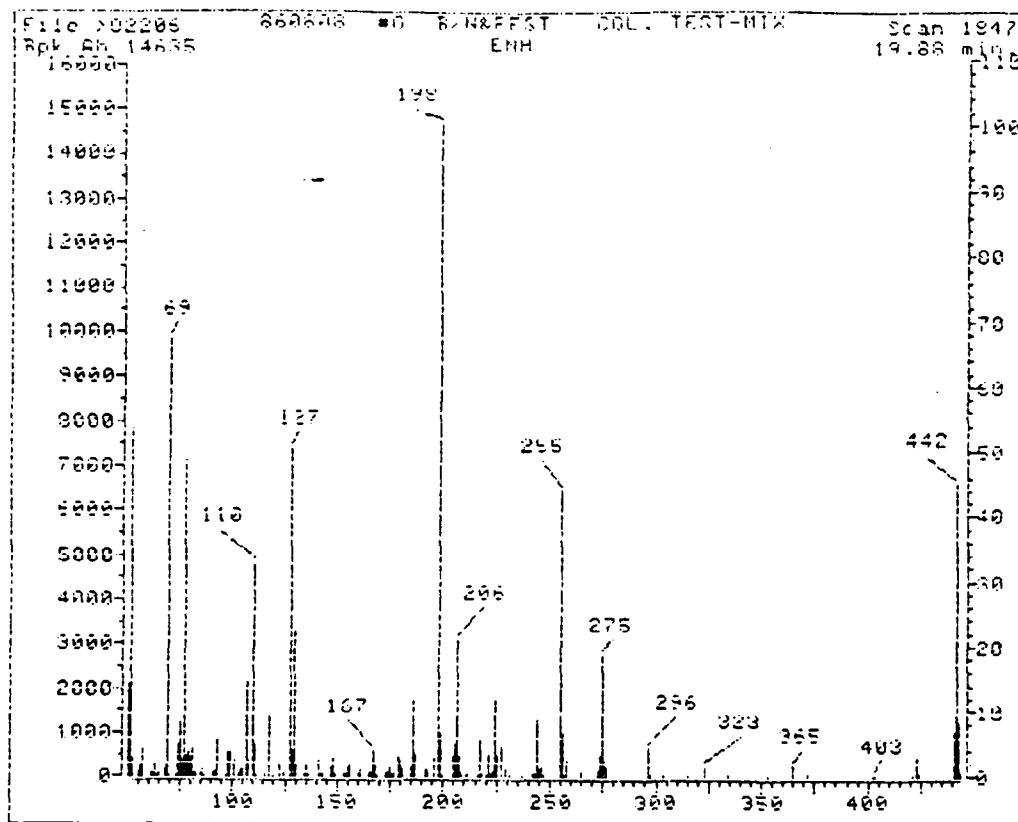


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	53.67	53.67	OK
69	Less than 2% of mass 69	1.18	1.76	OK
69	(reference only)	67.08	67.08	OK
70	Less than 2% of mass 69	.12	.18	OK
127	40-60% of mass 198	50.42	50.42	OK
197	Less than 1% of mass 198	.14	.14	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.52	6.52	OK
275	10-30% of mass 198	18.68	18.68	OK
365	Greater than 1% of mass 198	1.61	1.61	OK
441	0-100% of mass 443	6.71	78.75	OK
442	Greater than 40% of mass 198	44.76	44.76	OK
443	17-23% of mass 442	8.52	19.03	OK

Injection Date: 08/08/86

Injection Time: 14:18

Run No: >02206

Spectrum No: 1847

Analyst: *[Signature]*

Processor: *[Signature]*

QC Batch: 08.5420

Samples: N0161-N0165  
N0179-N0190

*VJ*  
*8/13/86*



AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0165 RESOURCE ENGINEERING

RES27514

SDB-6-48-50 860724 0410

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	62	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	62	ND	ND	ND	0	-	ND	3280	82
4B	Benzidine	ND	1400	ND	ND	ND	0	-	ND	3280	0a
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	82	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	82	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92a
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	72	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	62	ND	ND	ND	0	-	ND	3280	91

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0165 RESOURCE ENGINEERING

RES27514

SDB-6-48-50 860724 0410

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	52	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	72	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	52	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	62	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3280	90

A Recovery normally variable using established methodology.

B Recovery annually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0165	RESOURCE ENGINEERING	RES27514	SDB-6-48-50	86072	0410	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	88	23	120
2-Fluorobiphenyl	50	98	30	115
Terphenyl-D14	50	83	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* 178 EPA Control Limits				
** Advisory Limits Only				

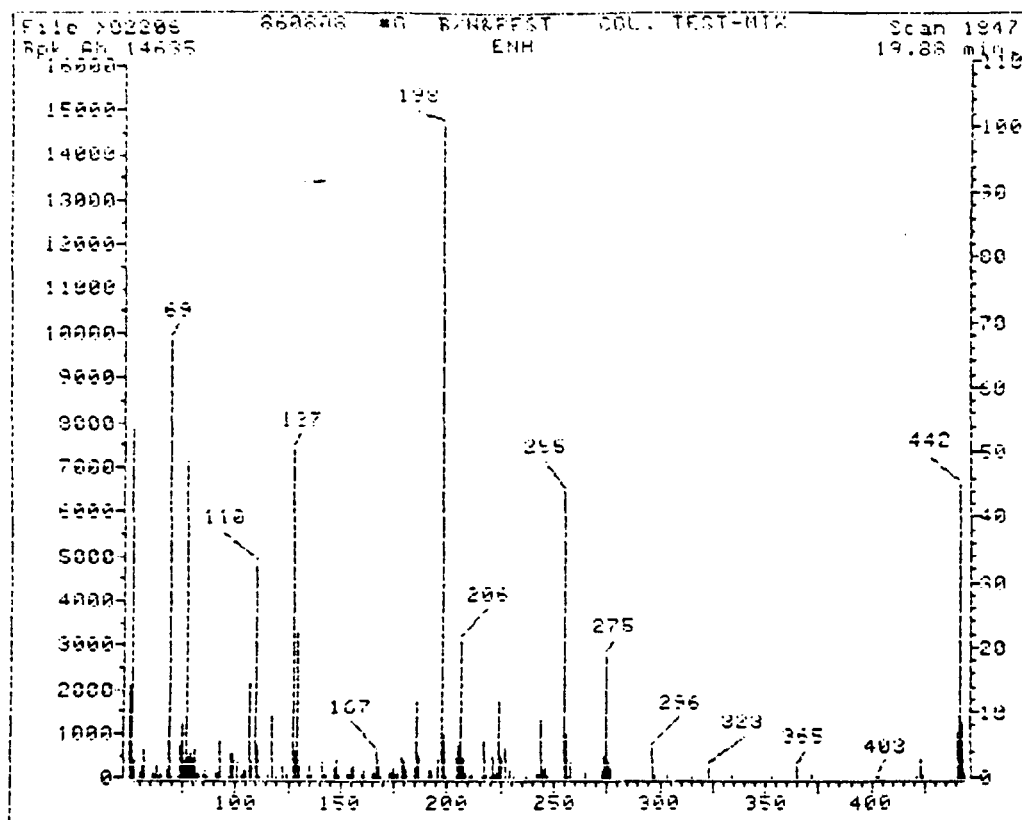


TABLE 2: METHOD PERFORMANCE DATA (GR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	53.67	53.67	OK
68	Less than 2% of mass 69	1.18	1.76	OK
69	(reference only)	67.08	67.08	OK
70	Less than 2% of mass 69	.12	.18	OK
127	40-60% of mass 198	50.42	50.42	OK
197	Less than 1% of mass 198	.14	.14	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.52	6.52	OK
275	10-30% of mass 198	18.68	18.68	OK
365	Greater than 1% of mass 198	1.61	1.61	OK
441	0-100% of mass 443	6.71	78.75	OK
442	Greater than 40% of mass 198	44.76	44.76	OK
443	17-23% of mass 442	8.52	19.03	OK

Injection Date: 08/08/86

Injection Time: 14:18

Run No: >02206

Spectrum No: 1847

Analyst: *V. J. White*

Processor: *Sharon M. Loeck*

QC Batch: *085720*

Samples: *N0161-N0165*  
*N0179-N0190*

*VJ*  
*8/13/86*

## TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N0163 RESOURCE ENGINEERING

RES27514 SDB-6-52-54 860724 0420

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3280	91
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3280	76
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3280	82
4B	Benizidine	ND	1500	ND	ND	ND	0	-	ND	3280	0 <sup>a</sup>
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3280	88
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3280	64
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3280	76
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3280	74
10B	bis(2-Chloroethoxy)methane	ND	180	ND	ND	ND	0	-	ND	3280	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3280	89
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3280	57
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	ND	0	-	ND	3280	82
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3280	100
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3280	90
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3280	89
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3280	98
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	83
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	84
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3280	87
23B	3,3'-Dichlorobenzidine	ND	550	ND	ND	ND	0	-	ND	3280	6
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	94
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	92 <sup>a</sup>
26B	Di-n-butyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	81
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3280	82
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3280	87
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3280	80
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3280	85
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3280	69
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3280	91

AUG 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0163 RESOURCE ENGINEERING

RES27514

SDB-6-52-54 860724 0420

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	100
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3280	91
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3280	92
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3280	90
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3280	90
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3280	93
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3280	87
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3280	74
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3280	96
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3280	66
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3280	90

A Recovery normally variable using established methodology.

B Recovery manually verified.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Aqueous Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0163	RESOURCE ENGINEERING	RES27514	SDB-6-52-54	86072	0420	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits .	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	88	110
p-Bromofluorobenzene	-	-	86	115
1,2-Dichloroethane-D4	-	-	76	114
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	10	94
2-Fluorophenol	-	-	21	100
2,4,6-Tribromophenol	-	-	10	123
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	83	35	114
2-Fluorobiphenyl	50	103	43	116
Terphenyl-D14	50	82	33	141
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	24..	154..
* IFB EPA Control Limits				
** Advisory Limits Only				

\* 17B EPA Control Limits

\*\* Advisory Limits Only

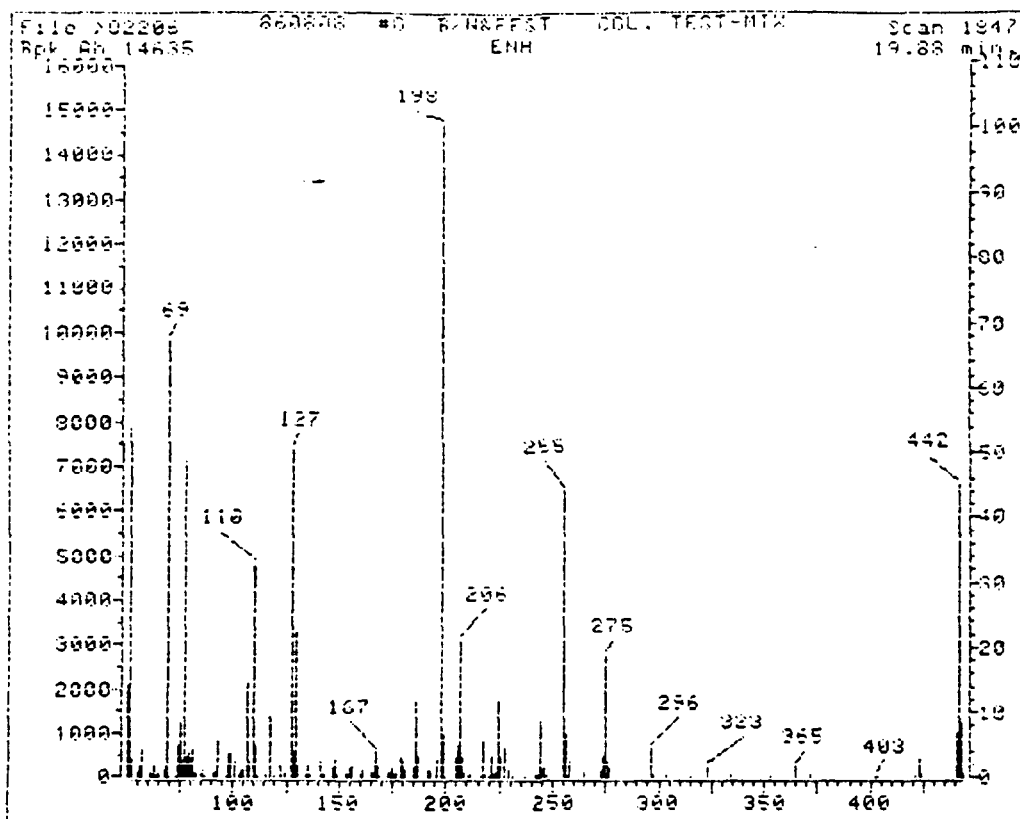


TABLE 2: METHOD PERFORMANCE DATA (GR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	53.67	53.67	Ok
69	Less than 2% of mass 69	1.18	1.76	Ok
69	(reference only)	67.08	67.08	Ok
70	Less than 2% of mass 69	.12	.18	Ok
127	40-60% of mass 198	50.42	50.42	Ok
197	Less than 1% of mass 198	.14	.14	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.52	6.52	Ok
275	10-30% of mass 198	18.68	18.68	Ok
365	Greater than 1% of mass 198	1.61	1.61	Ok
441	0-100% of mass 443	6.71	78.75	Ok
442	Greater than 40% of mass 198	44.76	44.76	Ok
443	17-23% of mass 442	8.52	19.03	Ok

Injection Date: 08/08/86

Injection Time: 14:18

Run No: >02206

Spectrum No: 1847

Analyst: *[Signature]*

Processor: *[Signature]*

QC Batch: 085420

Samples: N0161-N0165  
N0179-N0190

*VS*  
*8/13/86*



**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0132 RESOURCE ENGINEERING

RES27514

SDB-7-26-28 860719 0015

ETC Sample No.

Company

Facility

Sample Point

Date

Elapsed  
Time Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
1B	Acenaphthene	ND	77	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	77	ND	ND	ND	0	-	ND	4090	94
4B	Benazidine	ND	1800	ND	ND	ND	0	-	ND	4090	0
5B	Benzo(a)anthracene	ND	320	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(a)pyrene	ND	100	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	400	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	170	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl)ether	ND	230	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	BMDL	400	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	77	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	400	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	77	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	100	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	400	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	77	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	77	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	180	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	670	ND	ND	ND	0	-	ND	4090	32
24B	Diethyl phthalate	BMDL	400	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	BMDL	400	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	77	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	ND	400	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	400	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	89	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	ND	77	ND	ND	ND	0	-	ND	4090	86

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0132 RESOURCE ENGINEERING

RES27514

SDB-7-26-28 860719 0015

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov.	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov.
33B	Hexachlorobenzene	ND	77	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	ND	36	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	400	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	65	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	89	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	BMDL	65	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	77	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	400	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	400	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	77	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	ND	220	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	77	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	77	ND	ND	ND	0	-	ND	4090	88

A Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0132	RESOURCE ENGINEERING	RES27514	SDB-7-26-28 86071	0015	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	89	20	140
2-Fluorobiphenyl	50	74	20	140
Terphenyl-D14	50	69	20	150

\* IFB EPR Control Limits

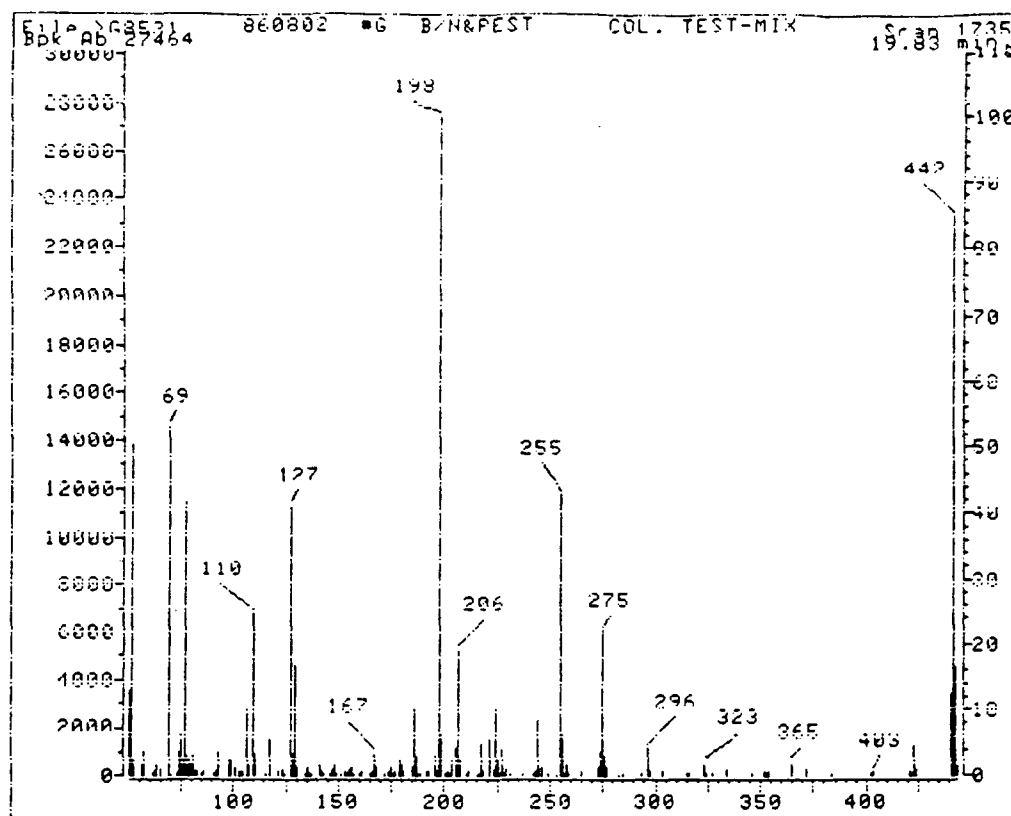


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86  
 Injection Time: 15:34  
 Run No: >G8531  
 Spectrun No: 1735

Analyst: *Straponech*  
 Processor: *Mita Mukherjee*  
 QC Batch: *Q85399*  
 Samples: *Calib. Stds.*

*N0131 - N0135, N0138 - N0143*

*CO 8/4/86*

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

NO135 RESOURCE ENGINEERING

RES27514

SDB-7-38-40 860719 0035

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	71	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	130	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	71	ND	ND	ND	0	-	ND	4090	94
4B	Benzo(a)anthracene	ND	1600	ND	ND	ND	0	-	ND	4090	0.
5B	Benzo(a)pyrene	ND	290	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(b)fluoranthene	ND	93	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	370	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	150	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	130	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	200	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	210	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl)ether	ND	210	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	ND	370	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	71	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	370	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	71	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	93	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	370	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	71	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	71	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	160	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	610	ND	ND	ND	0	-	ND	4090	32.
24B	Diethyl phthalate	ND	370	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	370	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	ND	370	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	210	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	71	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	ND	370	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	370	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	82	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	ND	71	ND	ND	ND	0	-	ND	4090	86

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0135 RESOURCE ENGINEERING RES27514 SDB-7-38-40 860719 0035  
ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	71	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	ND	33	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	370	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	59	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	170	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	82	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	ND	59	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	71	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	370	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	370	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	71	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	ND	200	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	71	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	71	ND	ND	ND	0	-	ND	4090	88

R Recovery normally variable using established methodology.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports					
N0135	RESOURCE ENGINEERING	RES27514	SDB-7-38-40	86071	0035 0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	92	20	140
2-Fluorobiphenyl	50	80	20	140
Terphenyl-D14	50	75	20	150

\* IFS EPR Control Limits

\* IFB EPR Control Limits

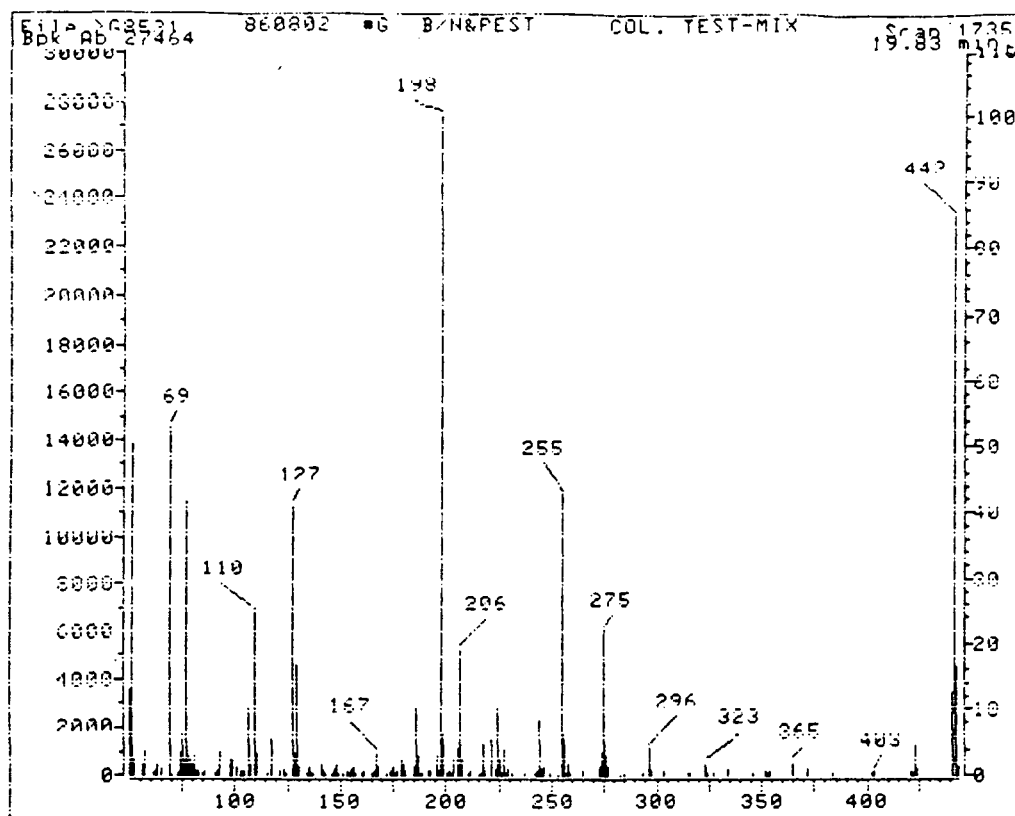


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86

Injection Time: 15:34

Run No: >G8531

Spectrum No: 1735

Analyst: *Strapouch*

Processor: *Mika Mukherjee*

QC Batch: *Q85399*

Samples: *Calib. Stds.*

*N0131 - N0135, N0138 - N0143*

*CO 8/4/86*



**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

NO134 RESOURCE ENGINEERING

RES27514

SDB-7-42-44 860719 0125

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	70	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	130	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	70	ND	ND	ND	0	-	ND	4090	94
4B	Benzidine	ND	1600	ND	ND	ND	0	-	ND	4090	0.
5B	Benzo(a)anthracene	ND	290	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(a)pyrene	ND	92	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	370	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	150	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	130	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	200	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	210	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl)ether	ND	210	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	BMDL	370	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	70	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	370	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	70	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	92	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	370	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	70	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	70	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	160	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	610	ND	ND	ND	0	-	ND	4090	32.
24B	Diethyl phthalate	ND	370	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	370	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	BMDL	370	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	210	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	70	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	ND	370	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	370	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	81	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	ND	70	ND	ND	ND	0	-	ND	4090	86

AUG 4, 1986

## TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0134 RESOURCE ENGINEERING

RES27514

SDB-7-42-44 860719 0125

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov.	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov.
33B	Hexachlorobenzene	ND	70	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	ND	33	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	370	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	59	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	170	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	81	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	ND	59	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	70	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	370	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	370	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	70	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	ND	200	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	70	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	70	ND	ND	ND	0	-	ND	4090	88

A Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0134 RESOURCE ENGINEERING RES27514 SDB-7-42-44 86071 0125 0  
 ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits %	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	102	20	140
2-Fluorobiphenyl	50	89	20	140
Terphenyl-D14	50	83	20	150

• IFB EPR Control Limits

• IFB EPA Control Limits

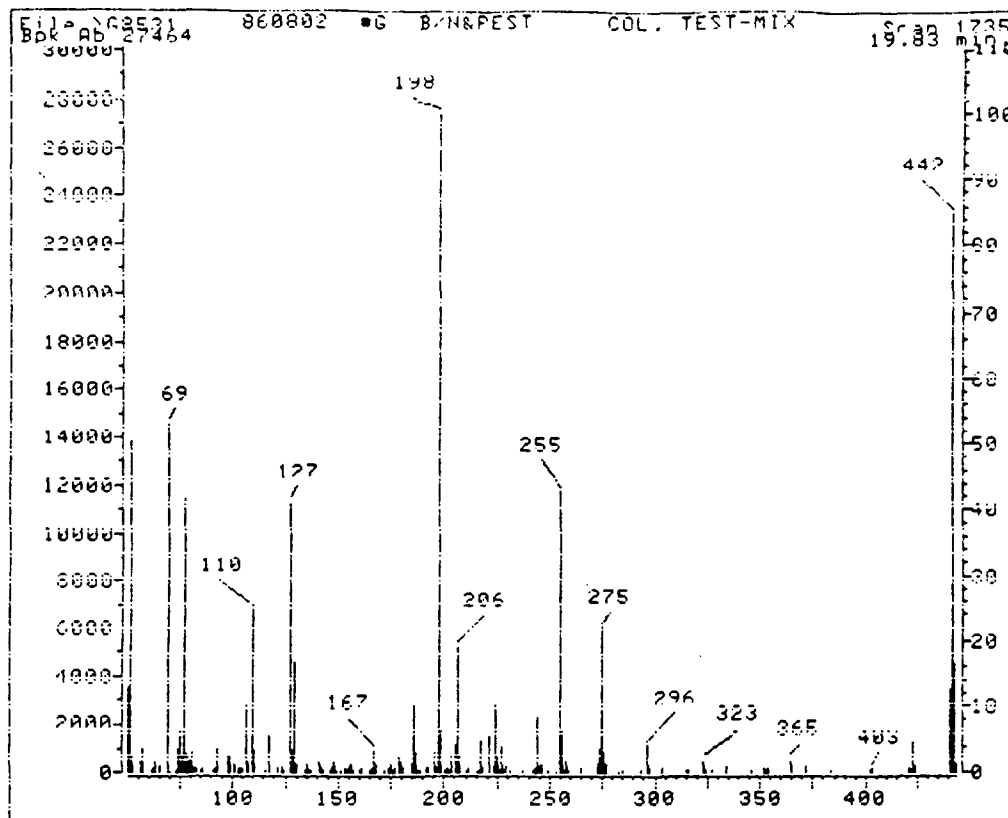


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86

Injection Time: 15:34

Run No: >G8531

Spectrum No: 1735

Analyst: *Slapovich*

Processor: *Nita Mulhargie*

QC Batch: *Q85399*

Samples: *Calib. Stds.*

*N0131 - N0135, N0138 - N0143*

*CO 8/4/86*



**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

NO131 RESOURCE ENGINEERING

RES27514 SDB-7-46-48 860719 0140

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
1B	Acenaphthene	ND	73	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	73	ND	ND	ND	0	-	ND	4090	94
4B	Benztidine	ND	1700	ND	ND	ND	0	-	ND	4090	0.
5B	Benzo(a)anthracene	ND	300	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(a)pyrene	ND	97	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	390	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	200	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	220	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl)ether	ND	220	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	BMDL	390	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	73	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	390	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	73	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	97	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	390	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	73	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	73	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	640	ND	ND	ND	0	-	ND	4090	32.
24B	Diethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	BMDL	390	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	220	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	73	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	ND	390	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	390	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	85	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	ND	73	ND	ND	ND	0	-	ND	4090	86

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0131 RESOURCE ENGINEERING

RES27514

SDB-7-46-48 860719 0140

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	73	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	ND	35	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	390	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	62	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	180	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	85	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	ND	62	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	73	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	390	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	390	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	73	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	ND	210	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	73	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	73	ND	ND	ND	0	-	ND	4090	88

a Recovery normally variable, using established methodology.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0131 RESOURCE ENGINEERING RES27514 SDB-7-46-48 86071 0140 0  
 ETC Sample No. Company Facility Sample Point Date Time Elapsed  
 Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	89	20	140
2-Fluorobiphenyl	50	76	20	140
Terphenyl-D14	50	83	20	150

© IFB EPR Control Limits

\* IPB EPR Control Limits

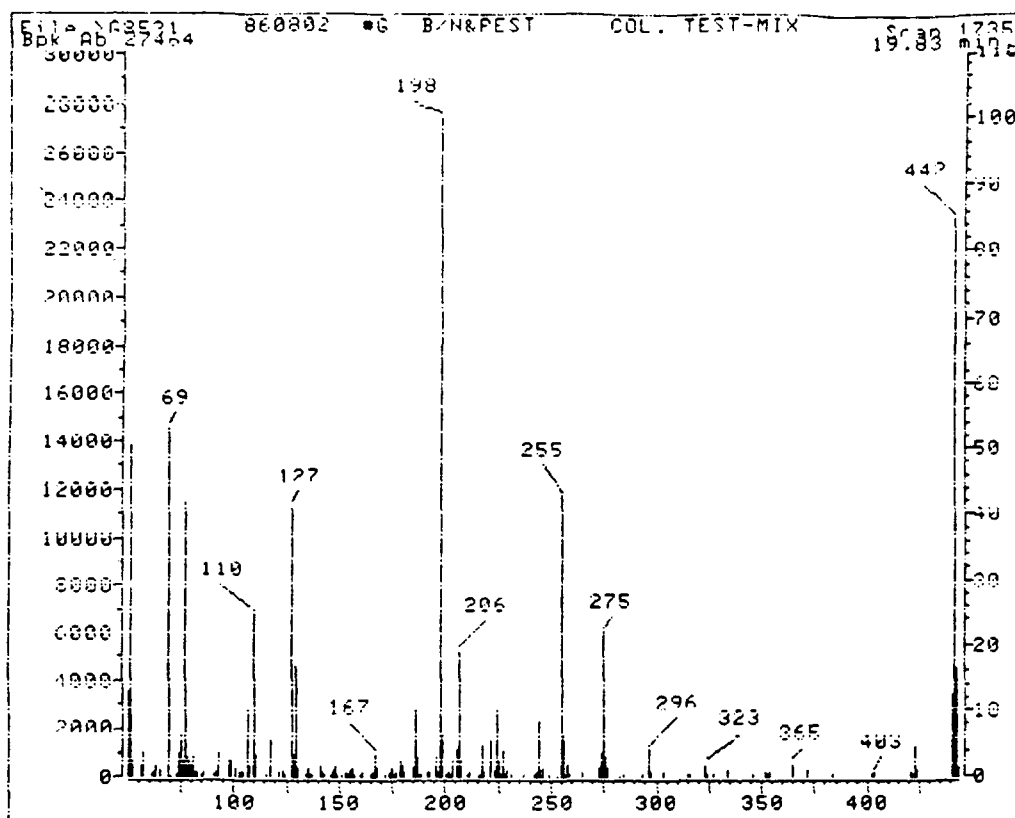


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
192	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86

Injection Time: 15:34

Run No: >G8531

Spectrum No: 1735

Analyst: *Slapovich*

Processor: *Mita Mulhargie*

QC Batch: *Q85399*

Samples: *Calib. Stds.*

*N0131 - N0135, N0138 - N043*

*CP 8/4/86*

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0133 RESOURCE ENGINEERING

RES27514

SDB-7-56-58 860719 0150

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	75	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	75	ND	ND	ND	0	-	ND	4090	94
4B	Benzidine	ND	1700	ND	ND	ND	0	-	ND	4090	0 <sup>a</sup>
5B	Benzo(a)anthracene	ND	310	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(a)pyrene	ND	99	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	400	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl)ether	ND	230	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	ND	400	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	75	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	400	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	75	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	99	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	400	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	660	ND	ND	ND	0	-	ND	4090	32 <sup>a</sup>
24B	Diethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	400	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	BMDL	400	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	75	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	ND	400	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	400	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	87	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	ND	75	ND	ND	ND	0	-	ND	4090	86

AUG 4, 1986

## TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N0133 RESOURCE ENGINEERING

RES27514

SDB-7-56-58 860719 0150

ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	75	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	ND	36	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	400	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	64	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	87	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	ND	64	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	75	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	400	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	400	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	75	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	ND	210	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	75	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4090	88

R Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0133	RESOURCE ENGINEERING	RES27514	SDB-7-56-58 86071	0150	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	102	20	140
2-Fluorobiphenyl	50	82	20	140
Terphenyl-D14	50	91	20	150

• IFB EPA Control Limits

\* IFB EPR Control Limits

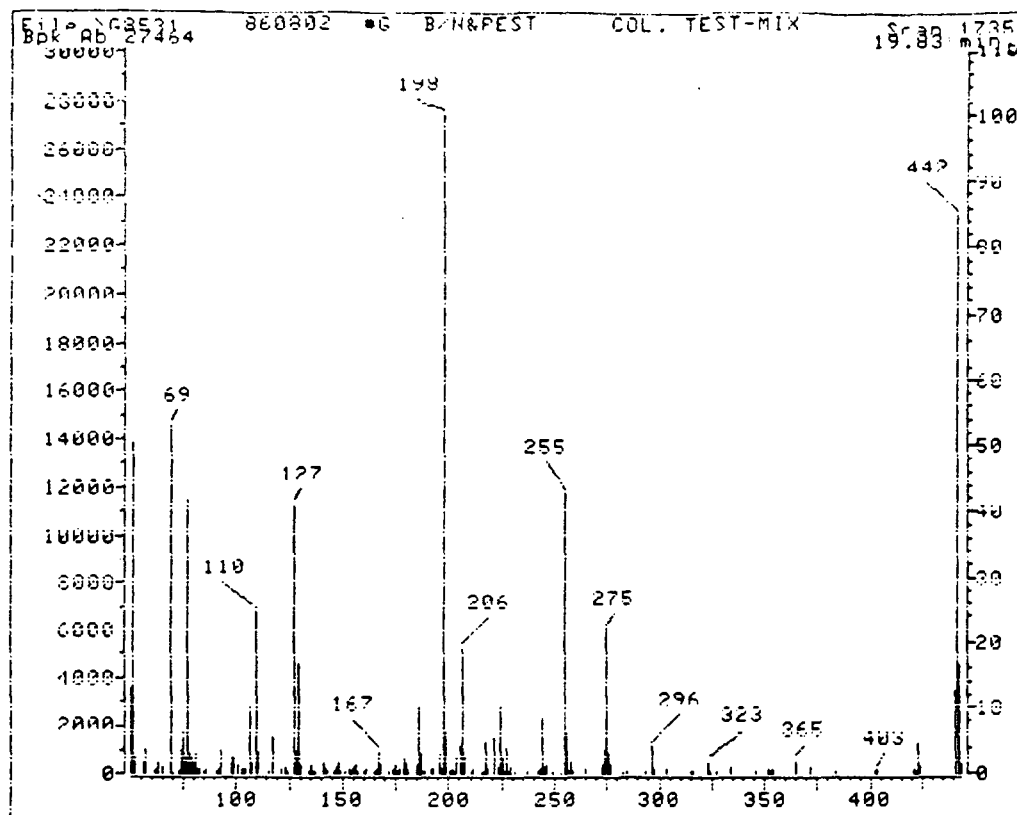


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86  
Injection Time: 15:34  
Run No: >G8531  
Spectrum No: 1735

Analyst: *Strawson*  
Processor: *Mika Mukherjee*  
QC Batch: *QB 5399*  
Samples: *Calb. Stds.*

*N0131 - N0135, N0138 - N0143*

*CO 8/4/86*



**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

NO142 RESOURCE ENGINEERING

RES27514

SDB-8-26-28 860720

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
1B	Acenaphthene	ND	78	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	78	ND	ND	ND	0	-	ND	4090	94
4B	Benzidine	ND	1800	ND	ND	ND	0	-	ND	4090	0.
5B	Benzo(a)anthracene	ND	320	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(a)pyrene	ND	100	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	410	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	170	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	220	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl)ether	ND	230	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	ND	410	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	78	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	410	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	78	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	100	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	410	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	78	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	78	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	180	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	670	ND	ND	ND	0	-	ND	4090	32.
24B	Diethyl phthalate	ND	410	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	410	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	BMDL	410	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	78	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	ND	410	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	410	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	90	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	ND	78	ND	ND	ND	0	-	ND	4090	86

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0142 RESOURCE ENGINEERING

RES27514

SDB-8-26-28 860720

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	78	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	ND	37	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	410	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	65	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	90	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	BMDL	65	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	78	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	410	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	410	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	78	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	ND	220	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	78	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	78	ND	ND	ND	0	-	ND	4090	88

R Recovery normally variable using established methodology.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0142	RESOURCE ENGINEERING	RES27514	SDB-8-26-28	86072	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	95	20	140
2-Fluorobiphenyl	50	80	20	140
Terphenyl-D14	50	88	20	150

• IFB EPA Control Limits

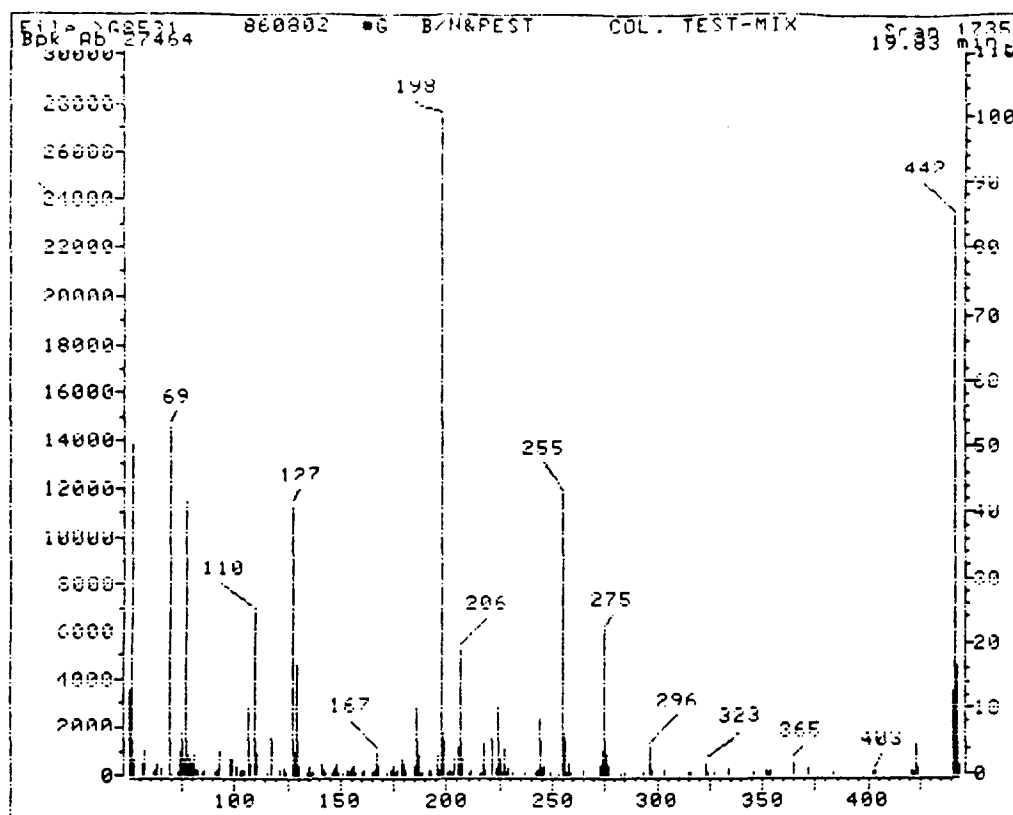


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86  
Injection Time: 15:34  
Run No: >G8531  
Spectrum No: 1735

Analyst: *Stagonich*  
Processor: *Mita Mukherjee*  
QC Batch: *QB5399*  
Samples: *Calib. Stds.*

*N0131 - N0135, N0138 - N0143*

*CO 8/4/86*



**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0138 RESOURCE ENGINEERING

RES27514 SDB-8-32-34 860720 2130

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	80	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	150	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	80	ND	ND	ND	0	-	ND	4090	94
4B	Benzidine	ND	1800	ND	ND	ND	0	-	ND	4090	0 <sub>a</sub>
5B	Benzo(a)anthracene	ND	330	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(a)pyrene	ND	100	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	420	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	170	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	150	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	220	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	240	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl)ether	ND	240	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	BMDL	420	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	80	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	420	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	80	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	180	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	100	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	420	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	80	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	80	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	180	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	690	ND	ND	ND	0	-	ND	4090	32 <sub>a</sub>
24B	Diethyl phthalate	ND	420	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	420	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	BMDL	420	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	240	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	80	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	BMDL	420	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	420	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	92	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	ND	80	ND	ND	ND	0	-	ND	4090	86

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0138 RESOURCE ENGINEERING

RES27514

SDB-8-32-34 860720 2130

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	80	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	ND	38	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	420	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	67	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	200	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	92	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	ND	67	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	80	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	420	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	420	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	80	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	ND	230	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	80	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	80	ND	ND	ND	0	-	ND	4090	88

A Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0138	RESOURCE ENGINEERING	RES27514	SDB-8-32-34	86072	2130	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added E4, SPA	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	72	20	140
2-Fluorobiphenyl	50	77	20	140
Terphenyl-D14	50	81	20	150

• 178 EPR Control Limits

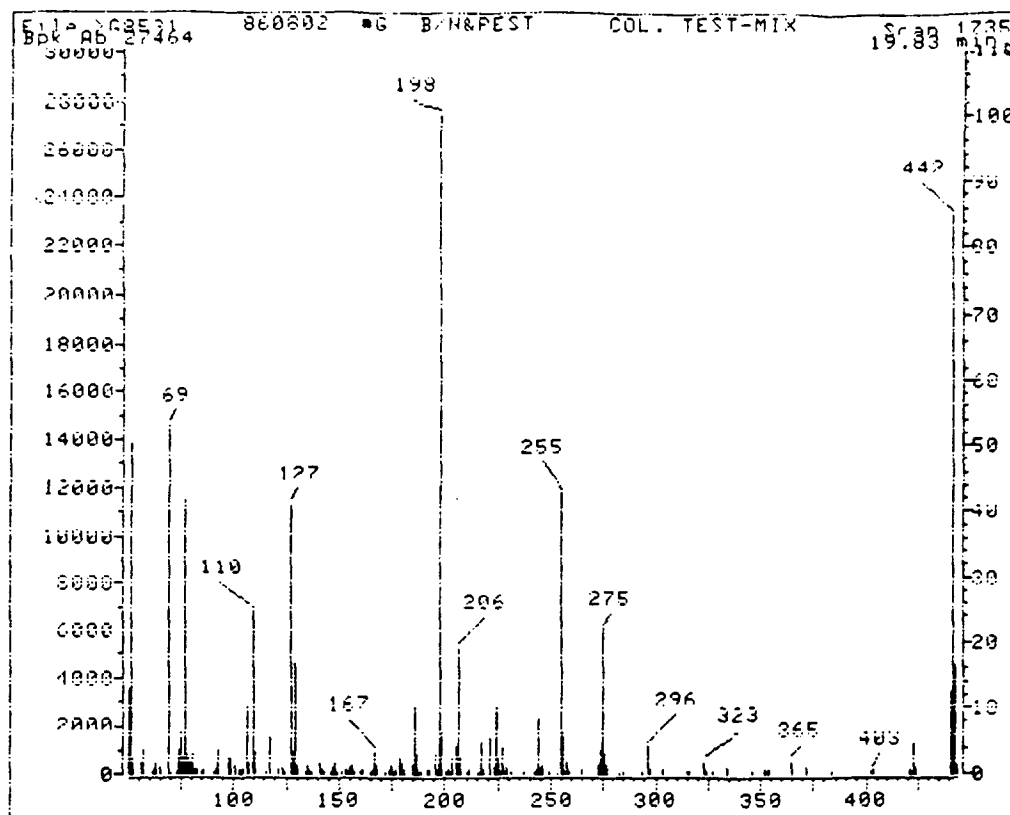


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86  
 Injection Time: 15:34  
 Run No: G8531  
 Spectrun No: 1735

Analyst: *Staponech*  
 Processor: *Nita Mulhargie*  
 QC Batch: *G85399*  
 Samples: *Calib. Stds.*

*N0131 - N0135, N0138 - N043*

*CO 8/4/86*

## TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N0139 RESOURCE ENGINEERING

RES27514

SDB-8-34-36 860720 2140

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
1B	Acenaphthene	ND	81	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	150	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	81	ND	ND	ND	0	-	ND	4090	94
4B	Benzidine	ND	1900	ND	ND	ND	0	-	ND	4090	0.
5B	Benzo(a)anthracene	ND	330	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(a)pyrene	ND	110	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	420	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	170	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	150	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	230	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	240	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl)ether	ND	240	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	ND	420	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	81	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	420	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	81	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	180	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	110	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	420	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	81	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	81	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	190	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	700	ND	ND	ND	0	-	ND	4090	32.
24B	Diethyl phthalate	ND	420	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	420	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	BMDL	420	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	240	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	81	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	ND	420	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	420	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	93	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	BMDL	81	ND	ND	ND	0	-	ND	4090	86

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0139 RESOURCE ENGINEERING

RES27514

SDB-8-34-36 860720 2140

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	148	81	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	3750	38	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	420	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	102	68	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	200	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	93	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	77.0	68	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	81	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	420	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	420	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	81	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	BMDL	230	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	81	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	81	ND	ND	ND	0	-	ND	4090	88

A Recovery normally variable using established methodology.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports					
NO139	RESOURCE ENGINEERING	RES27514	SDB-8-34-36	86072	2140 0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	82	20	140
2-Fluorobiphenyl	50	71	20	140
Terphenyl-D14	50	78	20	150
* IFB EPR Control Limits				

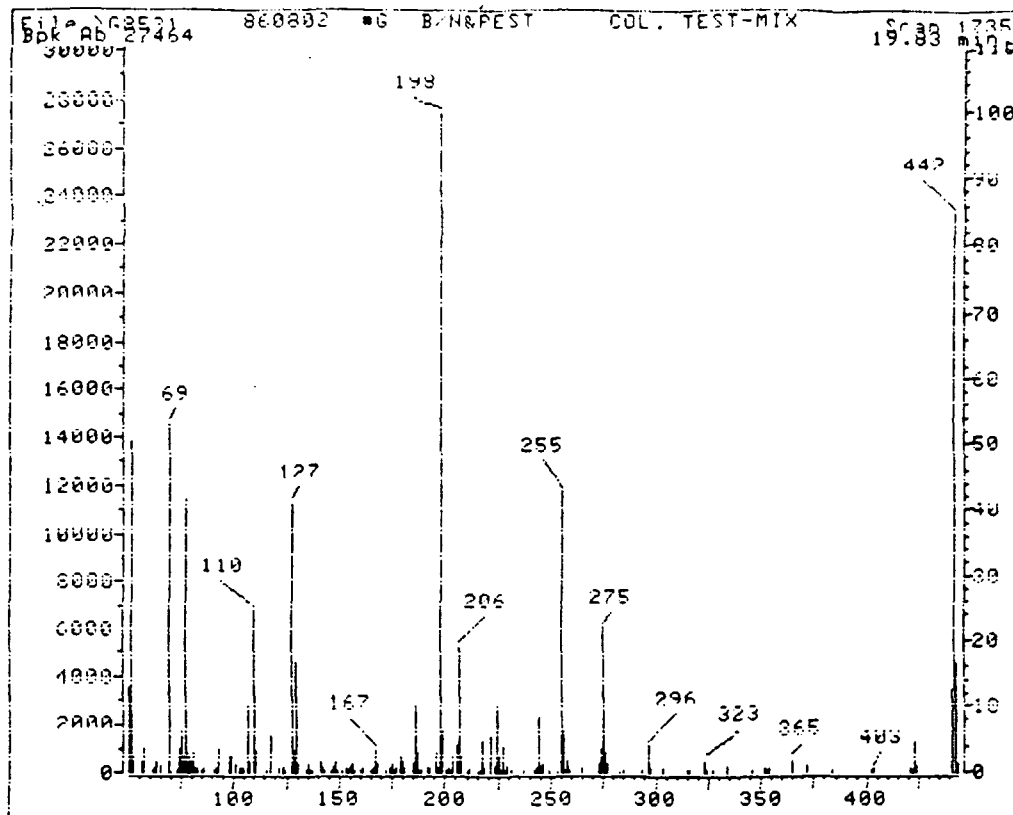


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86

Injection Time: 15:34

Run No: >G8531

Spectrum No: 1735

Analyst: *Strapouch*

Processor: *Mika Mukherjee*

QC Batch: *Q85399*

Samples: *Calib. Stds.*  
*N0131 - N0135, N0138 - N0141*

*CO*  
*8/4/86*

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0140 RESOURCE ENGINEERING

RES27514

SDB-8-48-50 860720 2210

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
1B	Acenaphthene	ND	75	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	75	ND	ND	ND	0	-	ND	4090	94
4B	Benzidine	ND	1700	ND	ND	ND	0	-	ND	4090	0 <sup>a</sup>
5B	Benzo(a)anthracene	ND	310	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(a)pyrene	ND	99	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	390	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl) ether	ND	230	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	ND	390	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	75	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	390	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	75	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	99	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	390	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	650	ND	ND	ND	0	-	ND	4090	32 <sup>a</sup>
24B	Diethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	BMDL	390	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	75	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	ND	390	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	390	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	87	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	ND	75	ND	ND	ND	0	-	ND	4090	86

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0140 RESOURCE ENGINEERING

RES27514

SDB-8-48-50 860720 2210

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	75	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	ND	36	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	390	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	63	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	87	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	ND	63	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	75	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	390	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	390	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	75	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	ND	210	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	75	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4090	88

R Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0140	RESOURCE ENGINEERING	RES27514	SDB-8-48-50	86072	2210	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits %	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	89	20	140
2-Fluorobiphenyl	50	80	20	140
Terphenyl-D14	50	83	20	150

\* IFB EPA Control Limits

\* IFB EPA Control Limits

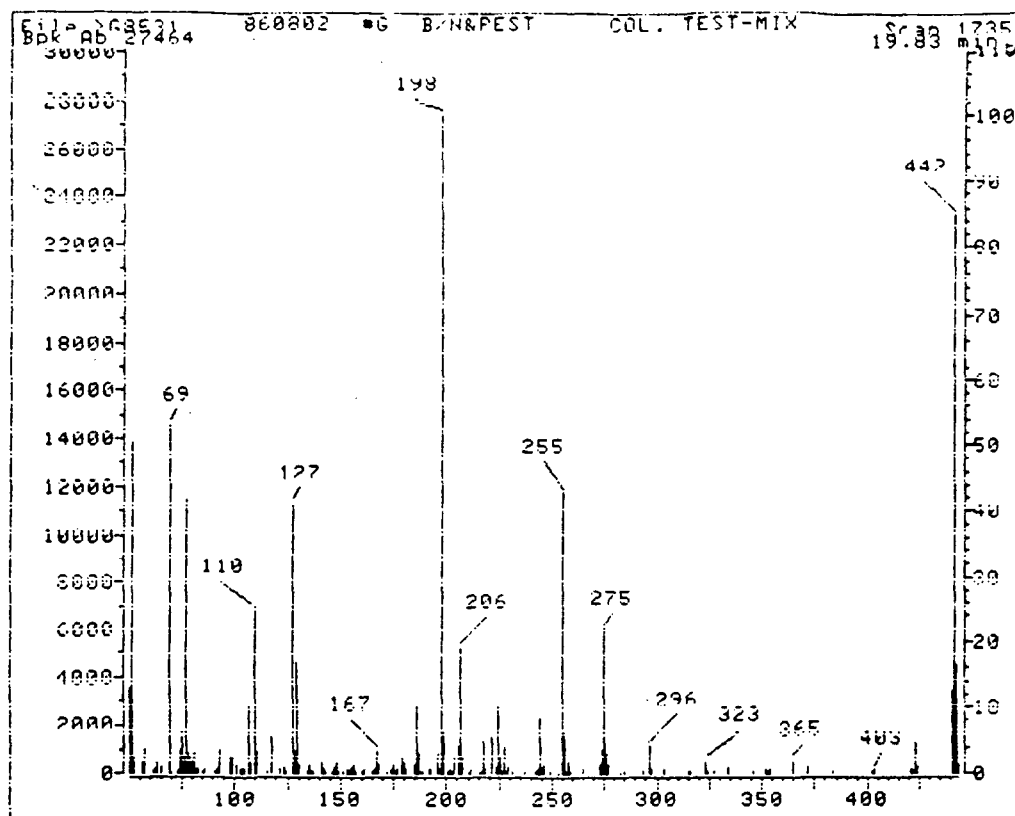


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86

Injection Time: 15:34

Run No: >G8531

Spectrum No: 1735

Analyst: *Strapman*

Processor: *Mita Mulhargie*

QC Batch: *QB 5399*

Samples: *Calb. Stds.*

*NO131 - NO135, NO138 - NO143*

*CO 8/4/86*

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0141 RESOURCE ENGINEERING

RES27514 SDB-8-54-56 860720 2225

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
1B	Acenaphthene	ND	77	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	77	ND	ND	ND	0	-	ND	4090	94
4B	Benizidine	ND	1800	ND	ND	ND	0	-	ND	4090	0.
5B	Benzo(a)anthracene	ND	320	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(a)pyrene	ND	100	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	410	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	170	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	220	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl)ether	ND	230	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	BMDL	410	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	77	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	410	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	77	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	100	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	410	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	77	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	77	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	180	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	670	ND	ND	ND	0	-	ND	4090	32.
24B	Diethyl phthalate	ND	410	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	410	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	BMDL	410	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	77	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	ND	410	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	410	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	90	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	ND	77	ND	ND	ND	0	-	ND	4090	86

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0141 RESOURCE ENGINEERING

RES27514

SDB-8-54-56 860720 2225

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	77	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	ND	37	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	410	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	65	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	90	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	ND	65	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	77	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	410	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	410	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	77	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	ND	220	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	77	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	77	ND	ND	ND	0	-	ND	4090	88

R Recovery normally variable using established methodology.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0141	RESOURCE ENGINEERING	RES27514	SDB-8-54-56	86072	2225	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	94	20	140
2-Fluorobiphenyl	50	79	20	140
Terphenyl-D14	50	89	20	150

\* IFB EPA Control Limits

\* IFB EPA Control Limits

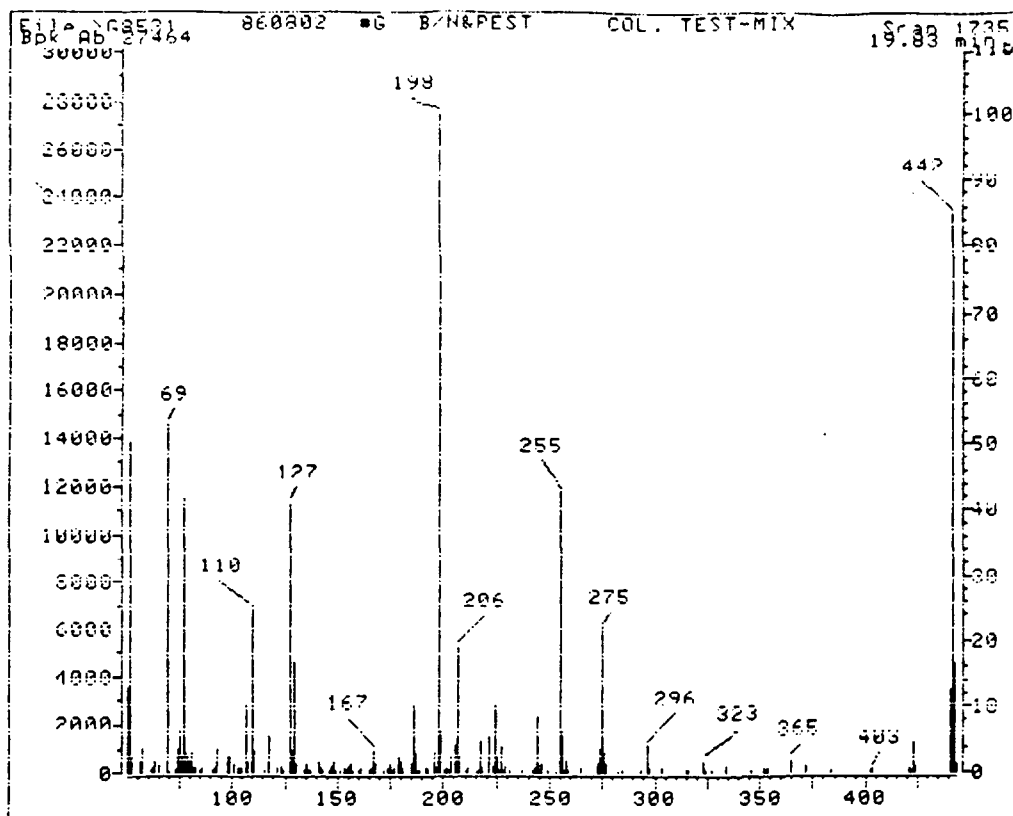


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86  
 Injection Time: 15:34  
 Run No: >G8531  
 Spectrum No: 1735

Analyst: *Slapovich*  
 Processor: *Mika Mulkarjee*  
 QC Batch: *QB 5399*  
 Samples: *Calib. Stds.*

*NO131 - NO135, NO138 - NO142*

*CO 8/4/86*

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N1252 RESOURCE ENGINEERING

RES27514

SDB-9-32-34 860721 0140

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	209	74	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	74	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	1700	ND	ND	ND	0	-	ND	4040	76
5B	Benzo(a)anthracene	ND	300	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	97	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	390	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	220	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	220	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	ND	390	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	74	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	74	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	97	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	390	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	640	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	390	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	220	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	74	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	BMDL	390	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	390	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	98.7	85	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	245	74	ND	ND	ND	0	-	ND	4040	90

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N1252 RESOURCE ENGINEERING

RES27514

SDB-9-32-34 860721 0140

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	124	74	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	3360	35	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	390	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	62	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	180	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	85	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	229	62	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	74	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	390	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	390	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	74	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	542	210	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	81.4	74	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	87

<sup>a</sup> Results variable due to Non-Homogeneous sample matrix.<sup>b</sup> Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports						
N1252	RESOURCE ENGINEERING	RES27514	SDB-9-32-34	86072	0140	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits .	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	103	23	120
2-Fluorobiphenyl	50	93	30	115
Terphenyl-D14	50	106	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits				
.. Advisory Limits Only				

\* IFB EPA Control Limits

\*\* Advisory Limits Only

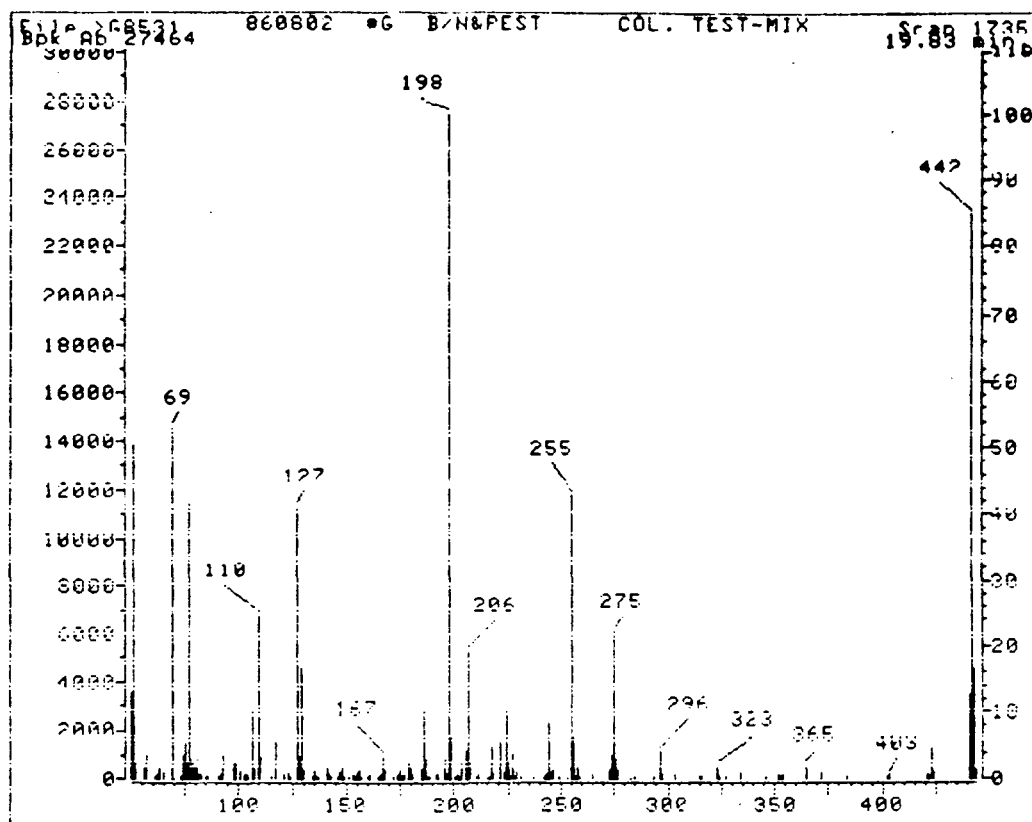


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
157	Less than 1% of mass 198	.24	.24	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	17-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 15:34

Run No: 68531

Spectrum No: 1735

Analyst: Slapnick

Processor: Tom Kuorikoski

QC Batch: QB5395

Samples:

N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 Dil)  
N1252-N1253

8/8/86

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N1250 RESOURCE ENGINEERING

RES27514

SDB-9-40-42 860721 0200

ETC Sample No

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	77	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	77	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	1800	ND	ND	ND	0	-	ND	4040	7 <sup>a</sup>
5B	Benzo(a)anthracene	ND	320	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	100	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	410	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	170	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	230	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	BMDL	410	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	77	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	410	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	77	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	100	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	410	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	77	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	77	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	180	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	670	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	410	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	410	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	410	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	77	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	BMDL	410	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	410	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	89	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	77	ND	ND	ND	0	-	ND	4040	90

AUG 8, 1986

## TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N1250 RESOURCE ENGINEERING

RES27514 SDB-9-40-42 860721 0200

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	77	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	36	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	410	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	65	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	89	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	254	65	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	77	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	410	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	410	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	77	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	220	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	77	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	77	ND	ND	ND	0	-	ND	4040	87

<sup>a</sup> Results variable due to Non-Homogenous sample matrix.<sup>b</sup> Recovery normally variable using established methodology.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N1250	RESOURCE ENGINEERING	RES27514	SDB-9-40-42	86072	0200	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	109	23	120
2-Fluorobiphenyl	50	91	30	115
Terphenyl-D14	50	91	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..

\* IFB EPA Control Limits  
\*\* Advisory Limits Only

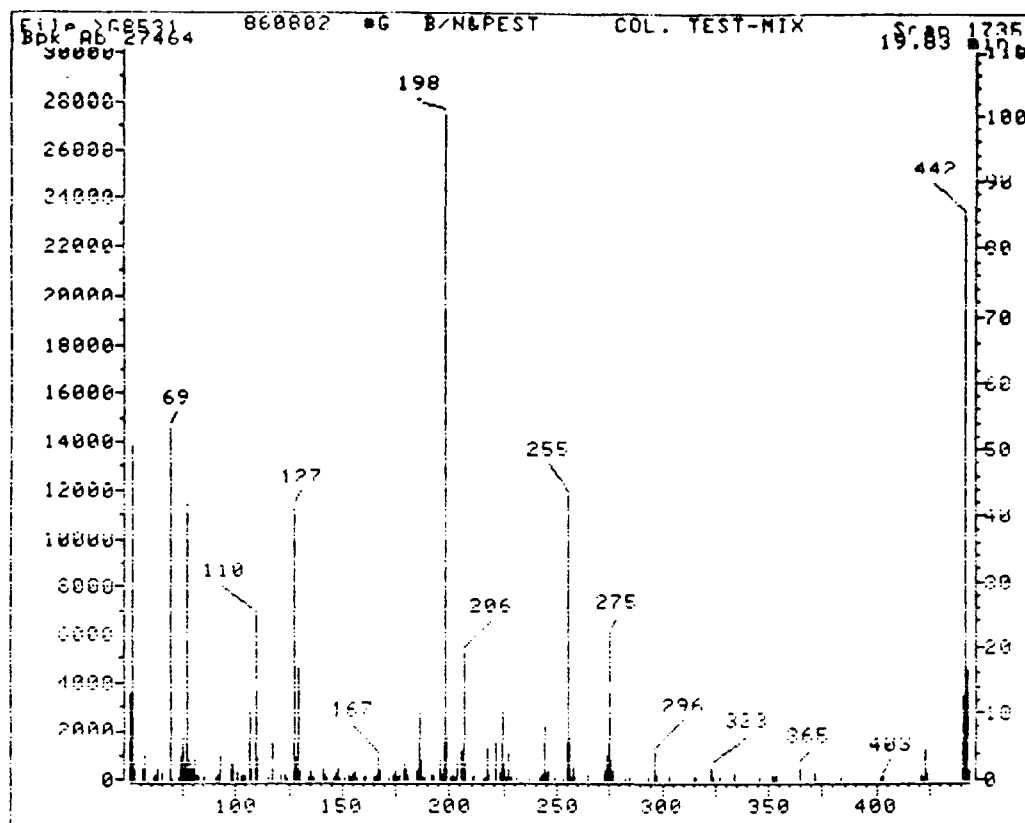


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
127	Less than 1% of mass 198	.74	.74	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	17-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86  
Injection Time: 19:34  
Run No: >G8531  
Spectrum No: 1735

Analyst: *Slapnick*  
Processor: *Tom Kuorikoski*  
QC Batch: *Q85395*  
Samples: N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 DIL)  
N1252-N1253

*8/8/86*

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N1251 RESOURCE ENGINEERING

RES27514

SDB-9-46-48 860721 0210

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	141000	830	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	2970	1500	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	12600	830	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	19000	ND	ND	ND	0	-	ND	4040	7
5B	Benzo(a)anthracene	13100	3400	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	2540	1100	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	4970	4400	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	3340	1800	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	5110	1500	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	2300	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	2500	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	2500	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	ND	4400	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	830	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	4400	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	830	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	1800	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	14600	1100	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	BMDL	4400	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	959	830	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	959	830	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	BMDL	1900	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	7200	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	4400	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	4400	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	4400	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	2500	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	830	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	ND	4400	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	4400	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	193000	960	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	116000	830	ND	ND	ND	0	-	ND	4040	90

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N1251 RESOURCE ENGINEERING

RES27514

SDB-9-46-48 860721 0210

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	207000	830	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	529000	390	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	4670	4400	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	559000	700	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	2730	2000	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	960	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	318000	700	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	830	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	4400	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	4400	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	830	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	259000	2400	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	167000	830	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	289000	830	ND	ND	ND	0	-	ND	4040	87

<sup>a</sup> Results variable due to Non-Homogeneous sample matrix.<sup>b</sup> Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

*Chain of Custody Data Required for ETC Data Management Summary Reports*

NI251

ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours
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Compound	Amount Added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	127 ***	23	120
2-Fluorobiphenyl	50	51 ****	30	115
Terphenyl-D14	50	92	18	137
PESTICIDE/PCB FRACTION (GC/MS)				
Dibutylchloroendate	-	-	20**	150**
* IFB EPA Control Limits. ** Advisory Limits Only. *** Recovery variable due to sample matrix interference. **** Reported from 1:50 Dilution.				

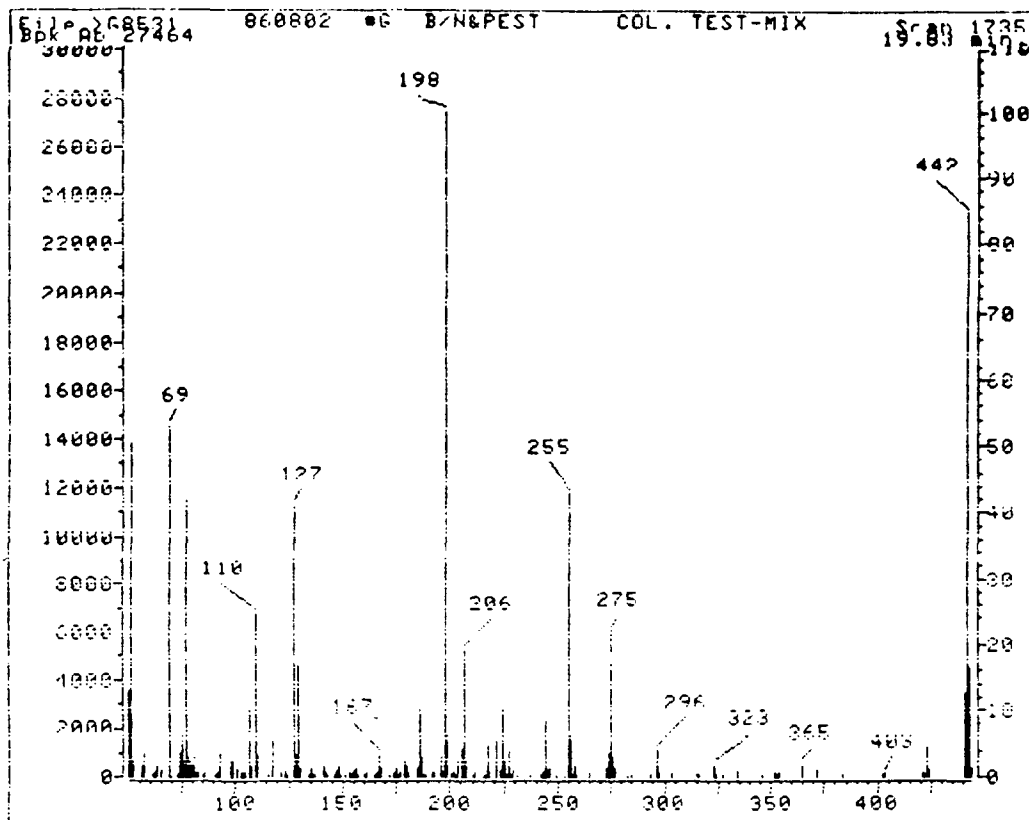


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
69	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.24	.24	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	17-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 15:34

Run No: >G8531

Spectrum No: 1735

Analyst: Slapnick

Processor: Tom Kurowski

QC Batch: QB5395

Samples: N0146-N0152, N0154-N0158,

N1250, N1251 (1:10 DIL)

N1252-N1253

8/8/86

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N1253 RESOURCE ENGINEERING

RES27514

SDB-9-54-56 860721 0230

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen: ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
1B	Acenaphthene	BMDL	81	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	150	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	81	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	1900	ND	ND	ND	0	-	ND	4040	7
5B	Benzo(a)anthracene	ND	330	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	110	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	430	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	180	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	150	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	230	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	240	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	240	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	BMDL	430	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	81	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	430	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	81	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	180	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	110	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	430	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	81	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	81	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	190	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	710	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	430	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	430	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	430	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	240	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	81	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	ND	430	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	430	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	BMDL	94	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	BMDL	81	ND	ND	ND	0	-	ND	4040	90

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N1253 RESOURCE ENGINEERING

RES27514

SDB-9-54-56 860721 0230

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	130	81	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	2470	39	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	430	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	128	68	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	200	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	94	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	68	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	81	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	430	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	430	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	81	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	BMDL	230	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	BMDL	81	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	81	ND	ND	ND	0	-	ND	4040	87

<sup>a</sup> Results variable due to Non-Homogeneous sample matrix.<sup>b</sup> Recovery normally variable using established methodology.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N1253	RESOURCE ENGINEERING	RES27514	SDB-9-54-56	86072	0230	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits .	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	78	23	120
2-Fluorobiphenyl	50	72	30	115
Terphenyl-D14	50	100	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IPB EPA Control Limits				
** Advisory Limits Only				

\* 17B EPA Control Limits

\*\* Advisory Limits Only

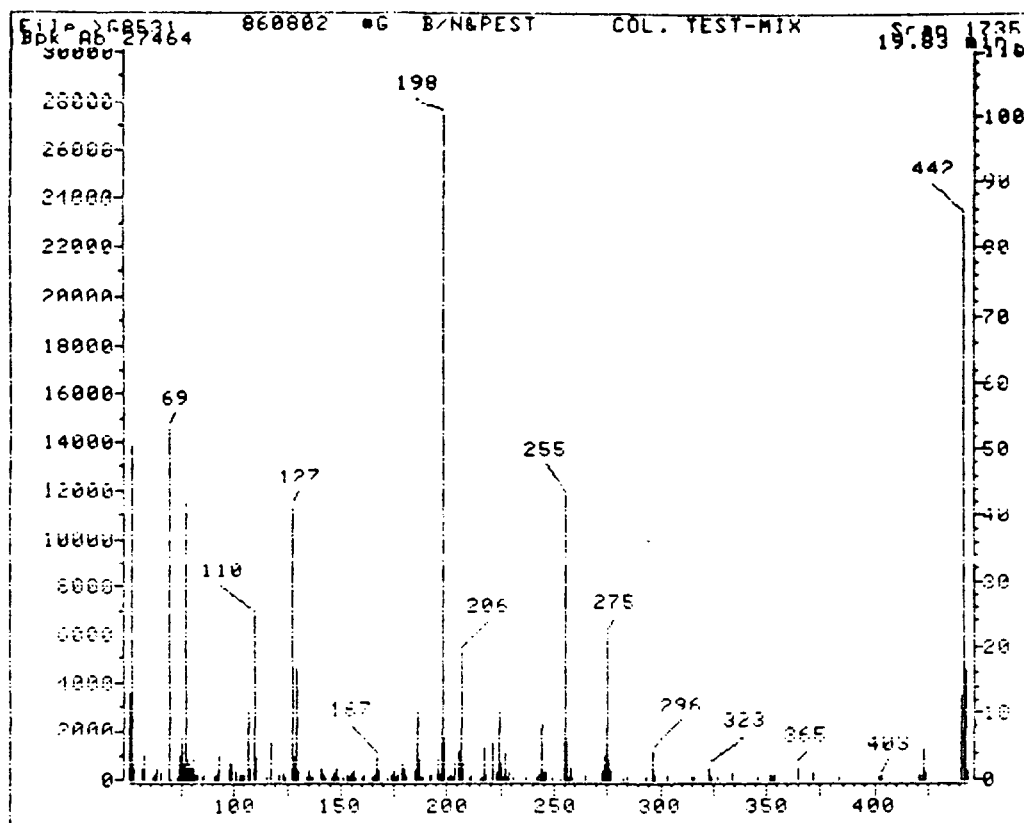


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
69	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
127	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86

Injection Time: 15:34

Run No: >G8531

Spectrum No: 1735

Analyst: Slapnick

Processor: Tom Kuornitz

QC Batch: Q85395

Samples:

N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 DIL)  
N1252-N1253

8/8/86

AUG 8, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N0147 RESOURCE ENGINEERING

RES27514

SDB-10-2830 860721 2125

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sub>a</sub>	Second ug/kg <sub>a</sub>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	84	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	160	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	84	ND	ND	BMDL	0	-	ND	4040	93
4B	Benizidine	ND	2000	ND	ND	ND	0	-	ND	4040	7 <sub>a</sub>
5B	Benzo(a)anthracene	ND	350	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	110	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	440	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	180	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	160	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	240	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	250	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	250	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	ND	440	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	84	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	440	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	84	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	190	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	110	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	440	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	84	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	84	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	200	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	730	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	440	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	440	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	440	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	250	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	84	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	ND	440	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	440	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	98	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	84	ND	ND	ND	0	-	ND	4040	90

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0147 RESOURCE ENGINEERING

RES27514

SDB-10-2830 860721 2125

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	BMDL	84	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	481	40	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	440	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	71	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	210	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	98	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	BMDL	71	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	84	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	440	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	440	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	84	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	BMDL	240	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	84	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	84	ND	ND	ND	0	-	ND	4040	87

<sup>a</sup> Results variable due to Non-Homogeneous sample matrix.<sup>b</sup> Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0147	RESOURCE ENGINEERING	RES27514	SDB-10-2830	86072	2125	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits .	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	97	23	120
2-Fluorobiphenyl	50	88	30	115
Terphenyl-D14	50	91	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits				
** Advisory Limits Only				

\* IFB EPR Control Limits  
 \*\* Advisory Limits Only

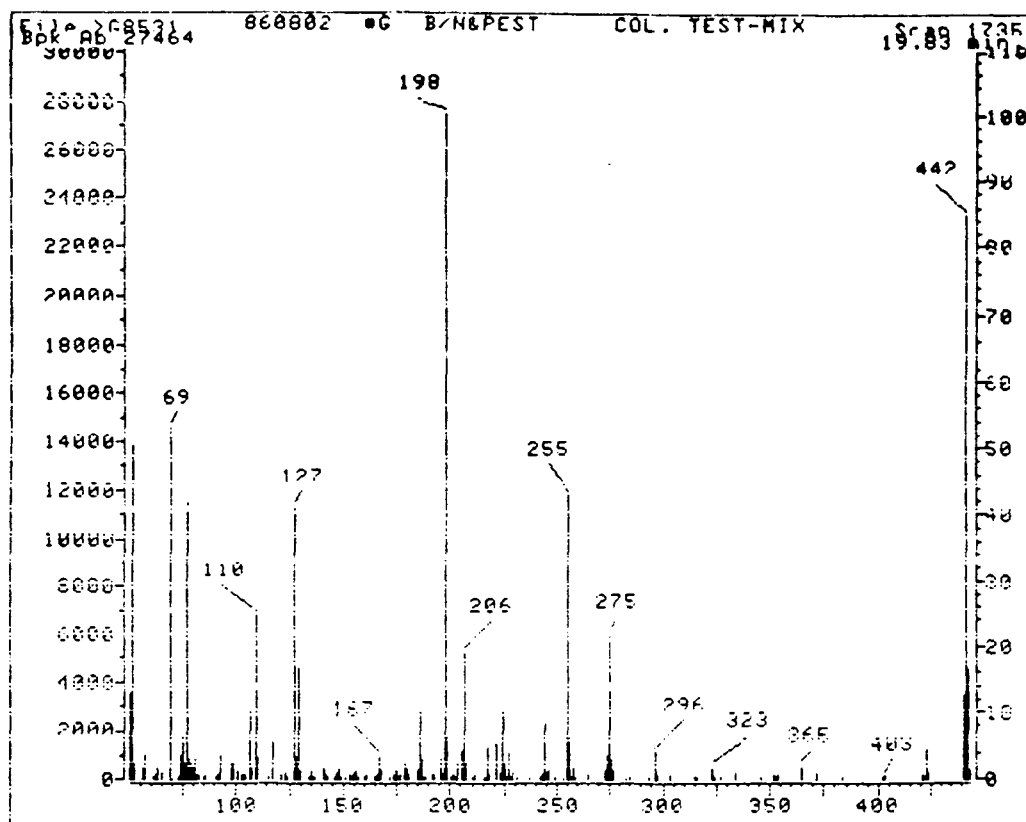


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.24	.24	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	12-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86

Injection Time: 15:34

Run No: 868882

Spectrum No: 1235

Analyst: Slapnick

Processor: Tom Kuorikoski

QC Batch: QB5395

Samples:

N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 Dil)  
N1252-N1253

8/8/86

AUG 4, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0143 RESOURCE ENGINEERING

RES27514

SDB-10-3436 860721 2120

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	74	ND	ND	ND	0	-	ND	4090	94
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4090	93
3B	Anthracene	ND	74	ND	ND	ND	0	-	ND	4090	94
4B	Benzidine	ND	1700	ND	ND	ND	0	-	ND	4090	0 <sub>a</sub>
5B	Benzo(a)anthracene	ND	300	ND	ND	ND	0	-	ND	4090	85
6B	Benzo(a)pyrene	ND	97	ND	ND	ND	0	-	ND	4090	70
7B	Benzo(b)fluoranthene	ND	390	ND	ND	ND	0	-	ND	4090	120
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4090	80
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4090	95
11B	bis(2-Chloroethyl) ether	ND	220	ND	ND	ND	0	-	ND	4090	90
12B	bis(2-Chloroisopropyl)ether	ND	220	ND	ND	ND	0	-	ND	4090	86
13B	bis(2-Ethylhexyl)phthalate	BMDL	390	ND	ND	ND	0	-	39.9	4090	79
14B	4-Bromophenyl phenyl ether	ND	74	ND	ND	ND	0	-	ND	4090	96
15B	Butyl benzyl phthalate	ND	390	ND	ND	ND	0	-	ND	4090	85
16B	2-Chloronaphthalene	ND	74	ND	ND	ND	0	-	ND	4090	97
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	4090	86
18B	Chrysene	ND	97	ND	ND	ND	0	-	ND	4090	95
19B	Dibenzo(a,h)anthracene	ND	390	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4090	86
21B	1,3-Dichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4090	87
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4090	88
23B	3,3'-Dichlorobenzidine	ND	640	ND	ND	ND	0	-	ND	4090	32 <sub>a</sub>
24B	Diethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4090	83
25B	Dimethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4090	88
26B	Di-n-butyl phthalate	BMDL	390	146	238	79.1	0	-	48.6	4090	94
27B	2,4-Dinitrotoluene	ND	220	ND	ND	ND	0	-	ND	4090	77
28B	2,6-Dinitrotoluene	ND	74	ND	ND	ND	0	-	ND	4090	89
29B	Di-n-octyl phthalate	ND	390	ND	ND	ND	0	-	63.2	4090	71
30B	1,2-Diphenylhydrazine	ND	390	ND	ND	ND	0	-	ND	4090	85
31B	Fluoranthene	ND	85	ND	ND	ND	0	-	ND	4090	92
32B	Fluorene	ND	74	ND	ND	ND	0	-	ND	4090	86

AUG 4, 1986

## TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N0143 RESOURCE ENGINEERING

RES27514

SDB-10-3436 860721 2120

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	BMDL	74	ND	ND	ND	0	-	ND	4090	98
34B	Hexachlorobutadiene	606	35	ND	ND	ND	0	-	ND	4090	94
35B	Hexachlorocyclopentadiene	ND	390	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	62	ND	ND	ND	0	-	ND	4090	91
37B	Indeno(1,2,3-c,d)pyrene	ND	180	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	85	ND	ND	ND	0	-	ND	4090	86
39B	Naphthalene	ND	62	ND	ND	ND	0	-	ND	4090	90
40B	Nitrobenzene	ND	74	ND	ND	ND	0	-	ND	4090	81
41B	N-Nitrosodimethylamine	ND	390	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	390	ND	ND	ND	0	-	ND	4090	93
43B	N-Nitrosodiphenylamine	ND	74	ND	ND	ND	0	-	ND	4090	78
44B	Phenanthrene	BMDL	210	ND	ND	ND	0	-	ND	4090	97
45B	Pyrene	ND	74	ND	ND	ND	0	-	ND	4090	92
46B	1,2,4-Trichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4090	88

A Recovery normally variable using established methodology.





**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery Soil - GC/MS Data (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0143 RESOURCE ENGINEERING

RES27514

SDB-10-3436 86072 2120 0

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

Compound	Amount added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION				
Toluene-D8	-	-	50	160
p-Bromofluorobenzene	-	-	50	160
1,2-Dichloroethane-D4	-	-	50	160
ACID FRACTION				
Phenol-D5	-	-	20	140
2-Fluorophenol	-	-	20	140
2,4,6-Tribromophenol	-	-	10	140
BASE/NEUTRAL FRACTION				
Nitrobenzene-D5	50	91	20	140
2-Fluorobiphenyl	50	71	20	140
Terphenyl-D14	50	91	20	150

\* IFB EPA Control Limits

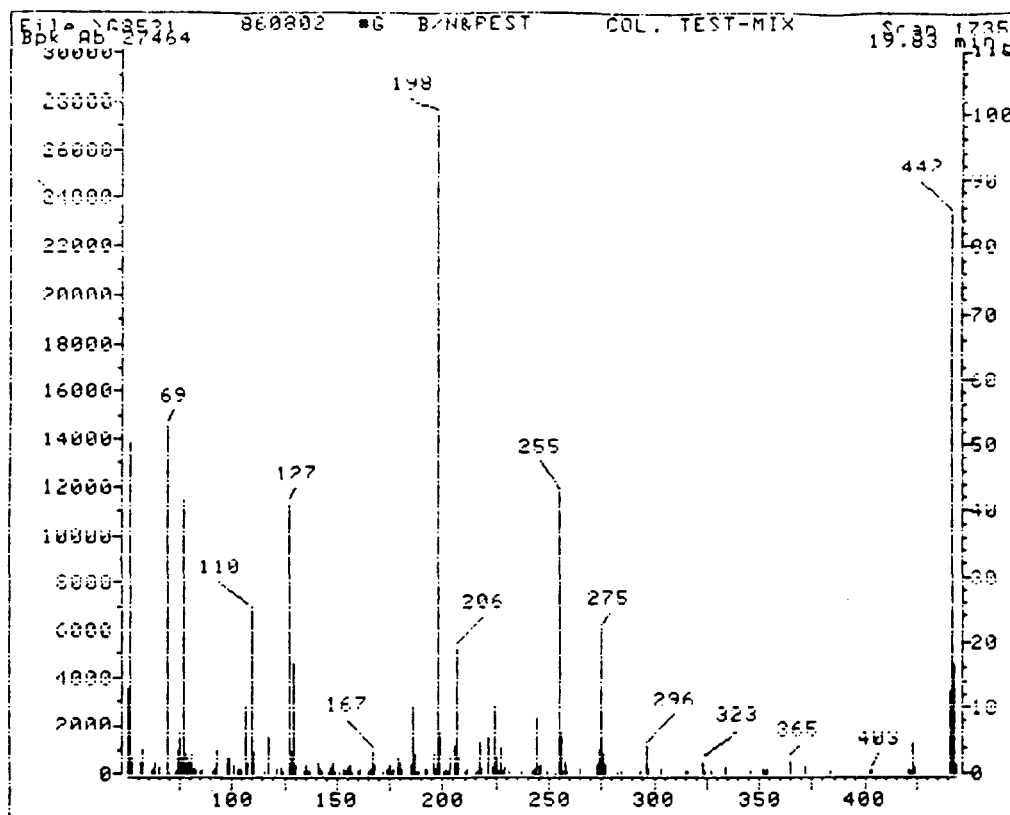


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
51	30-60% of mass 198	50.45	50.45	Ok
68	Less than 2% of mass 69	0.00	0.00	Ok
69	(reference only)	53.05	53.05	Ok
70	Less than 2% of mass 69	.24	.45	Ok
127	40-60% of mass 198	41.21	41.21	Ok
197	Less than 1% of mass 198	.74	.74	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.42	6.42	Ok
275	10-30% of mass 198	22.04	22.04	Ok
365	Greater than 1% of mass 198	2.02	2.02	Ok
441	0-100% of mass 443	12.57	77.21	Ok
442	Greater than 40% of mass 198	84.94	84.94	Ok
443	17-23% of mass 442	16.28	19.17	Ok

Injection Date: 08/02/86  
 Injection Time: 15:34  
 Run No: >G8531  
 Spectrun No: 1735

Analyst: *Stapovich*  
 Processor: *Mita Muthuraj*  
 QC Batch: *QB 5399*  
 Samples: *Calib. Stds.*

*N0131 - N0135, N0138 - N0143*

*CO 8/4/86*

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

NO148 RESOURCE ENGINEERING

RES27514

SDB-10-4244 860721 2135

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
1B	Acenaphthene	ND	74	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	74	ND	ND	BMDL	0	-	ND	4040	93
4B	Benzidine	ND	1700	ND	ND	ND	0	-	ND	4040	7.
5B	Benzo(a)anthracene	ND	300	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	97	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	390	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	220	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	220	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	1990	390	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	74	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	74	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	97	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	390	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	640	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	BMDL	390	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	220	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	74	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	BMDL	390	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	390	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	86	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	74	ND	ND	ND	0	-	ND	4040	90

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0148 RESOURCE ENGINEERING

RES27514

SDB-10-4244 860721 2135

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	35	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	390	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	62	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	180	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	86	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	62	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	74	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	390	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	390	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	74	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	210	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	74	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	74	ND	ND	ND	0	-	ND	4040	87

<sup>a</sup> Results variable due to Non-Homogeneous sample matrix.<sup>b</sup> Recovery normally variable using established methodology.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0148	RESOURCE ENGINEERING	RES27514	SDB-10-4244	86072	2135	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	103	23	120
2-Fluorobiphenyl	50	89	30	115
Terphenyl-D14	50	99	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..

\* IFB EPR Control Limits

\*\* Advisory Limits Only

\* IFB EPR Control Limits

.. Advisory Limits Only

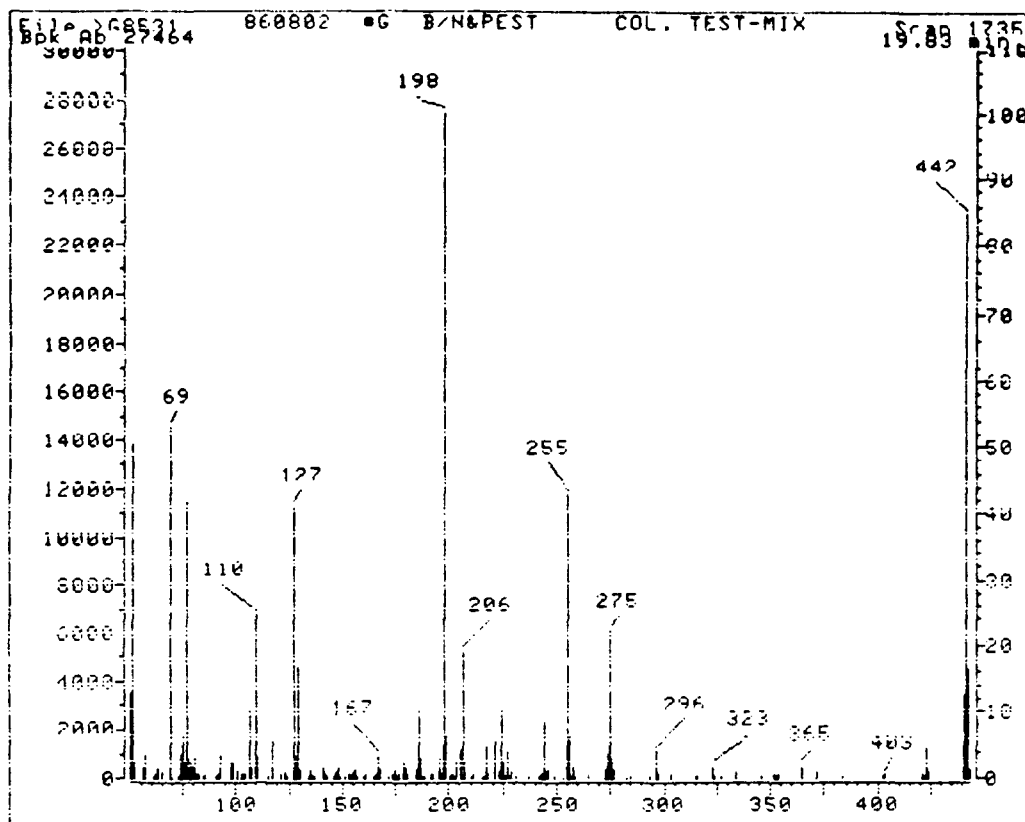


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.74	.74	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	12-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86

Injection Time: 15:34

Run No: 868531

Spectrum No: 1735

Analyst: Slapnick

Processor: Tom Kurowski

QC Batch: QB5395

Samples:

N0146-N0152, N0154-N0158,  
N1250, N1251 (1:10 Dil)  
N1252-N1253

8/8/86



**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports.

NO146 RESOURCE ENGINEERING RES27514 SDB-10-5052 860721 2150  
ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sub>a</sub>	Second ug/kg <sub>a</sub>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	75	ND	ND	ND	0	-	ND	4040	92
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	4040	89
3B	Anthracene	ND	75	ND	ND	BMDL	0	-	ND	4040	93
4B	Benztidine	ND	1700	ND	ND	ND	0	-	ND	4040	7 <sub>a</sub>
5B	Benzo(a)anthracene	ND	310	ND	ND	ND	0	-	ND	4040	91
6B	Benzo(a)pyrene	ND	98	ND	ND	ND	0	-	ND	4040	89
7B	Benzo(b)fluoranthene	ND	390	ND	ND	ND	0	-	ND	4040	79
8B	Benzo(ghi)perylene	ND	160	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	4040	102
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	4040	101
11B	bis(2-Chloroethyl) ether	ND	220	ND	ND	ND	0	-	ND	4040	93
12B	bis(2-Chloroisopropyl)ether	ND	220	ND	ND	ND	0	-	ND	4040	97
13B	bis(2-Ethylhexyl)phthalate	BMDL	390	60.8	ND	BMDL	0	-	159	4040	81
14B	4-Bromophenyl phenyl ether	ND	75	ND	ND	ND	0	-	ND	4040	92
15B	Butyl benzyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	93
16B	2-Chloronaphthalene	ND	75	ND	ND	ND	0	-	ND	4040	93
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	4040	88
18B	Chrysene	ND	98	ND	ND	ND	0	-	ND	4040	83
19B	Dibenzo(a,h)anthracene	ND	390	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	90
21B	1,3-Dichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	88
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	4040	87
23B	3,3'-Dichlorobenzidine	ND	650	ND	ND	ND	0	-	ND	4040	56
24B	Diethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	95
25B	Dimethyl phthalate	ND	390	ND	ND	ND	0	-	ND	4040	96
26B	Di-n-butyl phthalate	ND	390	29.2	61.6	BMDL	0	-	151	4040	97
27B	2,4-Dinitrotoluene	ND	220	ND	ND	ND	0	-	ND	4040	98
28B	2,6-Dinitrotoluene	ND	75	ND	ND	ND	0	-	ND	4040	99
29B	Di-n-octyl phthalate	ND	390	43.7	ND	ND	0	-	ND	4040	83
30B	1,2-Diphenylhydrazine	ND	390	ND	ND	ND	0	-	ND	4040	91
31B	Fluoranthene	ND	87	ND	ND	ND	0	-	ND	4040	90
32B	Fluorene	ND	75	ND	ND	ND	0	-	ND	4040	90

AUG 8, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0146 RESOURCE ENGINEERING

RES27514

SDB-10-5052 860721 2150

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	96
34B	Hexachlorobutadiene	ND	35	ND	ND	ND	0	-	ND	4040	87
35B	Hexachlorocyclopentadiene	ND	390	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	63	ND	ND	ND	0	-	ND	4040	76
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	87	ND	60.1	ND	0	-	ND	4040	89
39B	Naphthalene	ND	63	254	246	ND	0	-	ND	4040	88
40B	Nitrobenzene	ND	75	ND	ND	ND	0	-	ND	4040	89
41B	N-Nitrosodimethylamine	ND	390	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	390	ND	ND	ND	0	-	ND	4040	96
43B	N-Nitrosodiphenylamine	ND	75	ND	ND	ND	0	-	ND	4040	88
44B	Phenanthrene	ND	210	ND	ND	BMDL	0	-	ND	4040	98
45B	Pyrene	ND	75	ND	ND	ND	0	-	ND	4040	89
46B	1,2,4-Trichlorobenzene	ND	75	ND	ND	ND	0	-	ND	4040	87

<sup>a</sup> Results variable due to Non-Homogenous sample matrix.<sup>b</sup> Recovery normally variable using established methodology.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0146	RESOURCE ENGINEERING	RES27514	SDB-10-5052	86072	2150	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added	% Recovery	Control Limits .	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	99	23	120
2-Fluorobiphenyl	50	88	30	115
Terphenyl-D14	50	101	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* 100 EPA Control Limits				
** Advisory Limits Only				

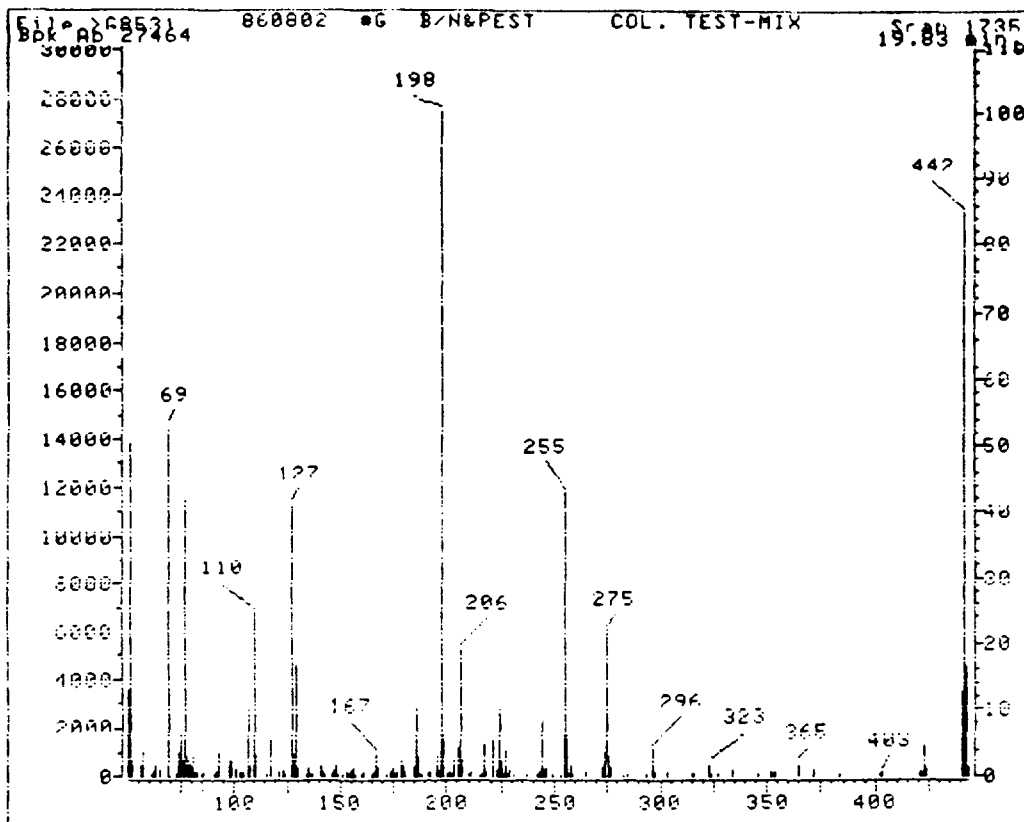


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
69	30-60% of mass 198	50.45	50.45	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	53.05	53.05	OK
70	Less than 2% of mass 69	.24	.45	OK
127	40-60% of mass 198	41.21	41.21	OK
197	Less than 1% of mass 198	.24	.24	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.42	6.42	OK
275	10-30% of mass 198	22.04	22.04	OK
365	Greater than 1% of mass 198	2.02	2.02	OK
441	0-100% of mass 443	12.57	77.21	OK
442	Greater than 40% of mass 198	84.94	84.94	OK
443	12-23% of mass 442	16.28	19.17	OK

Injection Date: 08/02/86  
 Injection Time: 15:34  
 Run No: >G8531  
 Spectrum No: 1735

Analyst: Slapnick  
 Processor: Tom Kuorikoski  
 GC Batch: QB5395  
 Samples: N0146-N0152, N0154-N0158,  
 N1250, N1251 (11:10 D/L)  
 N1252-N1253

8/8/86

AUG 20, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N0144 RESOURCE ENGINEERING

RES27514

SDB-10-5658 860721 2205

ETC Sample No.

Company

Facility

Sample Point

Date

Elapsed  
Time Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sub>a</sub>	Second ug/kg <sub>a</sub>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3330	88
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3330	85
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3330	77
4B	Benzidine	ND	1500	ND	ND	ND	0	-	ND	3330	0 <sub>a</sub>
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3330	79
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3330	79
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3330	75
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3330	93
10B	bis(2-Chloroethoxy)methane	ND	180	ND	ND	ND	0	-	ND	3330	102
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3330	168
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3330	108
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	559	ND	0	-	ND	3330	248 <sub>a</sub>
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3330	89
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3330	92
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3330	86
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3330	96
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3330	89
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3330	119
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3330	78
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3330	90
23B	3,3'-Dichlorobenzidine	ND	550	ND	ND	ND	0	-	ND	3330	0 <sub>a</sub>
24B	Diethyl phthalate	ND	330	77.3	43.1	ND	0	-	57.3	3330	102
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3330	101
26B	Di-n-butyl phthalate	ND	330	ND	ND	415	0	-	ND	3330	93
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3330	100
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3330	95
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3330	93
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3330	99
31B	Fluoranthene	ND	73	ND	61.2	ND	0	-	74.4	3330	62
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3330	* 86

AUG 20, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0144 RESOURCE ENGINEERING RES27514 SDB-10-5658 860721 2205  
ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3330	96
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3330	74
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3330	33
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3330	96
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3330	84
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3330	71
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3330	104
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3330	107
44B	Phenanthrene	ND	180	80.5	40.6	ND	0	-	62.9	3330	89
45B	Pyrene	ND	63	ND	ND	ND	0	-	57.3	3330	67
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3330	75

<sup>a</sup> Variable replication due to non-homogeneous nature of sample matrix.

<sup>b</sup> Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0144	RESOURCE ENGINEERING	RES27514	SDB-10-5658	86072	2205	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	75	23	120
2-Fluorobiphenyl	50	76	30	115
Terphenyl-D14	50	80	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..

\* IFB EPA Control Limits  
\*\* Advisory Limits Only

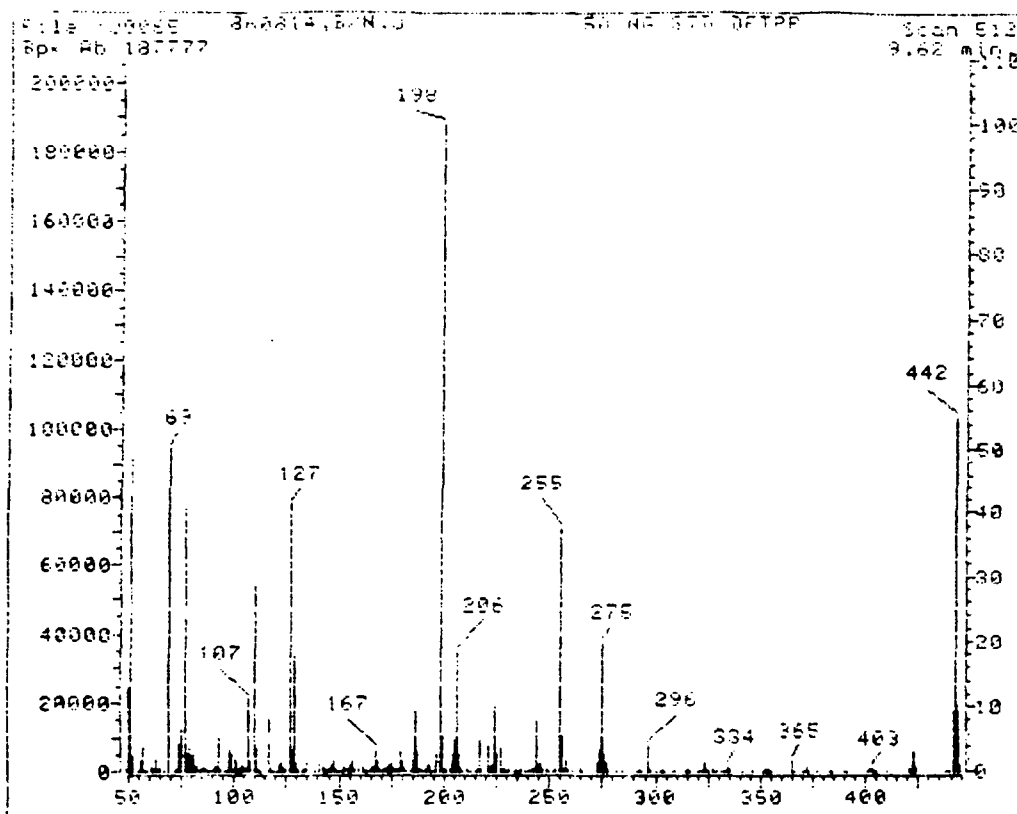


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GLC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	Appropriate Peak	Status
69	30-60% of mass 198	48.43	48.43	OK
68	Less than 2% of mass 69	0.00	0.00	OK
69	(reference only)	50.28	50.28	OK
70	Less than 2% of mass 69	0.00	0.00	OK
127	40-60% of mass 198	41.57	41.57	OK
197	Less than 1% of mass 198	0.00	0.00	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	5.67	5.67	OK
275	10-30% of mass 198	20.09	20.09	OK
365	Greater than 1% of mass 198	1.25	1.25	OK
441	0-100% of mass 443	9.62	96.70	OK
442	Greater than 40% of mass 198	54.98	54.98	OK
443	12-23% of mass 442	9.95	18.10	OK

Injection Date: 08/14/86

Injection Time: 16:31

Run No: >30005

Spectrum No: 512

Analyst: K. Valentin

Processor: Nita Markovici

QC Batch: QB 5418

Samples: Calib. stds. M9059-M9068,  
M9684-M9687, N0194

*VS*  
*8/19/86*

AUG 31, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0174 RESOURCE ENGINEERING

RES27514

SP1033-5

860729 2230

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen Added ug/l	% Recov %	Unspiked Sample ug/l	Concen Added ug/l	% Recov %
1B	Acenaphthene	ND	190000	440000 1	620000	-	-	-	-	-	-
2B	Acenaphthylene	ND	180000	55800	34700	-	-	-	-	-	-
3B	Anthracene	ND	190000	460000 2	090000	-	-	-	-	-	-
4B	Benidine	ND	2200000	ND	ND	-	-	-	-	-	-
5B	Benzo(a)anthracene	ND	390000	946000	608000	-	-	-	-	-	-
6B	Benzo(a)pyrene	ND	130000	316000	179000	-	-	-	-	-	-
7B	Benzo(b)fluoranthene	ND	500000	777000	482000	-	-	-	-	-	-
8B	Benzo(ghi)perylene	ND	210000	ND	ND	-	-	-	-	-	-
9B	Benzo(k)fluoranthene	ND	180000	ND	ND	-	-	-	-	-	-
10B	bis(2-Chloroethoxy)methane	ND	270000	ND	ND	-	-	-	-	-	-
11B	bis(2-Chloroethyl) ether	ND	290000	ND	ND	-	-	-	-	-	-
12B	bis(2-Chloroisopropyl)ether	ND	570000	ND	ND	-	-	-	-	-	-
13B	bis(2-Ethylhexyl)phthalate	ND	500000	ND	ND	-	-	-	-	-	-
14B	4-Bromophenyl phenyl ether	ND	95000	ND	ND	-	-	-	-	-	-
15B	Butyl benzyl phthalate	ND	500000	ND	ND	-	-	-	-	-	-
16B	2-Chloronaphthalene	ND	95000	ND	ND	-	-	-	-	-	-
17B	4-Chlorophenyl phenyl ether	ND	210000	ND	ND	-	-	-	-	-	-
18B	Chrysene	ND	130000	080000	670000	-	-	-	-	-	-
19B	Dibenzo(a,h)anthracene	ND	500000	ND	ND	-	-	-	-	-	-
20B	1,2-Dichlorobenzene	ND	95000	ND	ND	-	-	-	-	-	-
21B	1,3-Dichlorobenzene	ND	95000	ND	ND	-	-	-	-	-	-
22B	1,4-Dichlorobenzene	ND	220000	ND	ND	-	-	-	-	-	-
23B	3,3'-Dichlorobenzidine	ND	830000	ND	ND	-	-	-	-	-	-
24B	Diethyl phthalate	ND	500000	ND	ND	-	-	-	-	-	-
25B	Dimethyl phthalate	ND	1000000	ND	ND	-	-	-	-	-	-
26B	Di-n-butyl phthalate	ND	500000	ND	ND	-	-	-	-	-	-
27B	2,4-Dinitrotoluene	ND	290000	ND	ND	-	-	-	-	-	-
28B	2,6-Dinitrotoluene	ND	95000	ND	ND	-	-	-	-	-	-
29B	Di-n-octyl phthalate	ND	500000	ND	ND	-	-	-	-	-	-
30B	1,2-Diphenylhydrazine	ND	500000	ND	ND	-	-	-	-	-	-
31B	Fluoranthene	ND	110000	440000 3	500000	-	-	-	-	-	-
32B	Fluorene	ND	190000	520000 2	360000	-	-	-	-	-	-

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 31, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0174 RESOURCE ENGINEERING

RES27514

SP1033-5

860729 2230

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
33B	Hexachlorobenzene	ND	95000	ND	ND	-	-	-	-	-	-
34B	Hexachlorobutadiene	ND	45000	ND	ND	-	-	-	-	-	-
35B	Hexachlorocyclopentadiene	ND	500000	ND	ND	-	-	-	-	-	-
36B	Hexachloroethane	ND	80000	ND	ND	-	-	-	-	-	-
37B	Indeno(1,2,3-c,d)pyrene	ND	240000	ND	ND	-	-	-	-	-	-
38B	Isophorone	ND	110000	ND	ND	-	-	-	-	-	-
39B	Naphthalene	271000	80000	940000 1	220000	-	-	-	-	-	-
40B	Nitrobenzene	ND	95000	ND	ND	-	-	-	-	-	-
41B	N-Nitrosodimethylamine	ND	1000000	ND	ND	-	-	-	-	-	-
42B	N-Nitrosodi-n-propylamine	ND	500000	ND	ND	-	-	-	-	-	-
43B	N-Nitrosodiphenylamine	ND	190000	ND	ND	-	-	-	-	-	-
44B	Phenanthrene	BMDL	270000	400000 6	910000	-	-	-	-	-	-
45B	Pyrene	ND	95000	780000 2	090000	-	-	-	-	-	-
46B	1,2,4-Trichlorobenzene	ND	95000	ND	ND	-	-	-	-	-	-

A ETC established Method Detection Limit for this particular sample.

B Standard QA procedures not applicable to dilute and shoot analysis.



AUG 19, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0175

RESOURCE ENGINEERING

RES27514

SPT0323-25 860729 2350

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	134	63	ND	ND	ND	0	-	134	3120	80
2B	Acenaphthylene	BMDL	120	ND	ND	ND	0	-	74.4	3120	79
3B	Anthracene	108	63	ND	ND	ND	0	-	108	3120	71
4B	Benzidine	ND	1500	ND	ND	ND	0	-	ND	3120	0 <sub>a</sub>
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3120	77
6B	Benzo(a)pyrene	ND	82	ND	ND	ND	0	-	ND	3120	159
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3120	122
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3120	104
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3120	72
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3120	68
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3120	46
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	1550	BMDL	0	-	ND	3120	73
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3120	88
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	72
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3120	89
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3120	78
18B	Chrysene	ND	82	ND	ND	ND	0	-	ND	3120	83
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3120	58
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3120	61
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3120	69
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3120	0 <sub>a</sub>
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	74
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	75
26B	Di-n-butyl phthalate	BMDL	330	ND	40.4	BMDL	0	-	56.1	3120	77
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3120	69
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3120	69
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	97
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3120	75
31B	Fluoranthene	BMDL	73	ND	ND	ND	0	-	51.8	3120	35
32B	Fluorene	316	63	ND	ND	ND	0	-	316	3120	69



ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 19, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0175 RESOURCE ENGINEERING

RES27514 SP10323-25 860729 2350

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sub>a</sub>	Second ug/kg <sub>a</sub>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3120	83
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3120	78
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3120	84
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3120	77
39B	Naphthalene	982	53	ND	ND	ND	0	-	982	3120	78
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3120	83
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3120	83
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3120	87
44B	Phenanthrene	765	180	ND	ND	ND	0	-	765	3120	76
45B	Pyrene	91.5	63	ND	ND	ND	0	-	91.6	3120	28
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3120	80

A Variable replication due to non-homogeneous nature of sample matrix.

B Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports						
N0175						
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount Added ug	% Recovery	Control Limits *	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	92	23	120
2-Fluorobiphenyl	50	132***	30	115
Terphenyl-D14	50	54	18	137
PESTICIDE/PCB FRACTION (GC/MS)				
Dibutylchloroendate	-	-	20**	150**
* IFR EPA Control Limits.				
** Advisory Limits Only.				
*** Recovery manually verified.				

\* IFR EPA Control Limits.

\*\* Advisory Limits Only.

\*\*\* Recovery manually verified.

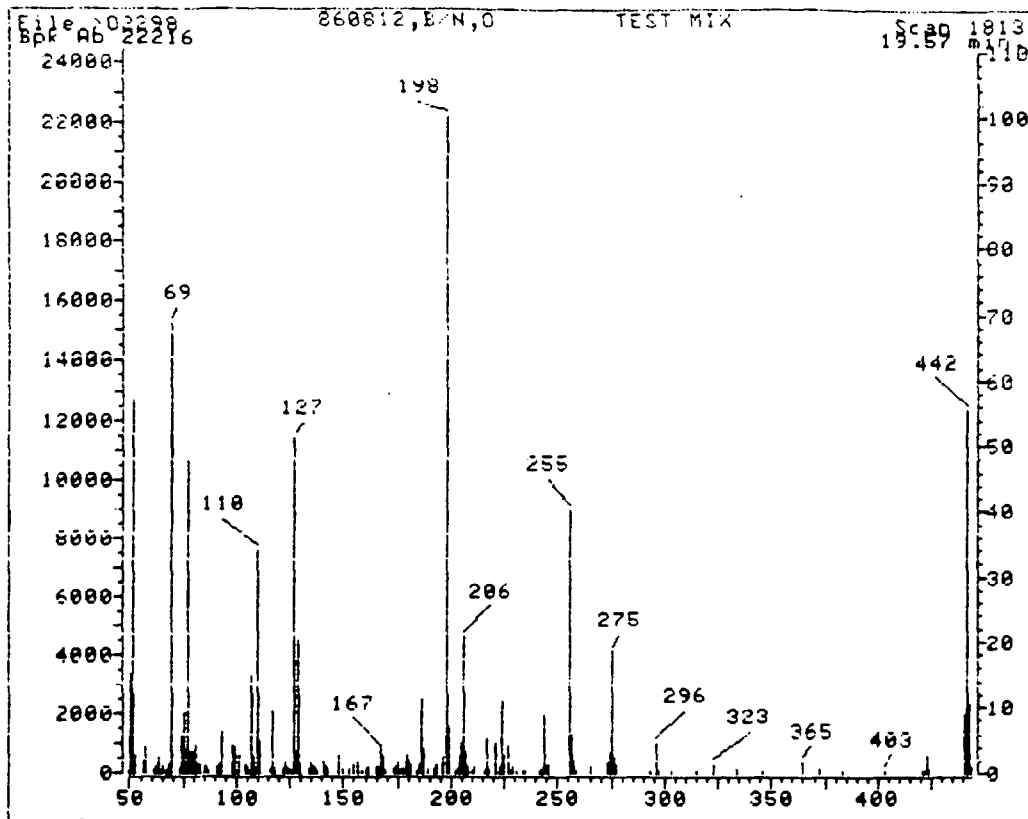


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	57.15	57.15	Ok
68	Less than 2% of mass 69	1.21	1.76	Ok
69	(reference only)	68.73	68.73	Ok
70	Less than 2% of mass 69	0.00	0.00	Ok
127	40-60% of mass 198	51.21	51.21	Ok
197	Less than 1% of mass 198	0.00	0.00	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	7.21	7.21	Ok
275	10-30% of mass 198	18.60	18.60	Ok
365	Greater than 1% of mass 198	1.85	1.85	Ok
441	0-100% of mass 443	8.64	84.28	Ok
442	Greater than 40% of mass 198	55.78	55.78	Ok
443	17-23% of mass 442	10.25	18.37	Ok

Injection Date: 08/12/86  
Injection Time: 16:31  
Run No: >02298  
Spectrum No: 1813

Analyst: [Signature]  
Processor: [Signature]  
QC Batch: QB5430  
Samples: N0173 N0174 N0178  
Calib. Std

AUG 19, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

NO178 RESOURCE ENGINEERING

RES27514

SP10328-30 860730 0045

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concn. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concn. Added ug/kg	% Recov
1B	Acenaphthene	168	62	ND	ND	ND	0	-	134	3120	80
2B	Acenaphthylene	BMDL	110	ND	ND	ND	0	-	74.4	3120	79
3B	Anthracene	ND	62	ND	ND	ND	0	-	108	3120	71
4B	Benidine	ND	1400	ND	ND	ND	0	-	ND	3120	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3120	77
6B	Benzo(a)pyrene	ND	82	ND	ND	ND	0	-	ND	3120	159
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3120	122
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3120	104
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3120	72
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3120	68
12B	bis(2-Chloroisopropyl) ether	ND	190	ND	ND	ND	0	-	ND	3120	46
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	1550	BMDL	0	-	ND	3120	73
14B	4-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3120	88
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	72
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3120	89
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3120	78
18B	Chrysene	ND	82	ND	ND	ND	0	-	ND	3120	83
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	58
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	61
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3120	69
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3120	0.
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	74
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	75
26B	Di-n-butyl phthalate	BMDL	330	ND	40.4	BMDL	0	-	56.1	3120	77
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3120	69
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3120	69
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	97
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3120	75
31B	Fluoranthene	BMDL	72	ND	ND	ND	0	-	51.8	3120	35
32B	Fluorene	246	62	ND	ND	ND	0	-	316	3120	69

AUG 19, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N0178 RESOURCE ENGINEERING RES27514 SP10328-30 860730 0045  
 ETC Sample No. Company Facility Sample Point Date Time Elapsed  
 Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	83
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3120	78
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	52	ND	ND	ND	0	-	ND	3120	84
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	72	ND	ND	ND	0	-	ND	3120	77
39B	Naphthalene	927	52	ND	ND	ND	0	-	982	3120	78
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3120	83
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3120	83
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3120	87
44B	Phenanthrene	682	180	ND	ND	ND	0	-	765	3120	76
45B	Pyrene	ND	62	ND	ND	ND	0	-	91.6	3120	28
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	80

<sup>a</sup> Variable replication due to non-homogeneous nature of sample matrix.<sup>b</sup> Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports						
N0178	RESOURCE ENGINEERING	RES27514	SP10328-30	86073	0045	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	82	23	120
2-Fluorobiphenyl	50	84	30	115
Terphenyl-D14	50	73	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPR Control Limits ** Advisory Limits Only				

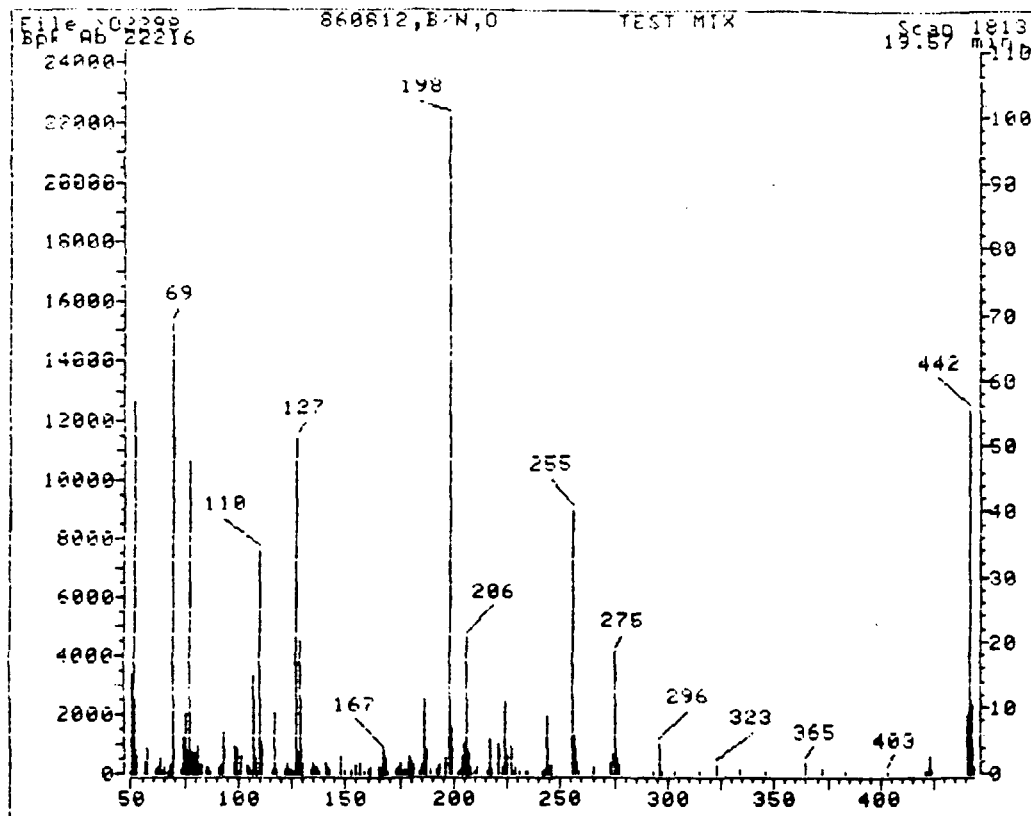


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	Appropriate Peak	Status
51	30-60% of mass 198	57.15	57.15	Ok
68	Less than 2% of mass 69	1.21	1.76	Ok
69	(reference only)	68.73	68.73	Ok
70	Less than 2% of mass 69	0.00	0.00	Ok
127	40-60% of mass 198	51.21	51.21	Ok
197	Less than 1% of mass 198	0.00	0.00	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	7.21	7.21	Ok
275	10-30% of mass 198	18.60	18.60	Ok
365	Greater than 1% of mass 198	1.85	1.85	Ok
441	0-100% of mass 443	8.64	84.28	Ok
442	Greater than 40% of mass 198	55.78	55.78	Ok
443	17-23% of mass 442	10.25	18.37	Ok

Injection Date: 08/12/86  
Injection Time: 16:31  
Run No: >02298  
Spectrum No: 1813

Analyst: M. A. Muthuraj  
Processor: RBS430  
QC Batch: N0173, N0174  
Samples: Calib. Std



AUG 19, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

## Chain of Custody Data Required for ETC Data Management: Summary Reports

N0176

RESOURCE ENGINEERING

RES27514

SP10338-40 860730 0115

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sub>a</sub>	Second ug/kg <sub>a</sub>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	BMDL	62	ND	ND	ND	0	-	134	3120	80
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	74.4	3120	79
3B	Anthracene	ND	62	ND	ND	ND	0	-	108	3120	71
4B	Benzidine	ND	1400	ND	ND	ND	0	-	ND	3120	0 <sub>a</sub>
5B	Benzo(a)anthracene	ND	250	ND	ND	ND	0	-	ND	3120	77
6B	Benzo(a)pyrene	ND	81	ND	ND	ND	0	-	ND	3120	159
7B	Benzo(b)fluoranthene	ND	320	ND	ND	ND	0	-	ND	3120	122
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3120	104
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3120	72
11B	bis(2-Chloroethyl) ether	ND	180	ND	ND	ND	0	-	ND	3120	68
12B	bis(2-Chloroisopropyl)ether	ND	180	ND	ND	ND	0	-	ND	3120	46
13B	bis(2-Ethylhexyl)phthalate	ND	320	ND	1550	BMDL	0	-	ND	3120	73
14B	4-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3120	88
15B	Butyl benzyl phthalate	ND	320	ND	ND	ND	0	-	ND	3120	72
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3120	89
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3120	78
18B	Chrysene	ND	81	ND	ND	ND	0	-	ND	3120	83
19B	Dibenzo(a,h)anthracene	ND	320	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	58
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	61
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3120	69
23B	3,3'-Dichlorobenzidine	ND	530	ND	ND	ND	0	-	ND	3120	0 <sub>a</sub>
24B	Diethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3120	74
25B	Dimethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3120	75
26B	Di-n-butyl phthalate	BMDL	320	ND	40.4	BMDL	0	-	56.1	3120	77
27B	2,4-Dinitrotoluene	ND	180	ND	ND	ND	0	-	ND	3120	69
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3120	69
29B	Di-n-octyl phthalate	ND	320	ND	ND	ND	0	-	ND	3120	97
30B	1,2-Diphenylhydrazine	ND	320	ND	ND	ND	0	-	ND	3120	75
31B	Fluoranthene	ND	71	ND	ND	ND	0	-	51.8	3120	35
32B	Fluorene	70.0	62	ND	ND	ND	0	-	316	3120	69

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 19, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0176 RESOURCE ENGINEERING RES27514 SP10338-40 860730 0115

ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/kg	MDL ug/kg	First ug/kg <sub>A</sub>	Second ug/kg <sub>A</sub>	Blank Data ug/kg	Concn. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concn. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	83
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3120	78
35B	Hexachlorocyclopentadiene	ND	320	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	52	ND	ND	ND	0	-	ND	3120	84
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	71	ND	ND	ND	0	-	ND	3120	77
39B	Naphthalene	609	52	ND	ND	ND	0	-	982	3120	78
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3120	83
41B	N-Nitrosodimethylamine	ND	320	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	320	ND	ND	ND	0	-	ND	3120	83
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3120	87
44B	Phenanthrene	BMDL	170	ND	ND	ND	0	-	765	3120	76
45B	Pyrene	ND	62	ND	ND	ND	0	-	91.6	3120	28
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	80

A Variable replication due to non-homogeneous nature of sample matrix.

B Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0176	RESOURCE ENGINEERING	RES27514	SP10338-40	86073	0115	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	83	23	120
2-Fluorobiphenyl	50	98	30	115
Terphenyl-D14	50	100	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits ** Advisory Limits Only				

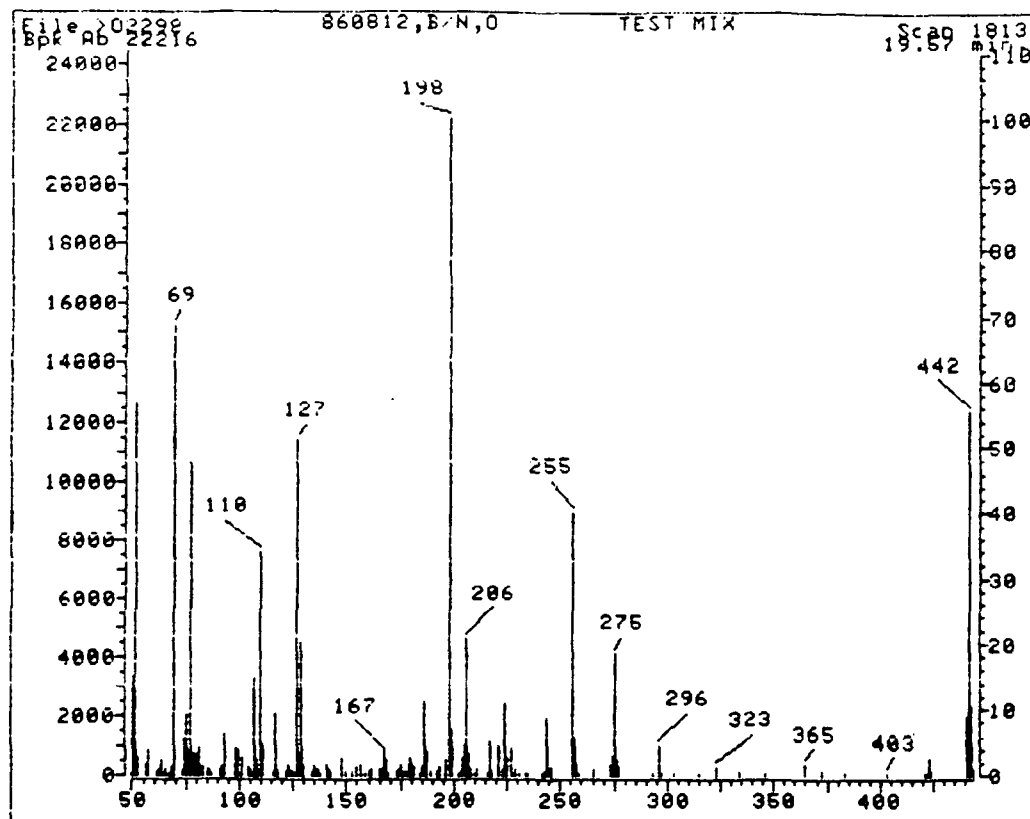


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	57.15	57.15	Ok
68	Less than 2% of mass 69	1.21	1.76	Ok
69	(reference only)	68.73	68.73	Ok
70	Less than 2% of mass 69	0.00	0.00	Ok
127	40-60% of mass 198	51.21	51.21	Ok
197	Less than 1% of mass 198	0.00	0.00	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	7.21	7.21	Ok
275	10-30% of mass 198	18.60	18.60	Ok
365	Greater than 1% of mass 198	1.85	1.85	Ok
441	0-100% of mass 443	8.64	84.28	Ok
442	Greater than 40% of mass 198	55.78	55.78	Ok
443	17-23% of mass 442	10.25	18.37	Ok

Injection Date: 08/12/86  
Injection Time: 16:31  
Run No: >02298  
Spectrum No: 1813

Analyst: *[Signature]*  
Processor: *[Signature]*  
QC Batch: *Q35430*  
Samples: *N0173, N0174, N0175, Calib. Std*

AUG 19, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0177 RESOURCE ENGINEERING

RES27514 SPT0348-50 860730 0130

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	62	ND	ND	ND	0	-	134	3120	80
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	74.4	3120	79
3B	Anthracene	ND	62	ND	ND	ND	0	-	108	3120	71
4B	Benzidine	ND	1400	ND	ND	ND	0	-	ND	3120	0.
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3120	77
6B	Benzo(a)pyrene	ND	82	ND	ND	ND	0	-	ND	3120	159
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3120	122
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3120	104
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3120	72
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3120	68
12B	bis(2-Chloroisopropyl) ether	ND	190	ND	ND	ND	0	-	ND	3120	46
13B	bis(2-Ethylhexyl)phthalate	587	330	ND	1550	BMDL	0	-	ND	3120	73
14B	4-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3120	88
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	72
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3120	89
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3120	78
18B	Chrysene	ND	82	ND	ND	ND	0	-	ND	3120	83
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	58
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	61
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3120	69
23B	3,3'-Dichlorobenzidine	ND	540	ND	ND	ND	0	-	ND	3120	0.
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	74
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	75
26B	Di-n-butyl phthalate	BMDL	330	ND	40.4	BMDL	0	-	56.1	3120	77
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3120	69
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3120	69
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3120	97
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3120	75
31B	Fluoranthene	ND	72	ND	ND	ND	0	-	51.8	3120	35
32B	Fluorene	ND	62	ND	ND	ND	0	-	316	3120	69

AUG 19, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0177 RESOURCE ENGINEERING RES27514 SPI0348-50 860730 0130  
ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	83
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3120	78
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3120	84
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	72	ND	ND	ND	0	-	ND	3120	77
39B	Naphthalene	ND	53	ND	ND	ND	0	-	982	3120	78
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3120	83
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3120	83
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3120	87
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	765	3120	76
45B	Pyrene	ND	62	ND	ND	ND	0	-	91.6	3120	28
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	80

<sup>a</sup> Variable replication due to non-homogeneous nature of sample matrix.

<sup>b</sup> Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports					
NO177	RESOURCE ENGINEERING	RES27514	SP10348-50	86073	0130 0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	80	23	120
2-Fluorobiphenyl	50	99	30	115
Terphenyl-D14	50	105	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFR EPA Control Limits				
** Advisory Limits Only				

\* IFB EPR Control Limits

\*\* Advisory Limits Only

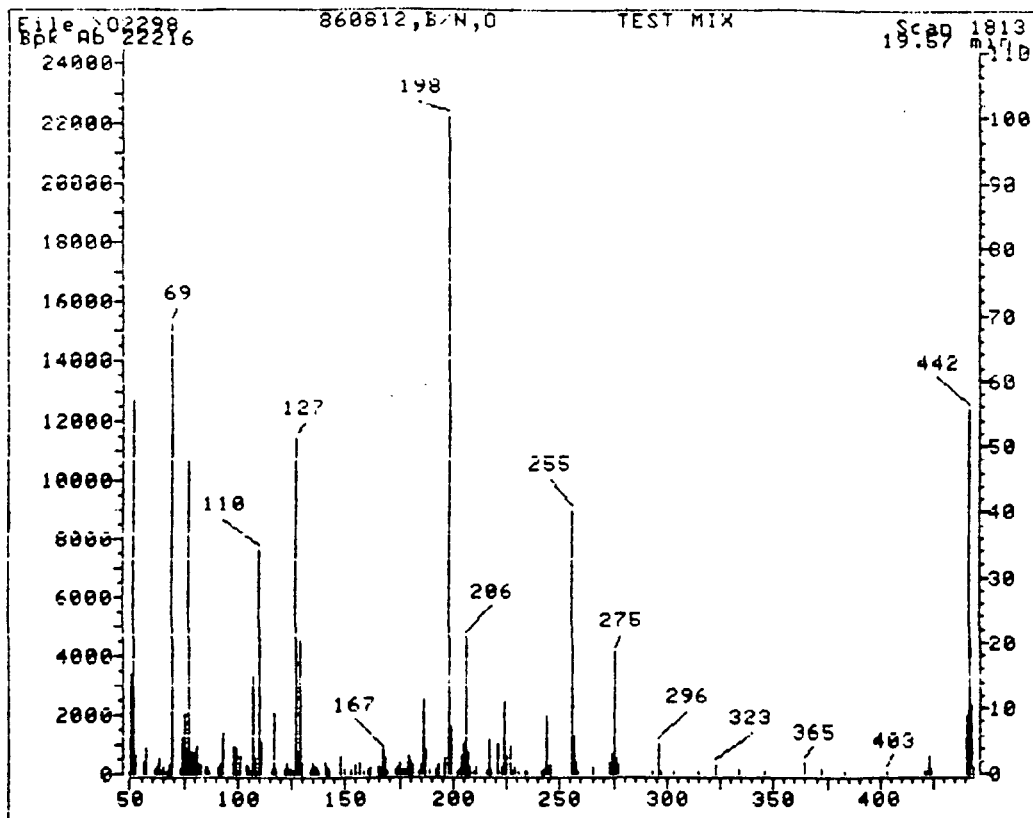


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
51	30-60% of mass 198	57.15	57.15	Ok
68	Less than 2% of mass 69	1.21	1.76	Ok
69	(reference only)	68.73	68.73	Ok
70	Less than 2% of mass 69	0.00	0.00	Ok
127	40-60% of mass 198	51.21	51.21	Ok
197	Less than 1% of mass 198	0.00	0.00	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	7.21	7.21	Ok
275	10-30% of mass 198	18.60	18.60	Ok
365	Greater than 1% of mass 198	1.85	1.85	Ok
441	0-100% of mass 443	8.64	84.28	Ok
442	Greater than 40% of mass 198	55.78	55.78	Ok
443	17-23% of mass 442	10.25	18.37	Ok

Injection Date: 08/12/86  
 Injection Time: 16:31  
 Run No: >02298  
 Spectrum No: 1813

Analyst: *[Signature]*  
 Processor: *[Signature]*  
 QC Batch: 0135430  
 Samples: N0173, N0174, ~~N0175~~,  
 Calib. Std



AUG 19, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0173

RESOURCE ENGINEERING

RES27514

SP10362-64 860730 0145

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	62	ND	ND	ND	0	-	134	3120	80
2B	Acenaphthylene	ND	110	ND	ND	ND	0	-	74.4	3120	79
3B	Anthracene	ND	62	ND	ND	ND	0	-	108	3120	71
4B	Benizidine	ND	1400	ND	ND	ND	0	-	ND	3120	0 <sup>a</sup>
5B	Benzo(a)anthracene	ND	250	ND	ND	ND	0	-	ND	3120	77
6B	Benzo(a)pyrene	ND	81	ND	ND	ND	0	-	ND	3120	159
7B	Benzo(b)fluoranthene	ND	320	ND	ND	ND	0	-	ND	3120	122
8B	Benzo(ghi)perylene	ND	130	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	110	ND	ND	ND	0	-	ND	3120	104
10B	bis(2-Chloroethoxy)methane	ND	170	ND	ND	ND	0	-	ND	3120	72
11B	bis(2-Chloroethyl) ether	ND	180	ND	ND	ND	0	-	ND	3120	68
12B	bis(2-Chloroisopropyl)ether	ND	180	ND	ND	ND	0	-	ND	3120	46
13B	bis(2-Ethylhexyl)phthalate	ND	320	ND	1550	BMDL	0	-	ND	3120	73
14B	4-Bromophenyl phenyl ether	ND	62	ND	ND	ND	0	-	ND	3120	88
15B	Butyl benzyl phthalate	ND	320	ND	ND	ND	0	-	ND	3120	72
16B	2-Chloronaphthalene	ND	62	ND	ND	ND	0	-	ND	3120	89
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3120	78
18B	Chrysene	ND	81	ND	ND	ND	0	-	ND	3120	83
19B	Dibenzo(a,h)anthracene	ND	320	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	58
21B	1,3-Dichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	61
22B	1,4-Dichlorobenzene	ND	140	ND	ND	ND	0	-	ND	3120	69
23B	3,3'-Dichlorobenzidine	ND	530	ND	ND	ND	0	-	ND	3120	0 <sup>a</sup>
24B	Diethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3120	74
25B	Dimethyl phthalate	ND	320	ND	ND	ND	0	-	ND	3120	75
26B	Di-n-butyl phthalate	ND	320	ND	40.4	BMDL	0	-	56.1	3120	77
27B	2,4-Dinitrotoluene	ND	180	ND	ND	ND	0	-	ND	3120	69
28B	2,6-Dinitrotoluene	ND	62	ND	ND	ND	0	-	ND	3120	69
29B	Di-n-octyl phthalate	ND	320	ND	ND	ND	0	-	ND	3120	97
30B	1,2-Diphenylhydrazine	ND	320	ND	ND	ND	0	-	ND	3120	75
31B	Fluoranthene	ND	71	ND	ND	ND	0	-	51.8	3120	35
32B	Fluorene	ND	62	ND	ND	ND	0	-	316	3120	69

AUG 19, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N0173 RESOURCE ENGINEERING

RES27514 SPI0362-64 860730 0145

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg <sup>a</sup>	Second ug/kg <sup>a</sup>	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	83
34B	Hexachlorobutadiene	ND	29	ND	ND	ND	0	-	ND	3120	78
35B	Hexachlorocyclopentadiene	ND	320	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	52	ND	ND	ND	0	-	ND	3120	84
37B	Indeno(1,2,3-c,d)pyrene	ND	150	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	71	ND	ND	ND	0	-	ND	3120	77
39B	Naphthalene	ND	52	ND	ND	ND	0	-	982	3120	78
40B	Nitrobenzene	ND	62	ND	ND	ND	0	-	ND	3120	83
41B	N-Nitrosodimethylamine	ND	320	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	320	ND	ND	ND	0	-	ND	3120	83
43B	N-Nitrosodiphenylamine	ND	62	ND	ND	ND	0	-	ND	3120	87
44B	Phenanthrene	ND	170	ND	ND	ND	0	-	765	3120	76
45B	Pyrene	ND	62	ND	ND	ND	0	-	91.6	3120	28
46B	1,2,4-Trichlorobenzene	ND	62	ND	ND	ND	0	-	ND	3120	80

<sup>a</sup> Variable replication due to non-homogeneous nature of sample matrix.<sup>b</sup> Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports						
N0173	RESOURCE ENGINEERING	RES27514	SP10362-64	86073	0145	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	65	23	120
2-Fluorobiphenyl	50	66	30	115
Terphenyl-D14	50	117	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits ** Advisory Limits Only				



AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9370 RESOURCE ENGINEERING

RES27511

XREI1128-30 860804 2024

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen Added ug/kg	% Recov
1B	Acenaphthene	ND	70	ND	ND	ND	0	-	ND	3390	89
2B	Acenaphthylene	ND	130	ND	ND	ND	0	-	ND	3390	95
3B	Anthracene	ND	70	ND	ND	ND	0	-	ND	3390	85
4B	Benzidine	ND	1600	ND	ND	ND	0	-	ND	3390	22 <sub>a</sub>
5B	Benzo(a)anthracene	ND	290	ND	ND	ND	0	-	ND	3390	82
6B	Benzo(a)pyrene	ND	92	ND	ND	ND	0	-	ND	3390	113
7B	Benzo(b)fluoranthene	ND	370	ND	ND	ND	0	-	ND	3390	109
8B	Benzo(ghi)perylene	ND	150	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	130	ND	ND	ND	0	-	ND	3390	96
10B	bis(2-Chloroethoxy)methane	ND	200	ND	ND	ND	0	-	ND	3390	86
11B	bis(2-Chloroethyl) ether	ND	210	ND	ND	ND	0	-	ND	3390	76
12B	bis(2-Chloroisopropyl) ether	ND	210	ND	ND	ND	0	-	ND	3390	126
13B	bis(2-Ethylhexyl)phthalate	BMDL	370	ND	ND	278	0	-	ND	3390	98
14B	4-Bromophenyl phenyl ether	ND	70	ND	ND	ND	0	-	ND	3390	66
15B	Butyl benzyl phthalate	ND	370	ND	ND	ND	0	-	ND	3390	90
16B	2-Chloronaphthalene	ND	70	ND	ND	ND	0	-	ND	3390	91
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	3390	87
18B	Chrysene	ND	92	ND	ND	ND	0	-	ND	3390	87
19B	Dibenzo(a,h)anthracene	ND	370	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	70	ND	ND	ND	0	-	ND	3390	82
21B	1,3-Dichlorobenzene	ND	70	ND	ND	ND	0	-	ND	3390	81
22B	1,4-Dichlorobenzene	ND	160	ND	ND	ND	0	-	ND	3390	80
23B	3,3'-Dichlorobenzidine	ND	610	ND	ND	ND	0	-	ND	3390	33 <sub>a</sub>
24B	Diethyl phthalate	ND	370	ND	ND	ND	0	-	ND	3390	87
25B	Dimethyl phthalate	ND	370	ND	ND	ND	0	-	ND	3390	89
26B	Di-n-butyl phthalate	ND	370	ND	96.1	394	0	-	ND	3390	144 <sub>a</sub>
27B	2,4-Dinitrotoluene	ND	210	ND	ND	ND	0	-	ND	3390	100
28B	2,6-Dinitrotoluene	ND	70	ND	ND	ND	0	-	ND	3390	83
29B	Di-n-octyl phthalate	BMDL	370	ND	ND	ND	0	-	ND	3390	108
30B	1,2-Diphenylhydrazine	ND	370	ND	ND	ND	0	-	ND	3390	90
31B	Fluoranthene	ND	81	ND	ND	ND	0	-	ND	3390	88
32B	Fluorene	ND	70	ND	ND	ND	0	-	ND	3390	88

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9370 RESOURCE ENGINEERING

RES27511 XREI1128-30 860804 2024 1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	70	ND	ND	ND	0	-	ND	3390	84
34B	Hexachlorobutadiene	ND	33	ND	ND	ND	0	-	ND	3390	104
35B	Hexachlorocyclopentadiene	ND	370	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	59	ND	ND	ND	0	-	ND	3390	109
37B	Indeno(1,2,3-c,d)pyrene	ND	170	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	81	ND	ND	ND	0	-	ND	3390	83
39B	Naphthalene	ND	59	ND	ND	ND	0	-	ND	3390	87
40B	Nitrobenzene	ND	70	ND	ND	ND	0	-	ND	3390	95
41B	N-Nitrosodimethylamine	ND	370	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	370	ND	ND	ND	0	-	ND	3390	96
43B	N-Nitrosodiphenylamine	ND	70	ND	ND	ND	0	-	ND	3390	114
44B	Phenanthrene	ND	200	ND	ND	ND	0	-	ND	3390	87
45B	Pyrene	ND	70	ND	ND	ND	0	-	ND	3390	78
46B	1,2,4-Trichlorobenzene	ND	70	ND	ND	ND	0	-	ND	3390	92

A Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

MS370	RESOURCE ENGINEERING	RES27511	XRE1128-30	86080	2024	1
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added	% Recovery	Control Limits ,	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	68	23	120
2-Fluorobiphenyl	50	78	30	115
Terphenyl-D14	50	103	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits				
.. Advisory Limits Only				

\* IFB EPR Control Limits

\*\* Advisory Limits Only

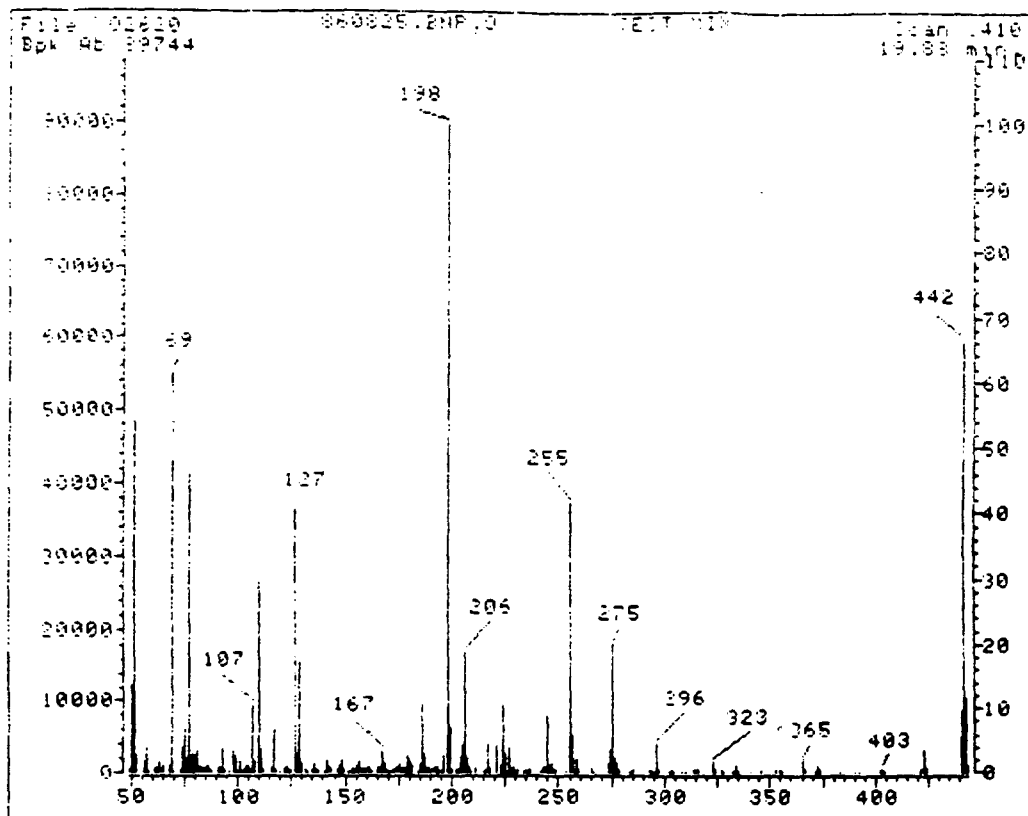


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	Appropriate Peak	Status
69	30-60% of mass 198	63.87	53.87	Ok
68	Less than 2% of mass 69	.89	1.45	Ok
69	(reference only)	61.49	61.49	Ok
70	Less than 2% of mass 69	.20	.33	Ok
127	40-60% of mass 198	40.35	40.35	Ok
197	Less than 1% of mass 198	0.00	0.00	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.79	6.79	Ok
275	10-30% of mass 198	19.84	19.84	Ok
365	Greater than 1% of mass 198	1.89	1.89	Ok
441	0-100% of mass 443	9.74	82.81	Ok
442	Greater than 40% of mass 198	66.19	66.19	Ok
443	17-23% of mass 442	11.76	17.76	Ok

Injection Date: 08/25/86  
Injection Time: 16:54  
Run No: 002620  
Spectrum No: 1410

Analyst: MLB  
Processor: MSB  
QC Batch: QR5465  
Samples: M9370, M9371, M9383, N1319, N1310, N1309, N1323, N1322



AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9371 RESOURCE ENGINEERING RES27511 XREI1130-32 860804 2048 1  
 ETC Sample No. Company Facility Sample Point Date Time Elapsed  
 Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	77	ND	ND	ND	0	-	ND	3390	89
2B	Acenaphthylene	ND	140	ND	ND	ND	0	-	ND	3390	95
3B	Anthracene	ND	77	ND	ND	ND	0	-	ND	3390	85
4B	Benidine	ND	1800	ND	ND	ND	0	-	ND	3390	22.
5B	Benzo(a)anthracene	ND	320	ND	ND	ND	0	-	ND	3390	82
6B	Benzo(a)pyrene	ND	100	ND	ND	ND	0	-	ND	3390	113
7B	Benzo(b)fluoranthene	ND	400	ND	ND	ND	0	-	ND	3390	109
8B	Benzo(ghi)perylene	ND	170	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	140	ND	ND	ND	0	-	ND	3390	96
10B	bis(2-Chloroethoxy)methane	ND	210	ND	ND	ND	0	-	ND	3390	86
11B	bis(2-Chloroethyl) ether	ND	230	ND	ND	ND	0	-	ND	3390	76
12B	bis(2-Chloroisopropyl)ether	ND	230	ND	ND	ND	0	-	ND	3390	126
13B	bis(2-Ethylhexyl)phthalate	ND	400	ND	ND	278	0	-	ND	3390	98
14B	4-Bromophenyl phenyl ether	ND	77	ND	ND	ND	0	-	ND	3390	66
15B	Butyl benzyl phthalate	ND	400	ND	ND	ND	0	-	ND	3390	90
16B	2-Chloronaphthalene	ND	77	ND	ND	ND	0	-	ND	3390	91
17B	4-Chlorophenyl phenyl ether	ND	170	ND	ND	ND	0	-	ND	3390	87
18B	Chrysene	ND	100	ND	ND	ND	0	-	ND	3390	87
19B	Dibenzo(a,h)anthracene	ND	400	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	77	ND	ND	ND	0	-	ND	3390	82
21B	1,3-Dichlorobenzene	ND	77	ND	ND	ND	0	-	ND	3390	81
22B	1,4-Dichlorobenzene	ND	180	ND	ND	ND	0	-	ND	3390	80
23B	3,3'-Dichlorobenzidine	ND	670	ND	ND	ND	0	-	ND	3390	33.
24B	Diethyl phthalate	ND	400	ND	ND	ND	0	-	ND	3390	87
25B	Dimethyl phthalate	ND	400	ND	ND	ND	0	-	ND	3390	89
26B	Di-n-butyl phthalate	ND	400	ND	96.1	394	0	-	ND	3390	144.
27B	2,4-Dinitrotoluene	ND	230	ND	ND	ND	0	-	ND	3390	100
28B	2,6-Dinitrotoluene	ND	77	ND	ND	ND	0	-	ND	3390	83
29B	Di-n-octyl phthalate	ND	400	ND	ND	ND	0	-	ND	3390	108
30B	1,2-Diphenylhydrazine	ND	400	ND	ND	ND	0	-	ND	3390	90
31B	Fluoranthene	ND	89	ND	ND	ND	0	-	ND	3390	88
32B	Fluorene	ND	77	ND	ND	ND	0	-	ND	3390	88

AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9371 RESOURCE ENGINEERING

RES27511

XREI1130-32 860804 2048

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	77	ND	ND	ND	0	-	ND	3390	84
34B	Hexachlorobutadiene	ND	36	ND	ND	ND	0	-	ND	3390	104
35B	Hexachlorocyclopentadiene	ND	400	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	65	ND	ND	ND	0	-	ND	3390	109
37B	Indeno(1,2,3-c,d)pyrene	ND	190	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	89	ND	ND	ND	0	-	ND	3390	83
39B	Naphthalene	ND	65	ND	ND	ND	0	-	ND	3390	87
40B	Nitrobenzene	ND	77	ND	ND	ND	0	-	ND	3390	95
41B	N-Nitrosodimethylamine	ND	400	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	400	ND	ND	ND	0	-	ND	3390	96
43B	N-Nitrosodiphenylamine	ND	77	ND	ND	ND	0	-	ND	3390	114
44B	Phenanthrene	ND	220	ND	ND	ND	0	-	ND	3390	87
45B	Pyrene	ND	77	ND	ND	ND	0	-	ND	3390	78
46B	1,2,4-Trichlorobenzene	ND	77	ND	ND	ND	0	-	ND	3390	92

A Recovery manually verified.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9371	RESOURCE ENGINEERING	RES27511	XREI1130-32	86080	2048	1
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	X Recovery	Control Limits	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	73	23	120
2-Fluorobiphenyl	50	73	30	115
Terphenyl-D14	50	102	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..

\* IFB EPA Control Limits  
 \*\* Advisory Limits Only

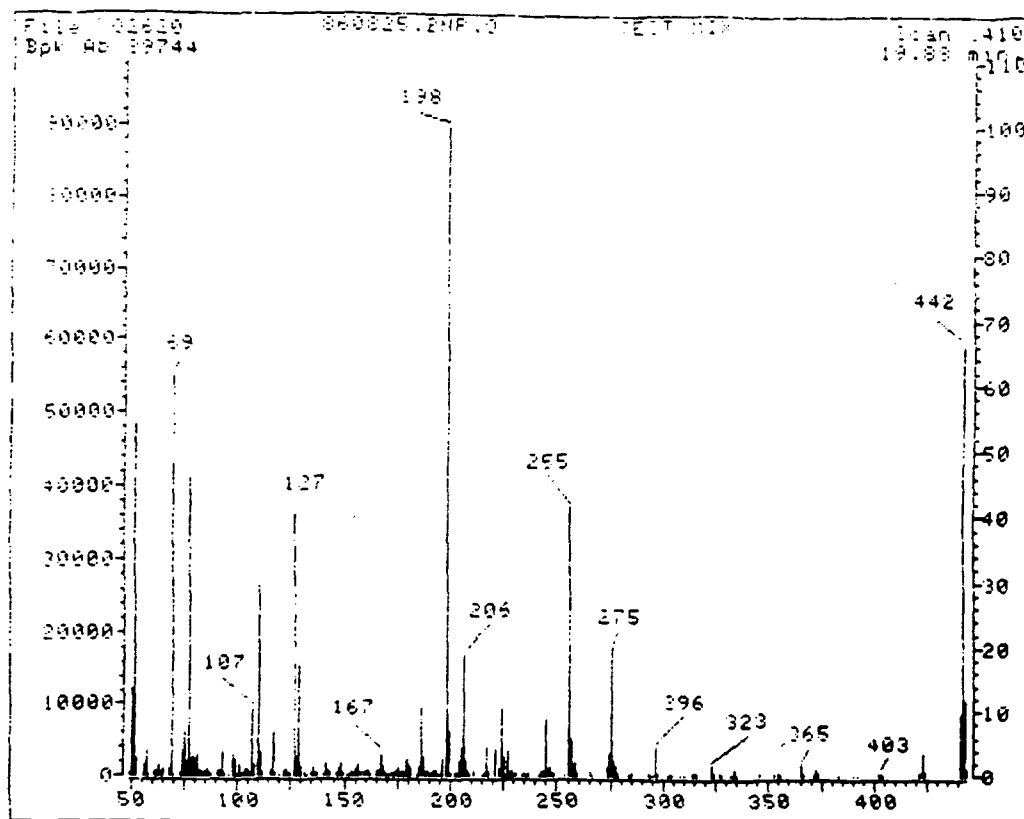


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
69	30-60% of mass 198	53.87	53.87	Ok
68	Less than 2% of mass 69	.89	1.45	Ok
69	(reference only)	61.49	61.49	Ok
70	Less than 2% of mass 69	.20	.33	Ok
127	40-60% of mass 198	40.35	40.35	Ok
197	Less than 1% of mass 198	0.00	0.00	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.79	6.79	Ok
275	10-30% of mass 198	19.84	19.84	Ok
365	Greater than 1% of mass 198	1.89	1.89	Ok
441	0-100% of mass 443	9.74	82.81	Ok
442	Greater than 40% of mass 198	66.19	66.19	Ok
443	17-23% of mass 442	11.76	17.76	Ok

Injection Date: 08/25/86

Injection Time: 16:54

Run No: 002620

Spectrum No: 1410

Analyst: L. G. 10

Processor: MSBANK

QC Batch: QR5465

Samples: M9370, M9371, M9383, N1319, N1314, N1310, N1309, N1323, N1322

AUG 28, 1986  
QB5465

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

M9382 RESOURCE ENGINEERING

RES27511

XRE11148-50 860804 2052

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concn Added ug/kg	% Recov	Unspiked Sample ug/kg	Concn Added ug/kg	% Recov
1B	Acenaphthene	ND	63	ND	ND	ND	0	-	ND	3390	89
2B	Acenaphthylene	ND	120	ND	ND	ND	0	-	ND	3390	95
3B	Anthracene	ND	63	ND	ND	ND	0	-	ND	3390	85
4B	Benzidine	ND	1500	ND	ND	ND	0	-	ND	3390	22
5B	Benzo(a)anthracene	ND	260	ND	ND	ND	0	-	ND	3390	82
6B	Benzo(a)pyrene	ND	83	ND	ND	ND	0	-	ND	3390	113
7B	Benzo(b)fluoranthene	ND	330	ND	ND	ND	0	-	ND	3390	109
8B	Benzo(ghi)perylene	ND	140	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	120	ND	ND	ND	0	-	ND	3390	96
10B	bis(2-Chloroethoxy)methane	ND	180	ND	ND	ND	0	-	ND	3390	86
11B	bis(2-Chloroethyl) ether	ND	190	ND	ND	ND	0	-	ND	3390	76
12B	bis(2-Chloroisopropyl)ether	ND	190	ND	ND	ND	0	-	ND	3390	126
13B	bis(2-Ethylhexyl)phthalate	ND	330	ND	ND	BMDL	0	-	ND	3390	98
14B	4-Bromophenyl phenyl ether	ND	63	ND	ND	ND	0	-	ND	3390	66
15B	Butyl benzyl phthalate	ND	330	ND	ND	ND	0	-	ND	3390	90
16B	2-Chloronaphthalene	ND	63	ND	ND	ND	0	-	ND	3390	91
17B	4-Chlorophenyl phenyl ether	ND	140	ND	ND	ND	0	-	ND	3390	87
18B	Chrysene	ND	83	ND	ND	ND	0	-	ND	3390	87
19B	Dibenzo(a,h)anthracene	ND	330	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3390	82
21B	1,3-Dichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3390	81
22B	1,4-Dichlorobenzene	ND	150	ND	ND	ND	0	-	ND	3390	80
23B	3,3'-Dichlorobenzidine	ND	550	ND	ND	ND	0	-	ND	3390	33
24B	Diethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3390	87
25B	Dimethyl phthalate	ND	330	ND	ND	ND	0	-	ND	3390	89
26B	Di-n-butyl phthalate	666	330	ND	96.1	394	0	-	ND	3390	144
27B	2,4-Dinitrotoluene	ND	190	ND	ND	ND	0	-	ND	3390	100
28B	2,6-Dinitrotoluene	ND	63	ND	ND	ND	0	-	ND	3390	83
29B	Di-n-octyl phthalate	ND	330	ND	ND	ND	0	-	ND	3390	108
30B	1,2-Diphenylhydrazine	ND	330	ND	ND	ND	0	-	ND	3390	90
31B	Fluoranthene	ND	73	ND	ND	ND	0	-	ND	3390	88
32B	Fluorene	ND	63	ND	ND	ND	0	-	ND	3390	88

AUG 28, 1986  
QB5465

## TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

## Chain of Custody Data Required for ETC Data Management Summary Reports

M9382 RESOURCE ENGINEERING

RES27511

XREI1148-50 860804 2052

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
33B	Hexachlorobenzene	ND	63	ND	ND	ND	0	-	ND	3390	84
34B	Hexachlorobutadiene	ND	30	ND	ND	ND	0	-	ND	3390	104
35B	Hexachlorocyclopentadiene	ND	330	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	53	ND	ND	ND	0	-	ND	3390	109
37B	Indeno(1,2,3-c,d)pyrene	ND	160	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	73	ND	ND	ND	0	-	ND	3390	83
39B	Naphthalene	ND	53	ND	ND	ND	0	-	ND	3390	87
40B	Nitrobenzene	ND	63	ND	ND	ND	0	-	ND	3390	95
41B	N-Nitrosodimethylamine	ND	330	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	330	ND	ND	ND	0	-	ND	3390	96
43B	N-Nitrosodiphenylamine	ND	63	ND	ND	ND	0	-	ND	3390	114
44B	Phenanthrene	ND	180	ND	ND	ND	0	-	ND	3390	87
45B	Pyrene	ND	63	ND	ND	ND	0	-	ND	3390	78
46B	1,2,4-Trichlorobenzene	ND	63	ND	ND	ND	0	-	ND	3390	92

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

M9382	RESOURCE ENGINEERING	RES27511	XRE11148-50	86080	2052	1
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	70	23	120
2-Fluorobiphenyl	50	74	30	115
Terphenyl-D14	50	130	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits ** Advisory Limits Only				

\* IFB EPA Control Limits

.. Advisory Limits Only

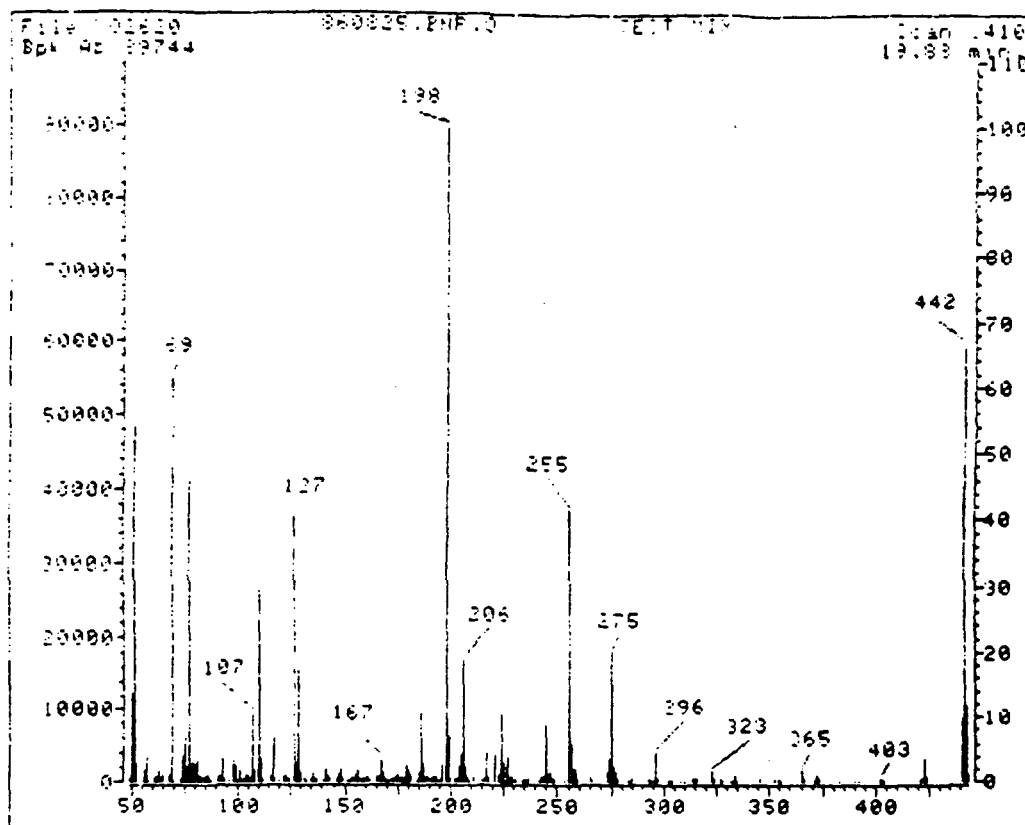


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
69	30-60% of mass 198	63.87	63.87	OK
68	Less than 1% of mass 69	.89	1.45	OK
69	(reference only)	61.49	61.49	OK
70	Less than 2% of mass 69	.20	.33	OK
127	40-60% of mass 198	40.35	40.35	OK
167	Less than 1% of mass 198	0.00	0.00	OK
198	Base peak, 100% relative abundance	100.00	100.00	OK
199	5-9% of mass 198	6.79	6.79	OK
275	10-30% of mass 198	19.84	19.84	OK
365	Greater than 1% of mass 198	1.89	1.89	OK
441	0-100% of mass 443	9.74	82.81	OK
442	Greater than 40% of mass 198	66.19	66.19	OK
443	17-23% of mass 442	11.76	17.76	OK

Injection Date: 03/25/86

Injection Time: 16:54

Run No: 02620

Spectrum No: 1410

Analyst: *[Signature]*

Processor: *[Signature]*

QC Batch: *985465*

Samples: *M9370, M9371, M9383, N1319, N1310, N1309, N1323, N1322*



AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9383 RESOURCE ENGINEERING

RES27511

XREI1150-51 860804 1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov.	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov.
33B	Hexachlorobenzene	ND	72	ND	ND	ND	0	-	ND	3390	84
34B	Hexachlorobutadiene	ND	34	ND	ND	ND	0	-	ND	3390	104
35B	Hexachlorocyclopentadiene	ND	380	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	60	ND	ND	ND	0	-	ND	3390	109
37B	Indeno(1,2,3-c,d)pyrene	ND	180	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	83	ND	ND	ND	0	-	ND	3390	83
39B	Naphthalene	ND	60	ND	ND	ND	0	-	ND	3390	87
40B	Nitrobenzene	ND	72	ND	ND	ND	0	-	ND	3390	95
41B	N-Nitrosodimethylamine	ND	380	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	380	ND	ND	ND	0	-	ND	3390	96
43B	N-Nitrosodiphenylamine	ND	72	ND	ND	ND	0	-	ND	3390	114
44B	Phenanthrene	ND	200	ND	ND	ND	0	-	ND	3390	87
45B	Pyrene	ND	72	ND	ND	ND	0	-	ND	3390	78
46B	1,2,4-Trichlorobenzene	ND	72	ND	ND	ND	0	-	ND	3390	92

A Recovery manually verified.

AUG 29, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

M9383

RESOURCE ENGINEERING

RES27511

XREI1150-51 860804 1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/kg	MDL ug/kg	First ug/kg	Second ug/kg	Blank Data ug/kg	Concen. Added ug/kg	% Recov	Unspiked Sample ug/kg	Concen. Added ug/kg	% Recov
1B	Acenaphthene	ND	72	ND	ND	ND	0	-	ND	3390	89
2B	Acenaphthylene	ND	130	ND	ND	ND	0	-	ND	3390	95
3B	Anthracene	ND	72	ND	ND	ND	0	-	ND	3390	85
4B	Benizidine	ND	1700	ND	ND	ND	0	-	ND	3390	22
5B	Benzo(a)anthracene	ND	290	ND	ND	ND	0	-	ND	3390	82
6B	Benzo(a)pyrene	ND	94	ND	ND	ND	0	-	ND	3390	113
7B	Benzo(b)fluoranthene	ND	380	ND	ND	ND	0	-	ND	3390	109
8B	Benzo(ghi)perylene	ND	150	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	130	ND	ND	ND	0	-	ND	3390	96
10B	bis(2-Chloroethoxy)methane	ND	200	ND	ND	ND	0	-	ND	3390	86
11B	bis(2-Chloroethyl) ether	ND	210	ND	ND	ND	0	-	ND	3390	76
12B	bis(2-Chloroisopropyl)ether	ND	210	ND	ND	ND	0	-	ND	3390	126
13B	bis(2-Ethylhexyl)phthalate	ND	380	ND	ND	278	0	-	ND	3390	98
14B	4-Bromophenyl phenyl ether	ND	72	ND	ND	ND	0	-	ND	3390	66
15B	Butyl benzyl phthalate	ND	380	ND	ND	ND	0	-	ND	3390	90
16B	2-Chloronaphthalene	ND	72	ND	ND	ND	0	-	ND	3390	91
17B	4-Chlorophenyl phenyl ether	ND	160	ND	ND	ND	0	-	ND	3390	87
18B	Chrysene	ND	94	ND	ND	ND	0	-	ND	3390	87
19B	Dibenzo(a,h)anthracene	ND	380	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	72	ND	ND	ND	0	-	ND	3390	82
21B	1,3-Dichlorobenzene	ND	72	ND	ND	ND	0	-	ND	3390	81
22B	1,4-Dichlorobenzene	ND	170	ND	ND	ND	0	-	ND	3390	80
23B	3,3'-Dichlorobenzidine	ND	620	ND	ND	ND	0	-	ND	3390	33
24B	Diethyl phthalate	ND	380	ND	ND	ND	0	-	ND	3390	87
25B	Dimethyl phthalate	ND	380	ND	ND	ND	0	-	ND	3390	89
26B	Di-n-butyl phthalate	1540	380	ND	96.1	394	0	-	ND	3390	144
27B	2,4-Dinitrotoluene	ND	210	ND	ND	ND	0	-	ND	3390	100
28B	2,6-Dinitrotoluene	ND	72	ND	ND	ND	0	-	ND	3390	83
29B	Di-n-octyl phthalate	ND	380	ND	ND	ND	0	-	ND	3390	108
30B	1,2-Diphenylhydrazine	ND	380	ND	ND	ND	0	-	ND	3390	90
31B	Fluoranthene	ND	83	ND	ND	ND	0	-	ND	3390	88
32B	Fluorene	ND	72	ND	ND	ND	0	-	ND	3390	88

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Solid Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports					
M9383	RESOURCE ENGINEERING	RES27511	XRE11150-51	86080	1 0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	-	-	81	117
p-Bromofluorobenzene	-	-	74	121
1,2-Dichloroethane-D4	-	-	70	121
ACID FRACTION (GC/MS)				
Phenol-D5	-	-	24	113
2-Fluorophenol	-	-	25	121
2,4,6-Tribromophenol	-	-	19	122
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	77	23	120
2-Fluorobiphenyl	50	70	30	115
Terphenyl-D14	50	116	18	137
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	20..	150..
* IFB EPA Control Limits ** Advisory Limits Only				

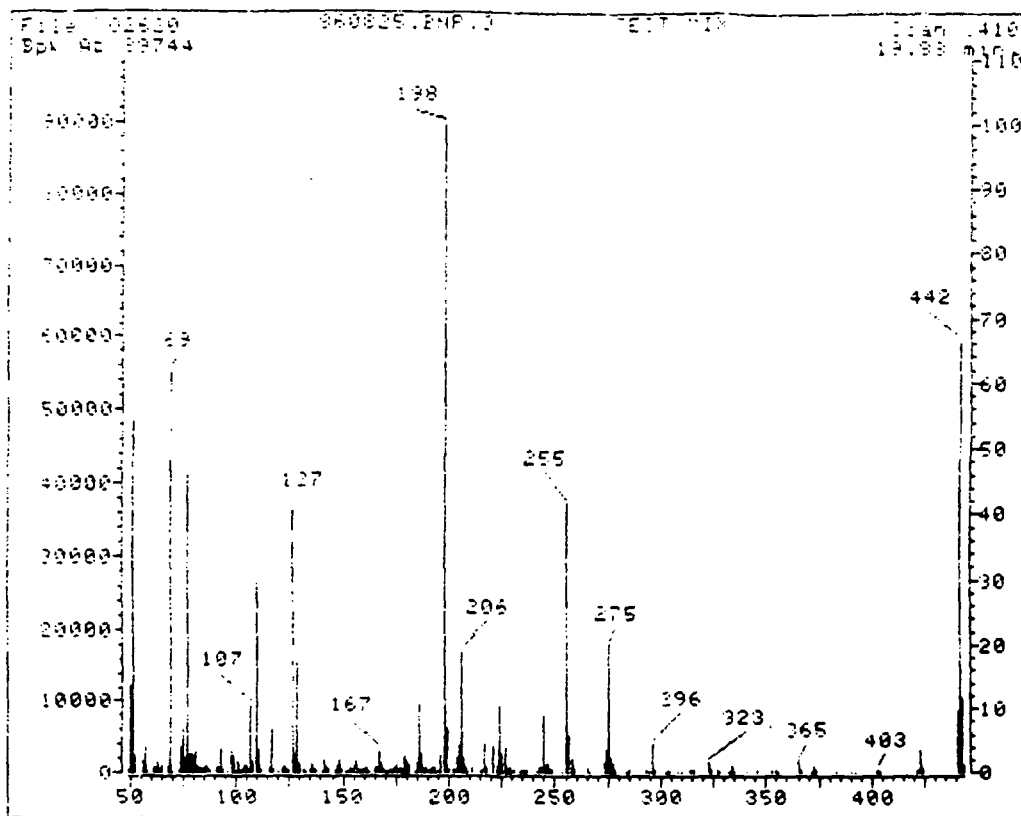


TABLE 2: METHOD PERFORMANCE DATA (QR23)

GC/MS Tuning Data - Decafluorotriphenylphosphine (DFTPP) for Base/Neutral Analysis

m/z	Ion Abundance Criteria	% Relative Abundance Base Peak	% Relative Abundance Appropriate Peak	Status
61	30-60% of mass 198	53.87	53.87	Ok
68	Less than 2% of mass 69	.89	1.45	Ok
69	(reference only)	61.49	61.49	Ok
76	Less than 2% of mass 69	.20	.33	Ok
127	40-60% of mass 198	40.35	40.35	Ok
197	Less than 1% of mass 198	0.00	0.00	Ok
198	Base peak, 100% relative abundance	100.00	100.00	Ok
199	5-9% of mass 198	6.79	6.79	Ok
275	10-30% of mass 198	19.84	19.84	Ok
365	Greater than 1% of mass 198	1.89	1.89	Ok
441	0-100% of mass 443	9.74	82.81	Ok
442	Greater than 40% of mass 198	66.19	66.19	Ok
443	17-23% of mass 442	11.76	17.76	Ok

Injection Date: 05/25/86

Injection Time: 16:54

Run No: 002620

Spectrum No: 1410

Analyst: J. L. 48

Processor: McConkko

QC Batch: Q85465

Samples: M9370, M9371, M9383, N1319, N1310, N1309, N1323, N1322

Appendix 7

Contaminated Soil Volume Calculations

## APPENDIX 7

### CONTAMINATED SOIL VOLUME CALCULATIONS

#### Dimensions:

Lagoon bottom area = 7.5 acres  
Sidewall length = 3300 feet  
Sidewall depth = 28 feet

#### Case 1: Contaminant Concentration level 1 ppm

##### Basis:

- Contamination extends beneath sludge/soil interface a distance of 16 feet.
- Three areas of the existing dike are identified as containing more than 1 ppm PNA's

##### Volumes:

Bottom:	7.5 acres x 43560 ft <sup>2</sup> /acre x 16 ft	= 193,600 yd <sup>3</sup>
Sides:	3300 ft x 28 ft x 16 ft	= 54,755
Dikes:	75 ft x 75 ft x 10 ft	= 2,083
	50 ft x 50 ft x 25 ft	= 2,315
	300 ft x 50 ft x 25 ft	= 13,888
		<u>266,641 yd<sup>3</sup></u>
	call	<u>267,000 yd<sup>3</sup></u>

#### Case 2: Contaminant Concentration level 10 ppm

##### Basis:

- Contamination extends beneath sludge/soil interface a distance of 3 feet
- Two areas of the existing dike are identified as containing more than 10 ppm PNA's

Bottom:	7.5 acres x 43560 ft <sup>2</sup> /acre x 3 ft	= 36,300 yd <sup>3</sup>
Sides:	3300 ft x 28 ft x 3.0 ft	= 10,267
Dikes:	75 ft x 75 ft x 10 ft	= 2,083
	50 ft x 50 ft x 25 ft	= 2,315
		<u>50,965</u>
	call	<u>51,000 yd<sup>3</sup></u>

Case 3: Contaminant Concentration of 100 ppm

Basis:

- Contamination extends beneath sludge/soil interface a distance of 2 feet
- Two areas of the existing dike are identified as containing more than 100 ppm PNA's

Bottom:	7.5 acres x 43560 ft <sup>2</sup> /acre x 2 ft	=	24,200 yd <sup>3</sup>
Sides:	3300 ft x 28 ft x 2 ft	=	6,844
Dikes:	75 ft x 75 ft x 10 ft	=	2,083
	50 ft x 50 ft x 25 ft	=	2,315
			<u>35,442</u>
		call	<u>35,400 yd<sup>3</sup></u>

Case 4: Contaminant Concentration to 1000 ppm

Basis:

- Contamination extends beneath sludge/soil interface a distance of 1.5 feet
- One area of the existing dike is identified as containing more than 1000 ppm PNA's

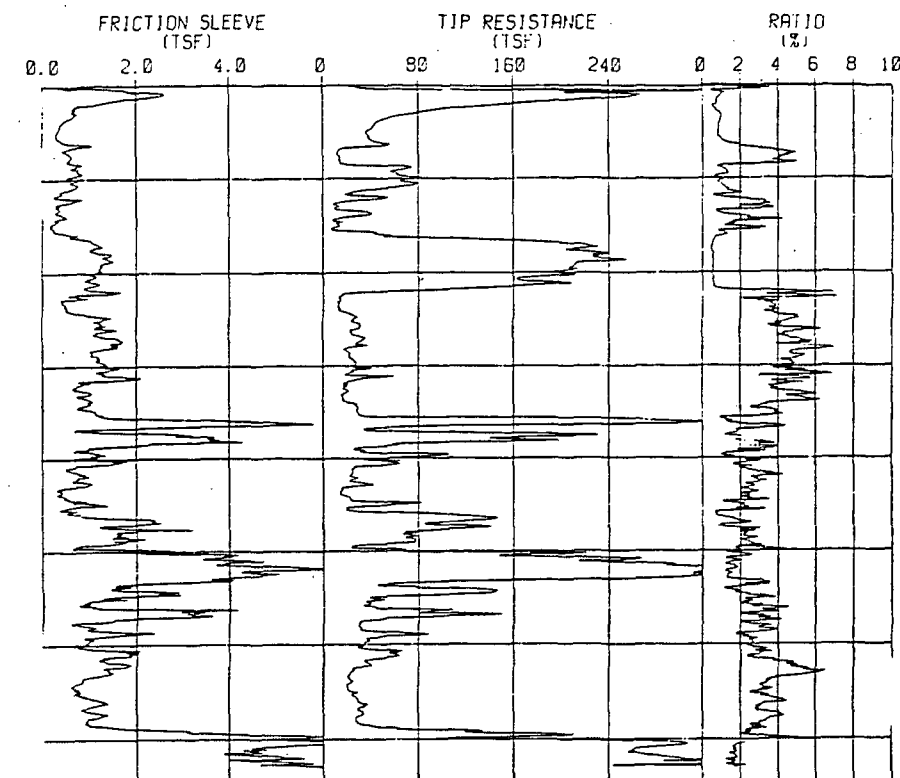
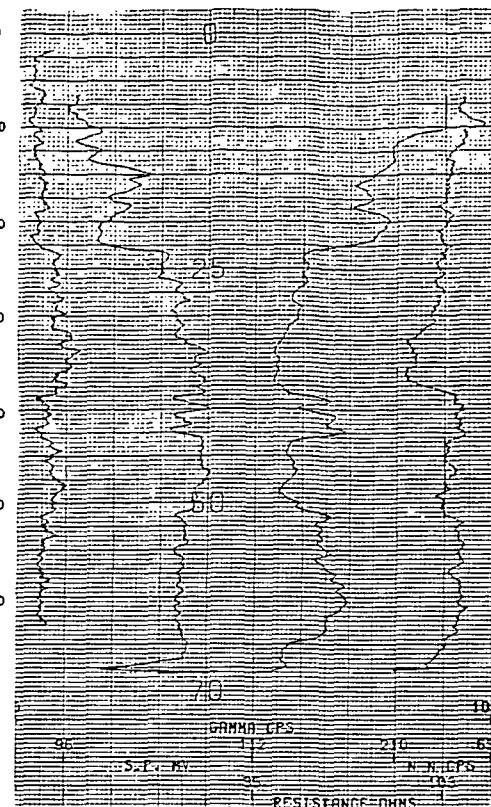
Bottom:	7.5 acres x 43560 ft <sup>2</sup> /acre x 1.5 ft	=	18,150 yd <sup>3</sup>
Sides:	3300 ft x 28 ft x 1.5 ft	=	5,133
Dikes:	75 ft x 75 ft x 10 ft	=	2,083
			<u>25,366</u>
		call	<u>25,500 yd<sup>3</sup></u>

Appendix 8

Alluvial Remnant Assessment Comparison  
of Logging Technique



CPT-10

R-1  
E-LOGR-1 (22' E CPT-10)  
CONTINUOUSLY SAMPLED BORING

SURFACE FILL, gravels and clay

VERY SANDY CLAY, tan and orange

SAND, tan, fine to medium grained, angular, wet

SILTY SAND, tan, very fine grained, wet

CLAYEY SAND, orange and tan, wet

VERY SANDY CLAY, gray

SILTY CLAY, gray

CLAYEY SILT, red, black pinpoint staining, white calcareous nodules

SILTY CLAY, red and blue with calcareous nodules

decreasing silt with depth

VERY CLAYEY SAND, gray and tan, very fine grained, wet

SILTY SAND, gray

CLAYEY SILT, gray and orange

SILTY CLAY, bluish gray

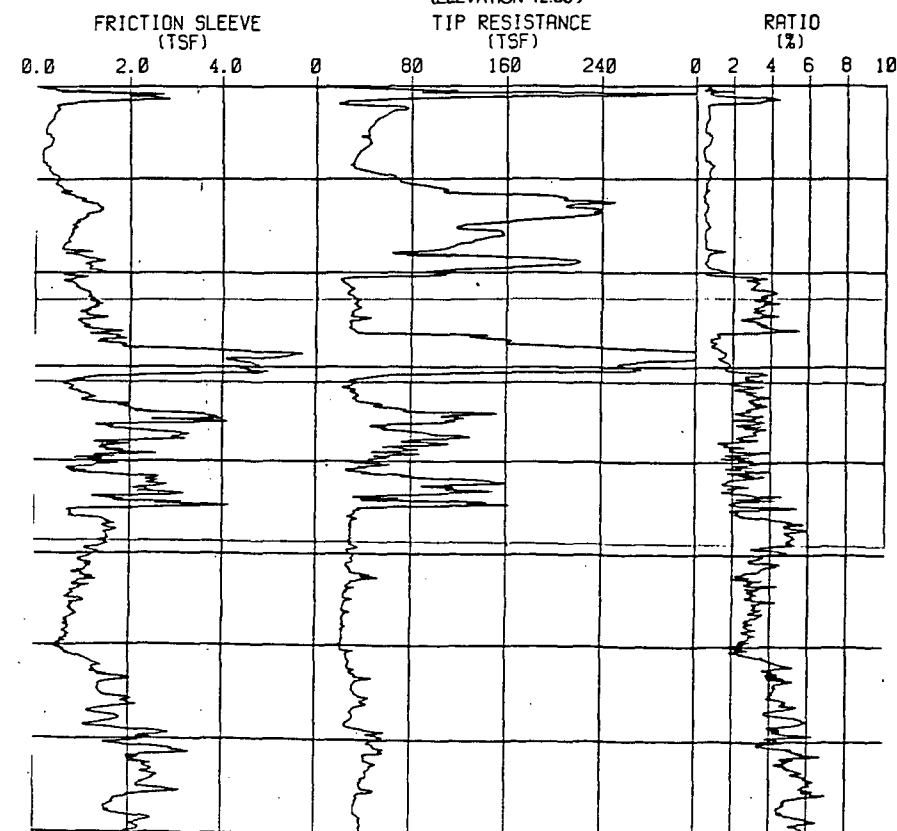
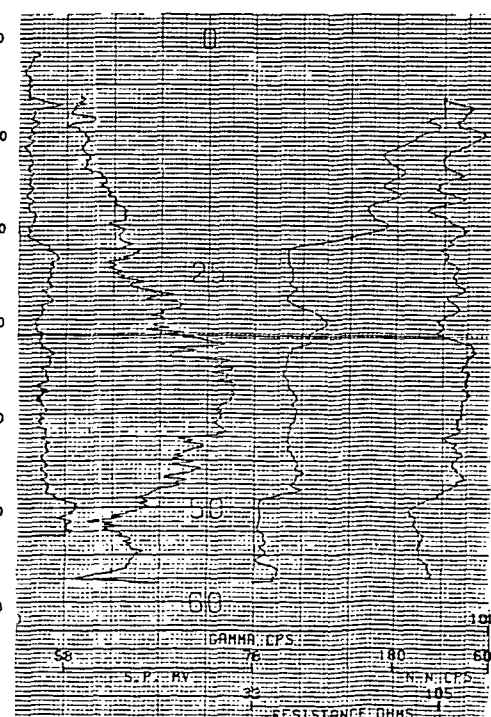
CLAYEY SAND, gray, wet

SILTY SAND, gray, damp

CLAYEY SAND, gray

SANDY SILT, gray

SILTY CLAY, green and brown, with gray silt lenses, calcareous nodules, very stiff

CPT-2  
(ELEVATION 12.66')  
TIP RESISTANCE (TSF)R-2  
E-LOGR-2 (3' E CPT-2)  
CONTINUOUSLY SAMPLED BORING

ROADFILL, black, asphalt, sandy clay

SLIGHTLY SILTY SAND, tan, medium grained, wet

SAND, tan, fine to medium grained quartz, angular to subrounded, some multicolored gravels, wet to saturated

SILTY SAND, brown, very fine grained

SLIGHTLY CLAYEY SAND, grayish white, some Fe staining

VERY SILTY CLAY, bluish gray with orange mottles

VERY CLAYEY SAND, blue and red

SLIGHTLY SANDY CLAY, rose and gold

VERY SILTY CLAY, gray with orange mottles

SILTY SAND, tan, wet

CLAYEY SAND, gray and orange, very fine grain, grain size increasing with depth, damp

SILTY SAND, tan, medium grain, wet

SILTY CLAY, red, some blue veining

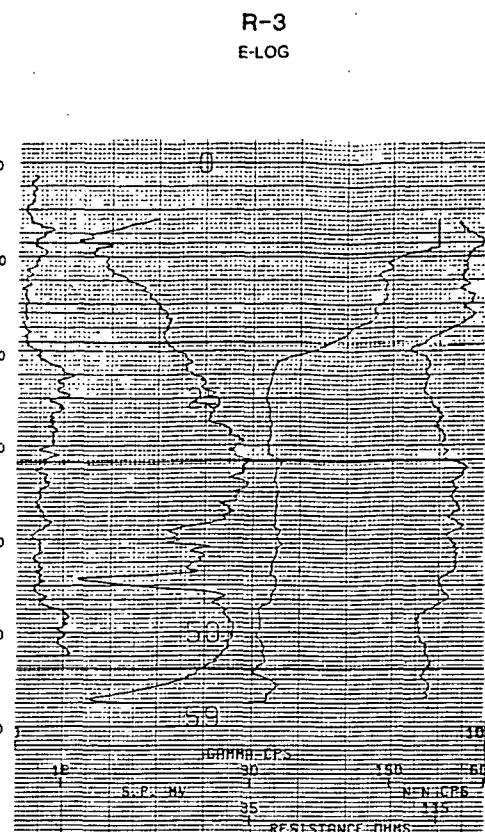
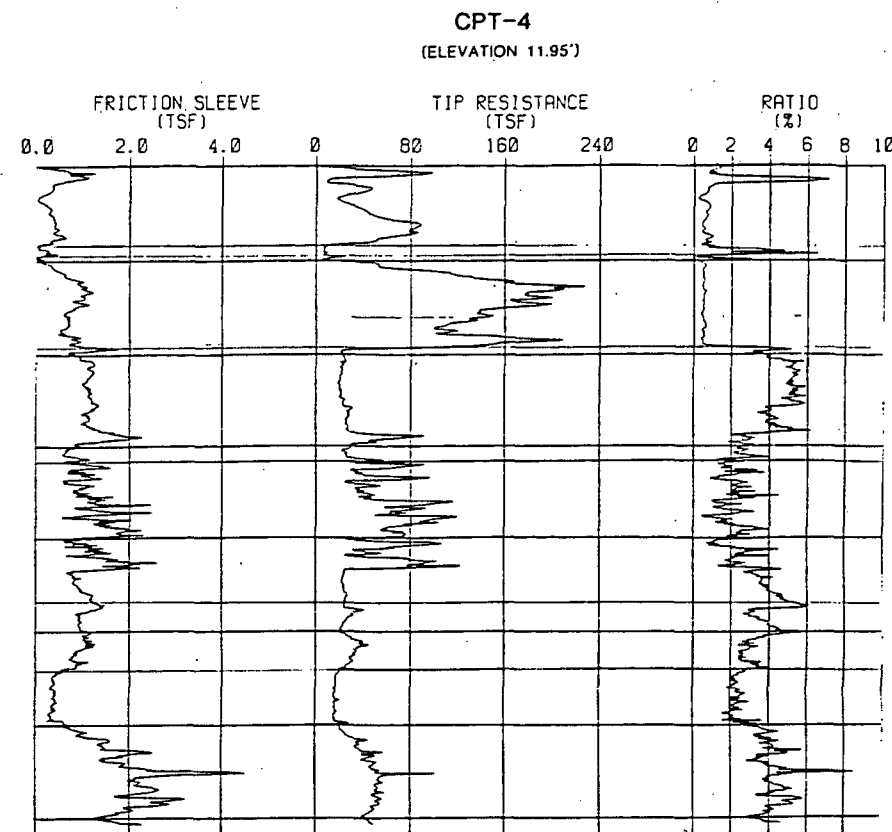
SILTY CLAY, brown and red, interbedded with silty sand, gray and gold, some calcareous nodules

CLAYEY SILT, dark brown, with layers of calcareous pebbles

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ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

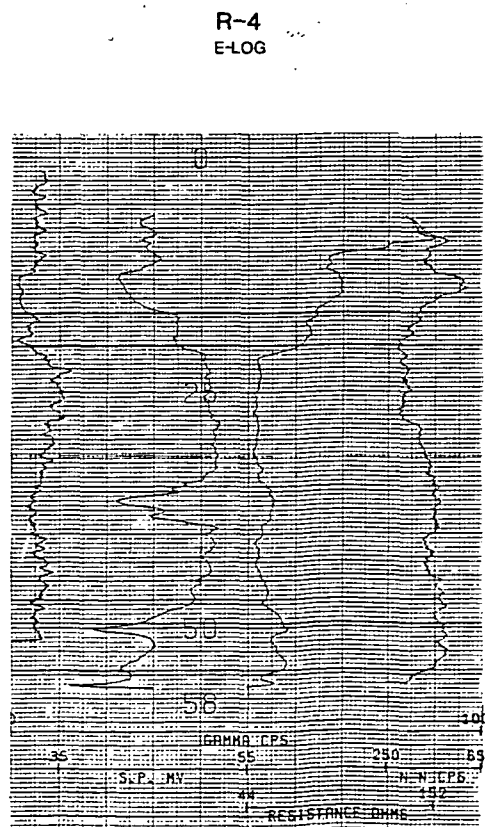
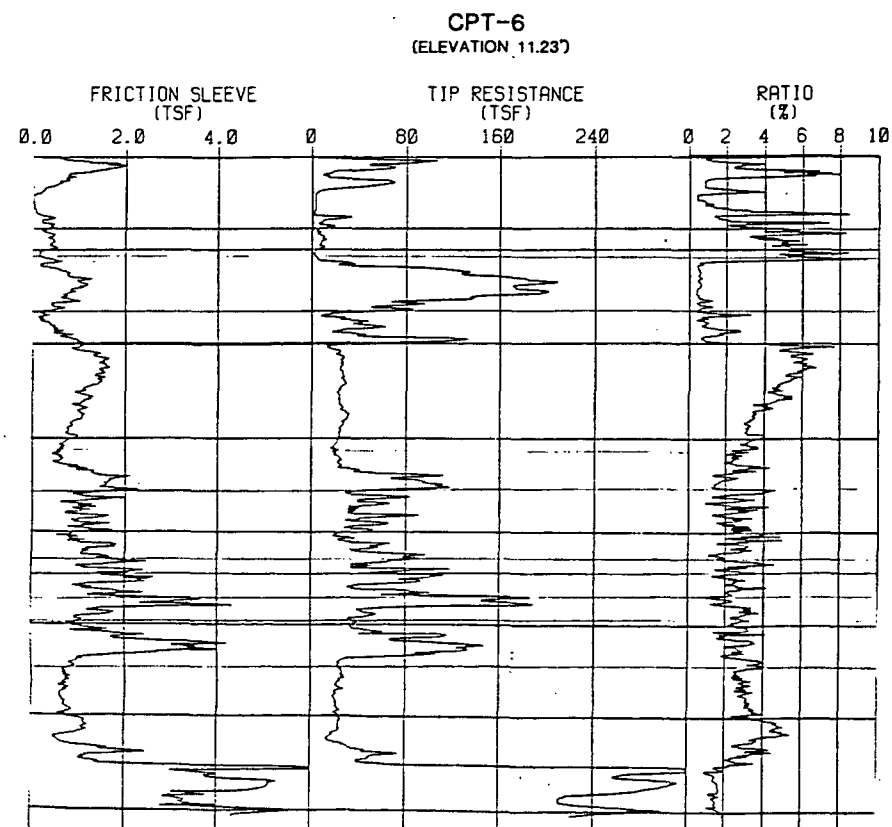
APPENDIX 8  
1986 F.I. ALLUVIAL REMNANT  
ASSESSMENT COMPARISON  
OF LOGGING TECHNIQUES  
FRENCH LIMITED

DRAWN BY: LCS DATE: 11-21-86 PROJECT NO.: 275-14  
CHK'D BY: SLB REVISED: DWG. NO.: 1



**R-3 (1'E CPT-4)**  
CONTINUOUSLY SAMPLED BORING

ROAD FILL, GRAVEL, SILTY SAND, black, glass and metal fragments
SILTY SAND, dark gray, medium grain, damp, color becoming brown
VERY SANDY CLAY, grayish green
SAND, white, fine to medium grained quartz, some multi-colored gravels
SILTY SAND, gray, fine grained, wet
SILTY CLAY, red with tan lenses, calcareous chips, black pinpoint staining, very stiff
increasing silt, gray and rose mottling color
VERY SANDY SILT, white
SANDY CLAY-CLAYEY SAND, gray, in alternating layers
thin layer of orange coarse sand
SILTY SAND, gray, rose, orange, wet, odor
VERY SILTY CLAY, gray, odor, color becoming red with depth
CLAYEY SILT, rose, drv
CLAY, brown, interbedded with gray and gold silt, calcareous pebbles
CLAYEY SILT, dark brown with gray silt lenses
SILTY CLAY, dark blue and brown, interbedded with gray silt



**R-4 (12.7' CPT-6)**  
CONTINUOUSLY SAMPLED BORING

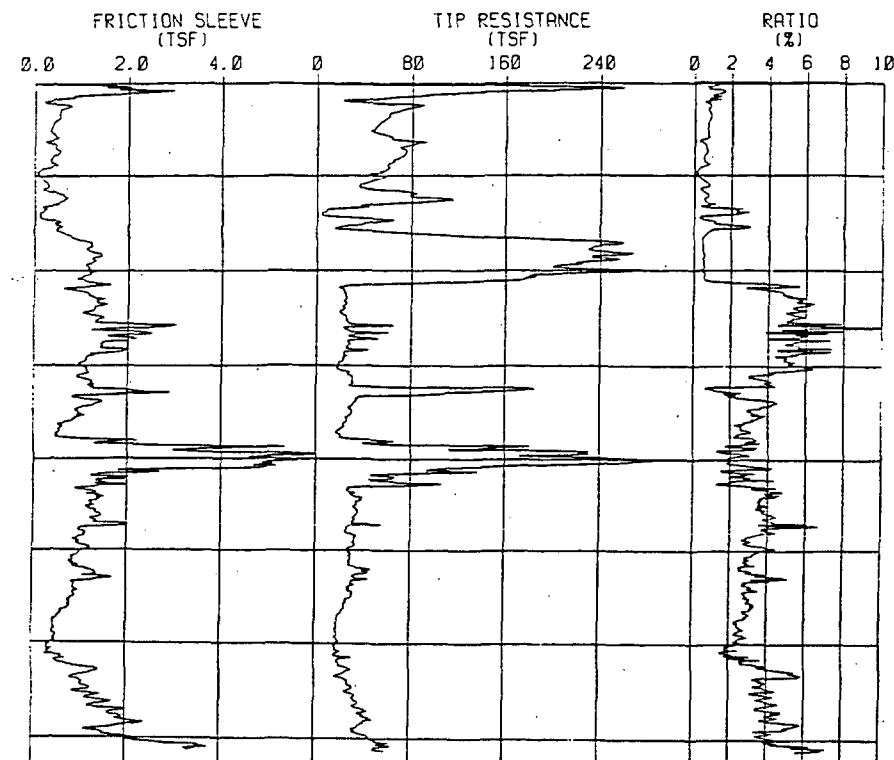
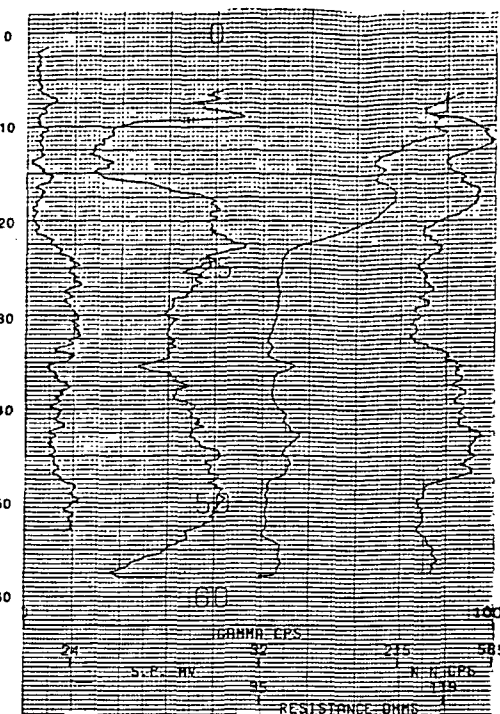
ASPHALT-ROAD FILL, black
SILTY CLAY, black, organic, ditch fill
SILTY SAND, black to dark gray, 30Z fines
SAND, dark gray to tan, quartz sand, medium to fine grained, multicolored grains, wet
SILTY SAND, gray with orange oxidized pockets, very fine grained, wet
CLAYEY SAND, medium gray, saturated, very fine grained
SILTY CLAY, red, very stiff, some calcareous nodules
Fe staining, blue veining
becoming gray in color
SLIGHTLY SANDY SILT, gray, compact
SILTY SAND, orange, damp, odor
color becoming gray
SANDY CLAY, gray, odor
SANDY SILT, gray, odor
SANDY CLAY, gray, odor, damp
SILTY SAND-SANDY SILT, pale gray, wet, odor
SILTY CLAY, brown and dark blue, interbedded with orange sand and gray silt
CLAYEY SILT, brown

**REI RESOURCE ENGINEERING**  
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

APPENDIX 8  
1986 F.I. ALLUVIAL REMNANT  
ASSESSMENT COMPARISON  
OF LOGGING TECHNIQUES  
FRENCH LIMITED

DRAWN BY: LCS	DATE: 11-21-86	PROJECT NO: 275-14
CHK'D BY: SLB	REVISED:	DWG. NO: 2

CPT-17

R-5  
E-LOGR-5 (.5 W CPT-17)  
CONTINUOUSLY SAMPLED BORING

ROAD FILL, Gravel, Asphalt, orange  
medium grained sand

CLAYEY SAND, pale gray

SAND, white, very fine grained

SILTY SAND, tan

SAND, solid, medium to coarse, some  
multicolored gravels

SILTY SAND, gray, medium grained,  
saturated, poor recovery

SILTY CLAY, red with blue veining, some  
calcareous pebbles, stiff to very  
stiff

SANDY CLAY, bluish gray, tan

CLAYEY SILT, red

SILTY CLAY, gray

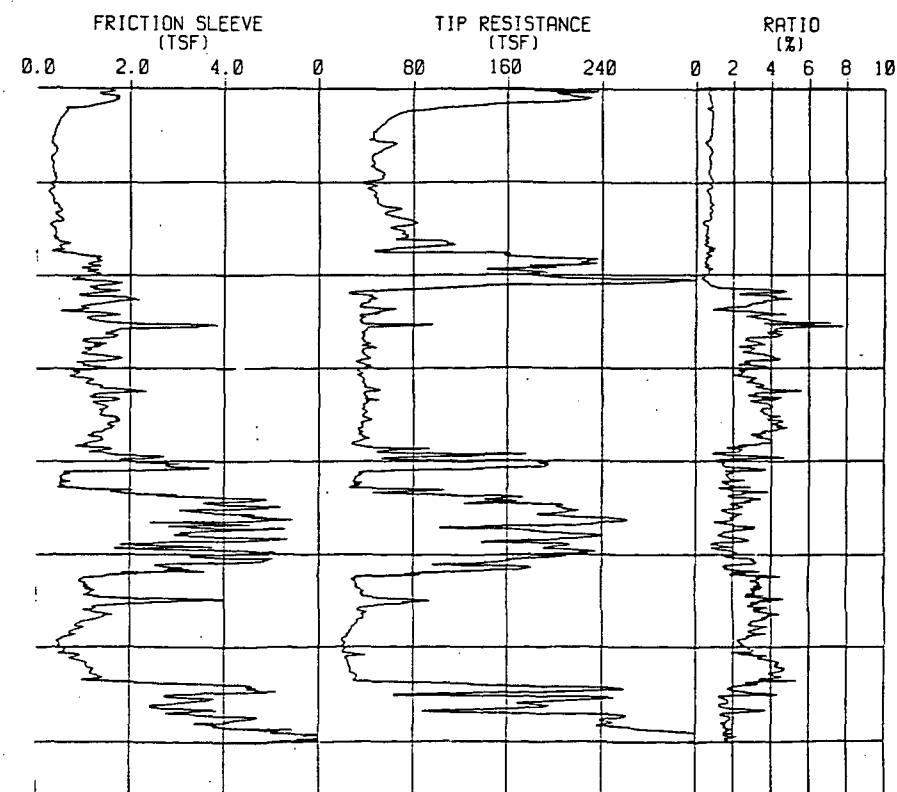
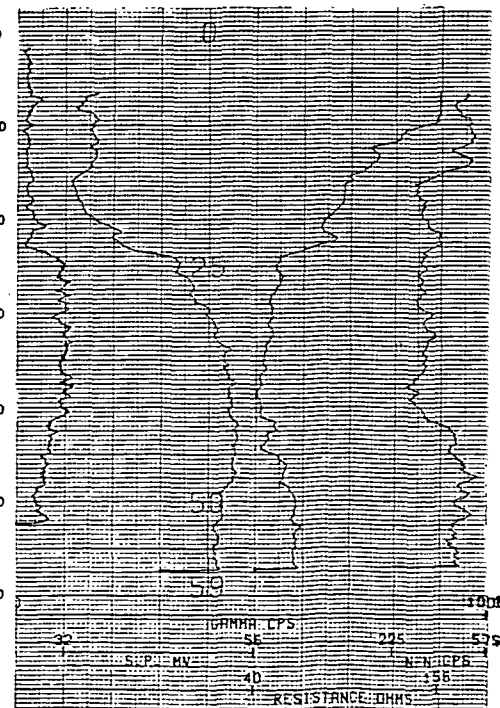
VERY CLAYEY SAND, gray

SILTY SAND, gray, very fine grained

SANDY CLAY, gray

CLAY, red and brown, interbedded with  
silt, blue and gold, some  
calcareous nodules

SILT, gray with dark brown clay

CPT-18  
(ELEVATION 14.81')R-6  
E-LOGR-6 (.5' E CPT-18)  
CONTINUOUSLY SAMPLED BORING

ROADFILL, sand and gravel

SILTY SAND, tan, fine grained, wet

SLIGHTLY CLAYEY SAND, white, fine grained saturated

SAND, white, medium to fine grain, angular to sub-  
rounded quarts, some multicolored gravels, wet

SAND, orange, lg-vlg some silt

SLIGHTLY SILTY SAND, white and gray fine, grained  
to very fine grained

CLAY, red, black pinpoints, calcareous nodules, stiff

sandy silt seam, red @ 27.4'

CLAYEY SILT, red and blue

some silty clay and sandy clay layers

SANDY CLAY, gray, damp

SANDY SILT, gray

CLAYEY SAND, gray and yellow, damp

CLAYEY SILT, red and gray

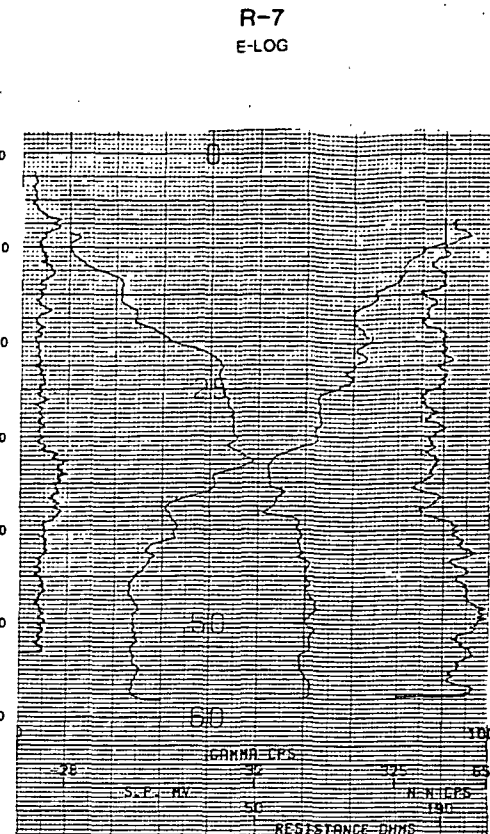
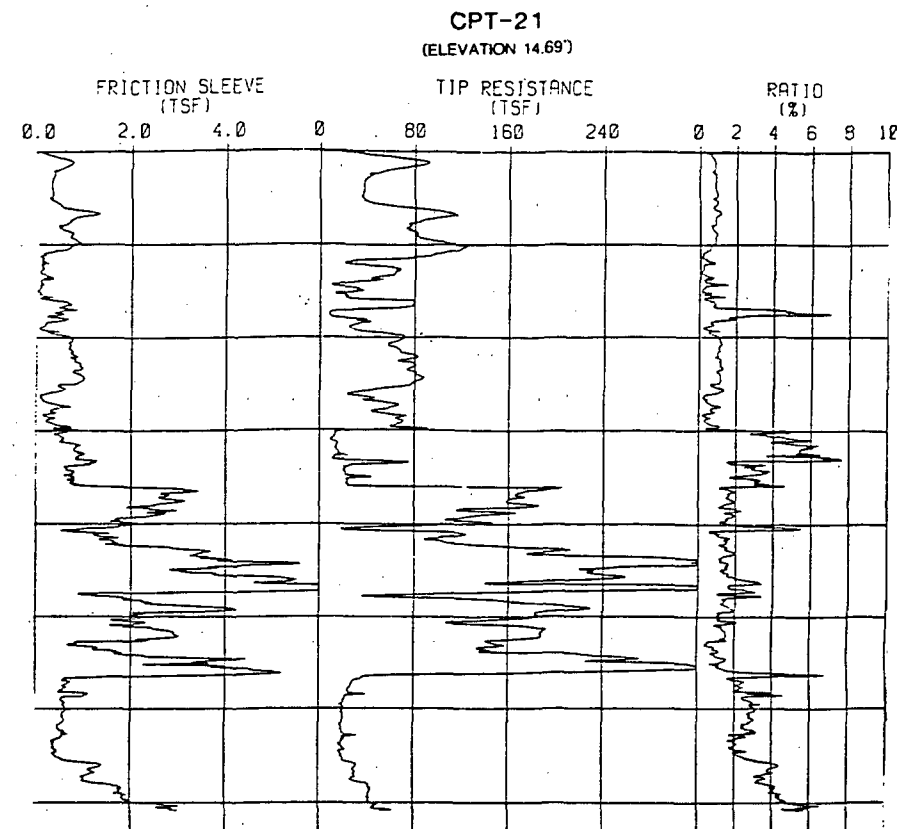
SANDY SILT, gray and yellow

SILTY CLAY, dark brown, interbedded with gray and  
yellow silt

**REI** RESOURCE ENGINEERING  
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

APPENDIX B  
1986 F.I. ALLUVIAL REMNANT  
ASSESSMENT COMPARISON  
OF LOGGING TECHNIQUES  
FRENCH LIMITED

DRAWN BY: LCS	DATE: 11-21-86	PROJECT NO: 275-14
CHK'D BY: SLB	REVISED:	DWG. NO.: 3



**R-7 (9' W CPT-21)**  
CONTINUOUSLY SAMPLED BORING

SAND AND GRAVELS, white and multicolored grains, subangular to subrounded, saturated

CLAYEY SAND, orange and gray, lg-vlk, odor

SILTY SAND, tan, subangular, wet

CLAYEY SAND SEAM, gray

SANDY SILT, gray

SILTY SAND, orange and tan, fine grained, saturated

SILTY CLAY, gray

SILTY SAND, gray, wet

CLAYEY SAND, gray, wet

SILTY CLAY, gray and orange, very stiff

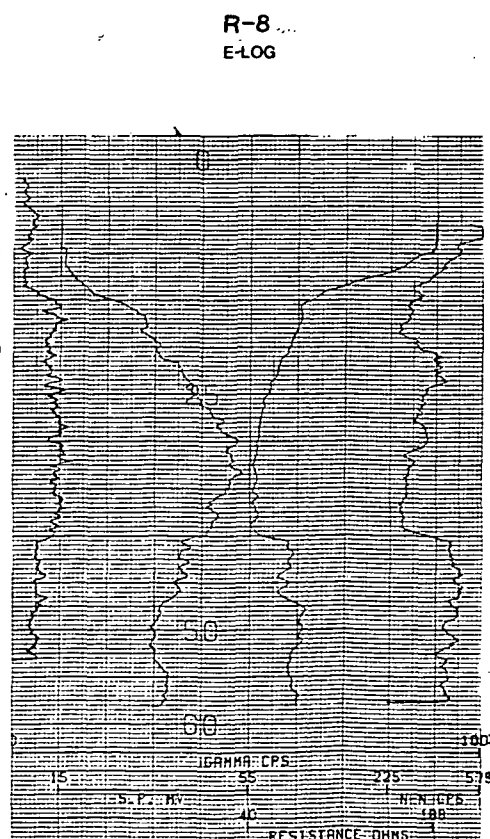
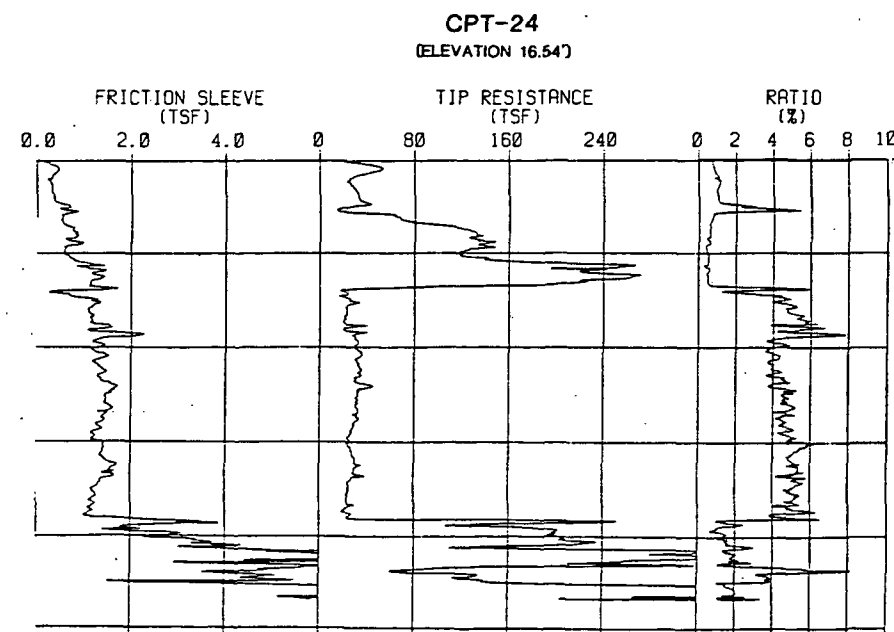
SANDY CLAY, bluish green

SILTY CLAY, bluish green with red veins

SILTY SAND, gray, Fe stains, saturated, very fine grain to fine grain

increasing grain size

CLAYEY SILT, tan



**R-8 (1' E CPT-24)**  
CONTINUOUSLY SAMPLED BORING

ASPHALT, roadfill, black

SAND, brown quartz, angular to subrounded, 10% fines

CLAYEY SAND, orange and tan, saturated

SILTY SAND, tan, some multicolored grains, fine grained, subrounded to rounded

SILTY CLAY, red and gray

CLAYEY SILT, rose and gray with layers of calcareous pebbles

CLAY, red, stiff, calcareous pebbles, gray veining

SANDY SILT, gray

SLIGHTLY CLAYEY SILT, gray, damp

SILTY SAND, gray, very fine grained sand, wet

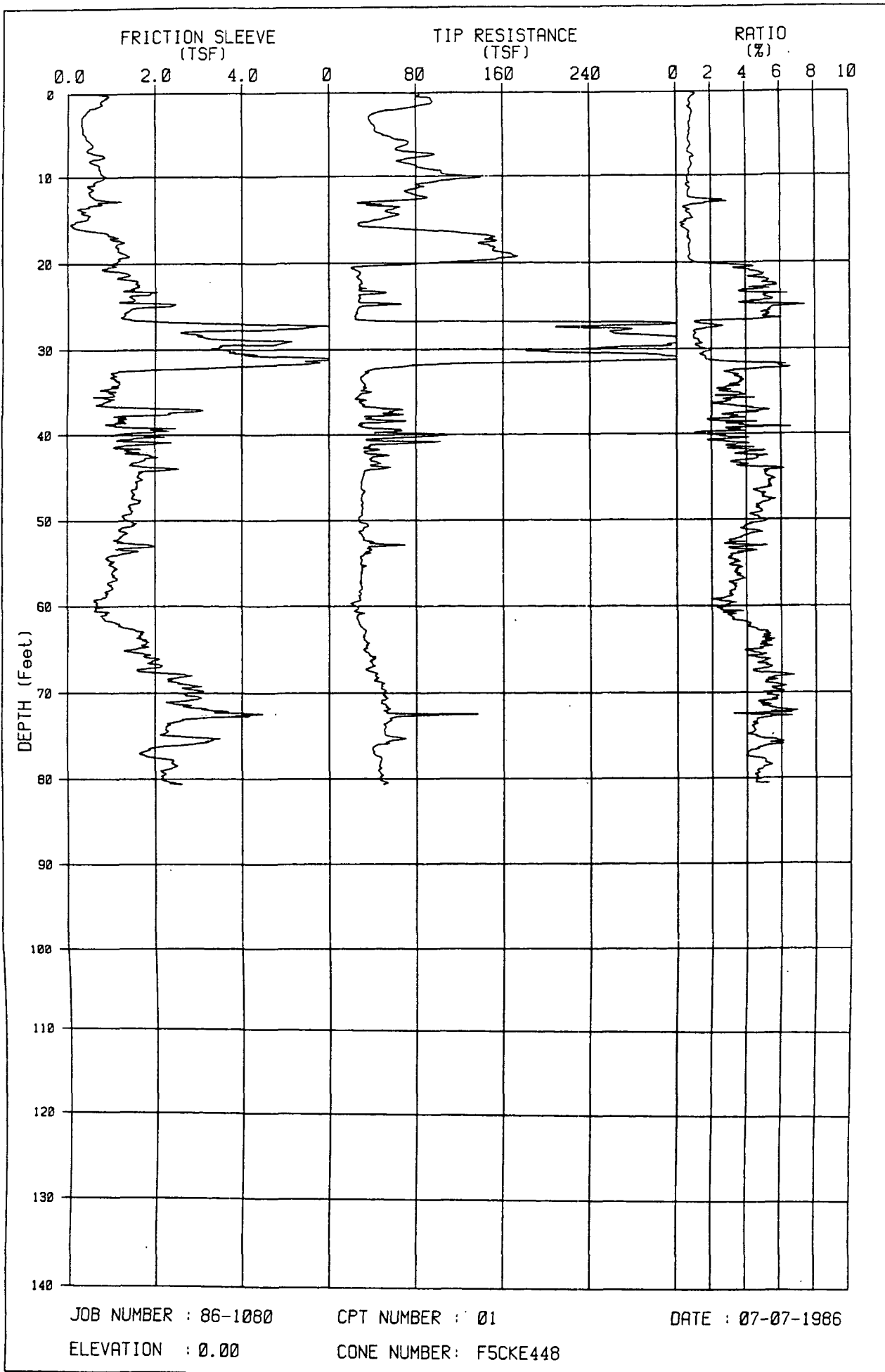
**REI RESOURCE ENGINEERING**  
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

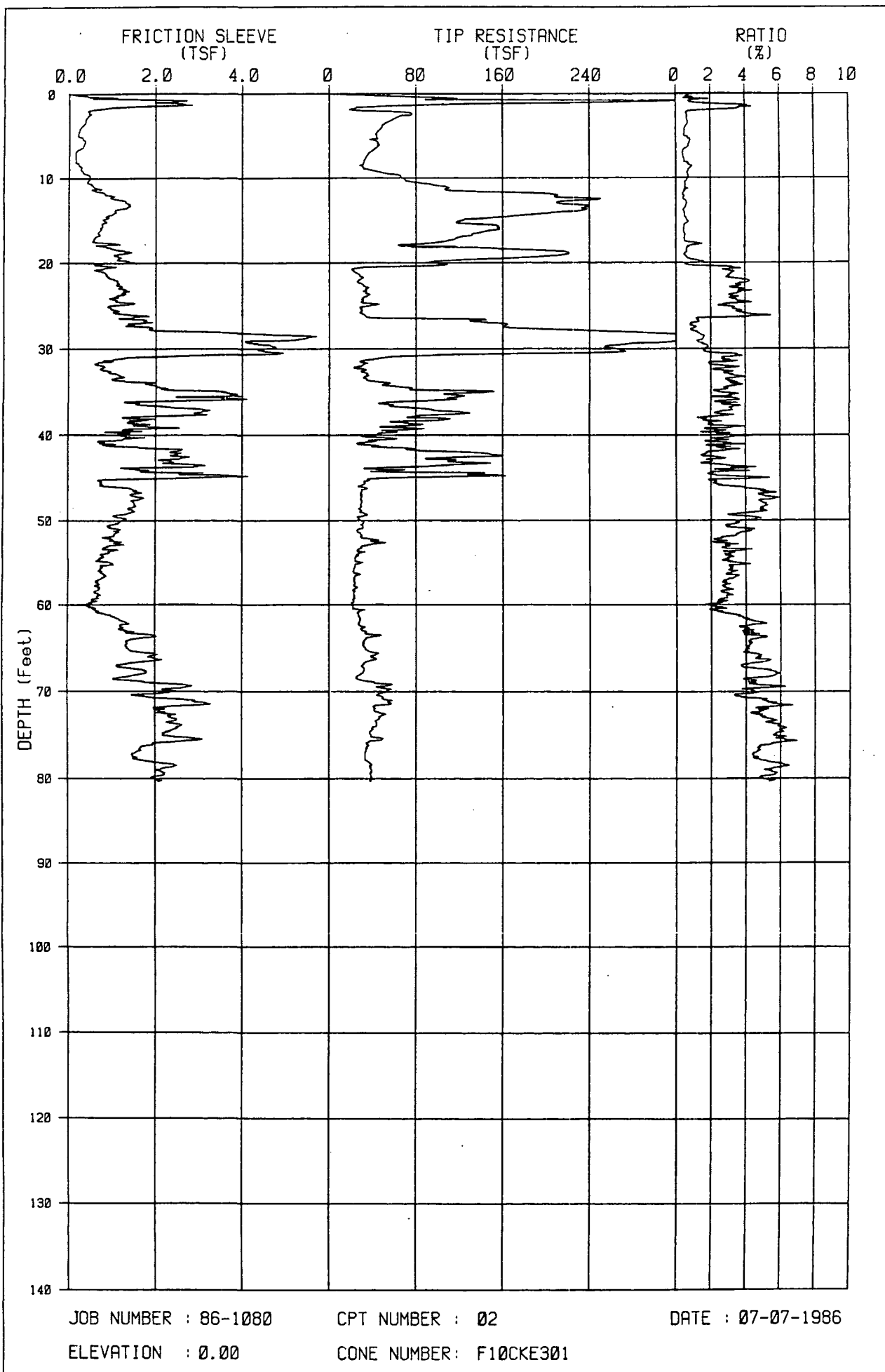
APPENDIX 8  
1986 F.I. ALLUVIAL REMNANT  
ASSESSMENT COMPARISON  
OF LOGGING TECHNIQUES  
FRENCH LIMITED

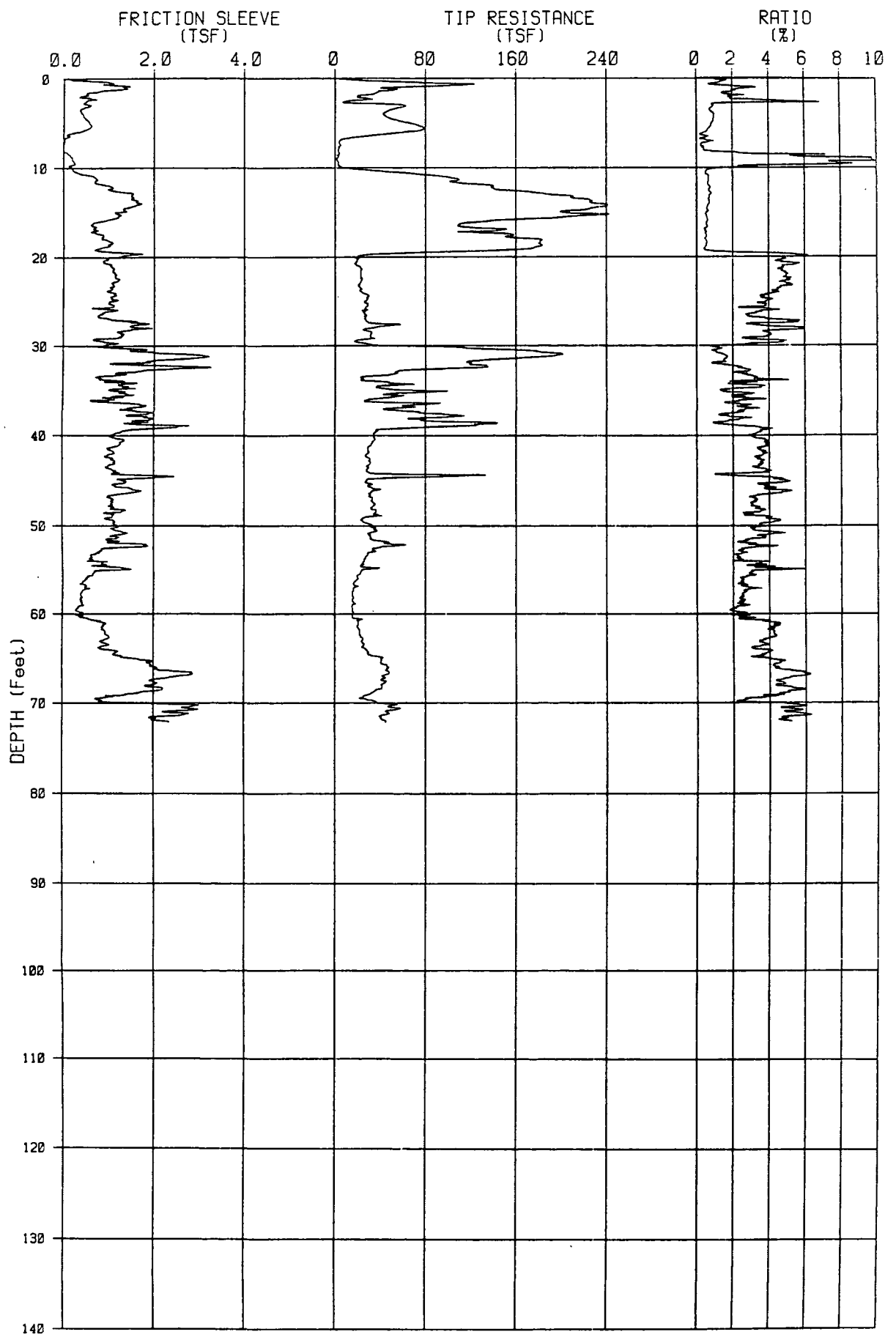
DRAWN BY: LCS	DATE: 11-21-86	PROJECT NO.: 275-14
CHK'D BY: SLB	REVISED:	DWG. NO.: 4

Appendix 9

Cone Penetrometer Sounding Logs (CPT 1  
through 28)







JOB NUMBER : 86-1080

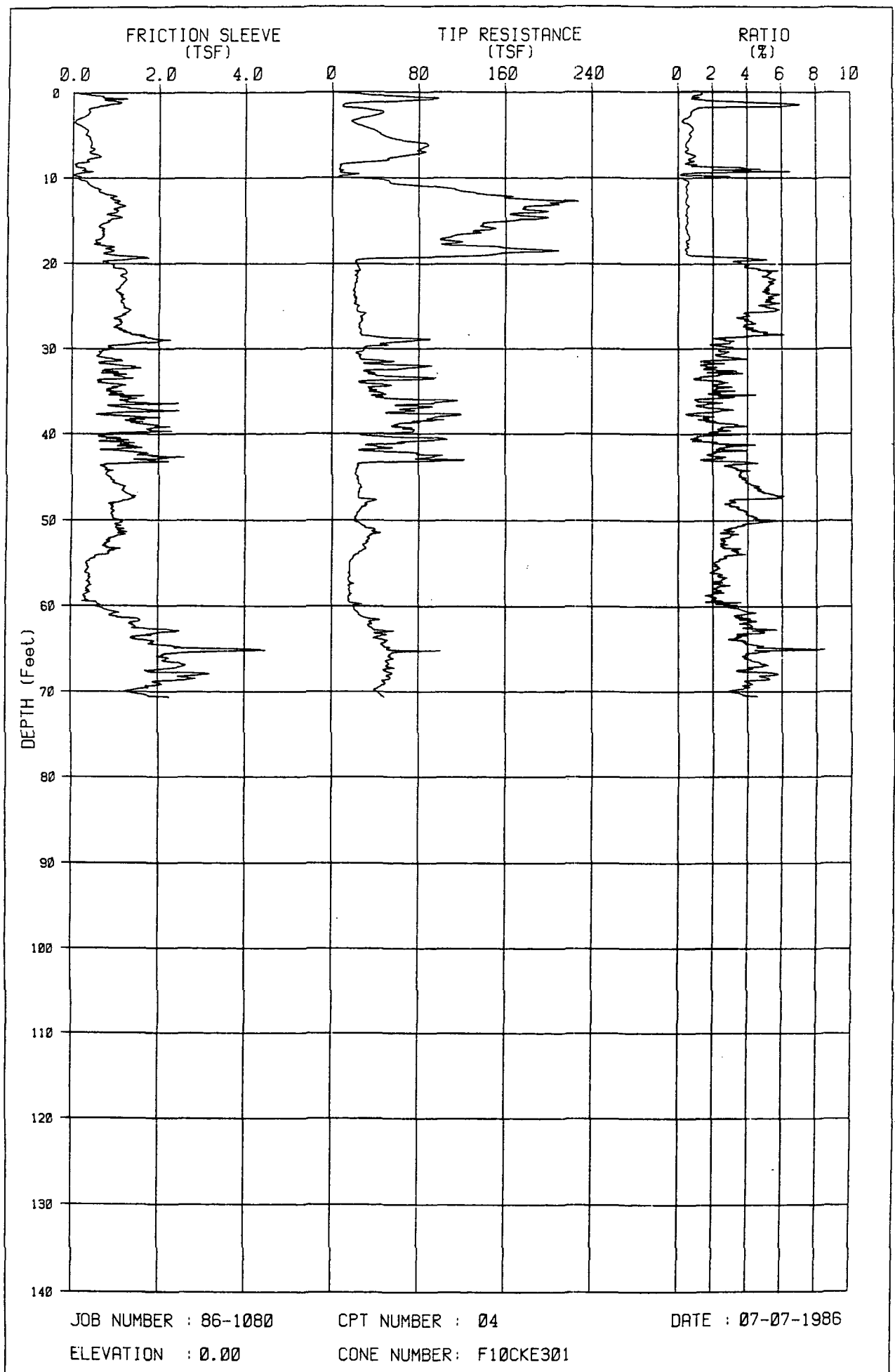
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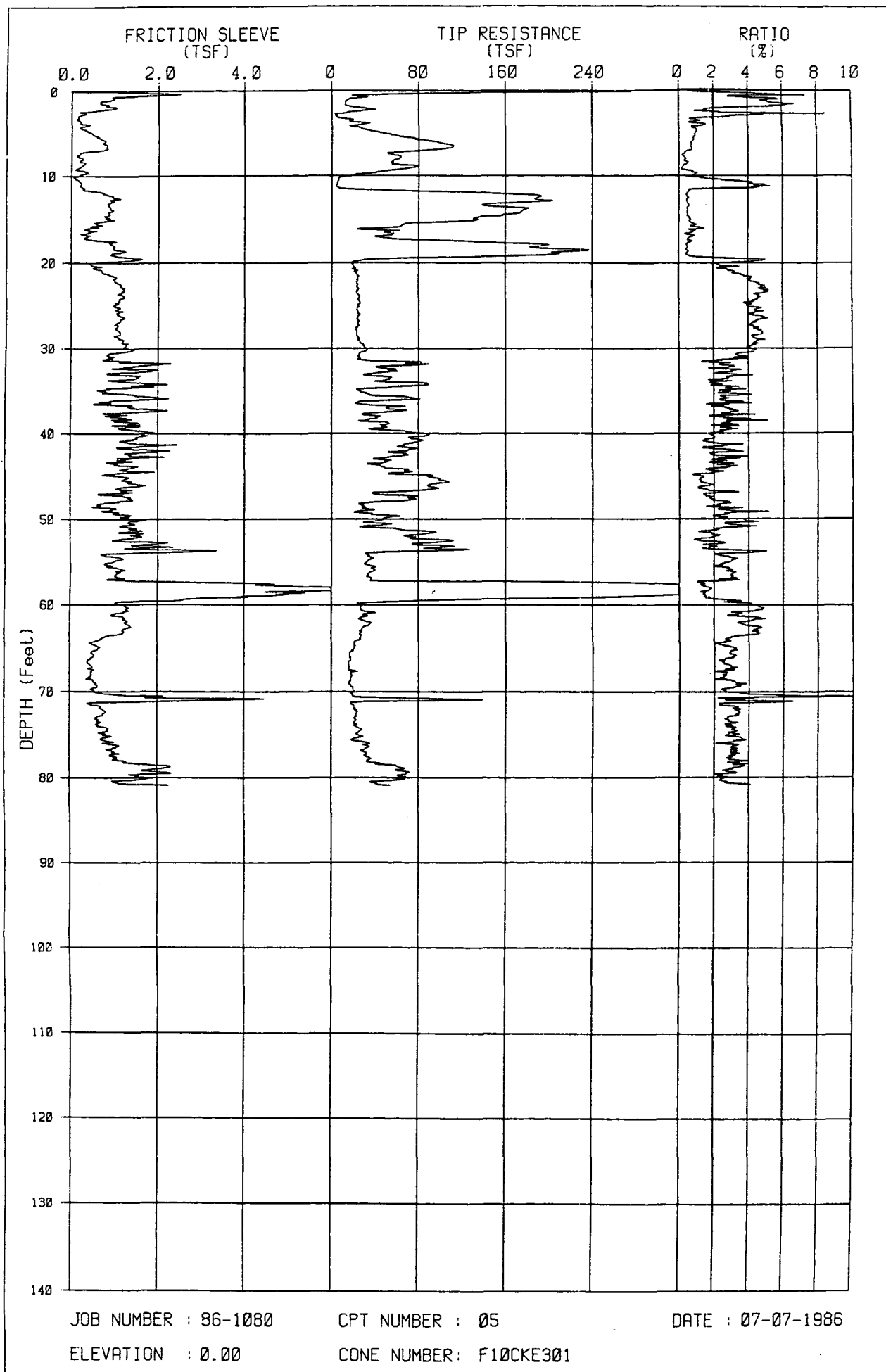
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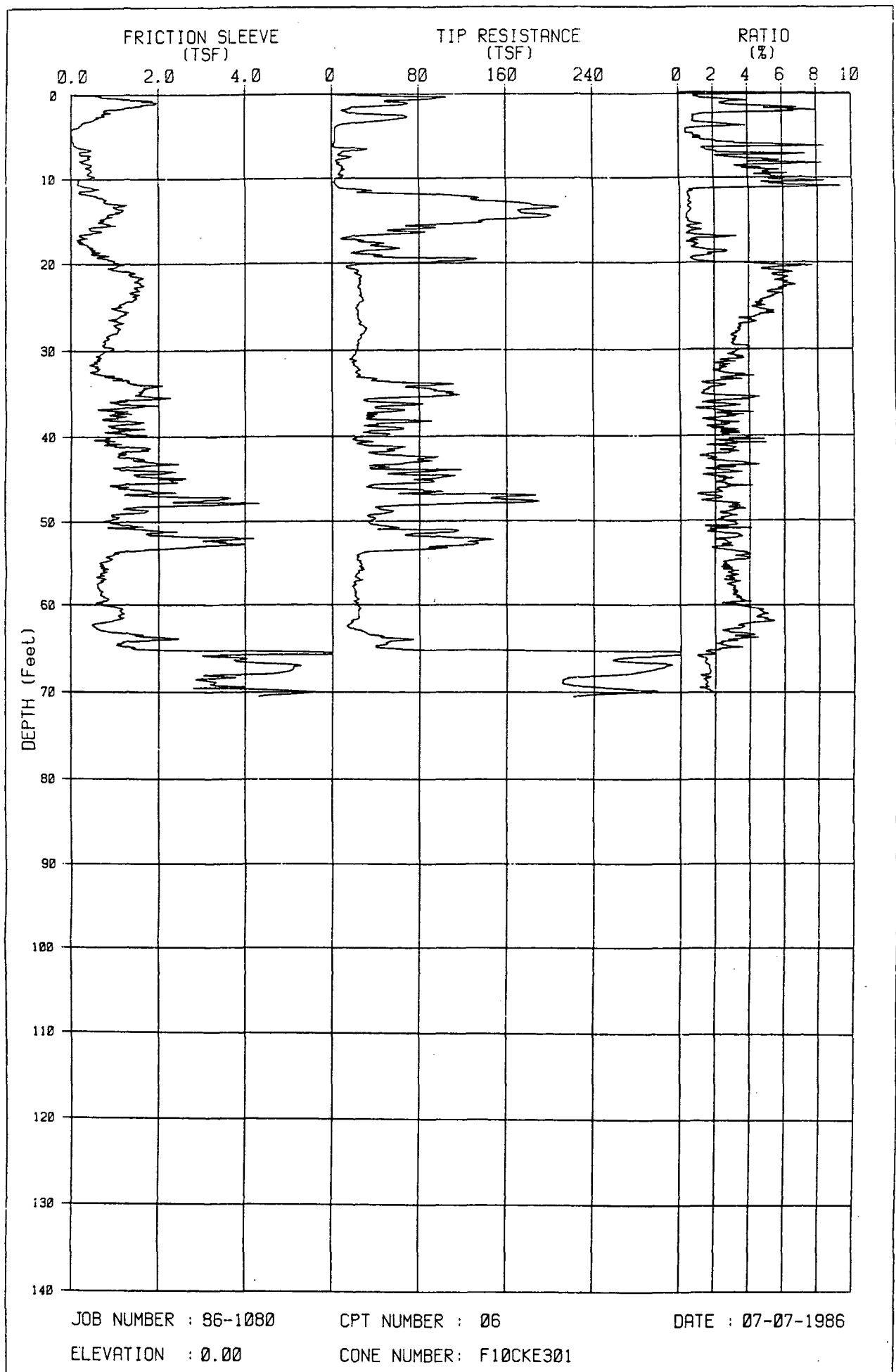
ELEVATION : 0.00

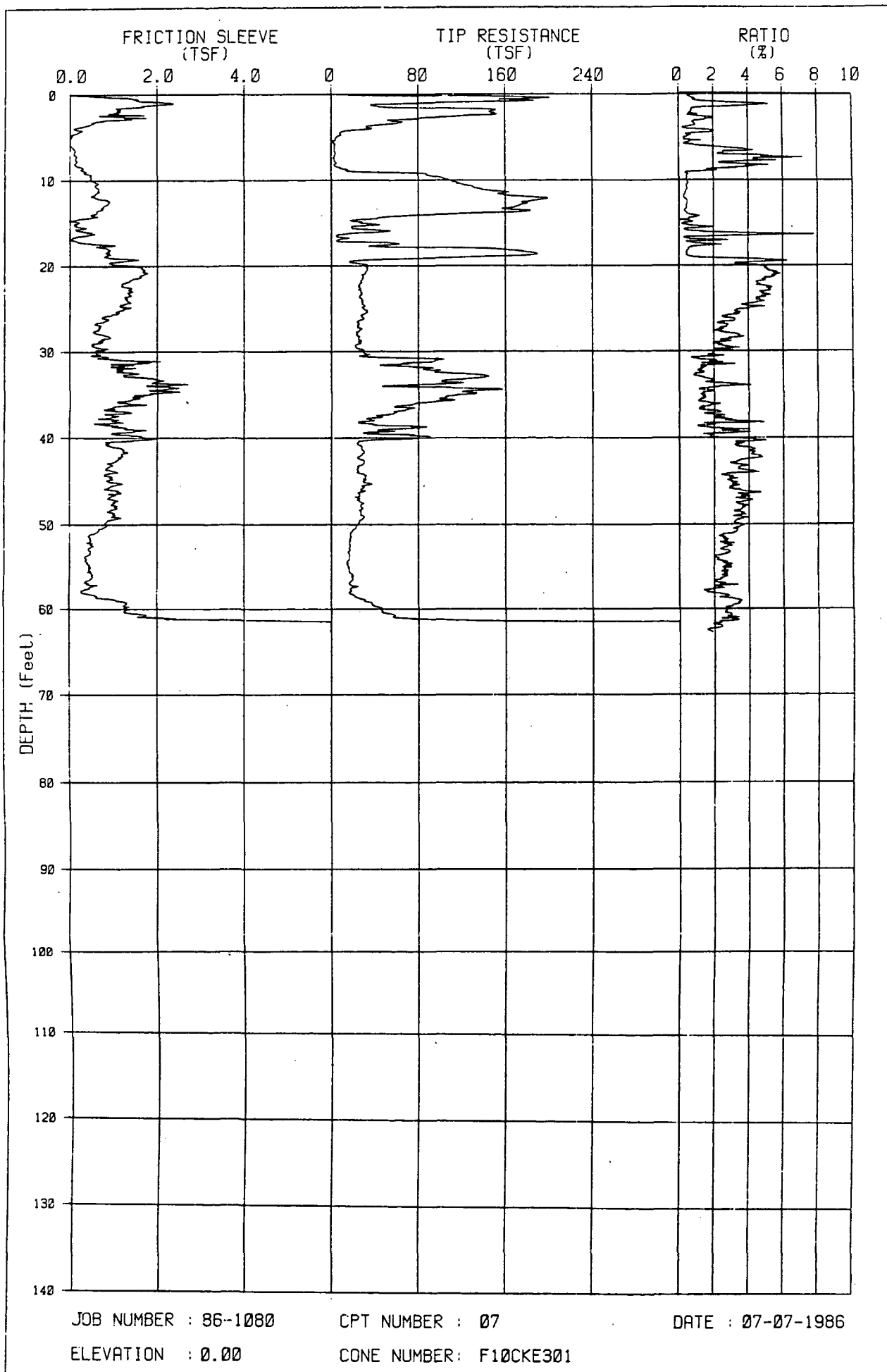
CONE NUMBER: F10CKE301

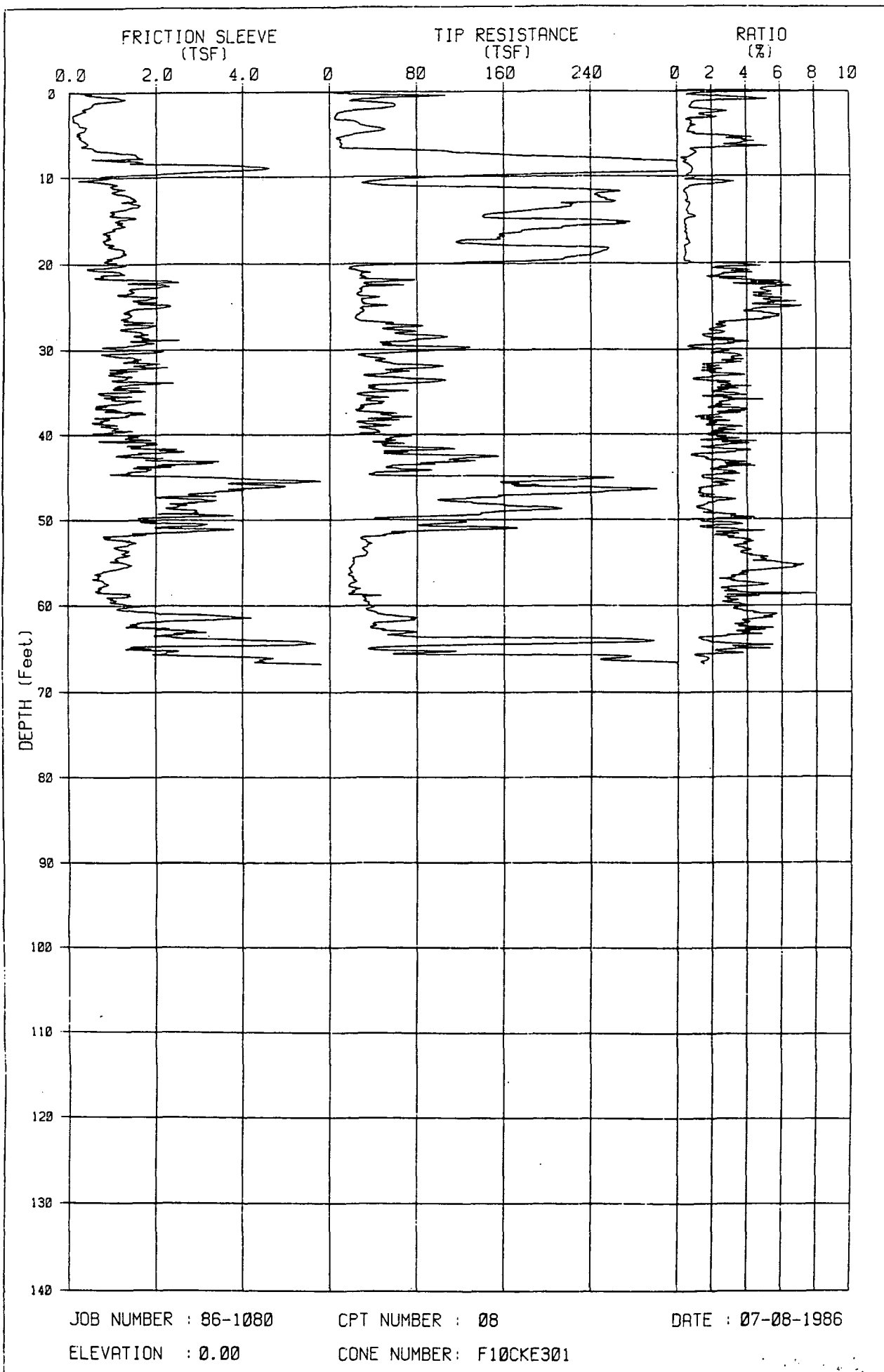


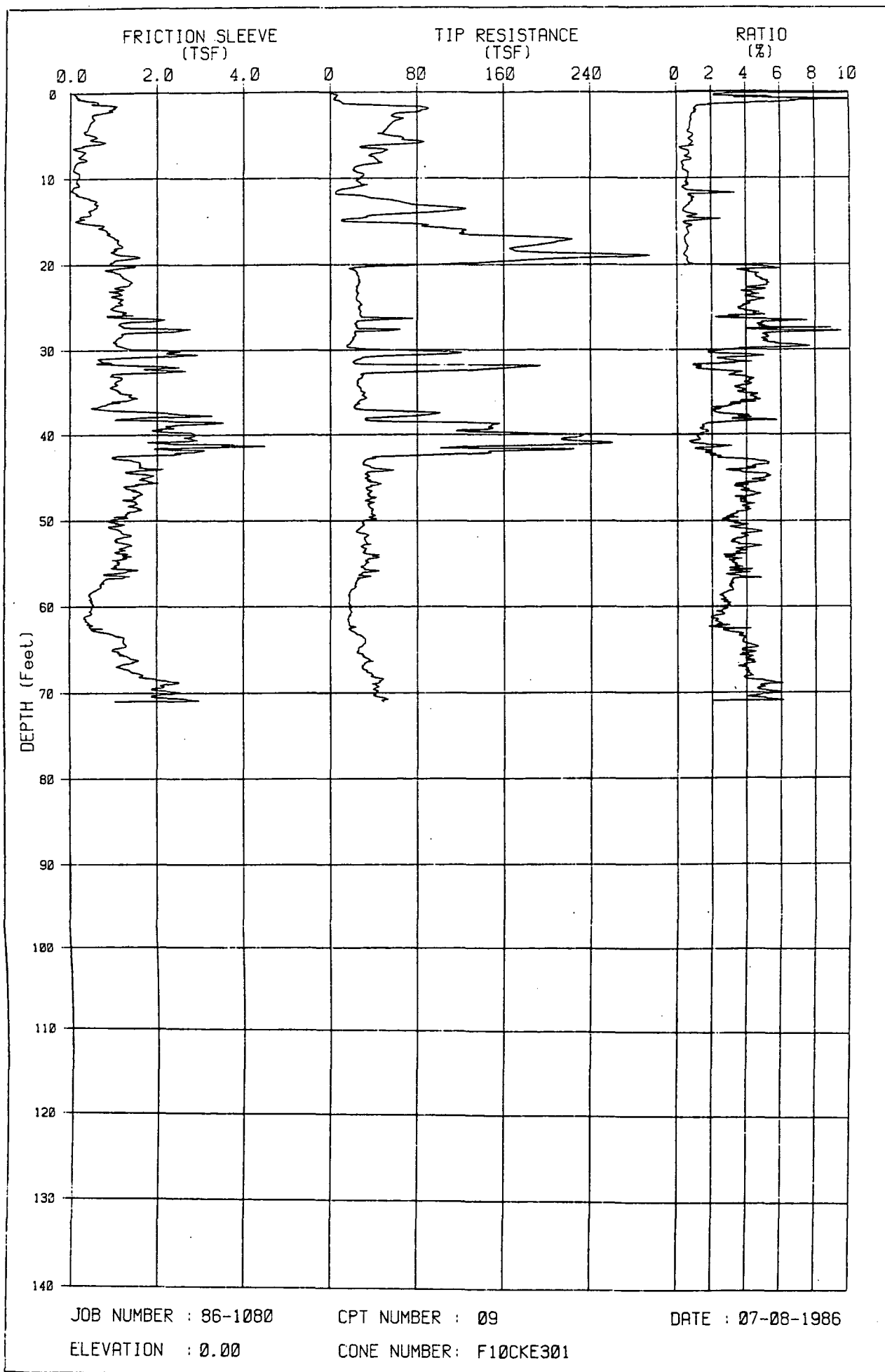


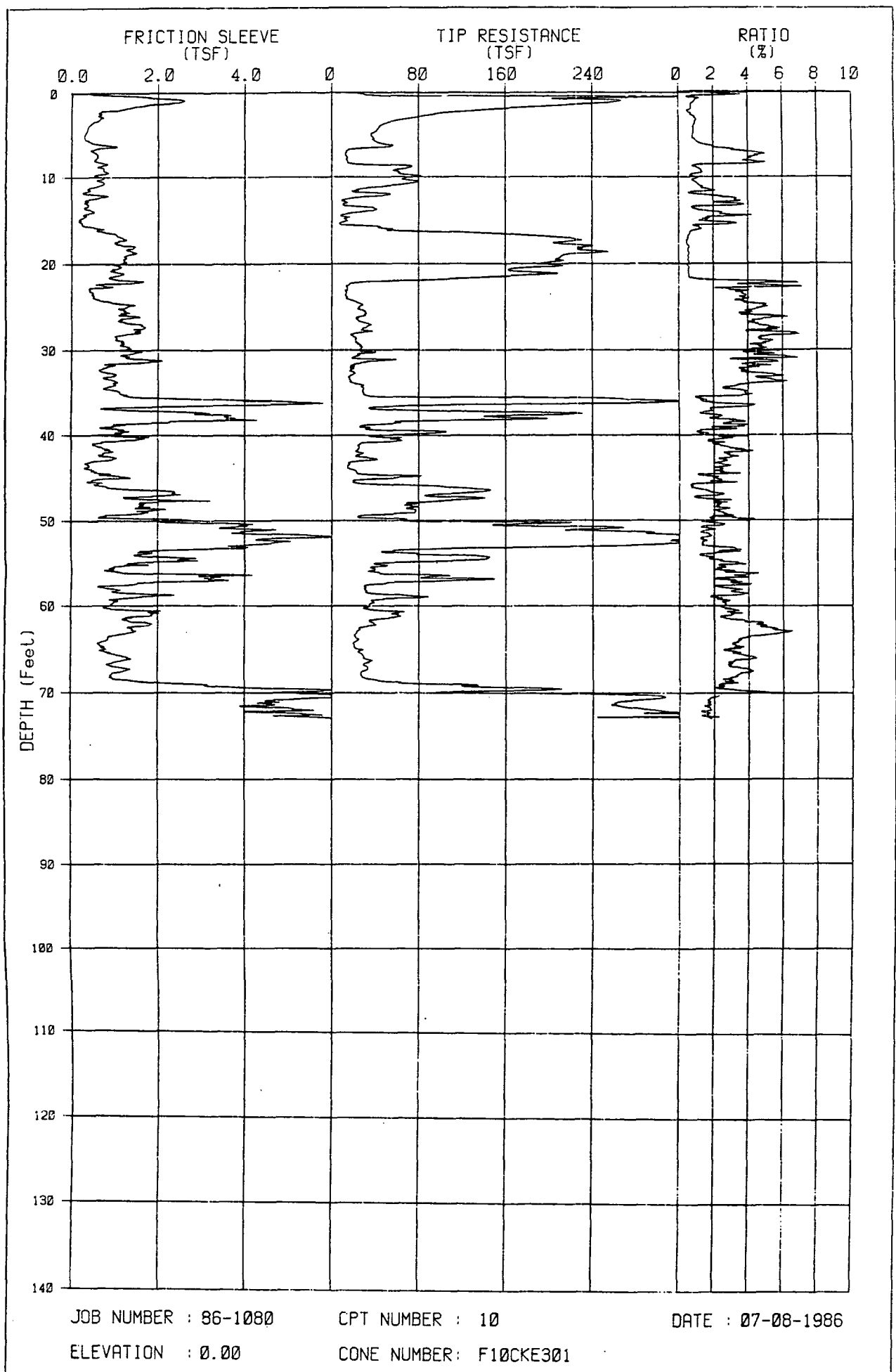


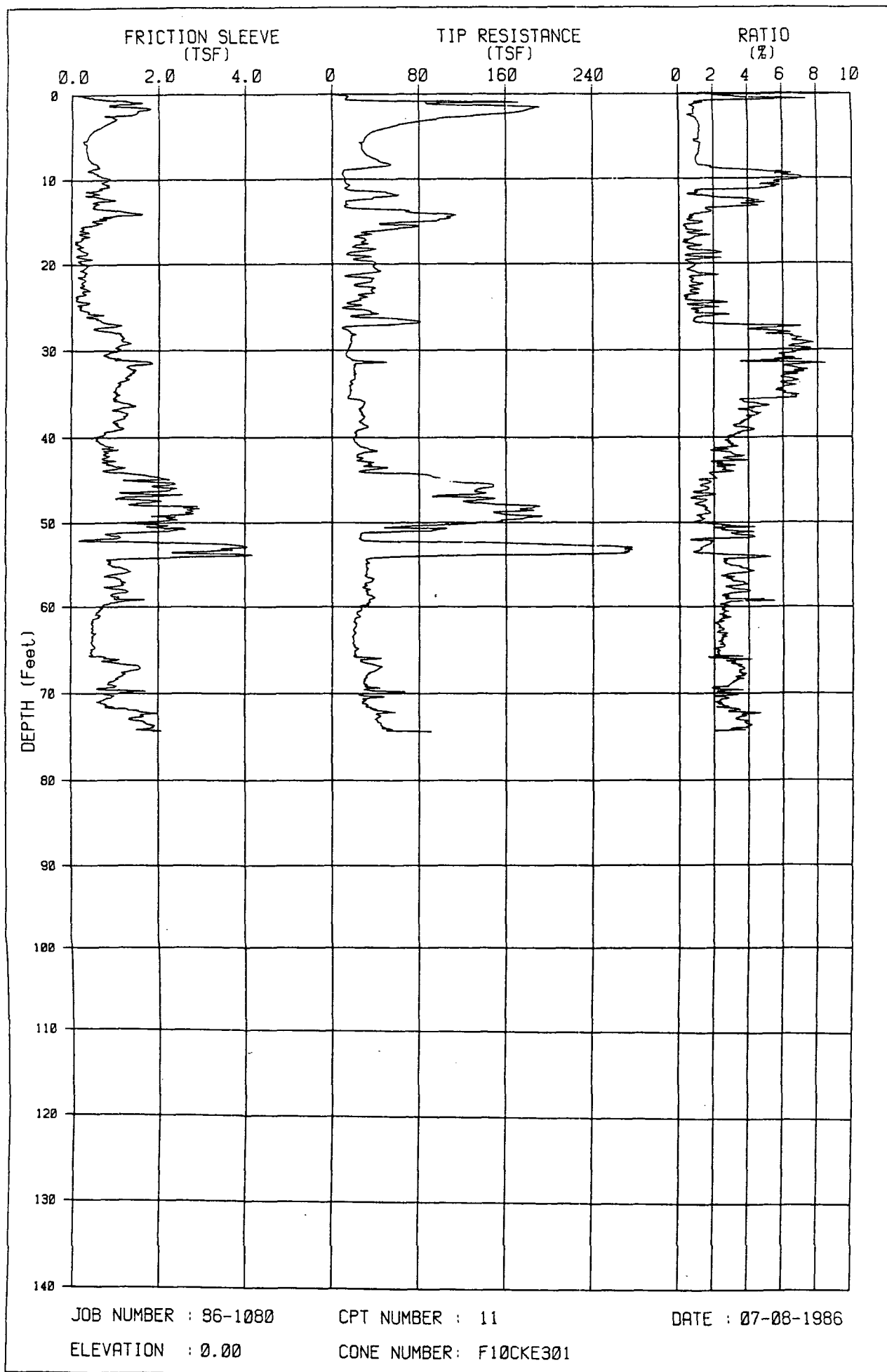




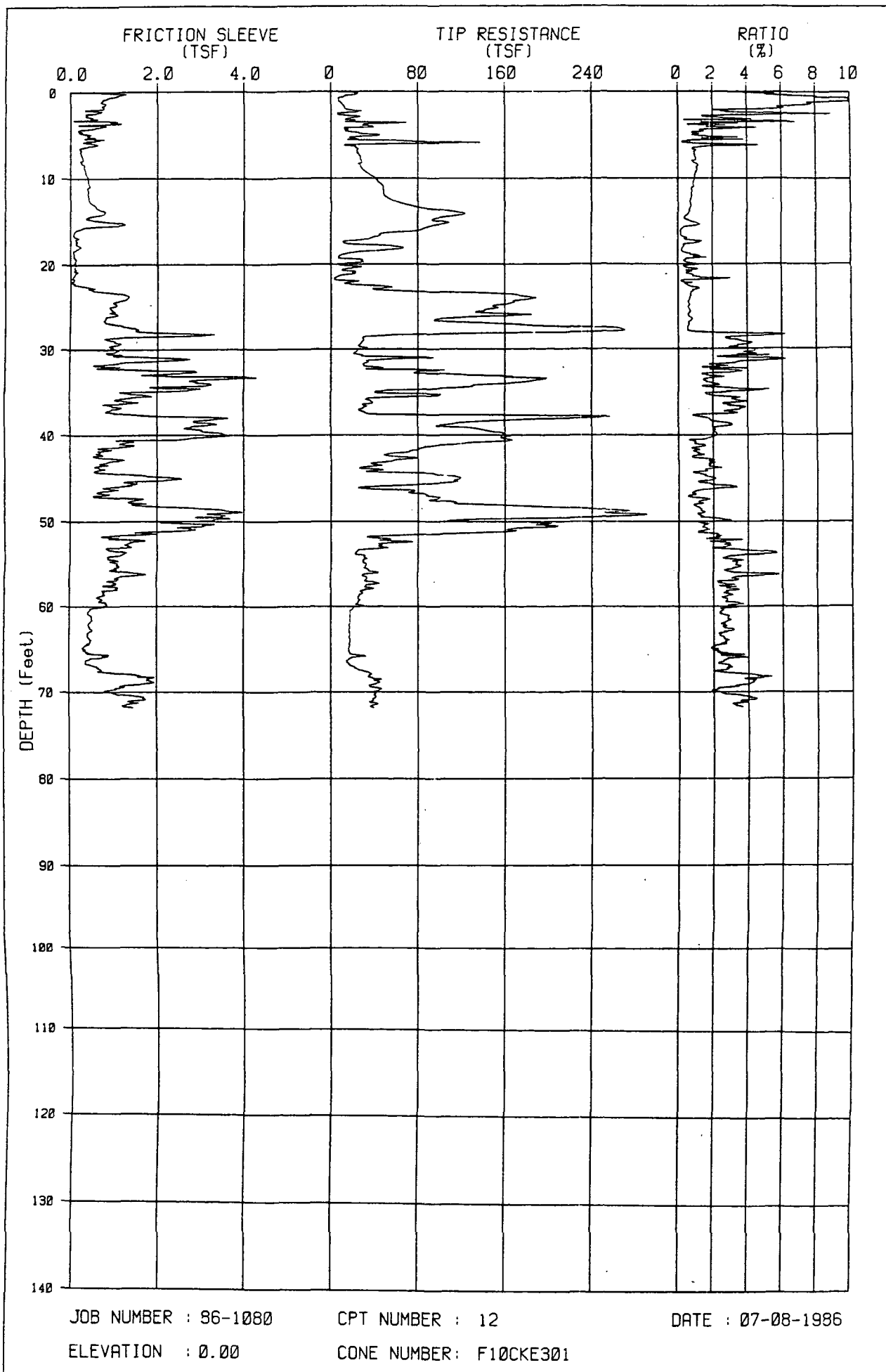


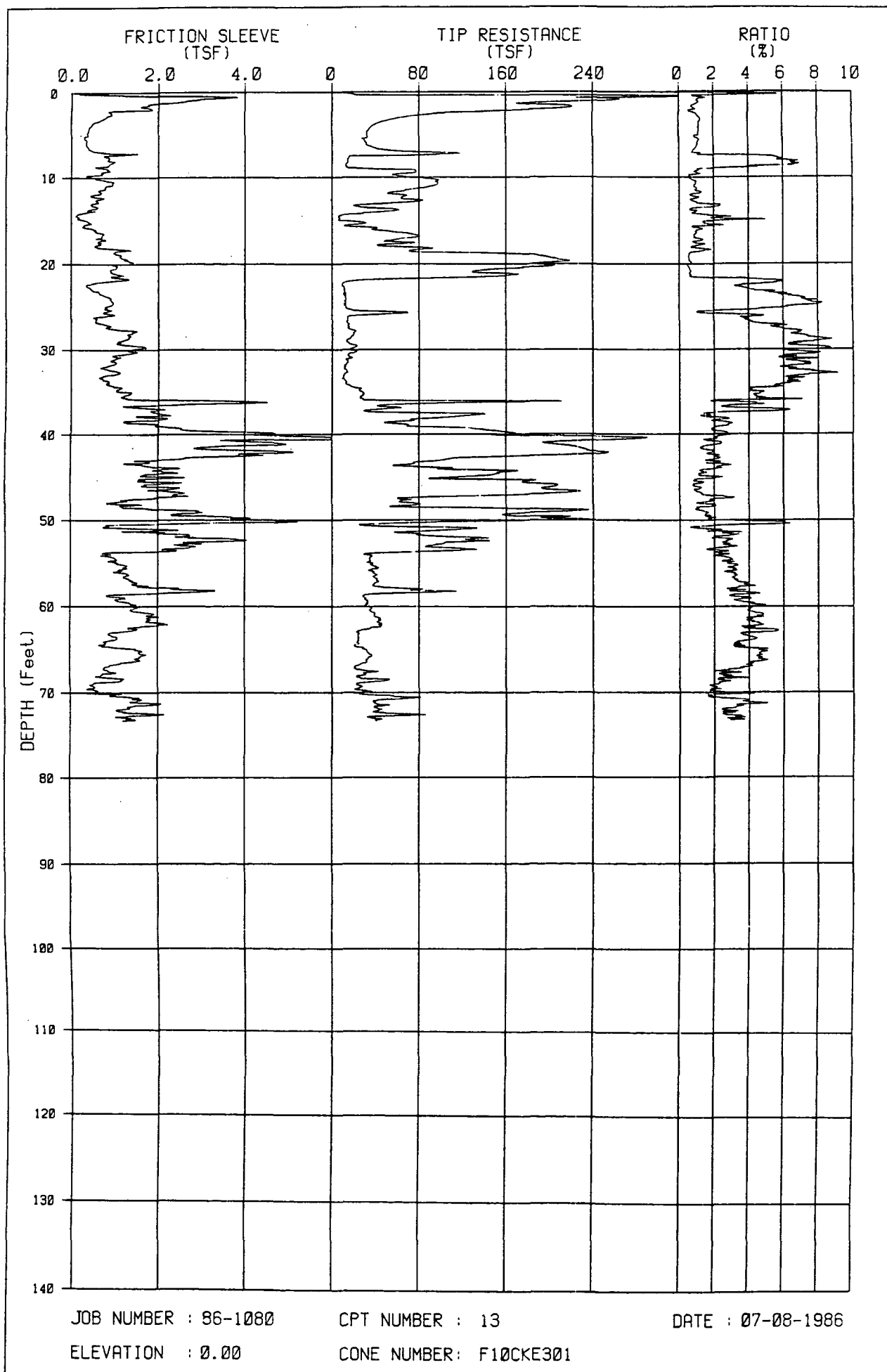


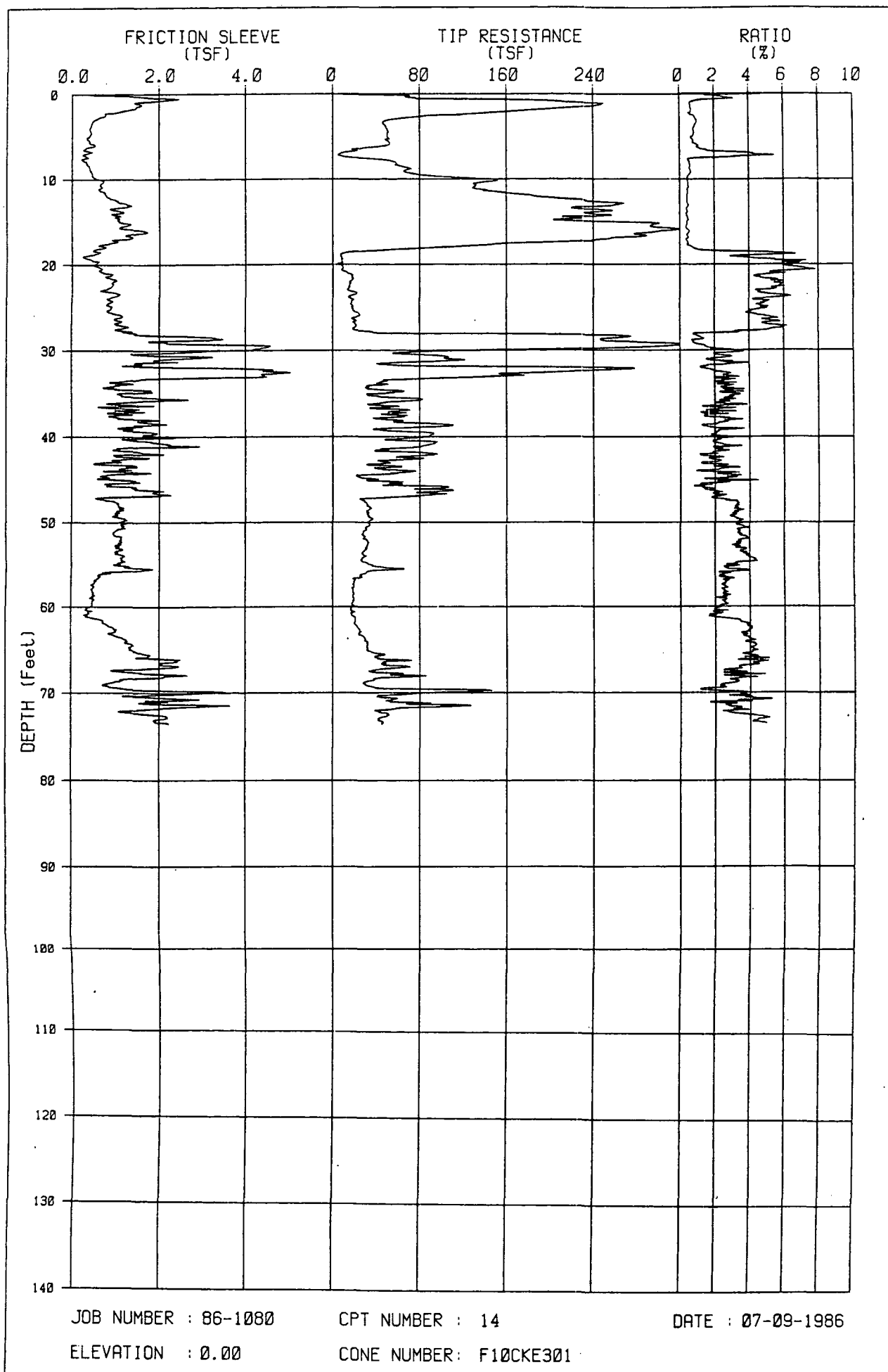


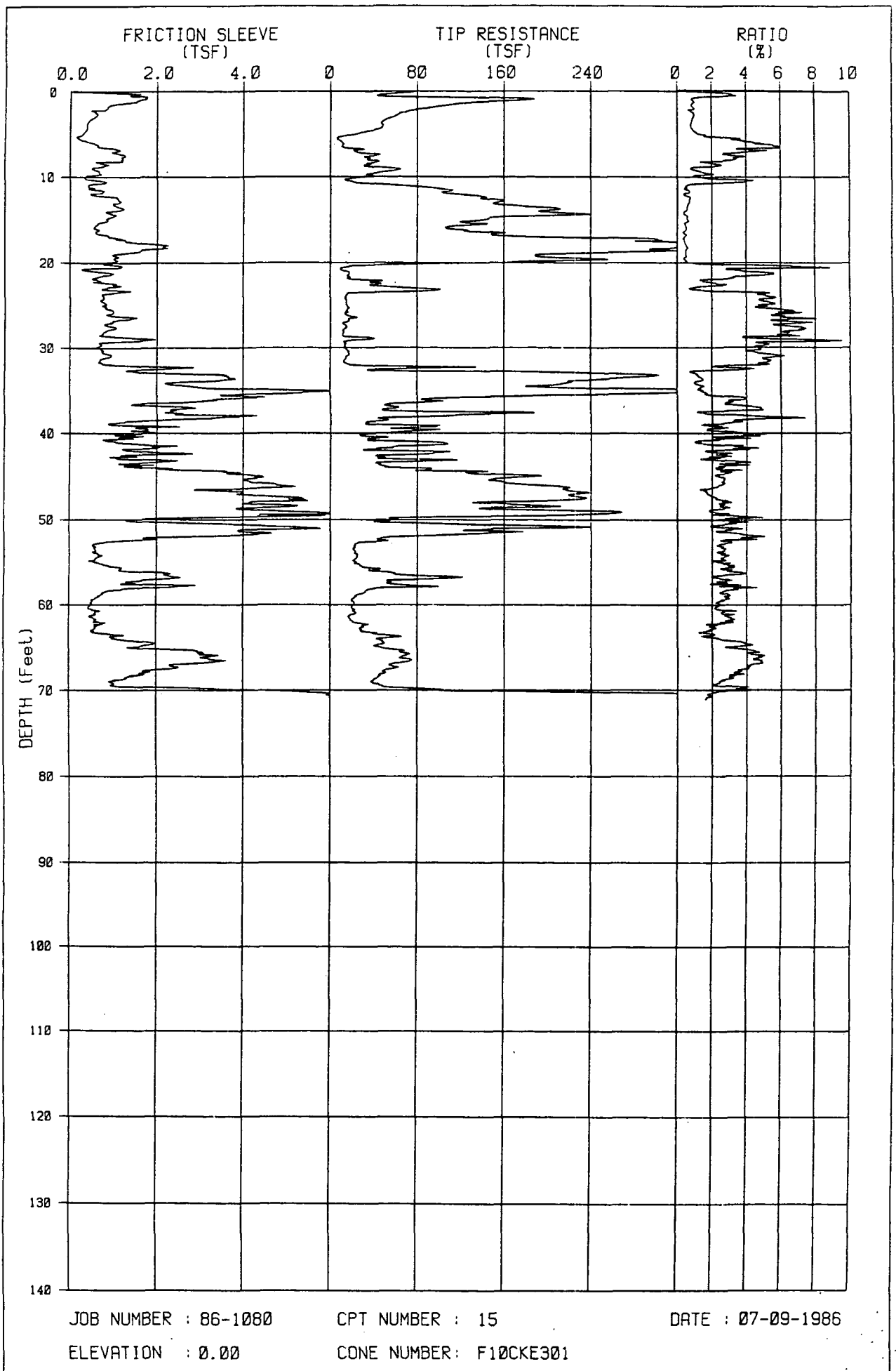


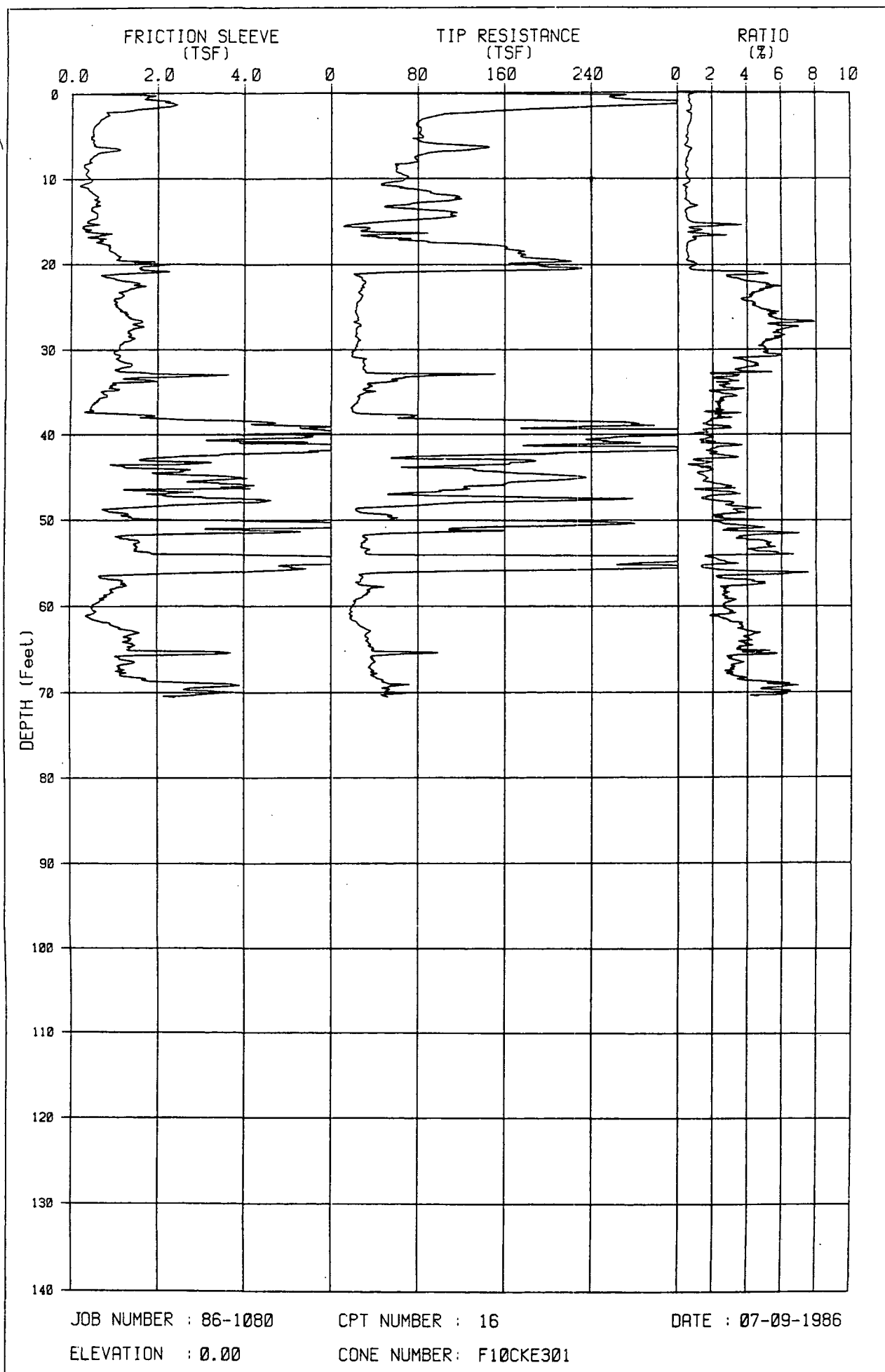


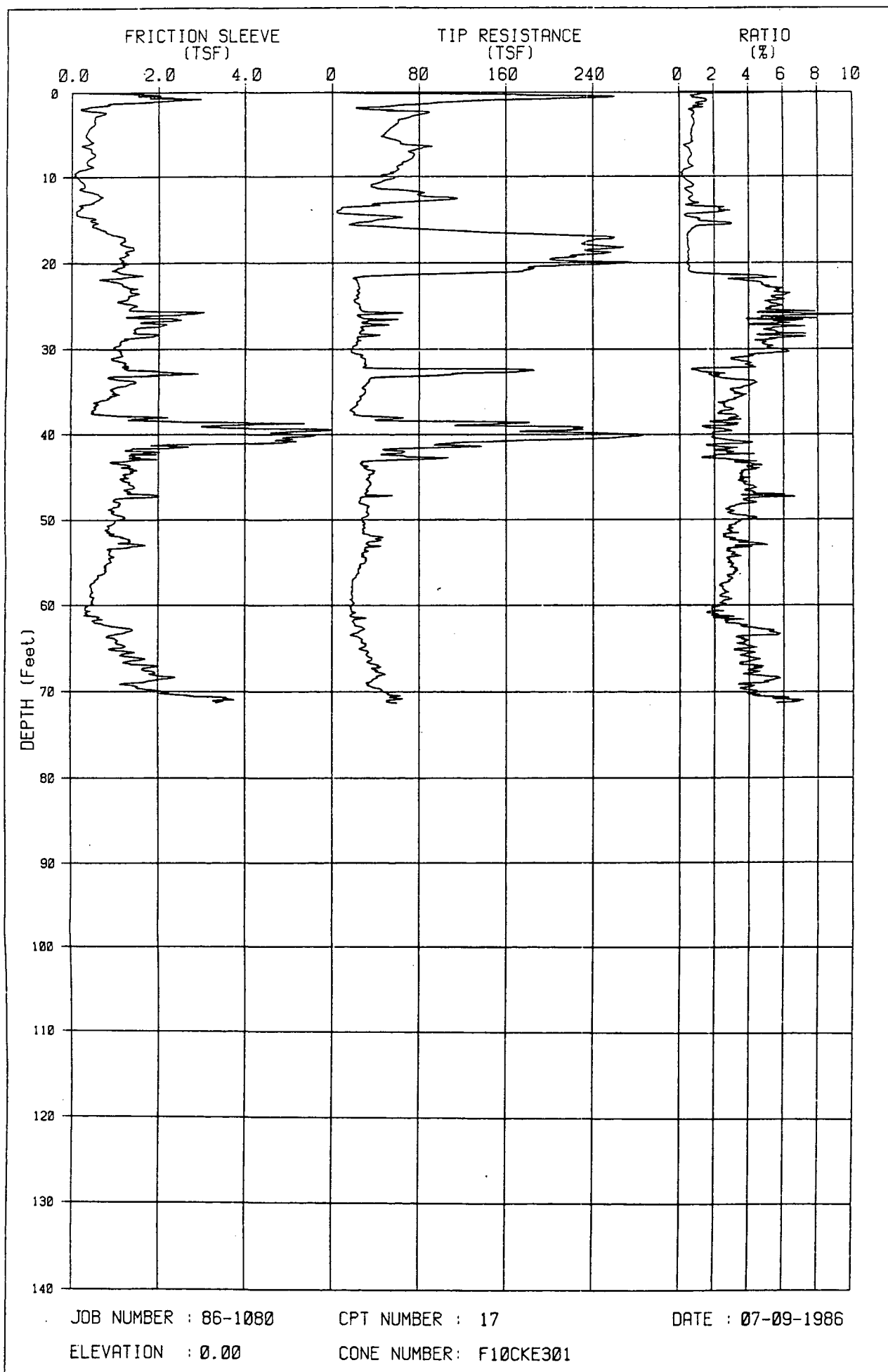


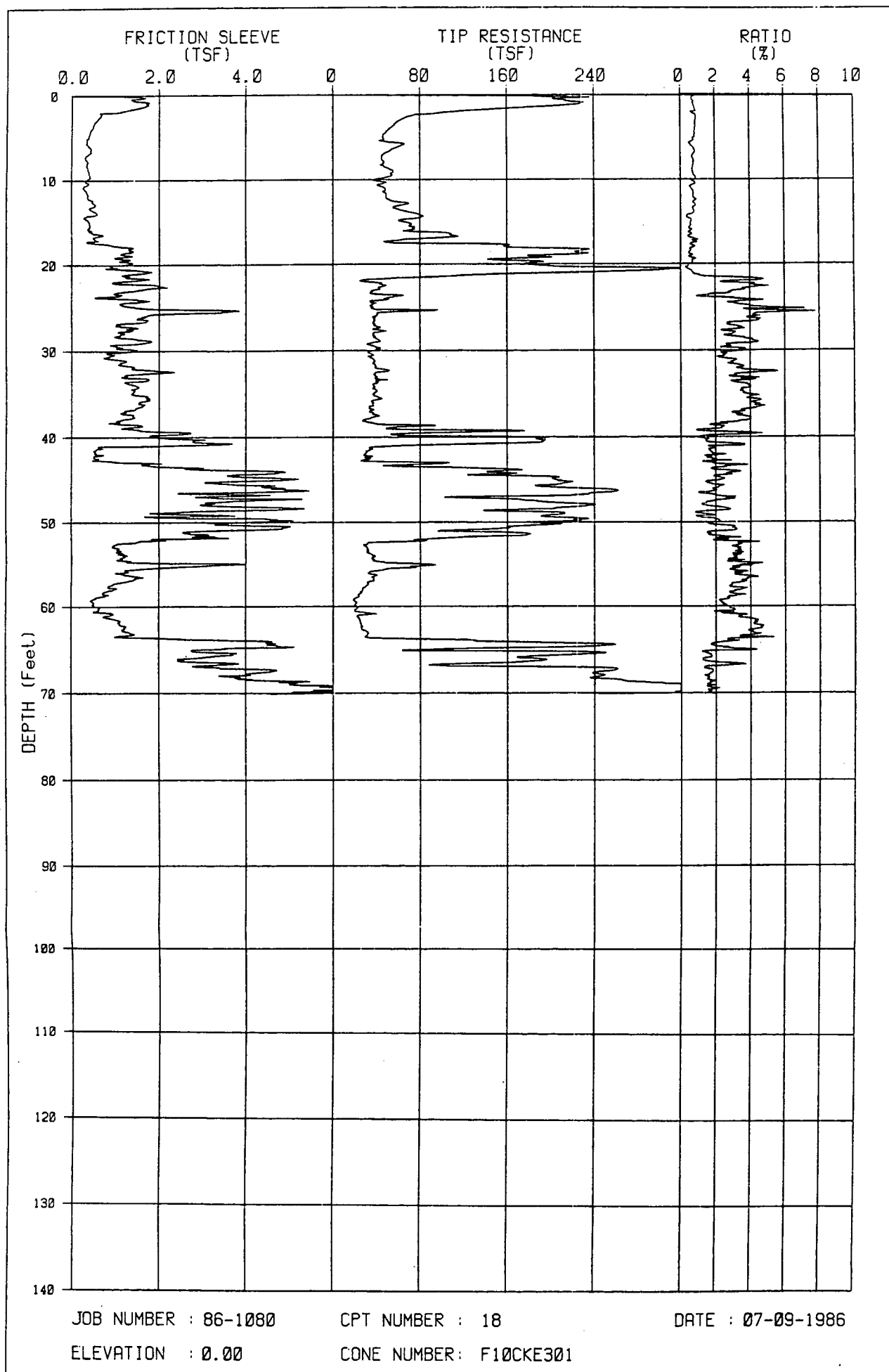


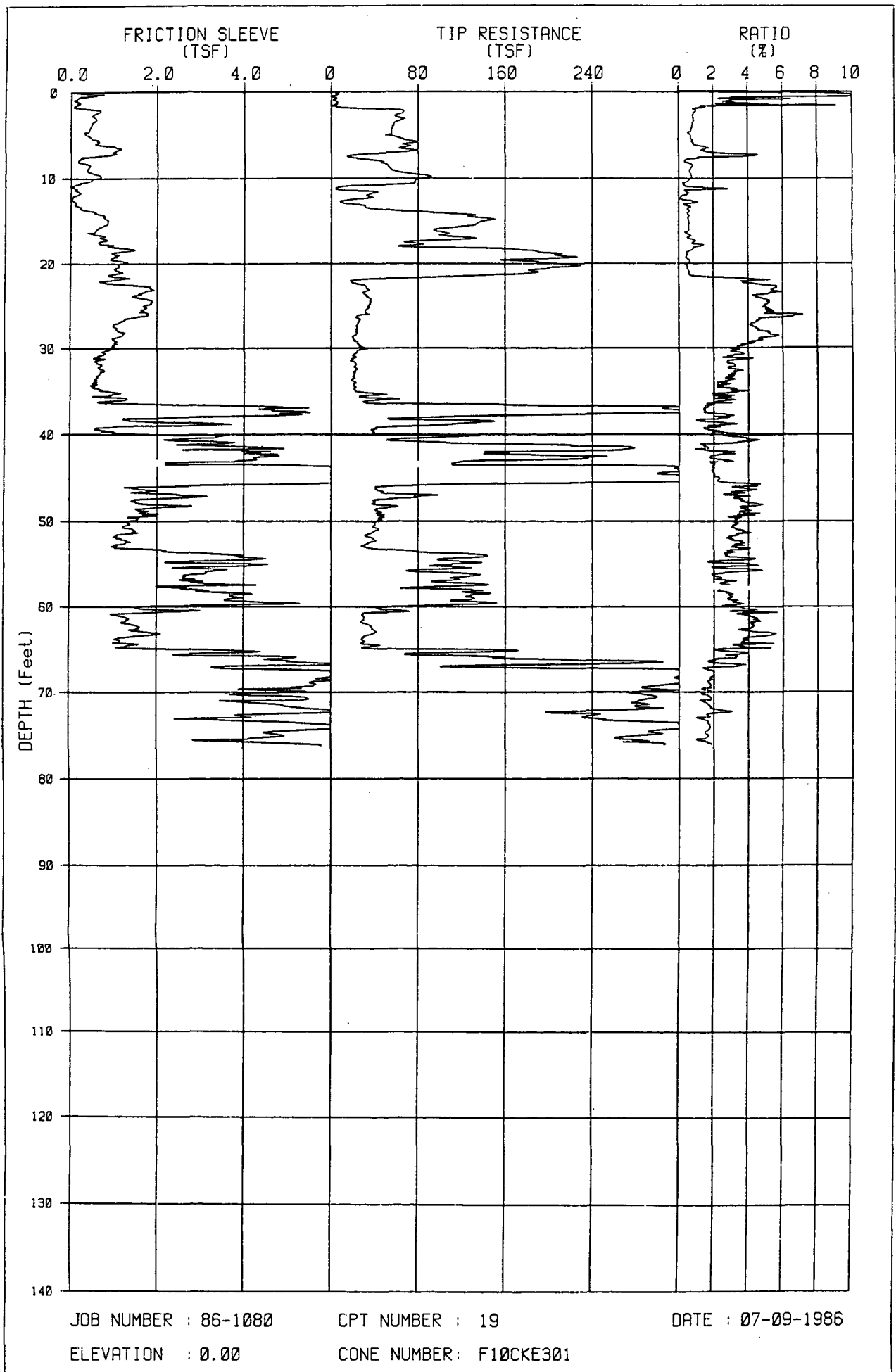




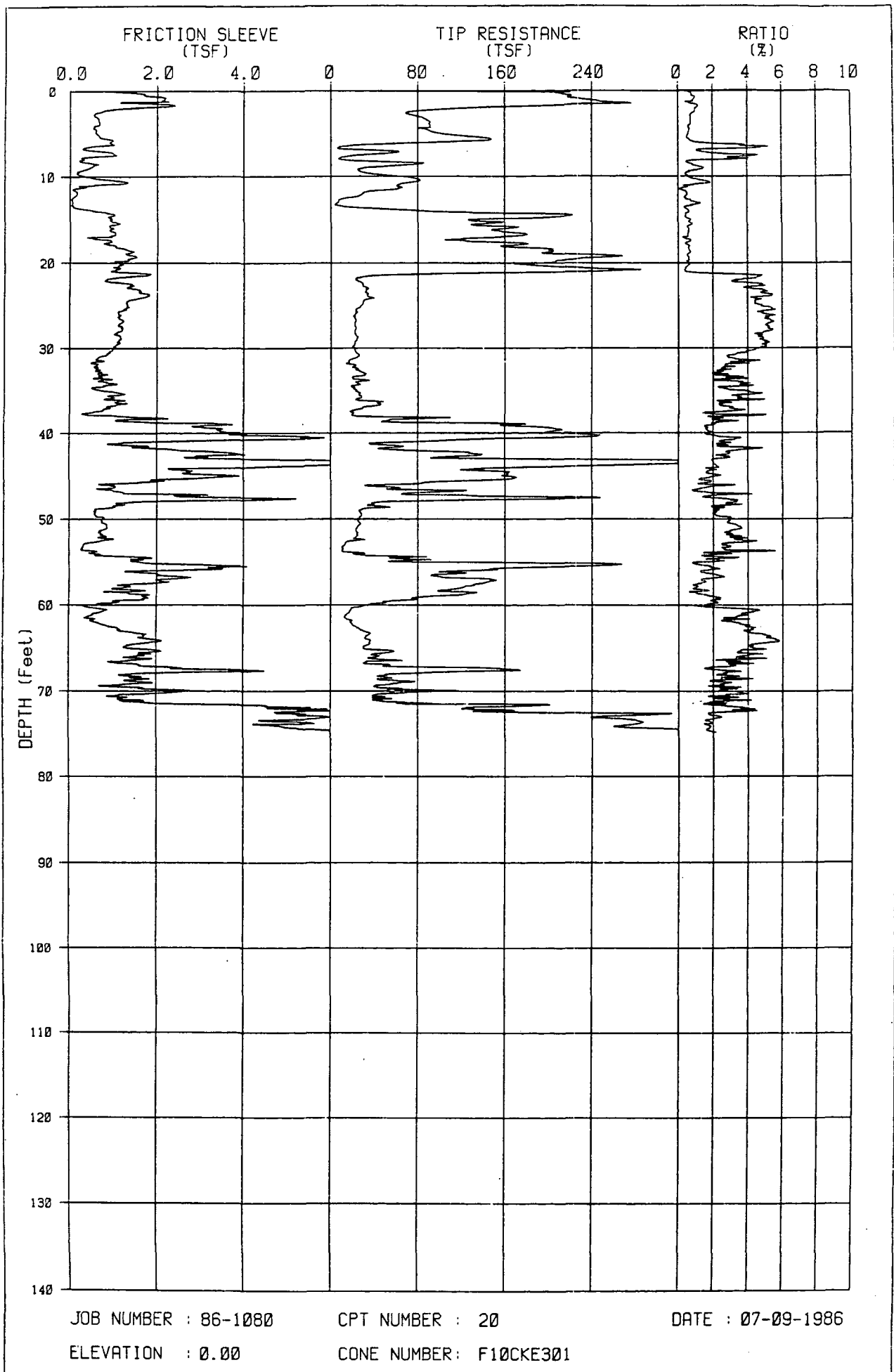


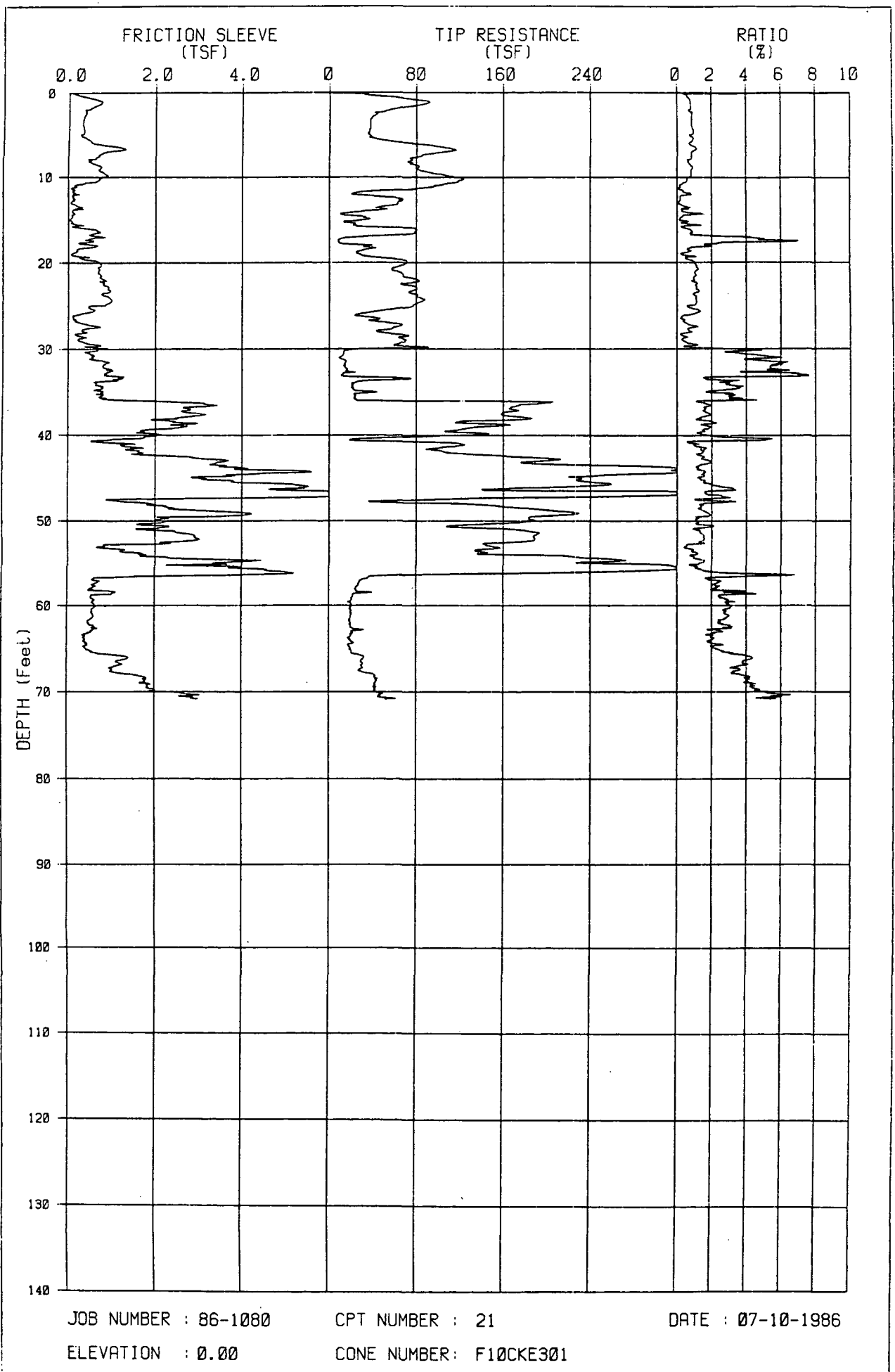


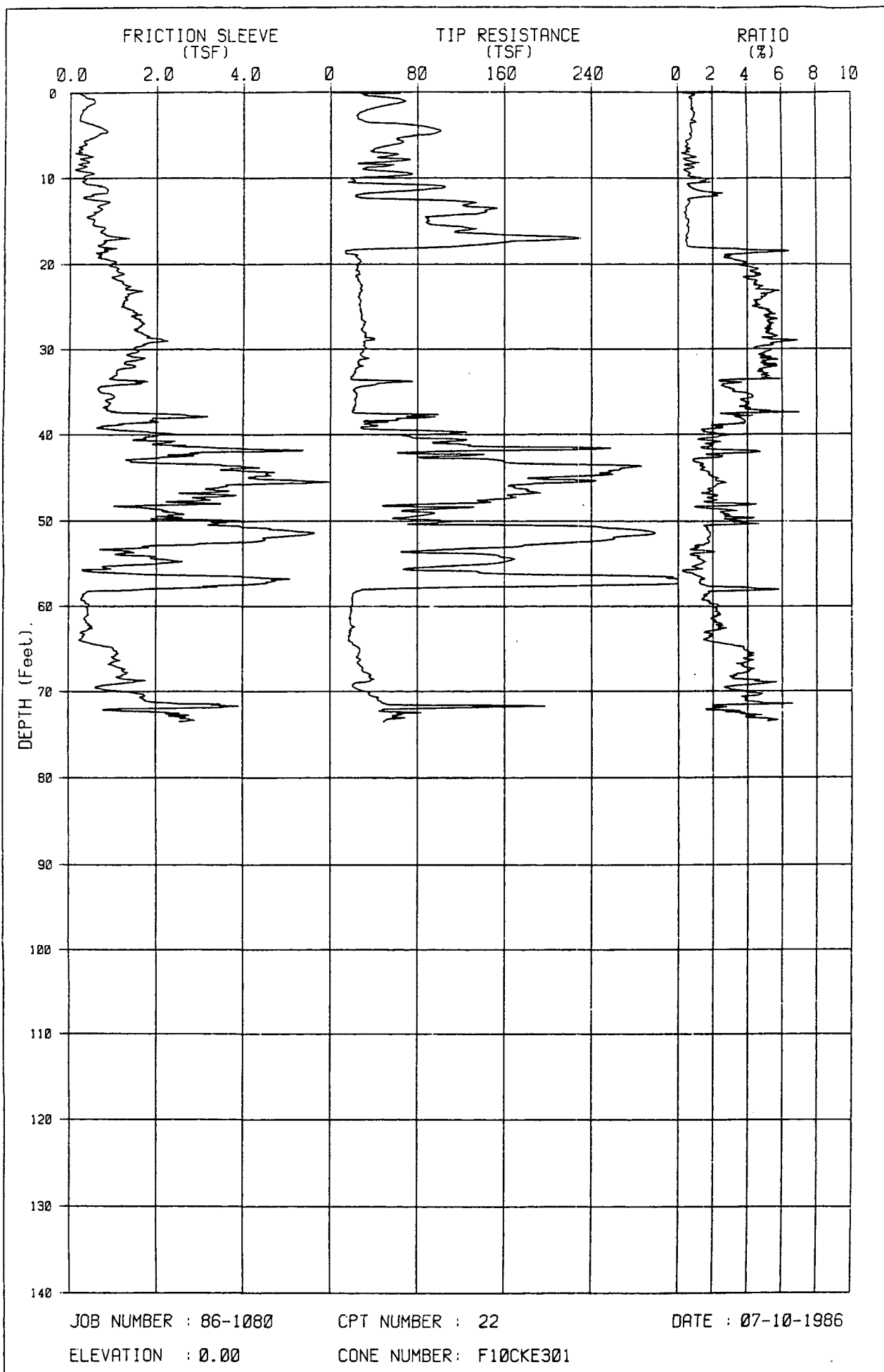


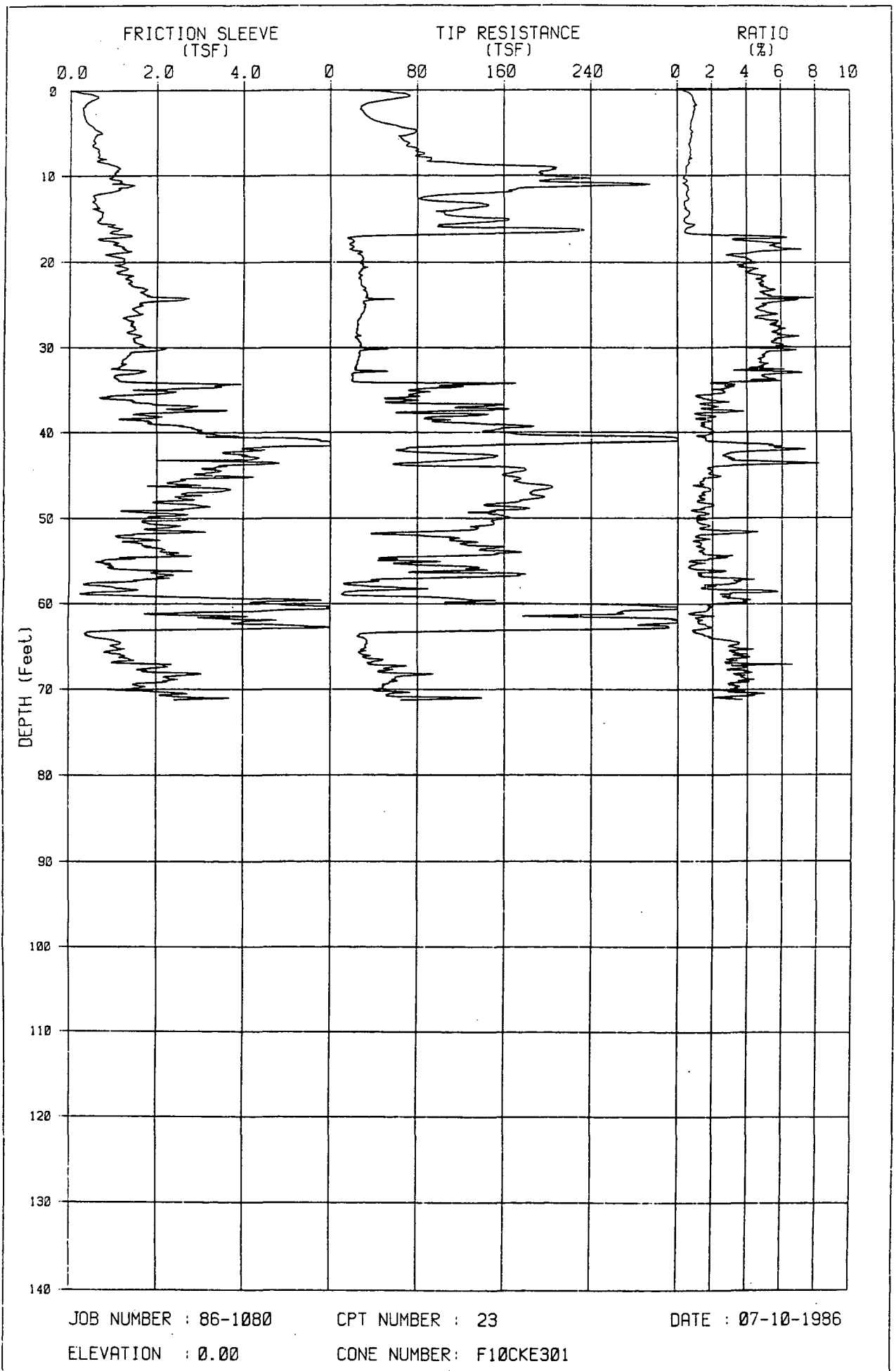


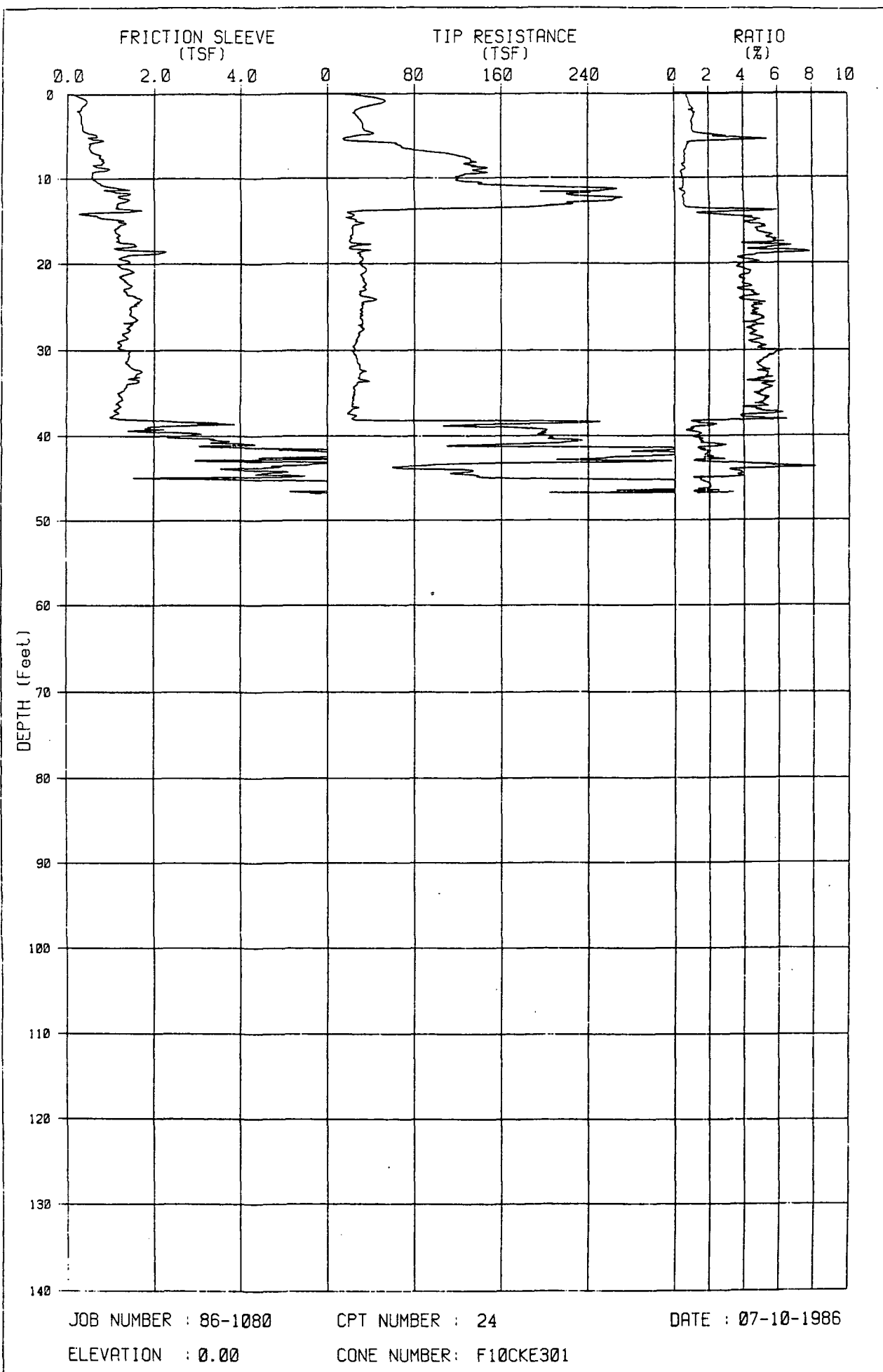


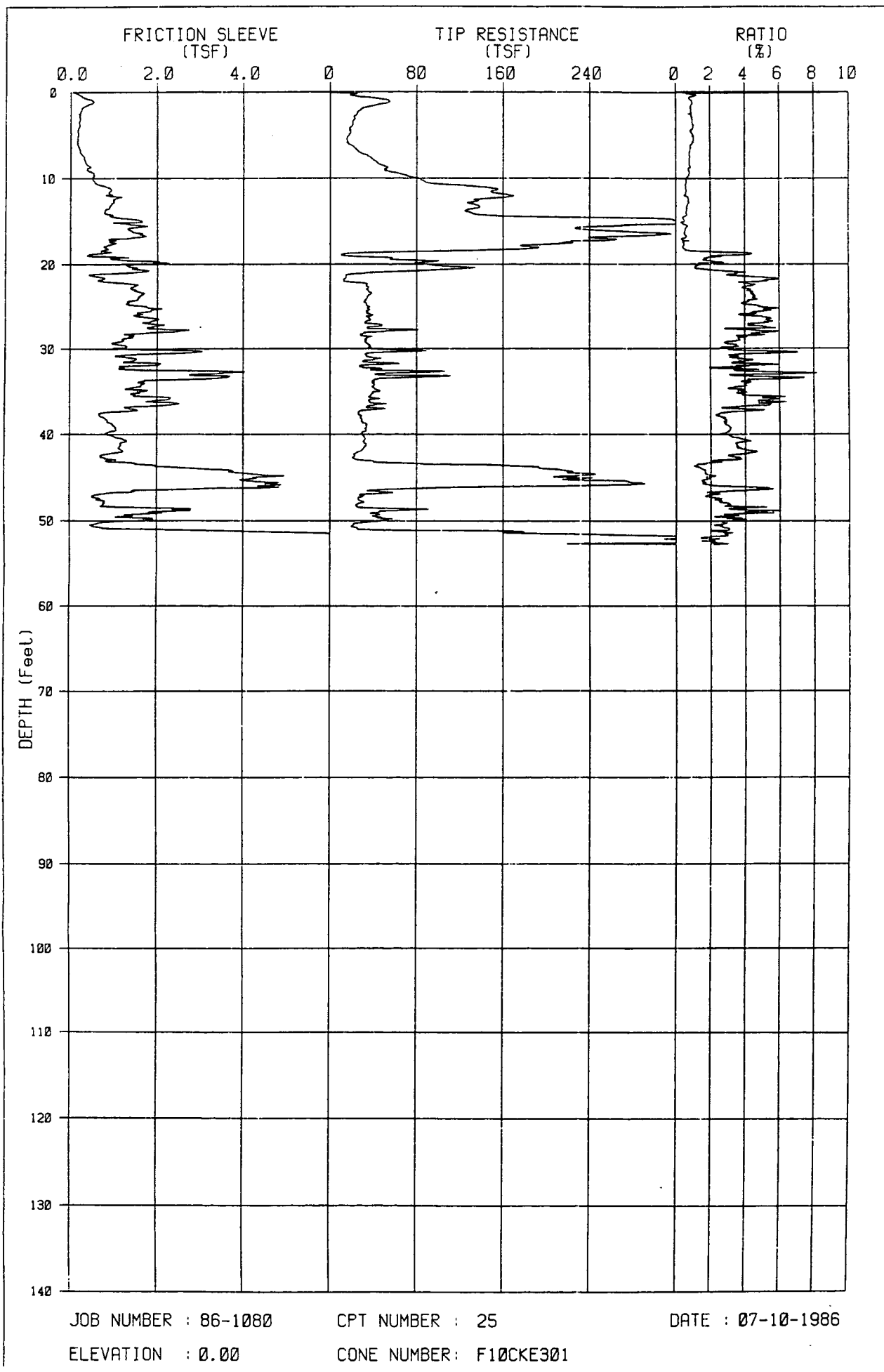


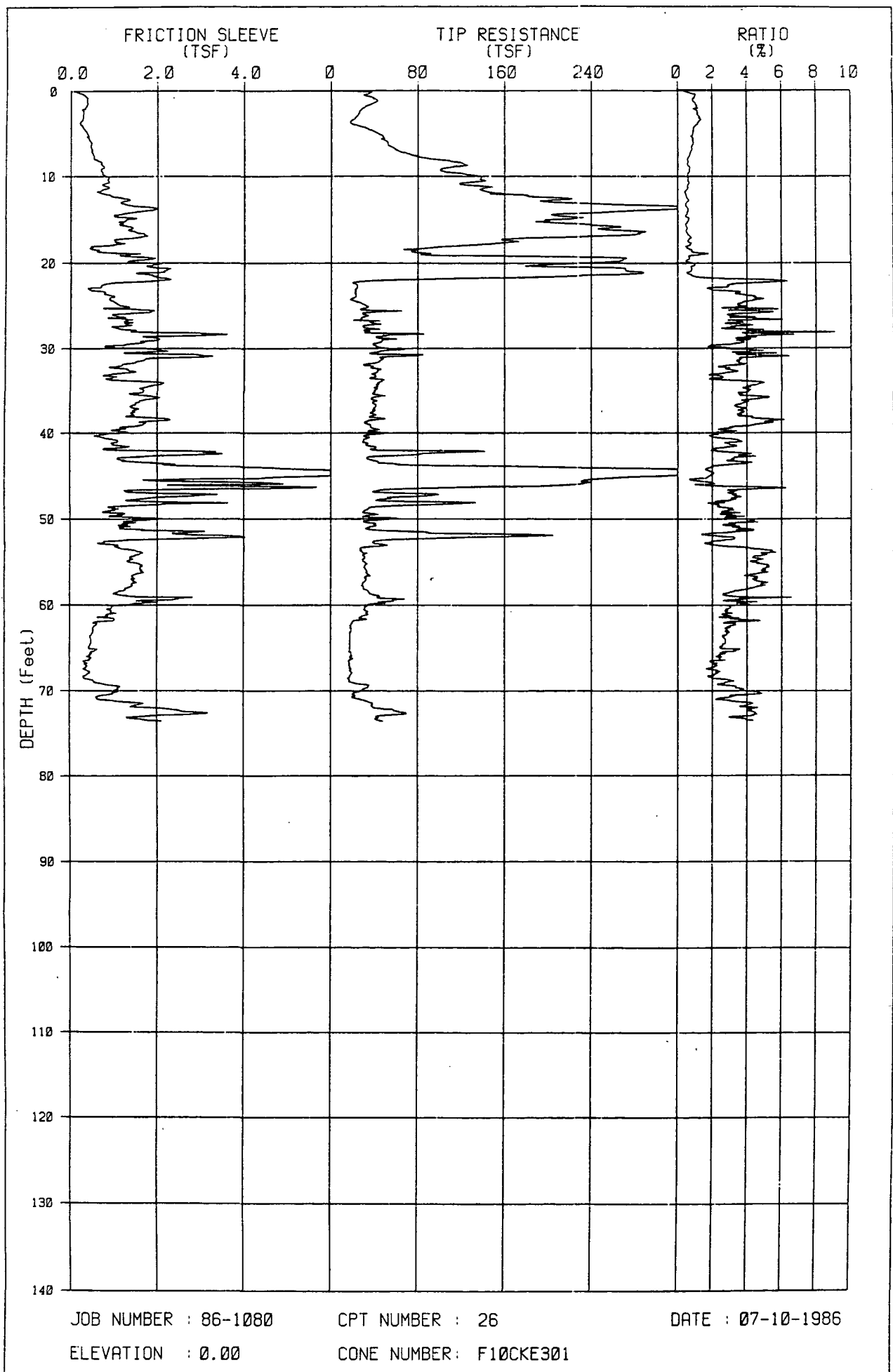


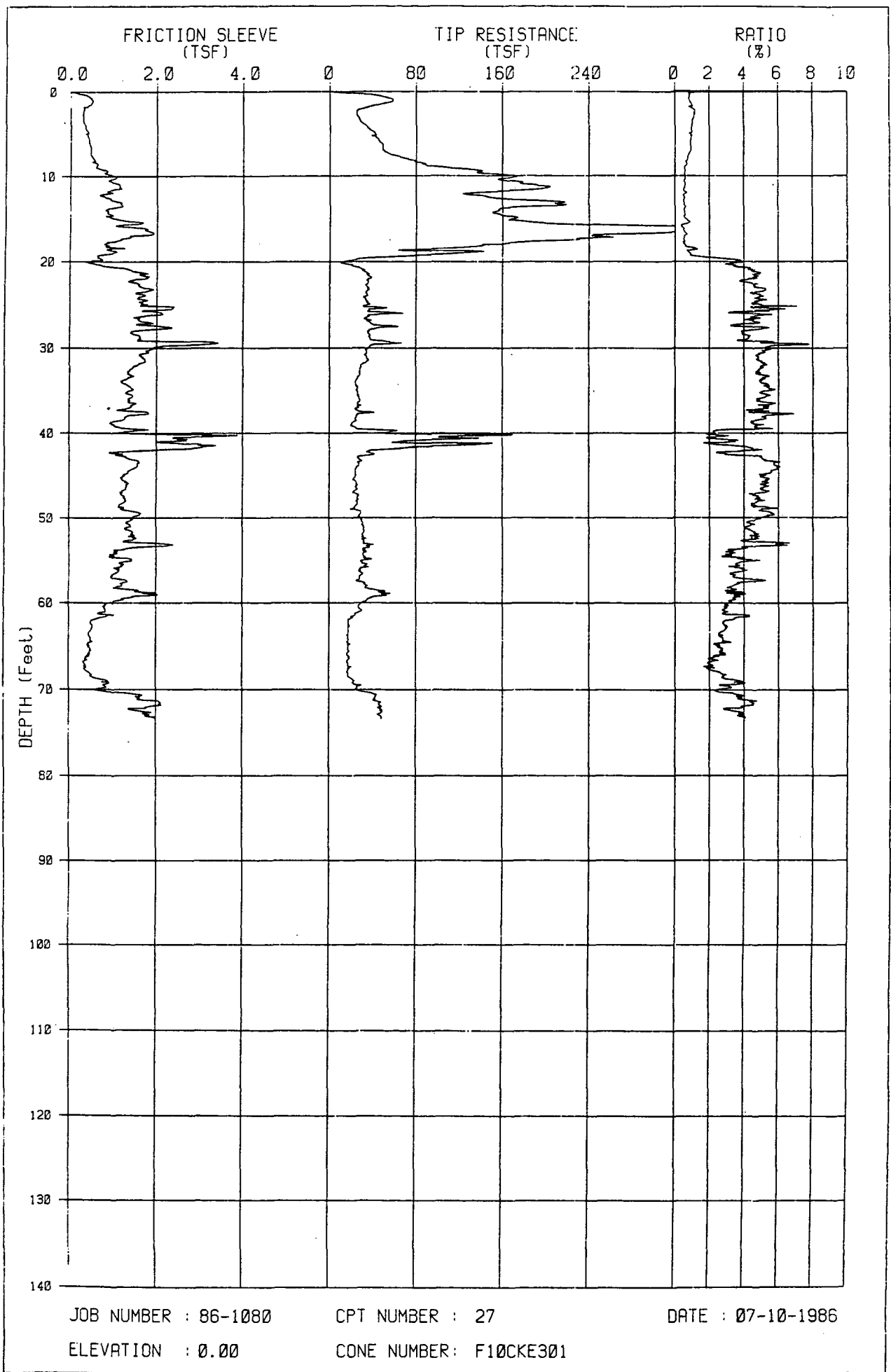




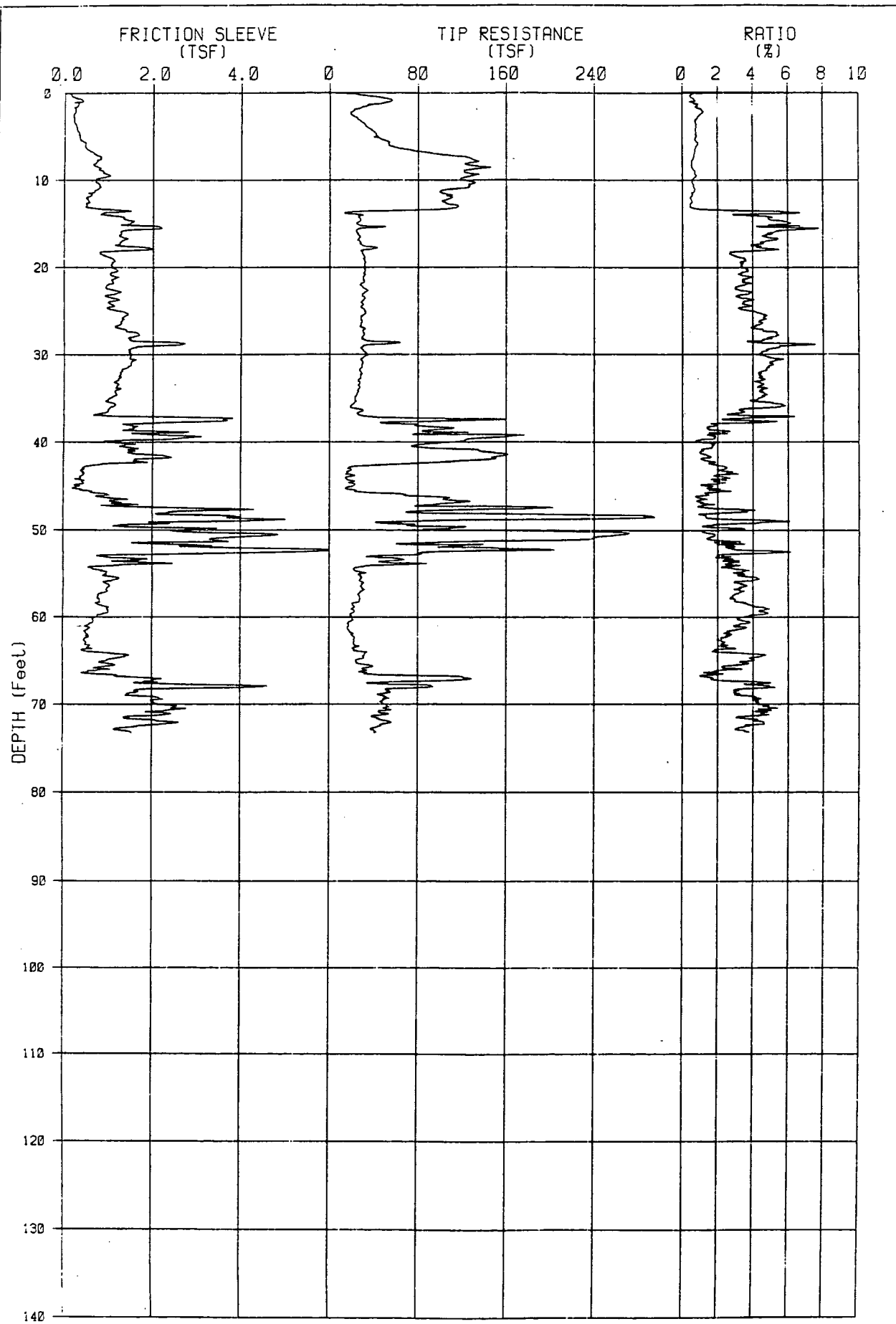












JOB NUMBER : 86-1080

CPT NUMBER : 28

DATE : 07-10-1986

ELEVATION : 0.00

CONE NUMBER: F10CKE301

Appendix 10

Soil Geotechnical Test Results



## RESOURCE ENGINEERING

### DIRECT SHEAR ANALYSIS

PROJECT : FRENCH

JOB NO. 275-14

TESTED BY: JBm DATE: 9/16/86

SPRING NO. 4

SAMPLE NO.		R 2	R 3	R 3	R 8		
DEPTH		22'-24'	22'-24'	46'-48'	22'-24'		
SOIL		LT BRN-GRAY CL	LT BRN CL W/ CALCAR-FOUS NODULES	BRN CLAY W/ SILT POCKETS	BN CLAY W/ CALCAR-FOUS NODULES		
START PT.		0	0	345	0		
END PT.		112	212	157	298		
DEGREES DEFLECTION		112	212	172	298		
TORQUE :							
Kg/cm <sup>2</sup>		3.808	7.208	5.848	10.132		

PROJECT: FRENCH JOB NO.: 275-14 TESTED BY: King DATE: 9/16/86

BORING + SAMPLE NO.		R 3		R 3				
DEPTH		46' - 48'		22' - 24'				
SOIL		BRN CL w/ silt pebbles		LT BRN CL w/ small calcare- ous nodules				
CUP #		13		2				
TOTAL SAMPLE + TARE		168.26		171.12				
TOTAL SAMPLE		126.98		129.69				
WEIGHT RETAIN + TARE		44.01		50.15				
WEIGHT RETAIN		2.73		8.72				
TARE		41.28		41.43				
% PASSING # 200		97.9 %		93.3 %				

BORING + SAMPLE NO.		R 2		R 8				
DEPTH		22' - 24'		22' - 24'				
SOIL		LT BRN - GRAY CL		BRN CL w/ small calcareous nodules				
CUP #		19		1				
TOTAL SAMPLE + TARE		210.06		172.53				
TOTAL SAMPLE		168.75		131.16				
WEIGHT RETAIN + TARE		16.74		52.19				
WEIGHT RETAIN		25.43		10.82				
TARE		41.31		41.57				
% PASSING # 200		84.9 %		91.7 %				

BORING + SAMPLE NO.								
DEPTH								
SOIL								
CUP #								
TOTAL SAMPLE + TARE								
TOTAL SAMPLE								
WEIGHT RETAIN + TARE								
WEIGHT RETAIN								
TARE								
% PASSING # 200								

# SIEVE ANALYSIS

PROJECT: FRENCH JOB NUMBER: 275-14  
 SAMPLED BY: \_\_\_\_\_ DATE: \_\_\_\_\_ TESTED BY: Surge DATE: 9/12/86  
 BORING NO.: \_\_\_\_\_ SAMPLE NO.: R 2 DEPTH: 8'-10'

CLASSIFICATION: \_\_\_\_\_

## BEFORE WASHING:

DRY WT. TOTAL SAMPLE + TARE 101.6  
 WT. TARE NO. 9 41.1  
 DRY WT. TOTAL SAMPLE 60.5

## AFTER WASHING ON #200:

DRY WT. WASHED SAMPLE + TARE \_\_\_\_\_  
 WT. TARE NO. \_\_\_\_\_  
 DRY WT. WASHED SAMPLE \_\_\_\_\_  
 WT. WASHED- #200 \_\_\_\_\_  
 PERCENT WASHED- #200 \_\_\_\_\_

	SIEVE SIZE	WEIGHT RETAINED CUMULATIVE	PERCENT RETAINED CUMULATIVE	CUMULATIVE PERCENT FINER		CLASS 2 1½" max	AGGREGATE BASE
	2"					100	
	1½"					90-100	
	1"						100
	¾"					50-85	90-100
	½"						
	¼"						
	4	2.3	3.8	96.2		25-45	35-55
	10	10.0	16.5	83.5			
	<del>20</del> 30	46.0	76.0	24.0			
	<del>40</del>						
	60	55.2	91.2	8.8			
	<del>80</del>						
	100	57.6	95.2	4.8			
	<del>120</del>						
	140	58.9	97.4	2.6			
	<del>170</del>						
	200	59.3	98.0	2.0		2-9	2-9
	PAN	60.2	99.5				
	TOTAL						

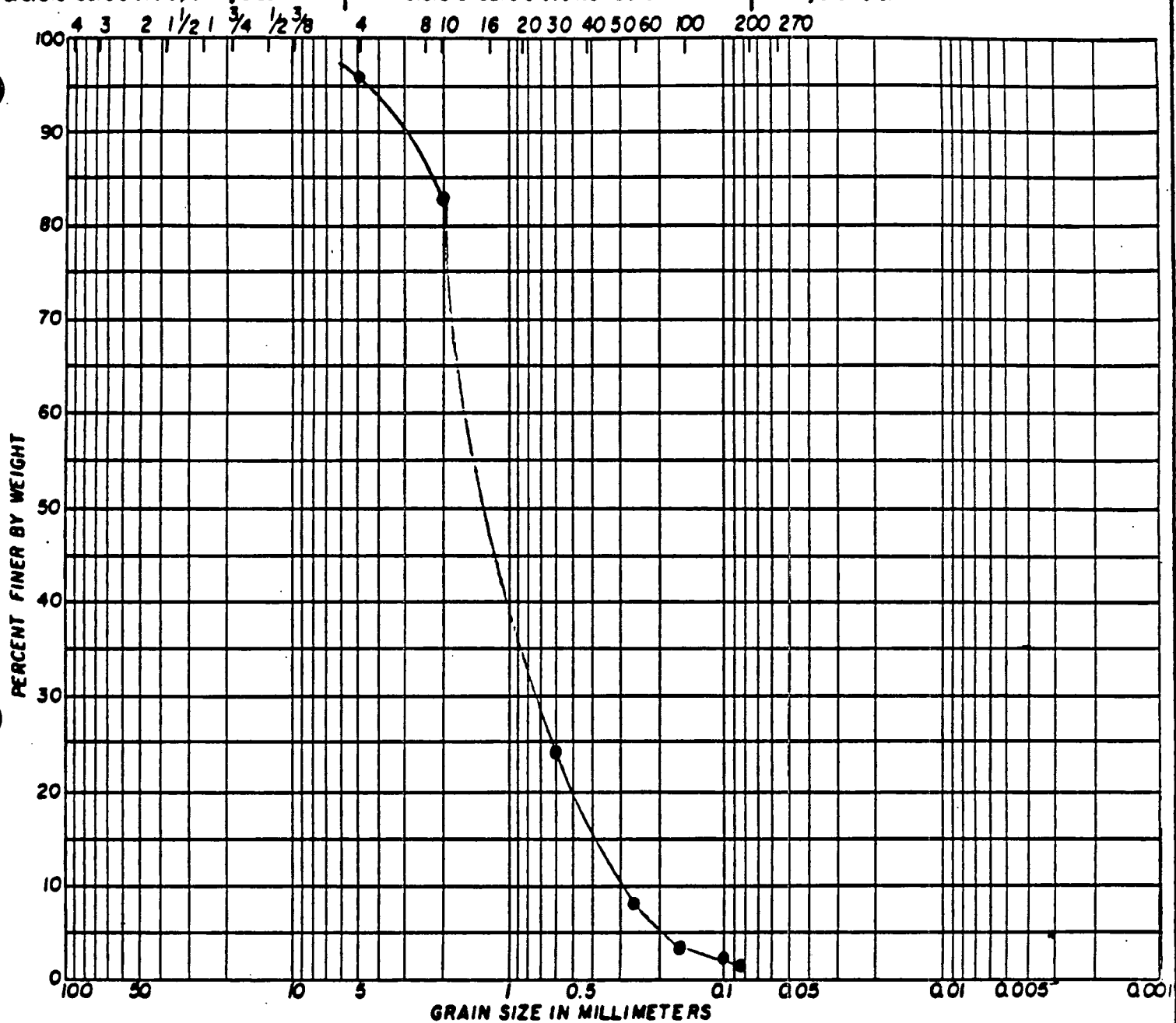


**RESOURCE ENGINEERING INC.**  
 Consulting Engineers

U.S. Standard Sieve Opening Size

U.S. Standard Sieve Numbers

Hydrometer



COBBLES

GRAVEL

SAND

SILT OR CLAY

COARSE

FINE

COARSE

MEDIUM

FINE

Symbol

Sample Source

Classification



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

PARTICLE SIZE ANALYSIS

PLATE

R 2

8'-10'

Job No. \_\_\_\_\_ Appr: \_\_\_\_\_ Date \_\_\_\_\_

# SIEVE ANALYSIS

PROJECT: FRENCH JOB NUMBER: 275-14  
 SAMPLED BY: \_\_\_\_\_ DATE: \_\_\_\_\_ TESTED BY: Sign DATE: 9/12/86  
 BORING NO.: \_\_\_\_\_ SAMPLE NO.: R 2 DEPTH: 10'-12'

CLASSIFICATION: \_\_\_\_\_

## BEFORE WASHING:

DRY WT. TOTAL SAMPLE + TARE 120.0  
 WT. TARE NO. 9 41.1  
 DRY WT. TOTAL SAMPLE 78.9

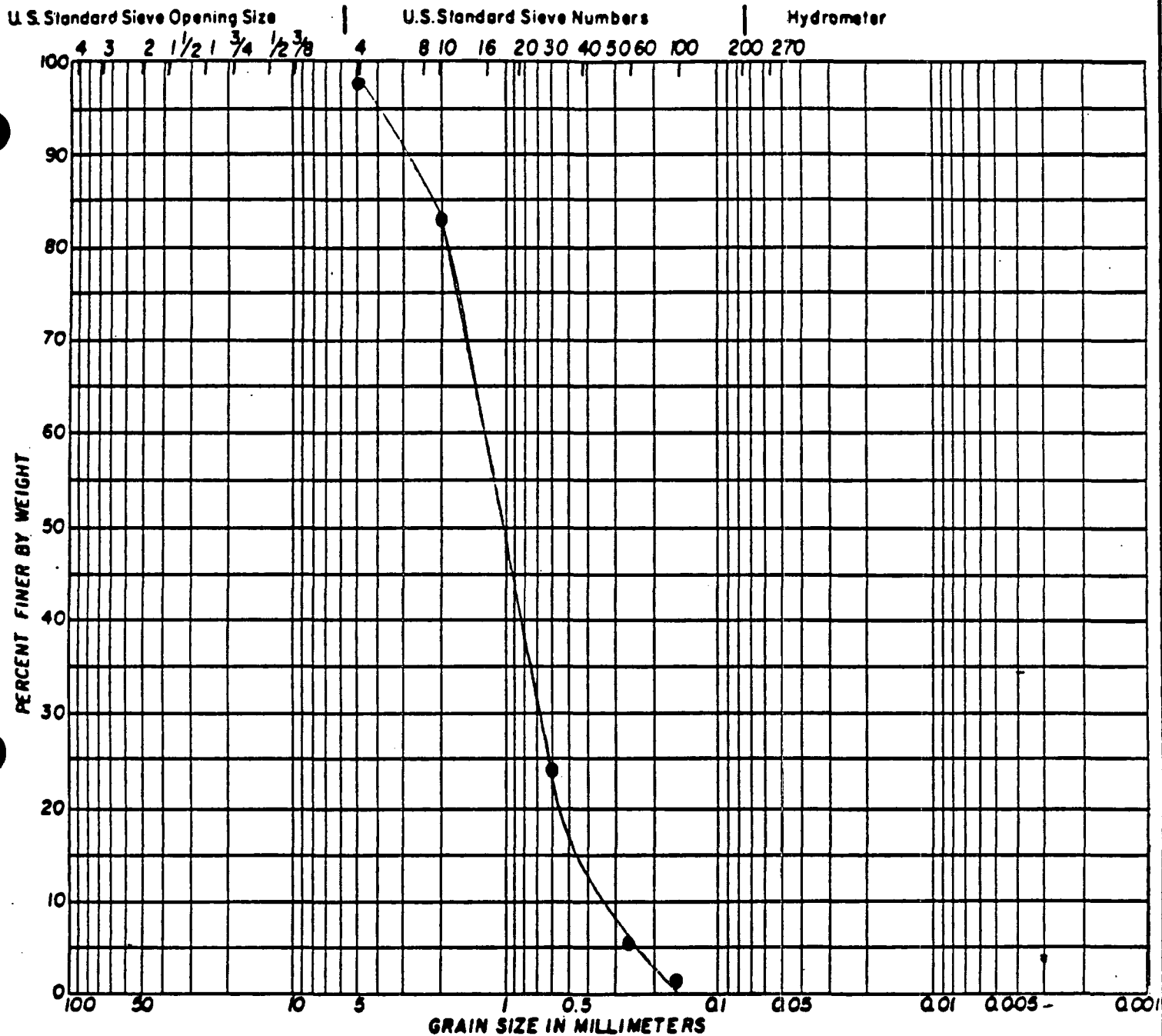
## AFTER WASHING ON #200:

DRY WT. WASHED SAMPLE + TARE \_\_\_\_\_  
 WT. TARE NO. \_\_\_\_\_  
 DRY WT. WASHED SAMPLE \_\_\_\_\_  
 WT. WASHED- #200 \_\_\_\_\_  
 PERCENT WASHED- #200 \_\_\_\_\_

	SIEVE SIZE	WEIGHT RETAINED CUMULATIVE	PERCENT RETAINED CUMULATIVE	CUMULATIVE PERCENT FINER		CLASS 2 1½" max	AGGREGATE BASE
	2"					100	
	1½"					90-100	
	1"						100
	¾"					50-85	90-100
	½"						
	¼"						
	4	2.7	3.4	96.6		25-45	35-55
	10	13.2	16.7	83.3			
	<del>20</del> 30	60.1	76.2	23.8			
	<del>40</del>						
	60	74.9	94.9	5.1			
	<del>80</del>						
	100	77.5	98.2	1.8			
	<del>120</del>						
	140	78.1	98.9	1.1			
	<del>170</del> 200	78.3	99.2	0.8			
	<del>200</del> 230	78.7	99.7	0.3		2-9	2-9
	PAN	78.8	99.9				
	TOTAL						



**RESOURCE ENGINEERING INC.**  
 Consulting Engineers



COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	

Symbol	Sample Source	Classification



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

**PARTICLE SIZE ANALYSIS**

**PLATE**

R 2 10' - 12'

Job No. \_\_\_\_\_ Appr: \_\_\_\_\_ Date \_\_\_\_\_



# Atterberg Limit Determinations

Data & Computation Sheet

Project: FRENCH

Job No.: 275-14

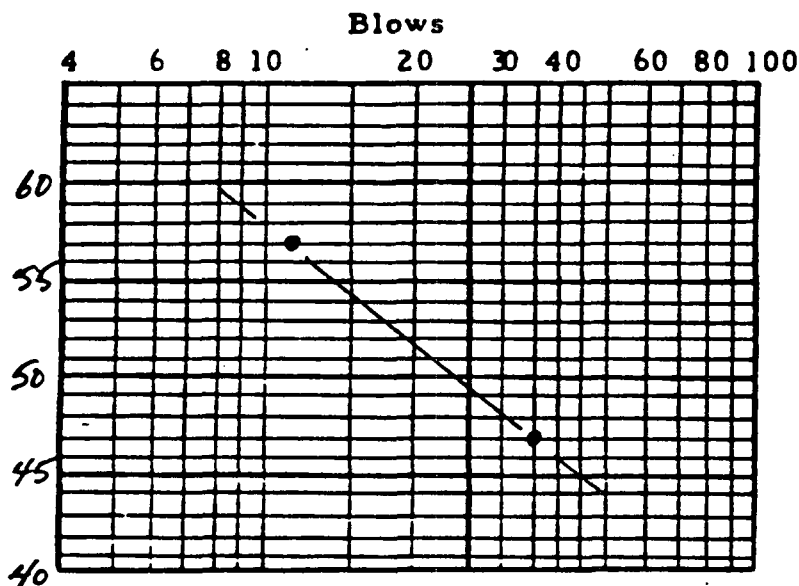
Hole No.: \_\_\_\_\_ Sample: R 2 Depth.: 22' - 24'

Date of Test: 9/12/86 Material: yu-6y SC Apparatus No.: \_\_\_\_\_

Preparation: \_\_\_\_\_ Washed - #40: \_\_\_\_\_ Air-dried \_\_\_\_\_ @Nat. M. C. X

## Determination of Liquid Limit

Dish No.:		1	2			
A	Wt. Wet Sple & Dish, g <sup>(2)</sup>	12.36	13.29			
B	Wt. Dry Sple & Dish, g <sup>(2)</sup>	8.91	9.05			
C	Weight of Dish g <sup>(2)</sup>	1.62	1.61			
D	Dry Wt. Sple = B - C g <sup>(2)</sup>	7.29	7.44			
E	Wt. Moisture = A - B g <sup>(2)</sup>	3.45	4.24			
	% Moisture = 100 E/D <sup>(1)</sup>	47.3	56.9			
	Number of Blows:	35	12			



## Summary:

Liquid Limit = 49.5 %

Plastic Limit = 16.8 %

Plas. Index = 32.7 %

Flow Index = Numerical difference in moisture content for 1 cycle on log plot = \_\_\_\_\_ %

Toughness Index = \_\_\_\_\_

P.I. / F.I. = \_\_\_\_\_ %

## Determination of Plastic Limit

Dish No.						
A	Wt. Wet Sple & Dish, g <sup>(2)</sup>	10.41				
B	Wt. Dry Sple & Dish, g <sup>(2)</sup>	9.15				
C	Weight of Dish g <sup>(2)</sup>	1.63				
D	Dry Wt. Sple = B - C g <sup>(2)</sup>	7.52				
E	Wt. Moisture = A - B g <sup>(2)</sup>	1.26				
	Plastic Limit = 100 E/D <sup>(1)</sup>	16.8				



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

Tested By: J Simpson

Computed By: JS

Checked By: \_\_\_\_\_

# SIEVE ANALYSIS

PROJECT: FRENCH JOB NUMBER: 275-14  
 SAMPLED BY: \_\_\_\_\_ DATE: \_\_\_\_\_ TESTED BY: Smpr DATE: 8/12/86  
 BORING NO.: \_\_\_\_\_ SAMPLE NO.: R 2 DEPTH: 22'-24'

CLASSIFICATION: \_\_\_\_\_

## BEFORE WASHING:

DRY WT. TOTAL SAMPLE + TARE 164.4  
 WT. TARE NO. 1 41.3  
 DRY WT. TOTAL SAMPLE 123.1

## AFTER WASHING ON #200:

DRY WT. WASHED SAMPLE + TARE \_\_\_\_\_  
 WT. TARE NO. \_\_\_\_\_  
 DRY WT. WASHED SAMPLE \_\_\_\_\_  
 WT. WASHED- #200 \_\_\_\_\_  
 PERCENT WASHED- #200 \_\_\_\_\_

	SIEVE SIZE	WEIGHT RETAINED CUMULATIVE	PERCENT RETAINED CUMULATIVE	CUMULATIVE PERCENT FINER		CLASS 2 1½" max	AGGREGATE BASE
	2"					100	
	1½"					90-100	
	1"						100
	¾"					50-85	90-100
	½"						
	¼"						
	4	0	0	100		25-45	35-55
	10	0.4	0.3	99.7			
	<del>20</del> 30	10.0	8.1	91.9			
	<del>40</del>						
	60	51.7	44.9	58.1			
	<del>80</del>						
	100	75.1	61.0	39.0			
	<del>120</del>						
	140	86.4	70.2	29.8			
	<del>170</del> 200	98.1	79.7	20.3			
	<del>200</del> 230	103.4	83.9	16.1		2-9	2-9
	PAN	123.0	99.9				
	TOTAL						

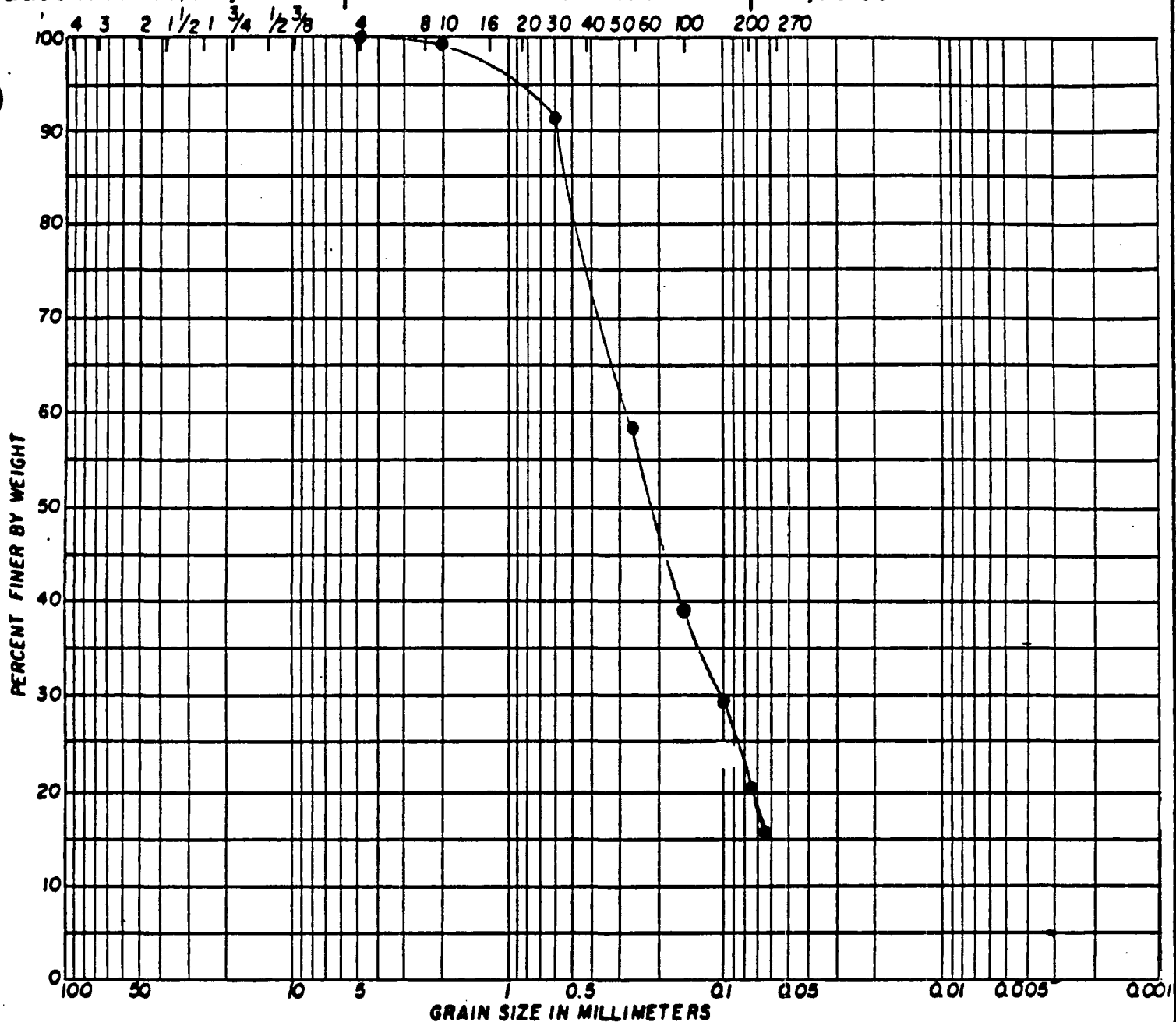


**RESOURCE ENGINEERING INC.**  
 Consulting Engineers

U.S. Standard Sieve Opening Size

U.S. Standard Sieve Numbers

Hydrometer



COBBLES

GRAVEL

SAND

SILT OR CLAY

COARSE

FINE

COARSE

MEDIUM

FINE

Symbol

Sample Source

Classification



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

PARTICLE SIZE ANALYSIS

PLATE

R 2 22' - 24'

Job No. \_\_\_\_\_ Appr: \_\_\_\_\_ Date \_\_\_\_\_

# SIEVE ANALYSIS

PROJECT: FRENCH JOB NUMBER: 275-14  
 SAMPLED BY: \_\_\_\_\_ DATE: \_\_\_\_\_ TESTED BY: Simpson DATE: 9/15/86  
 BORING NO.: \_\_\_\_\_ SAMPLE NO.: R2 DEPTH: 38'-40'

CLASSIFICATION: \_\_\_\_\_

## BEFORE WASHING:

DRY WT. TOTAL SAMPLE + TARE 160.1  
 WT. TARE NO. 8 41.3  
 DRY WT. TOTAL SAMPLE 118.8

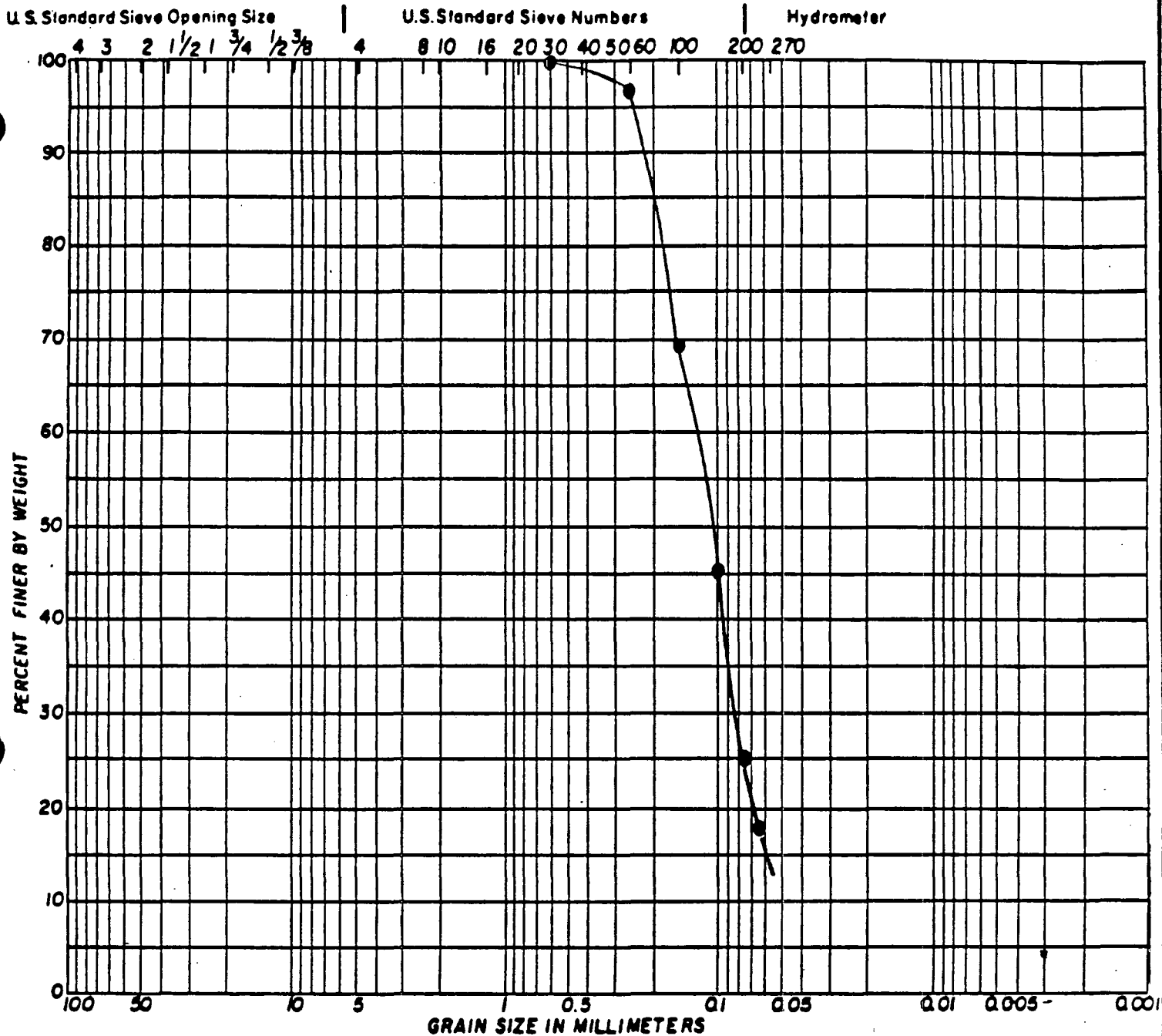
## AFTER WASHING ON #200:

DRY WT. WASHED SAMPLE + TARE \_\_\_\_\_  
 WT. TARE NO. \_\_\_\_\_  
 DRY WT. WASHED SAMPLE \_\_\_\_\_  
 WT. WASHED- #200 \_\_\_\_\_  
 PERCENT WASHED- #200 \_\_\_\_\_

	SIEVE SIZE	WEIGHT RETAINED CUMULATIVE	PERCENT RETAINED CUMULATIVE	CUMULATIVE PERCENT FINER		CLASS 2 1½" max	AGGREGATE BASE
	2"					100	
	1½"					90-100	
	1"						100
	¾"					50-85	90-100
	½"						
	¼"						
	4	0	0	100		25-45	35-55
	10	0	0	100			
	20-30	0	0	100			
	40						
	60	4.1	3.5	96.5			
	80						
	100	36.2	30.5	69.5			
	120						
	140	64.6	54.4	45.6			
	170-200	89.1	75.0	25.0			
	200-230	98.4	82.8	17.2		2-9	2-9
	PAN	118.5	99.7				
	TOTAL						



**RESOURCE ENGINEERING INC.**  
 Consulting Engineers



COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	

Symbol	Sample Source	Classification



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

PARTICLE SIZE ANALYSIS

PLATE

Job No. 275-14 Appr. AS Date 9/15/86

R 2 38'-40'

## SIEVE ANALYSIS

PROJECT: FRENCH JOB NUMBER: 275-14  
 SAMPLED BY: \_\_\_\_\_ DATE: \_\_\_\_\_ TESTED BY: Smiles DATE: 9/15/86  
 BORING NO.: \_\_\_\_\_ SAMPLE NO.: R2 DEPTH: 48' - 50'

CLASSIFICATION: \_\_\_\_\_

## BEFORE WASHING:

DRY WT. TOTAL SAMPLE + TARE 254.6  
 WT. TARE NO. #8 41.3  
 DRY WT. TOTAL SAMPLE 213.3

## AFTER WASHING ON #200:

DRY WT. WASHED SAMPLE + TARE \_\_\_\_\_  
 WT. TARE NO. \_\_\_\_\_  
 DRY WT. WASHED SAMPLE \_\_\_\_\_  
 WT. WASHED- #200 \_\_\_\_\_  
 PERCENT WASHED- #200 \_\_\_\_\_

	SIEVE SIZE	WEIGHT RETAINED CUMULATIVE	PERCENT RETAINED CUMULATIVE	CUMULATIVE PERCENT FINER		CLASS 2 1½" max	AGGREGATE BASE
	2"					100	
	1½"					90-100	
	1"						100
	¾"					50-85	90-100
	½"						
	¼"						
	4					25-45	35-55
	10						
	20						
	<del>40</del> 30	0	0	100			
	60	8.8	4.1	95.8			
	<del>80</del>						
	100	83	38.9	61.1			
	<del>120</del>						
	140	132.9	62.3	37.7			
	<del>170</del> 200	169.7	79.5	20.5			
	<del>200</del> 230	182.2	85.4	14.6		2-9	2-9
	PAN	212.9	99.8				
	TOTAL						

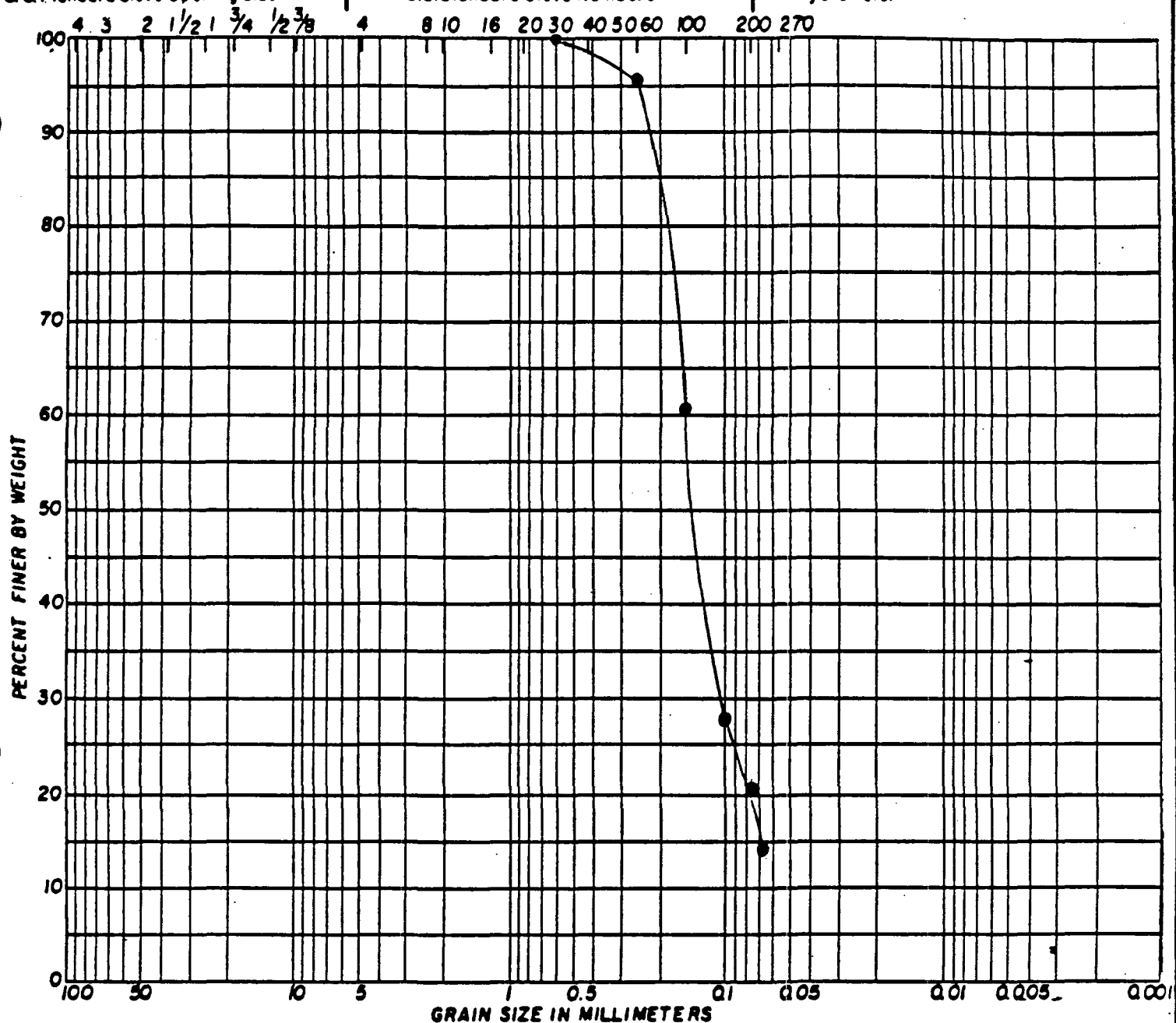


**RESOURCE ENGINEERING INC.**  
 Consulting Engineers

U.S. Standard Sieve Opening Size

U.S. Standard Sieve Numbers

Hydrometer



COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	

Symbol	Sample Source	Classification



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

PARTICLE SIZE ANALYSIS

PLATE

Job No. 275-14 Appr. JS Date 9/15/86

R2 48'-50'

# Atterberg Limit Determinations

Data & Computation Sheet

Project: FRENCH

Job No.: 275-14

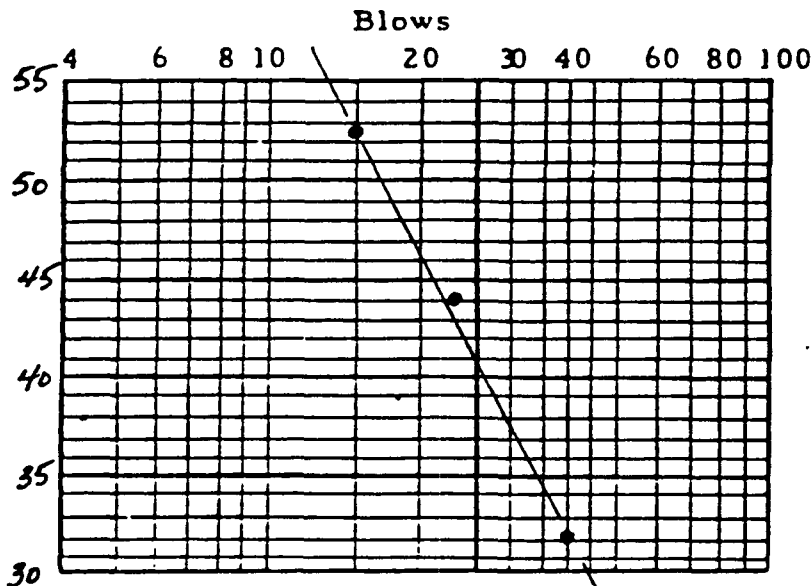
Hole No.: \_\_\_\_\_ Sample: R3 Depth.: 22'-24'

Date of Test: 9/12/86 Material: BRN CL Apparatus No.: \_\_\_\_\_

Preparation: \_\_\_\_\_ Washed - #40: \_\_\_\_\_ Air-dried \_\_\_\_\_ @Nat. M.C. X

## Determination of Liquid Limit

Dish No.:	1	2	3		
A Wt. Wet Sple & Dish, g <sup>(2)</sup>	16.52	18.68	19.78		
B Wt. Dry Sple & Dish, g <sup>(2)</sup>	12.90	13.47	13.53		
C Weight of Dish g <sup>(2)</sup>	1.62	1.63	1.62		
D Dry Wt. Sple = B - C g <sup>(2)</sup>	11.28	11.84	11.91		
E Wt. Moisture = A - B g <sup>(2)</sup>	3.62	5.21	6.25		
% Moisture = 100 E/D <sup>(1)</sup>	32.1	44.0	52.5		
Number of Blows:	40	23	15		



## Summary:

Liquid Limit = 47.0 %

Plastic Limit = 15.7 %

CL Plas. Index = 25.3 %

Flow Index = Numerical difference in moisture content for 1 cycle on log plot = \_\_\_\_\_ %

Toughness Index = \_\_\_\_\_

P.I. / F.I. = \_\_\_\_\_ %

## Determination of Plastic Limit

Dish No.					
A Wt. Wet Sple & Dish, g <sup>(2)</sup>	9.21				
B Wt. Dry Sple & Dish, g <sup>(2)</sup>	8.18				
C Weight of Dish g <sup>(2)</sup>	1.63				
D Dry Wt. Sple = B - C g <sup>(2)</sup>	6.55				
E Wt. Moisture = A - B g <sup>(2)</sup>	1.03				
Plastic Limit = 100 E/D <sup>(1)</sup>	15.7				



RESOURCE ENGINEERING INC.  
Consulting Engineers

Tested By: J. Simpson

Computed By: JB

Checked By: \_\_\_\_\_



# SIEVE ANALYSIS

PROJECT: FRENCH JOB NUMBER: 275-14  
 SAMPLED BY: \_\_\_\_\_ DATE: \_\_\_\_\_ TESTED BY: Jungson DATE: 9/12/86  
 BORING NO.: \_\_\_\_\_ SAMPLE NO.: R 3 DEPTH: 4'-6'

CLASSIFICATION: \_\_\_\_\_

## BEFORE WASHING:

DRY WT. TOTAL SAMPLE + TARE 364.7  
 WT. TARE NO. 1 41.3  
 DRY WT. TOTAL SAMPLE 323.4

## AFTER WASHING ON #200:

DRY WT. WASHED SAMPLE + TARE \_\_\_\_\_  
 WT. TARE NO. \_\_\_\_\_  
 DRY WT. WASHED SAMPLE \_\_\_\_\_  
 WT. WASHED- #200 \_\_\_\_\_  
 PERCENT WASHED- #200 \_\_\_\_\_

	SIEVE SIZE	WEIGHT RETAINED CUMULATIVE	PERCENT RETAINED CUMULATIVE	CUMULATIVE PERCENT FINER		CLASS 2 1½" max	AGGREGATE BASE
	2"					100	
	1½"					90-100	
	1"						100
	¾"					50-85	90-100
	½"						
	¼"						
	4	0	0	100		25-45	35-55
	10	3.3	1.0	99.0			
	<del>20</del> 30	20.4	6.3	93.7			
	<del>40</del>						
	60	202.3	62.6	37.4			
	<del>80</del>						
	100	276.8	85.6	14.4			
	<del>120</del>						
	140	298.7	92.4	7.6			
	<del>170</del> 200	309.0	95.5	4.5			
	<del>200</del> 250	311.7	96.4	3.6		2-9	2-9
	PAN	322.8	99.				
	TOTAL						

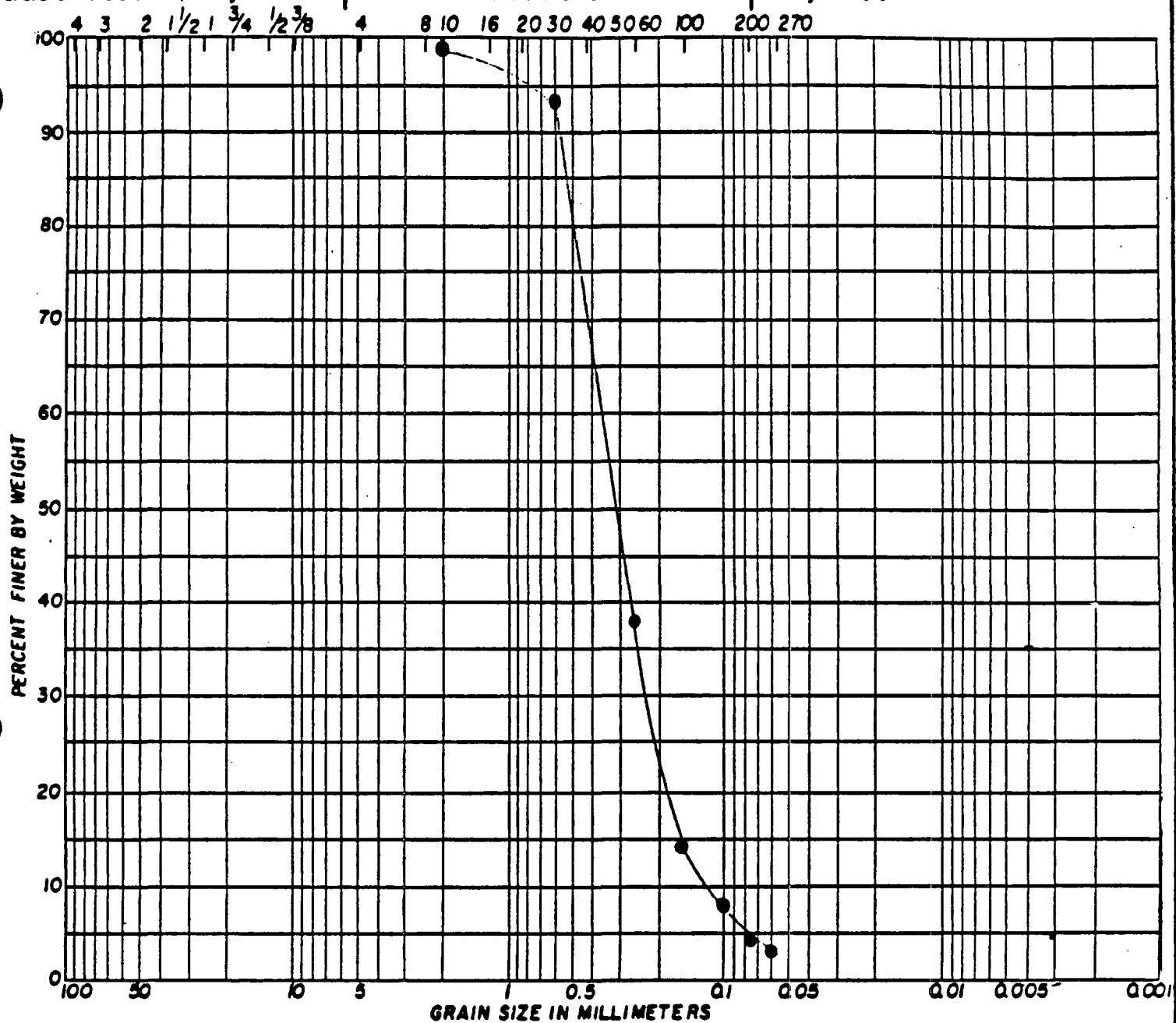


**RESOURCE ENGINEERING INC.**  
 Consulting Engineers

U.S. Standard Sieve Opening Size

U.S. Standard Sieve Numbers

Hydrometer



COBBLES

GRAVEL

SAND

SILT OR CLAY

COARSE

FINE

COARSE

MEDIUM

FINE

Symbol

Sample Source

Classification



RESOURCE ENGINEERING INC.

Consulting Engineers

PARTICLE SIZE ANALYSIS

PLATE

R 3 4'-6'

Job No. \_\_\_\_\_ Appr. \_\_\_\_\_ Date \_\_\_\_\_

## SIEVE ANALYSIS

PROJECT: FRENCH JOB NUMBER: 275-14  
 SAMPLED BY: \_\_\_\_\_ DATE: \_\_\_\_\_ TESTED BY: J. Simpson DATE: 9/12/86  
 BORING NO.: \_\_\_\_\_ SAMPLE NO.: R 3 DEPTH: 14'-16'

CLASSIFICATION: \_\_\_\_\_

## BEFORE WASHING:

DRY WT. TOTAL SAMPLE + TARE 327.8  
 WT. TARE NO. 9 41.1  
 DRY WT. TOTAL SAMPLE 286.7

## AFTER WASHING ON #200:

DRY WT. WASHED SAMPLE + TARE \_\_\_\_\_  
 WT. TARE NO. \_\_\_\_\_  
 DRY WT. WASHED SAMPLE \_\_\_\_\_  
 WT. WASHED- #200 \_\_\_\_\_  
 PERCENT WASHED- #200 \_\_\_\_\_

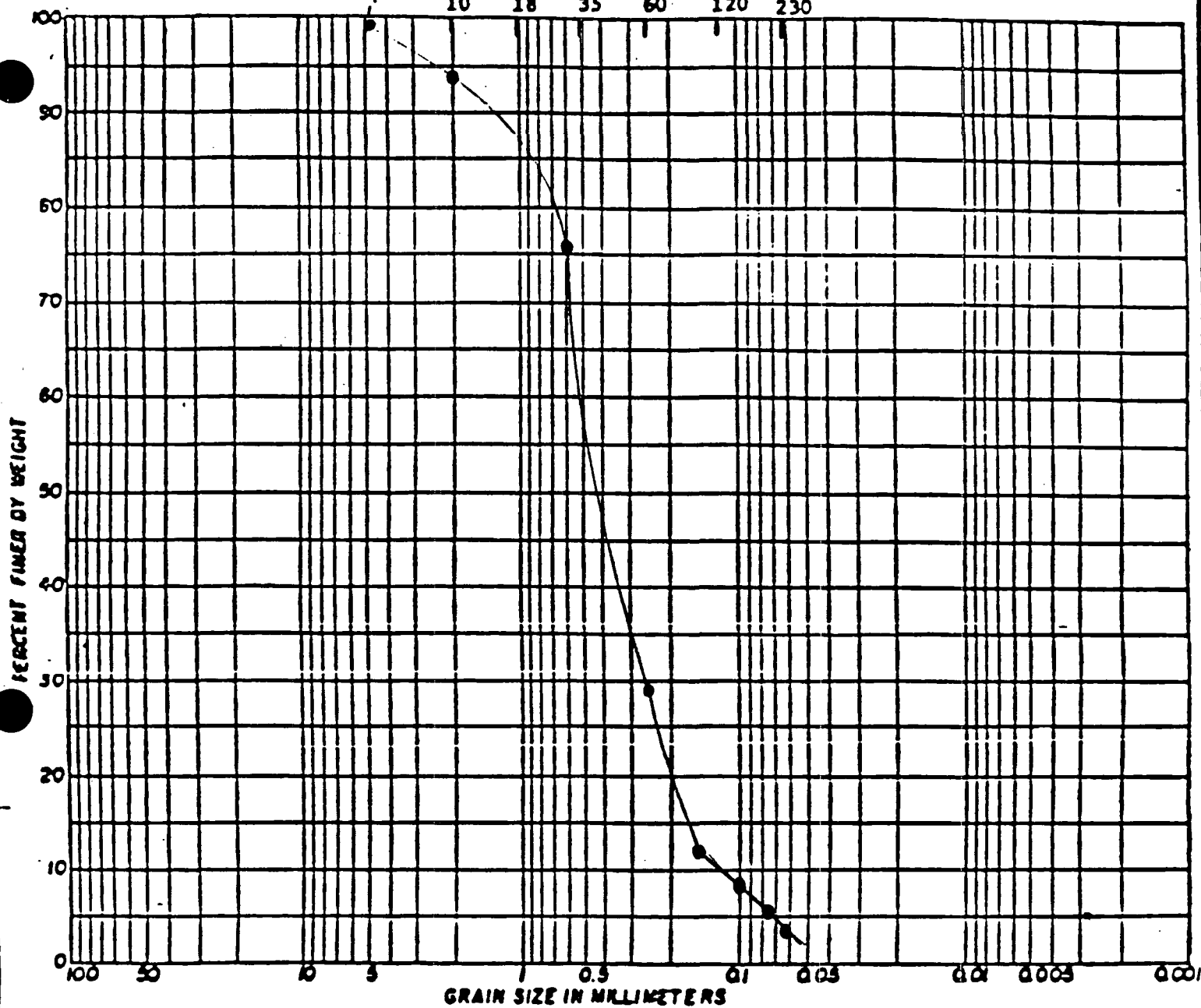
	SIEVE SIZE	WEIGHT RETAINED CUMULATIVE	PERCENT RETAINED CUMULATIVE	CUMULATIVE PERCENT FINER		CLASS 2 1½" max	AGGREGATE BASE
	2"					100	
	1½"					90-100	
	1"						100
	¾"					50-85	90-100
	½"						
	¼"						
	4	5.5	1.9	98.1		25-45	35-55
	10	16.1	5.6	94.4			
	<del>30</del>	69.4	24.2	75.7			
	40						
	60	203.0	70.8	29.2			
	80						
	100	250.2	87.3	12.7			
	120						
	140	263.6	91.9	8.1			
	170						
	200	270.2	94.2	5.8		2-9	2-9
	<del>230 PAN</del>	273.5	95.4	4.6			
	TOTAL	286.5	99.9				



**RESOURCE ENGINEERING INC.**  
 Consulting Engineers

U.S. Standard Sieve Numbers

10 18 35 60 120 230



GRAIN SIZE IN MILLIMETERS

COBBLES	VC	C	M	F	VF	VC	C	M	F	VF	C	M	F	VF	C	M


Symbol	Sample Source	Classification
	R 3 14'-16'	



RESOURCE ENGINEERING INC.  
Consulting Engineers

PARTICLE SIZE ANALYSIS

PLATE

Job No. 275-14 Appr. *[Signature]* Date 9/12/86

# Atterberg Limit Determinations

Data & Computation Sheet

Project: FRENCH

Job No.: 275-14

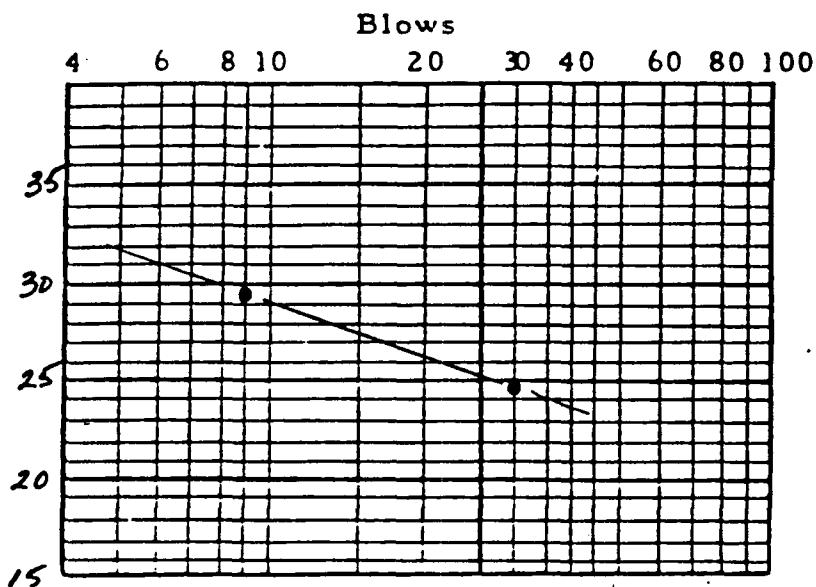
Hole No.: \_\_\_\_\_ Sample: R3 Depth.: 34'-36'

Date of Test: 9/15/86 Material: GRAY SL Apparatus No.: \_\_\_\_\_

Preparation: \_\_\_\_\_ Washed - #40: \_\_\_\_\_ Air-dried \_\_\_\_\_ @Nat. M.C. X

## Determination of Liquid Limit

Dish No.:	1	2			
A Wt. Wet Sple & Dish, g <sup>(2)</sup>	17.65	23.27			
B Wt. Dry Sple & Dish, g <sup>(2)</sup>	14.00	18.99			
C Weight of Dish g <sup>(2)</sup>	1.61	1.61			
D Dry Wt. Sple = B - C g <sup>(2)</sup>	12.39	17.38			
E Wt. Moisture = A - B g <sup>(2)</sup>	3.65	4.28			
% Moisture = 100 E/D <sup>(1)</sup>	29.5	24.6			
Number of Blows:	9	30			



## Summary:

Liquid Limit = 25.2 %

Plastic Limit = 13.9 %

Plas. Index = 11.3 %

Flow Index = Numerical difference in moisture content for 1 cycle on log plot = \_\_\_\_\_ %

Toughness Index = \_\_\_\_\_  
P.I. / F.I. = \_\_\_\_\_ %

## Determination of Plastic Limit

Dish No.					
A Wt. Wet Sple & Dish, g <sup>(2)</sup>	11.0				
B Wt. Dry Sple & Dish, g <sup>(2)</sup>	7.85				
C Weight of Dish g <sup>(2)</sup>	1.62				
D Dry Wt. Sple = B - C g <sup>(2)</sup>	9.23				
E Wt. Moisture = A - B g <sup>(2)</sup>	1.15				
Plastic Limit = 100 E/D <sup>(1)</sup>	13.9				



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

Tested By: J. Simpson

Computed By: JS

Checked By: \_\_\_\_\_

## SIEVE ANALYSIS

PROJECT: FRENCH JOB NUMBER: 275-14  
 SAMPLED BY: \_\_\_\_\_ DATE: \_\_\_\_\_ TESTED BY: Simpson DATE: 9/15/86  
 BORING NO.: \_\_\_\_\_ SAMPLE NO.: R 3 DEPTH: 34' - 36'

CLASSIFICATION: \_\_\_\_\_

## BEFORE WASHING:

DRY WT. TOTAL SAMPLE + TARE 119.8  
 WT. TARE NO. 8 41.3  
 DRY WT. TOTAL SAMPLE 78.5

## AFTER WASHING ON #200:

DRY WT. WASHED SAMPLE + TARE \_\_\_\_\_  
 WT. TARE NO. \_\_\_\_\_  
 DRY WT. WASHED SAMPLE \_\_\_\_\_  
 WT. WASHED- #200 \_\_\_\_\_  
 PERCENT WASHED- #200 \_\_\_\_\_

	SIEVE SIZE	WEIGHT RETAINED CUMULATIVE	PERCENT RETAINED CUMULATIVE	CUMULATIVE PERCENT FINER		CLASS 2 1½" max	AGGREGATE BASE
	2"					100	
	1½"					90-100	
	1"						100
	¾"					50-85	90-100
	½"						
	¼"						
	4	0	0	100		25-45	35-55
	10	0	0	100			
	<del>20-30</del>	0.6	0.8	99.2			
	<del>40</del>						
	60	6.9	8.8	91.2			
	<del>80</del>						
	100	10.2	12.9	87.1			
	<del>120</del>						
	140	24.6	31.3	68.7			
	<del>170-200</del>	41.4	52.7	47.3			
	<del>200-230</del>	50.8	64.7	35.3		2-9	2-9
	PAN	78.2	99.				
	TOTAL						

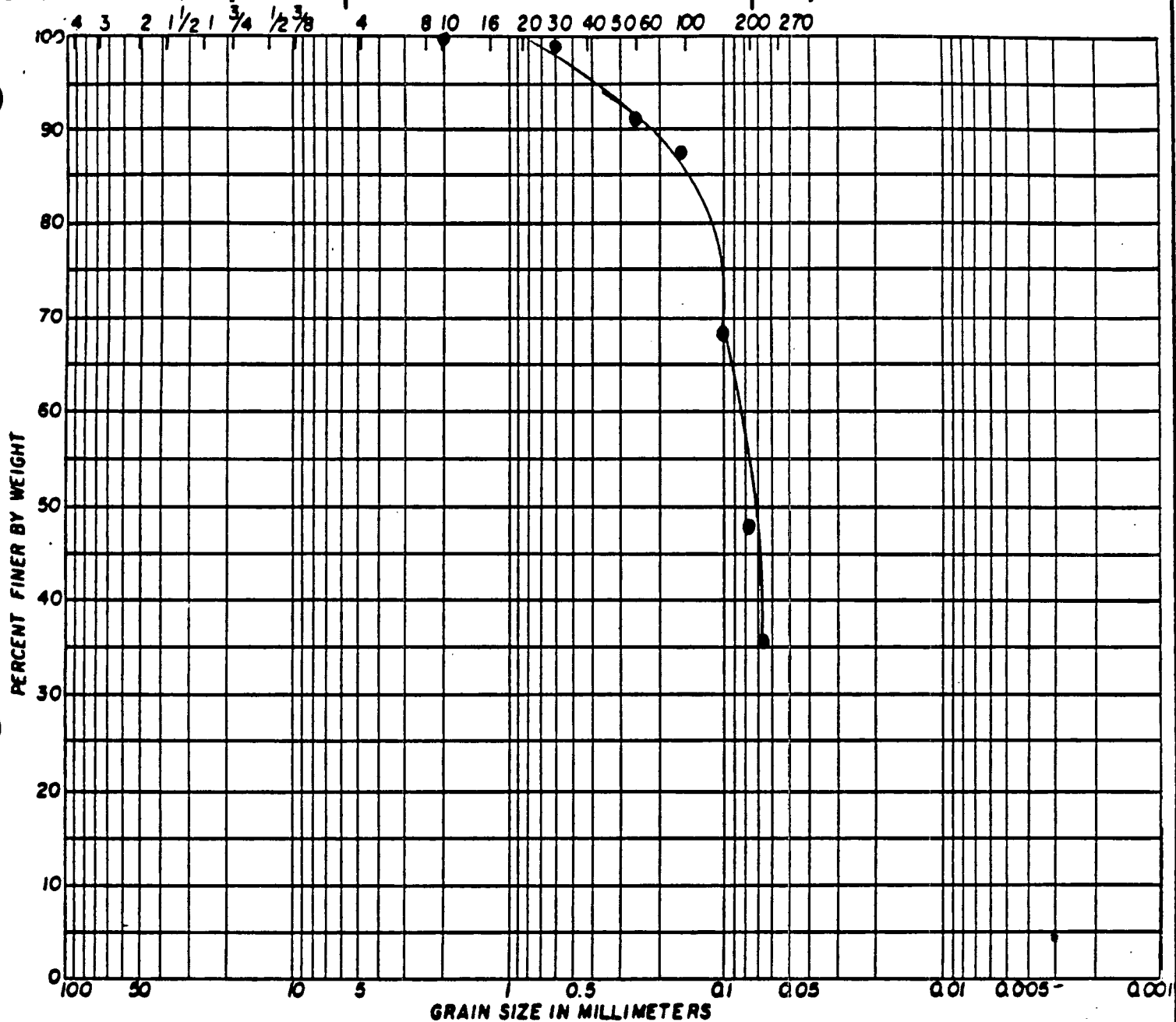


**RESOURCE ENGINEERING INC.**  
 Consulting Engineers

U.S. Standard Sieve Opening Size

U.S. Standard Sieve Numbers

Hydrometer



COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	

Symbol	Sample Source	Classification



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

PARTICLE SIZE ANALYSIS

PLATE

Job No. 275-14 Appr. JS Date 9/15/86

R 3 34'-36'

# Atterberg Limit Determinations

Data & Computation Sheet

Project: FRENCH

Job No.: 275-14

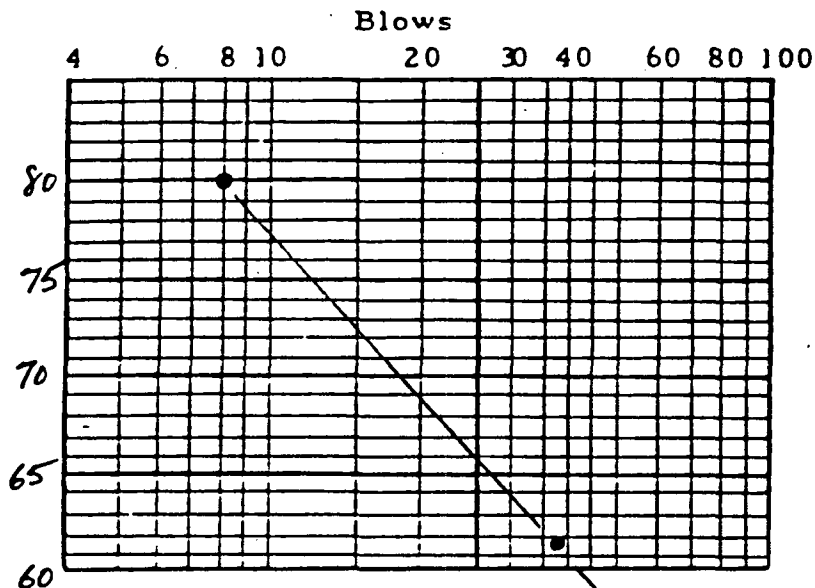
Hole No.: \_\_\_\_\_ Sample: R3 Depth.: 46' - 48'

Date of Test: 9/15/86 Material: BROWN CL Apparatus No.: \_\_\_\_\_

Preparation: \_\_\_\_\_ Washed - #40: \_\_\_\_\_ Air-dried \_\_\_\_\_ @Nat. M. C. X

## Determination of Liquid Limit

Dish No.:	1	2			
A Wt. Wet Sple & Dish, g <sup>(2)</sup>	11.12	11.94			
B Wt. Dry Sple & Dish, g <sup>(2)</sup>	7.49	7.36			
C Weight of Dish g <sup>(2)</sup>	1.61	1.63			
D Dry Wt. Sple = B - C g <sup>(2)</sup>	5.88	5.73			
E Wt. Moisture = A - B g <sup>(2)</sup>	3.63	4.58			
% Moisture = 100 E/D(1)	61.7	79.9			
Number of Blows:	38	8			



## Summary:

Liquid Limit = 66.0 %

Plastic Limit = 27.4 %

Plas. Index = 38.6 %

Flow Index = Numerical difference in moisture content for 1 cycle on log plot = \_\_\_\_\_ %

Toughness Index = \_\_\_\_\_  
P.I. / F.I. = \_\_\_\_\_ %

## Determination of Plastic Limit

Dish No.					
A Wt. Wet Sple & Dish, g <sup>(2)</sup>	7.46				
B Wt. Dry Sple & Dish, g <sup>(2)</sup>	6.21				
C Weight of Dish g <sup>(2)</sup>	1.64				
D Dry Wt. Sple = B - C g <sup>(2)</sup>	4.57				
E Wt. Moisture = A - B g <sup>(2)</sup>	1.25				
Plastic Limit = 100 E/D(1)	27.4				



**RESOURCE ENGINEERING INC.**

Consulting Engineers

Tested By: [Signature]

Computed By: [Signature]

Checked By: \_\_\_\_\_



## SIEVE ANALYSIS

PROJECT: FRENCH JOB NUMBER: 275-14  
 SAMPLED BY: \_\_\_\_\_ DATE: \_\_\_\_\_ TESTED BY: Simpson DATE: 9/12/86  
 BORING NO.: \_\_\_\_\_ SAMPLE NO.: R 8 DEPTH: 4'-6'  
 CLASSIFICATION: \_\_\_\_\_

## BEFORE WASHING:

DRY WT. TOTAL SAMPLE + TARE 249.0  
 WT. TARE NO. 9 41.1  
 DRY WT. TOTAL SAMPLE 207.9

## AFTER WASHING ON #200:

DRY WT. WASHED SAMPLE + TARE \_\_\_\_\_  
 WT. TARE NO. \_\_\_\_\_  
 DRY WT. WASHED SAMPLE \_\_\_\_\_  
 WT. WASHED- #200 \_\_\_\_\_  
 PERCENT WASHED- #200 \_\_\_\_\_

	SIEVE SIZE	WEIGHT RETAINED CUMULATIVE	PERCENT RETAINED CUMULATIVE	CUMULATIVE PERCENT FINER		CLASS 2 1½" max	AGGREGATE BASE
	2"					100	
	1½"					90-100	
	1"						100
	¾"					50-85	90-100
	½"						
	¼"						
	4	0	0	100		25-45	35-55
	10	0.1	0.05	99.9			
	<del>20</del> 30	7.4	3.6	96.4			
	<del>40</del>						
	60	84.9	40.8	59.2			
	<del>80</del>						
	100	151.0	72.6	27.4			
	<del>120</del>						
	140	168.8	81.2	18.8			
	<del>170</del> 200	182.7	87.9	12.1			
	<del>200</del> 230	187.6	90.2	9.8		2-9	2-9
	PAN	207.6	99.9				
	TOTAL						

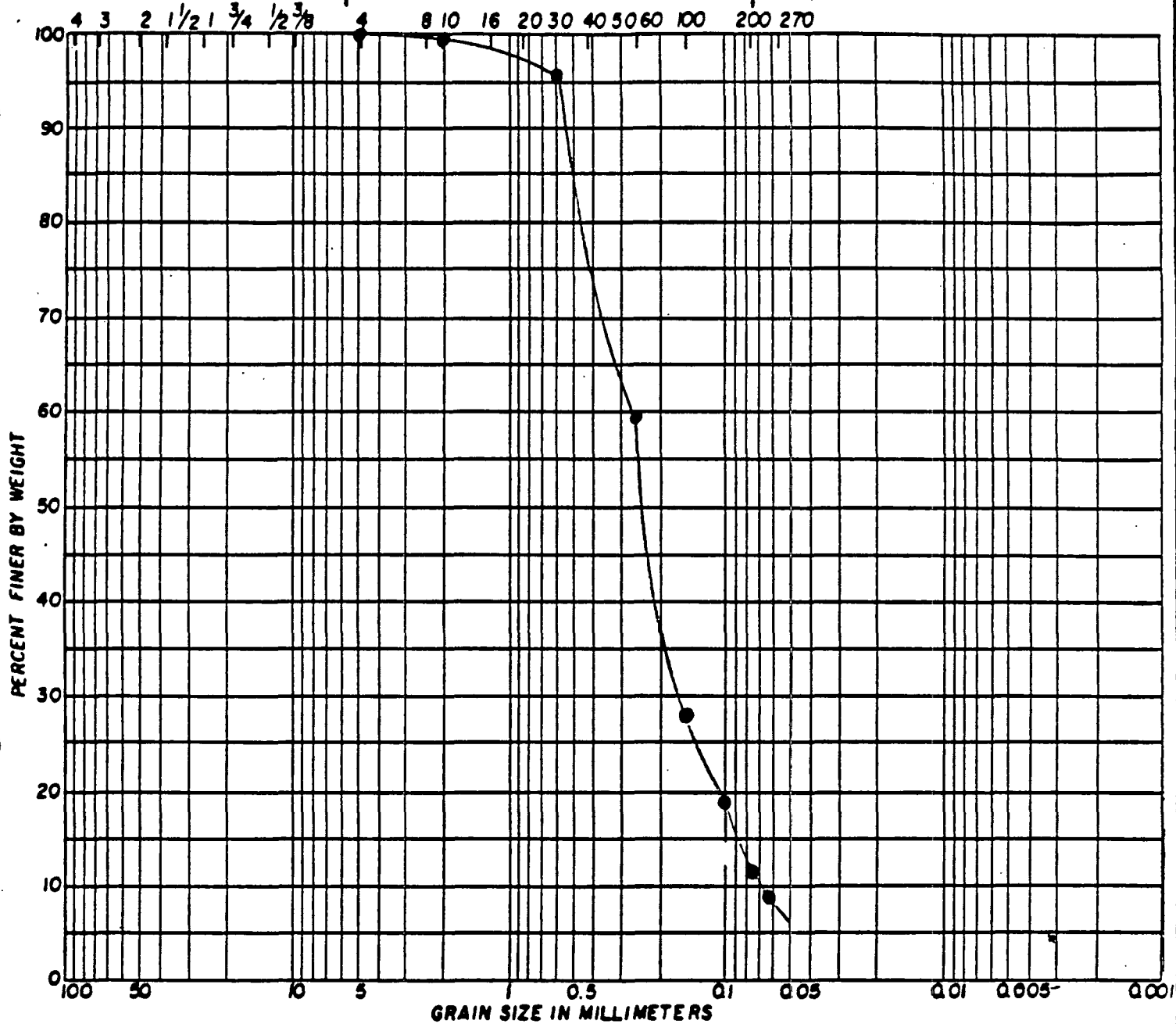


**RESOURCE ENGINEERING INC.**  
 Consulting Engineers

U.S. Standard Sieve Opening Size

U.S. Standard Sieve Numbers

Hydrometer



COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
Symbol	Sample Source				Classification	
<b>REI RESOURCE ENGINEERING INC.</b> Consulting Engineers						<b>PARTICLE SIZE ANALYSIS</b> <i>R 8 4'-6'</i>
Job No. _____ Appr: _____ Date _____						PLATE

# Atterberg Limit Determinations

Data & Computation Sheet

Project: FRENCH

Job No.: 275-14

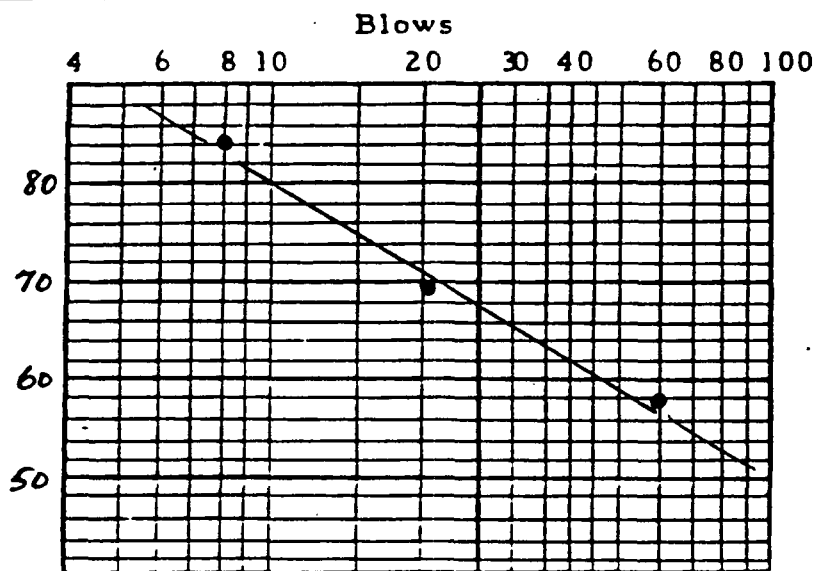
Hole No.: \_\_\_\_\_ Sample: R8 Depth.: 16'-18'

Date of Test: 9/15/86 Material: BR CL Apparatus No.: \_\_\_\_\_

Preparation: \_\_\_\_\_ Washed - #40: \_\_\_\_\_ Air-dried \_\_\_\_\_ @Nat. M. C. X

## Determination of Liquid Limit

Dish No.:	1	2	3		
A Wt. Wet Sple & Dish, g <sup>(2)</sup>	12.83	12.48	12.04		
B Wt. Dry Sple & Dish, g <sup>(2)</sup>	8.73	8.02	7.25		
C Weight of Dish g <sup>(2)</sup>	1.64	1.63	1.63		
D Dry Wt. Sple = B - C g <sup>(2)</sup>	7.09	6.39	5.62		
E Wt. Moisture = A - B g <sup>(2)</sup>	4.1	4.46	4.79		
% Moisture = 100 E/D <sup>(1)</sup>	57.8	69.8	85.2		
Number of Blows:	60	21	8		



## Summary:

Liquid Limit = 68.0 %

Plastic Limit = 30.8 %

Plas. Index = 37.2 %

Flow Index = Numerical difference in moisture content for 1 cycle on log plot = \_\_\_\_\_ %

Toughness Index = \_\_\_\_\_  
P.I. / F.I. = \_\_\_\_\_ %

## Determination of Plastic Limit

Dish No.					
A Wt. Wet Sple & Dish, g <sup>(2)</sup>	6.80				
B Wt. Dry Sple & Dish, g <sup>(2)</sup>	5.58				
C Weight of Dish g <sup>(2)</sup>	1.63				
D Dry Wt. Sple = B - C g <sup>(2)</sup>	3.95				
E Wt. Moisture = A - B g <sup>(2)</sup>	1.22				
Plastic Limit = 100 E/D <sup>(1)</sup>	30.8				



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

Tested By: [Signature]

Computed By: [Signature]

Checked By: \_\_\_\_\_

# Atterberg Limit Determinations

Data & Computation Sheet

Project: FRENCH

Job No.: 275-14

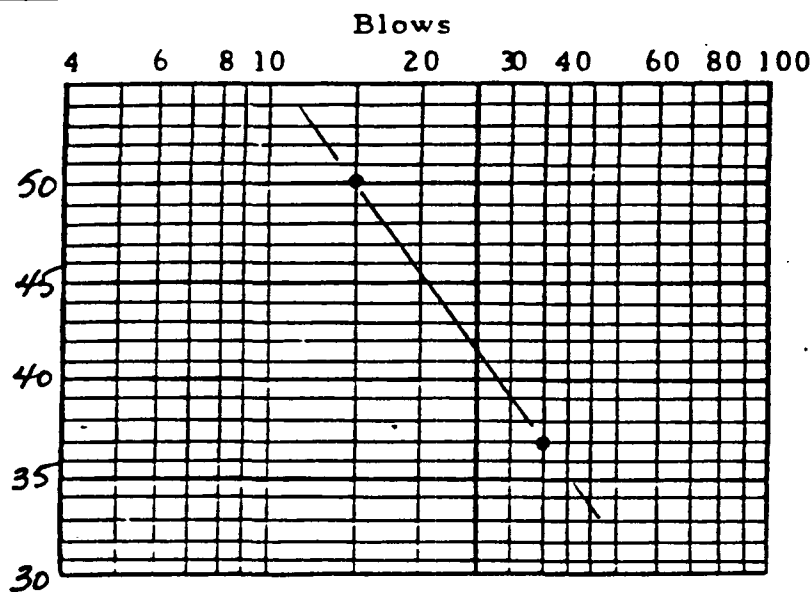
Hole No.: \_\_\_\_\_ Sample: R8 Depth.: 22'-24'

Date of Test: 9/12/86 Material: BH CL Apparatus No.: \_\_\_\_\_

Preparation: \_\_\_\_\_ Washed - #40: \_\_\_\_\_ Air-dried \_\_\_\_\_ @Nat. M.C. X

## Determination of Liquid Limit

Dish No.:		1	2			
A	Wt. Wet Sple & Dish, g <sup>(2)</sup>	17.73	18.31			
B	Wt. Dry Sple & Dish, g <sup>(2)</sup>	12.56	13.81			
C	Weight of Dish g <sup>(2)</sup>	1.63	1.62			
D	Dry Wt. Sple = B - C g <sup>(2)</sup>	10.73	12.19			
E	Wt. Moisture = A - B g <sup>(2)</sup>	5.57	4.5			
	% Moisture = 100 E/D <sup>(1)</sup>	50.04	36.9			
	Number of Blows:	15	35			



## Summary:

Liquid Limit = 41.5 %

Plastic Limit = 15.2 %

Plas. Index = 26.3 %

Flow Index = Numerical difference in moisture content for 1 cycle on log plot = \_\_\_\_\_ %

Toughness Index = \_\_\_\_\_  
P.I. / F.I. = \_\_\_\_\_ %

## Determination of Plastic Limit

Dish No.					
A	Wt. Wet Sple & Dish, g <sup>(2)</sup>	9.42			
B	Wt. Dry Sple & Dish, g <sup>(2)</sup>	8.40			
C	Weight of Dish g <sup>(2)</sup>	1.64			
D	Dry Wt. Sple = B - C g <sup>(2)</sup>	6.72			
E	Wt. Moisture = A - B g <sup>(2)</sup>	1.02			
	Plastic Limit = 100 E/D <sup>(1)</sup>	15.2			



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

Tested By: J Simpson

Computed By: JB

Checked By: \_\_\_\_\_

# Atterberg Limit Determinations

Data & Computation Sheet

Project: FRENCH

Job No.: 275-14

Hole No.: R 8

Sample: \_\_\_\_\_

Depth.: 40'-42'

Date of Test: 7/12/86

Material: GRAY - BRN SM

Apparatus No.: \_\_\_\_\_

Preparation: \_\_\_\_\_

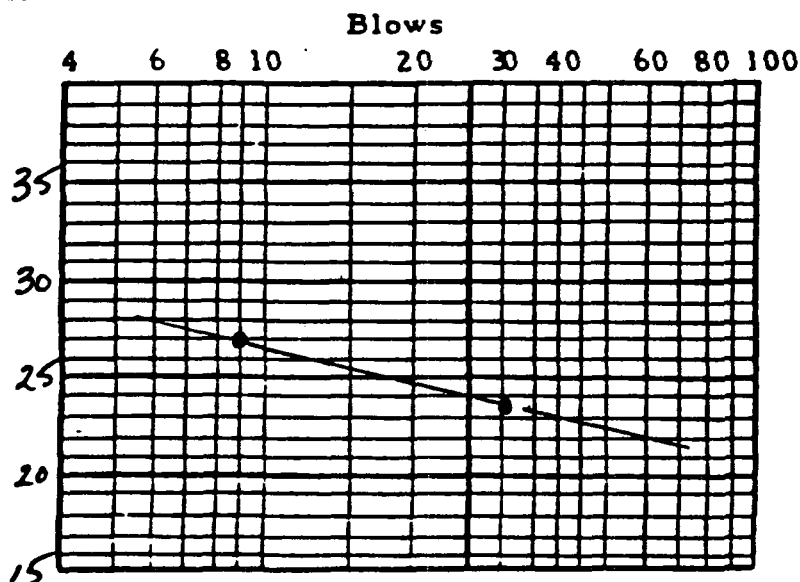
Washed - #40: \_\_\_\_\_

Air-dried \_\_\_\_\_

@Nat. M.C. X

## Determination of Liquid Limit

Dish No.:		1	2		
A	Wt. Wet Sple & Dish, g <sup>(2)</sup>	14.53	20.82		
B	Wt. Dry Sple & Dish, g <sup>(2)</sup>	11.87	17.16		
C	Weight of Dish g <sup>(2)</sup>	1.60	1.60		
D	Dry Wt. Sple = B - C g <sup>(2)</sup>	10.27	15.56		
E	Wt. Moisture = A - B g <sup>(2)</sup>	2.66	3.66		
	% Moisture = 100 E/D <sup>(1)</sup>	25.9	23.5		
	Number of Blows:	9	31		



## Summary:

Liquid Limit = 24.0 %

Plastic Limit = 15.7 %

Plas. Index = 8.3 %

Flow Index = Numerical difference in moisture content for 1 cycle on log plot = \_\_\_\_\_ %

Toughness Index = \_\_\_\_\_

P.I. / F.I. = \_\_\_\_\_ %

## Determination of Plastic Limit

Dish No.					
A	Wt. Wet Sple & Dish, g <sup>(2)</sup>	7.04			
B	Wt. Dry Sple & Dish, g <sup>(2)</sup>	6.30			
C	Weight of Dish g <sup>(2)</sup>	1.61			
D	Dry Wt. Sple = B - C g <sup>(2)</sup>	4.69			
E	Wt. Moisture = A - B g <sup>(2)</sup>	.74			
	Plastic Limit = 100 E/D <sup>(1)</sup>	15.7			



**RESOURCE ENGINEERING INC.**

Consulting Engineers

Tested By: J. Simpson

Computed By: JS

Checked By: \_\_\_\_\_

## SIEVE ANALYSIS

PROJECT: FRENCH JOB NUMBER: 275-14  
 SAMPLED BY: \_\_\_\_\_ DATE: \_\_\_\_\_ TESTED BY: Simpson DATE: 9/12/86  
 BORING NO.: \_\_\_\_\_ SAMPLE NO.: R 8 DEPTH: 40' - 42'

CLASSIFICATION: \_\_\_\_\_

## BEFORE WASHING:

DRY WT. TOTAL SAMPLE + TARE 275.1  
 WT. TARE NO. 9 41.1  
 DRY WT. TOTAL SAMPLE 234.0

## AFTER WASHING ON #200:

DRY WT. WASHED SAMPLE + TARE \_\_\_\_\_  
 WT. TARE NO. \_\_\_\_\_  
 DRY WT. WASHED SAMPLE \_\_\_\_\_  
 WT. WASHED- #200 \_\_\_\_\_  
 PERCENT WASHED- #200 \_\_\_\_\_

	SIEVE SIZE	WEIGHT RETAINED CUMULATIVE	PERCENT RETAINED CUMULATIVE	CUMULATIVE PERCENT FINER		CLASS 2 1½" max	AGGREGATE BASE
	2"					100	
	1½"					90-100	
	1"						100
	¾"					50-85	90-100
	½"						
	¼"						
	4					25-45	35-55
	10	0.8	0.3	99.7			
	<del>20</del> 30	10.7	4.6	93.4			
	<del>40</del>						
	60	48.2	20.6	79.4			
	<del>80</del>						
	100	72.0	30.8	69.2			
	<del>120</del>						
	140	109.0	46.6	53.4			
	<del>170</del> 200	152.0	64.9	35.1			
	<del>200</del> 230	167.8	71.7	28.3		2-9	2-9
	PAN	233.2	99.6				
	TOTAL						

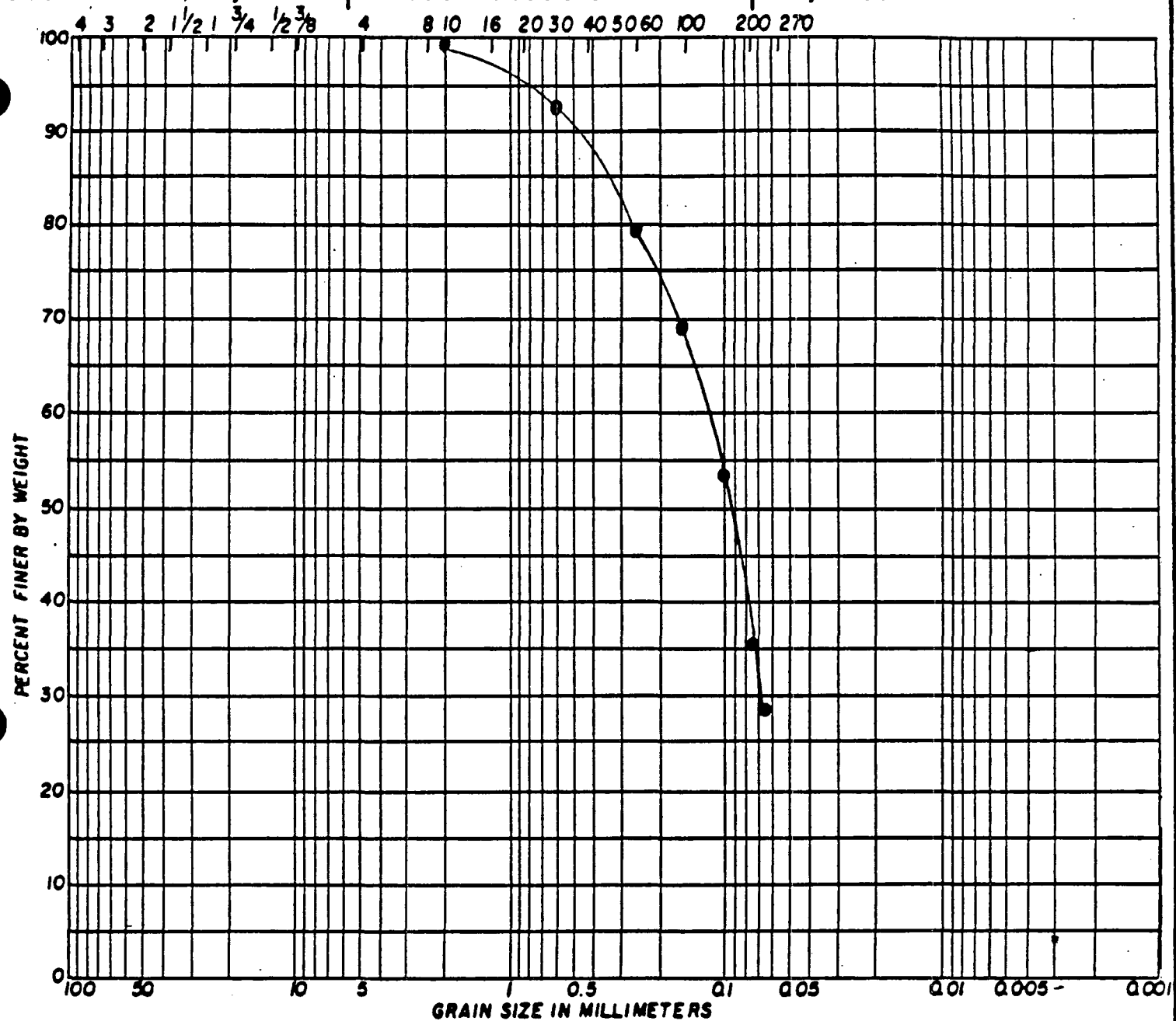


**RESOURCE ENGINEERING INC.**  
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U.S. Standard Sieve Opening Size

U.S. Standard Sieve Numbers

Hydrometer



COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	

Symbol	Sample Source	Classification



**RESOURCE ENGINEERING INC.**  
Consulting Engineers

PARTICLE SIZE ANALYSIS

PLATE

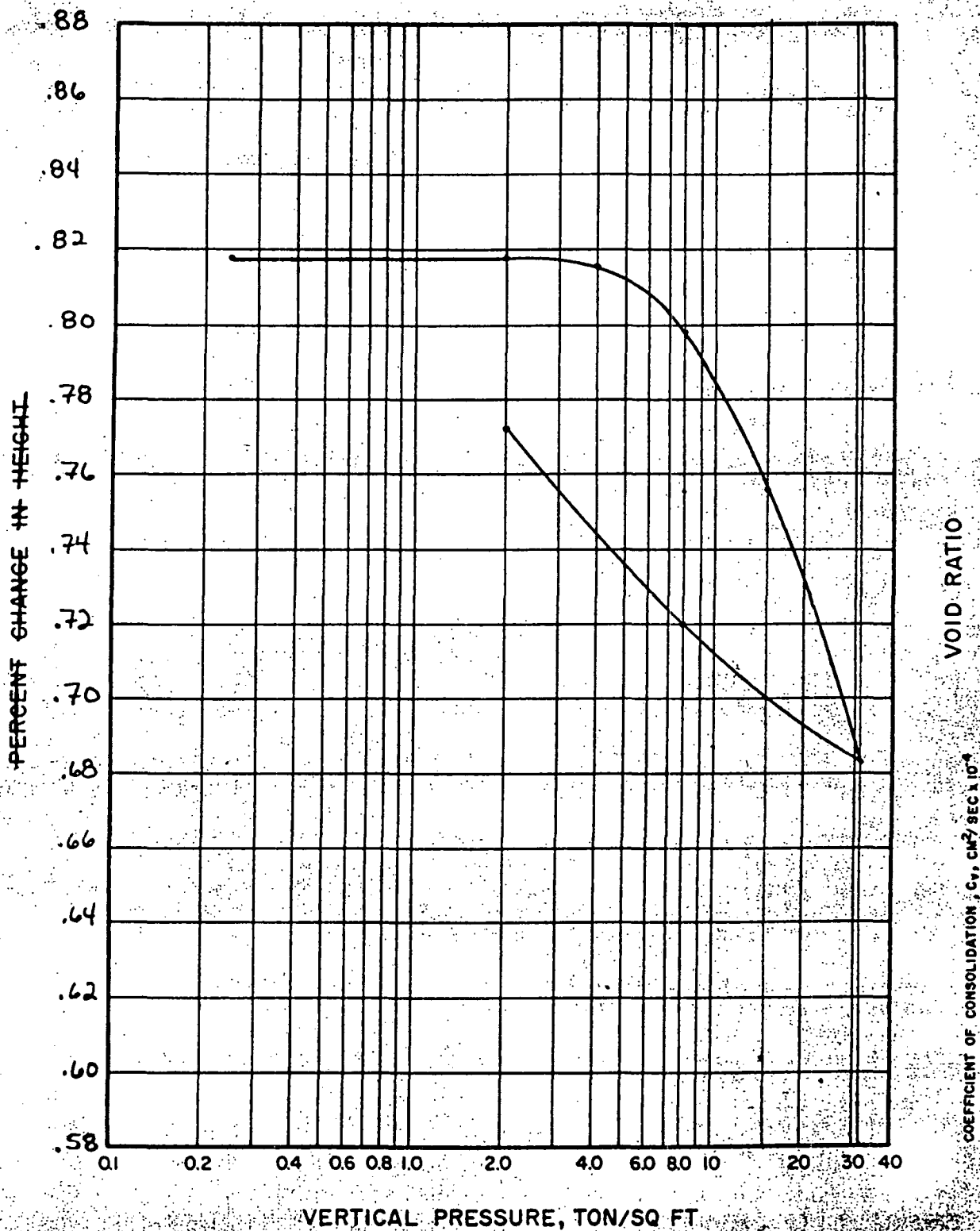
R 8 40' - 42'

Job No. \_\_\_\_\_ Appr. \_\_\_\_\_ Date \_\_\_\_\_

Job No. \_\_\_\_\_

BORING NO:      SAMPLE NO:  
DEPTH, FT: 78.79  
DESCRIPTION:

UNIT DRY WEIGHT: 96.1 PCF  
WATER CONTENT: 28.4 %  
LIQUID LIMIT:  
PLASTIC LIMIT:



VERTICAL PRESSURE, TON/SQ FT  
CONSOLIDATION TEST RESULTS



## CONSOLIDATION TEST

Date: \_\_\_\_\_ Project: REI P10-4 Job No. \_\_\_\_\_  
Boring No. \_\_\_\_\_ Sample No. \_\_\_\_\_ Depth: 78-80 Ring No. 1  
Description: Very stiff red - light gray clay w/ Liquid Limit \_\_\_\_\_  
calcareous nodules, slickensided Plastic Limit \_\_\_\_\_

Test Specimen	Initial	Final
Wet wt sple + ring	133.81	132.94
Dry wt sple + ring	117.09	117.09
Wt of ring	59.38	59.38
Dry wt of sple		
Wt of water		
Water content, %	29.0	27.5

Trimming, Can No. 473	
Wet wt + tare	51.53
Dry wt - tare	48.56
Tare wt	15.49
Dry wt	
Wt of water	
Water content, %	28.4

A. Specific Gravity 2.75 B. Volume of Sp<sup>l</sup> 37.468 c.c.  
C. Initial Ht of Sp<sup>l</sup> 0.750 in.  
D. Final Ht of Sp<sup>l</sup> \_\_\_\_\_ in. E. Unit Wet Wt 124.0 lb/ft<sup>3</sup>  
F. Unit Dry Wt 96.1 lb/ft<sup>3</sup>  
G. Ht of Solids =  $\frac{\text{Final Dry Wt Sp<sup>l</sup>}}{A} \times \frac{C}{B} = \underline{0.179}$  in.  
 $\frac{1}{G} = \underline{\hspace{2cm}}$   
H. Initial Void Ratio: =  $\frac{C - G}{G} = \underline{0.8179}$

**Percent Saturation:**

$$\text{Before Test} = \frac{\text{Initial Wt Water}}{\text{B. - Dry Wt Sple}} \times 100 = \underline{\hspace{2cm}} \%$$

$$\text{After Test} = \frac{\text{Final Wt Water}}{B \times \frac{D}{C} - \frac{\text{Dry Wt Spile}}{A}} \times 100 = \underline{\hspace{2cm}} \%$$

**Consolidometer No:**

$$P = 70.9(C-J)^2 / N$$

[illegible]

Tested By: DRJ  
Computed By: DRJ  
Checked By: DRJ

## CONSOLIDATION TEST DATA SHEET

Job No. P10-4

**Boring No.**

Depth 78-79

Consol. No. 1

Observ. By	Date	Time	Elapsed Time min.	Dial Reading in.	Load No.
QZ	15 Aug	1145	0	.2520	.25 Kg/cm <sup>2</sup>
			.1	.2516	
			.25	.2515	
			.5	.2514	
		add H <sub>2</sub> O →	1	.2513½	
			2	.2520	(SWELL)
QZ		1148	0	.2520	.5 Kg/cm <sup>2</sup>
			.1	.2519	
			.25	.2519	
			.5	.2519	
			1	.2520	
			2	.2521	(SWELL)
QZ	15 Aug 86	1150	0	.2521	1.0 Kg/cm <sup>2</sup>
			.1	.2518	
			.25	.2517	
			.5	.2516½	
			1	.2516	
			2	.2516	
			4	.2516	
			8	.2517½	
			15	.2521	(SWELL)
QZ	15 Aug 86	1205	0	.2521	2.0 Kg/cm <sup>2</sup>
			.1	.2509	
			.25	.2507½	
			.5	.2506½	
			1	.2505½	
			2	.2504½	
			4	.2503½	
			8	.2503	
			15	.2502½	
			30	.2502	
			60	.2501½	
		1405	120	.2501	
		1605	240	.2500	
	16 Aug	0800		.2499	
Observ. By	Date	Time	Elapsed Time min.	Dial Reading in.	Load No.
QZ	16 Aug	0900	0	.2499	4 Kg/cm <sup>2</sup>
			.1	.2486	
			.25	.2484	
			.5	.2482	
			1	.2480	
			2	.2478	
			4	.2476	
			8	.2473	
			15	.2470½	
			30	.2468	
			60	.2466	
			120	.2463½	
			240	—	
		1700	480	.2461½	
			1380	.2459	
QZ	17 Aug	0800	0	.2459	8 Kg/cm <sup>2</sup>
			.1	.2435	
			.25	.2431	
			.5	.2428	
			1	.2423	
			2	.2418	
			4	.2410	
			8	.240¼	
			15	.2392	
			30	.238½	
			60	.2373	
			120	.2368	
			240	.2364	
			480	.2361	
	18 Aug	0835		.2357	
R.T.	19 Aug	0940	0	.2357	16 Kg/cm <sup>2</sup>
			.1	.2325	
			.25	.2319	
			.5	.2314	
			1	.2307	
			2	.2297½	
			4	.2285	
			8	.2267	
			15	.2246	
			35	.2215	
			60	.2196	
		1140	120	.2178	
		1340	240	.2166	
		1640	420	.2161	
		0810		.2149	

## CONSOLIDATION TEST

Date: \_\_\_\_\_ Project: \_\_\_\_\_ Job No. \_\_\_\_\_

Boring No. \_\_\_\_\_ Sample No. \_\_\_\_\_ Depth: \_\_\_\_\_ Ring No. \_\_\_\_\_

**Description:** \_\_\_\_\_ **Liquid Limit** \_\_\_\_\_

Plastic Limit \_\_\_\_\_

Test Specimen	Initial	Final
Wet wt sple + ring		
Dry wt sple + ring		
Wt of ring		
Dry wt of sple		
Wt of water		
Water content, %		

Trimming, Can No.	
Wet wt + tare	
Dry wt - tare	
Tare wt	
Dry wt	
Wt of water	
Water content, %	

A. Specific Gravity\_\_\_\_\_ B. Volume of Sple\_\_\_\_\_ c. c. C. Initial Ht of Sple\_\_\_\_\_ in.

D. Final Ht of Sple\_\_\_\_\_ in.    E. Unit Wet Wt\_\_\_\_\_ lb/ft<sup>3</sup>    F. Unit Dry Wt\_\_\_\_\_ lb/ft<sup>3</sup>

G. Ht of Solids =  $\frac{\text{Final Dry Wt Sple}}{A} \times \frac{C}{B} = \underline{\hspace{2cm}} \text{ in.}$        $\frac{1}{G} = \underline{\hspace{2cm}}$

H. Initial Void Ratio:  $= \frac{C - G}{G} = \underline{\hspace{2cm}}$

**Percent Saturation:**

$$\text{Before Test} = \frac{\text{Initial Wt Water}}{\text{B} - \frac{\text{Dry Wt Sple}}{\text{A}}} \times 100 = \text{_____} \%$$
$$\text{After Test} = \frac{\text{Final Wt Water}}{B \times \frac{D}{C} - \frac{\text{Dry Wt Sple}}{A}} \times 100 = \underline{\hspace{2cm}} \%$$

**Consolidometer No:**

$$* P = 70.9(C-J)^2/N$$

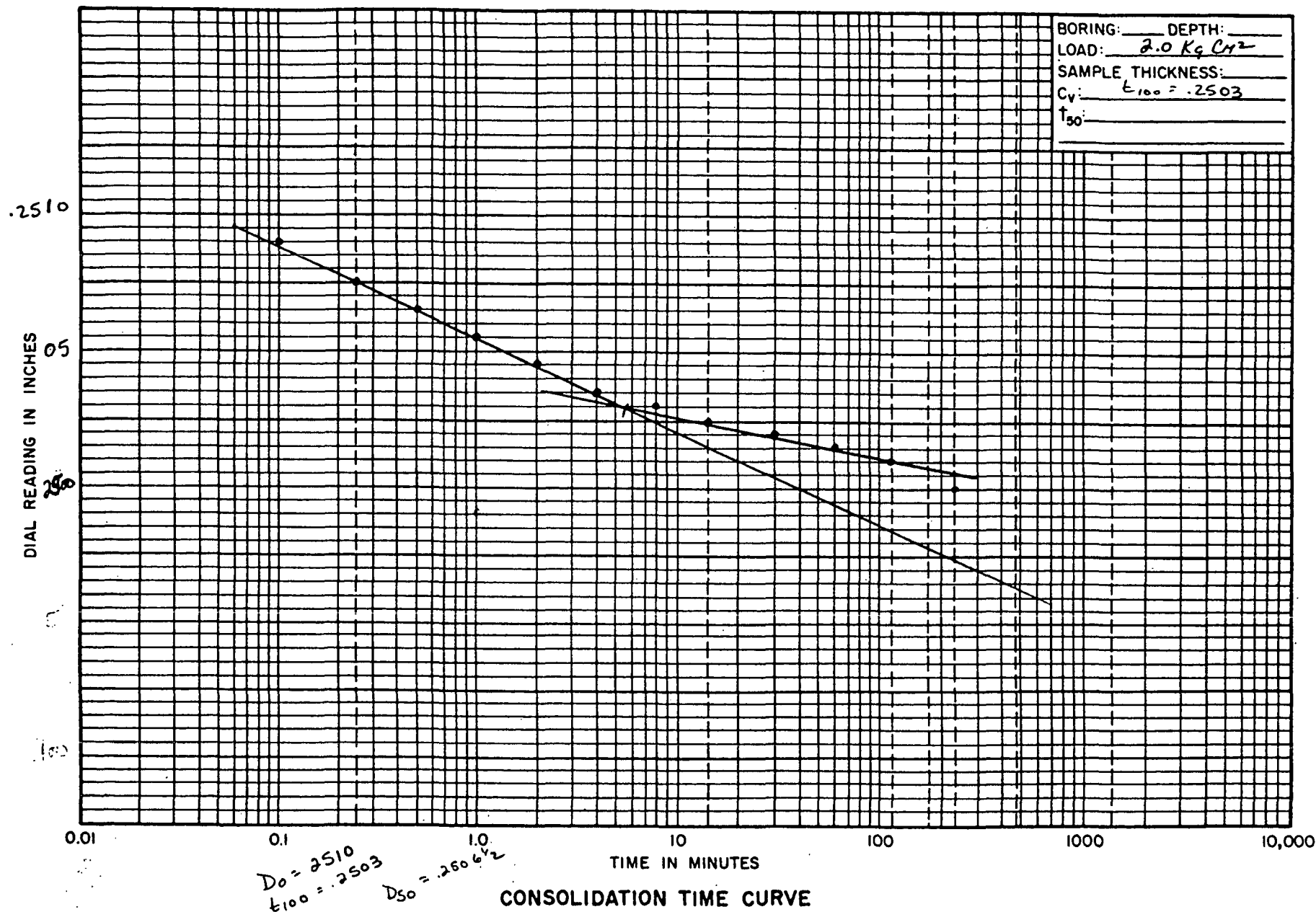
[illegible]

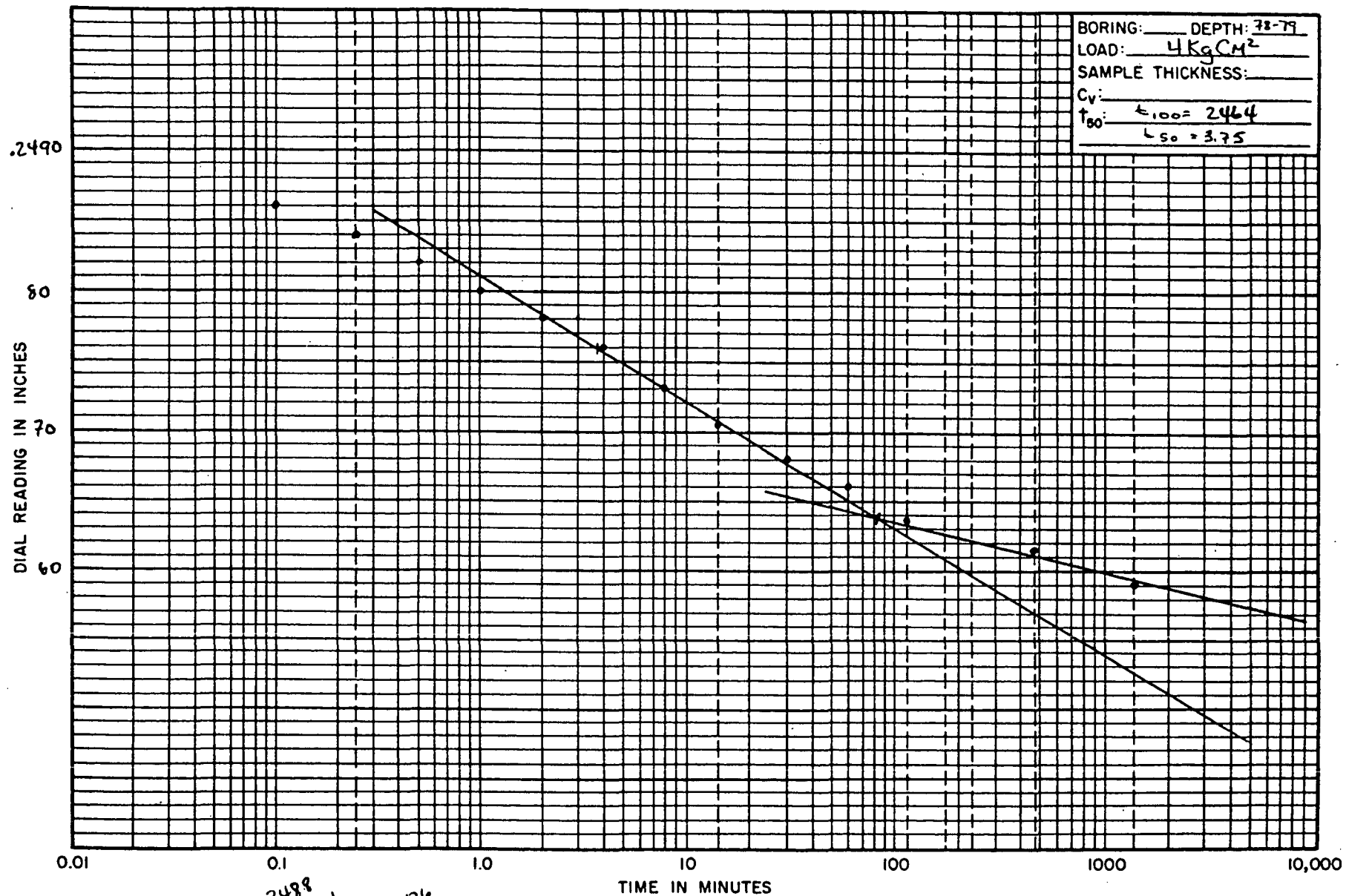
Tested By: \_\_\_\_\_  
Computed By: \_\_\_\_\_  
Checked By: \_\_\_\_\_

## CONSOLIDATION TEST DATA SHEET

Job No. \_\_\_\_\_ Boring No. \_\_\_\_\_ Depth \_\_\_\_\_ Consol. No. \_\_\_\_\_

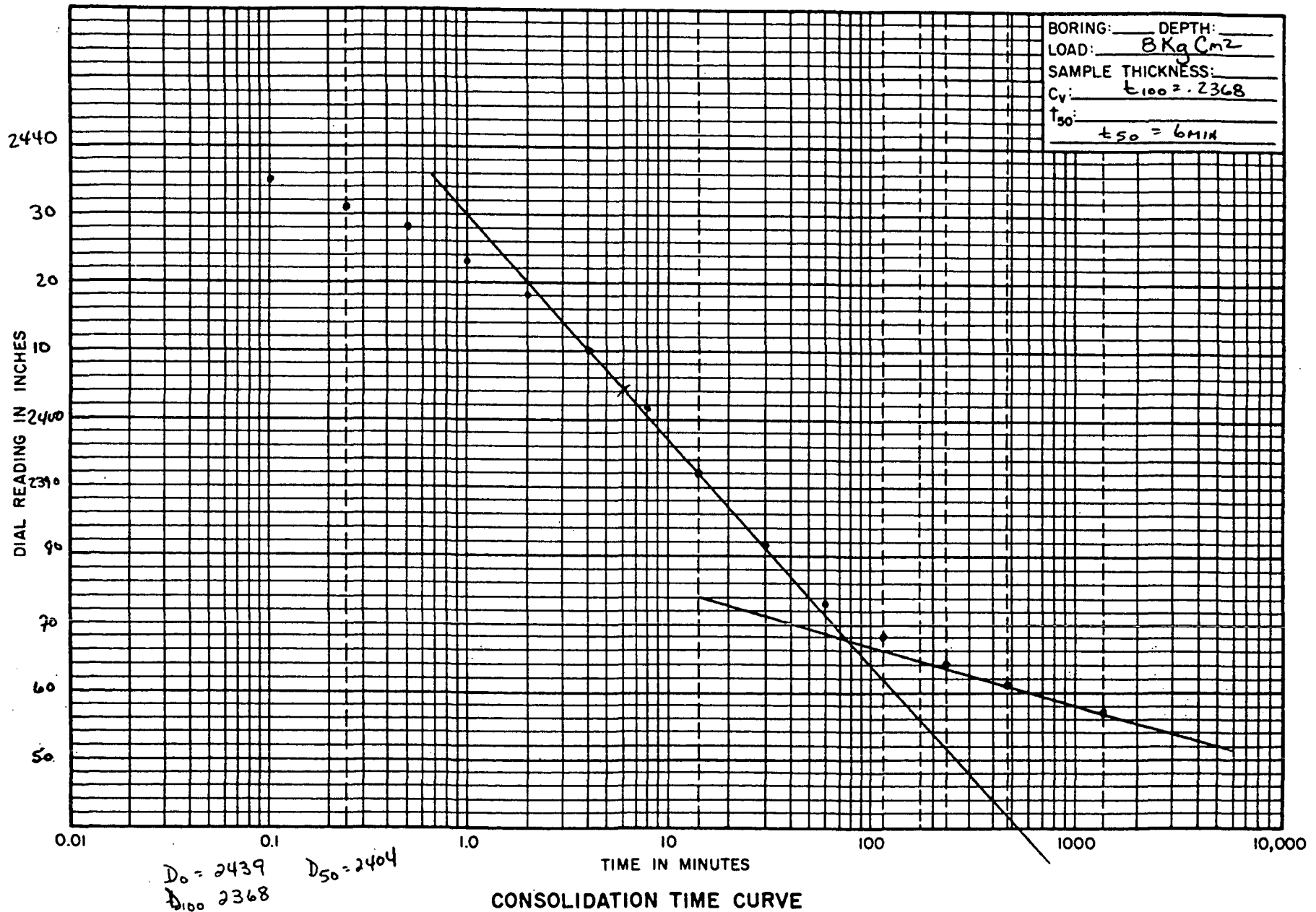
Observ. By	Date	Time	Elapsed Time min.	Dial Reading in.	Load No.
B.T.	20 Aug	0815	0	.2149	32 Kg/cm <sup>2</sup>
			.1	.2117	
			.25	.2110	
			.50	.2104	
			1	.2095	
			2	.2082	
			4	.2064	
			8	.2039	
			15	.2009	
			30	.1968	
			60	.1918	
		1030	12035	.1875	
			240	.1855	
		420	485	1840	
		0820		.1826	
<b>Rebound</b>					
21 Aug	0835	0		.1826	8 Kg/cm <sup>2</sup>
21 Aug	1130			.2026	
22 Aug	1130	0		.2026	2 Kg/cm <sup>2</sup>
				.2263	

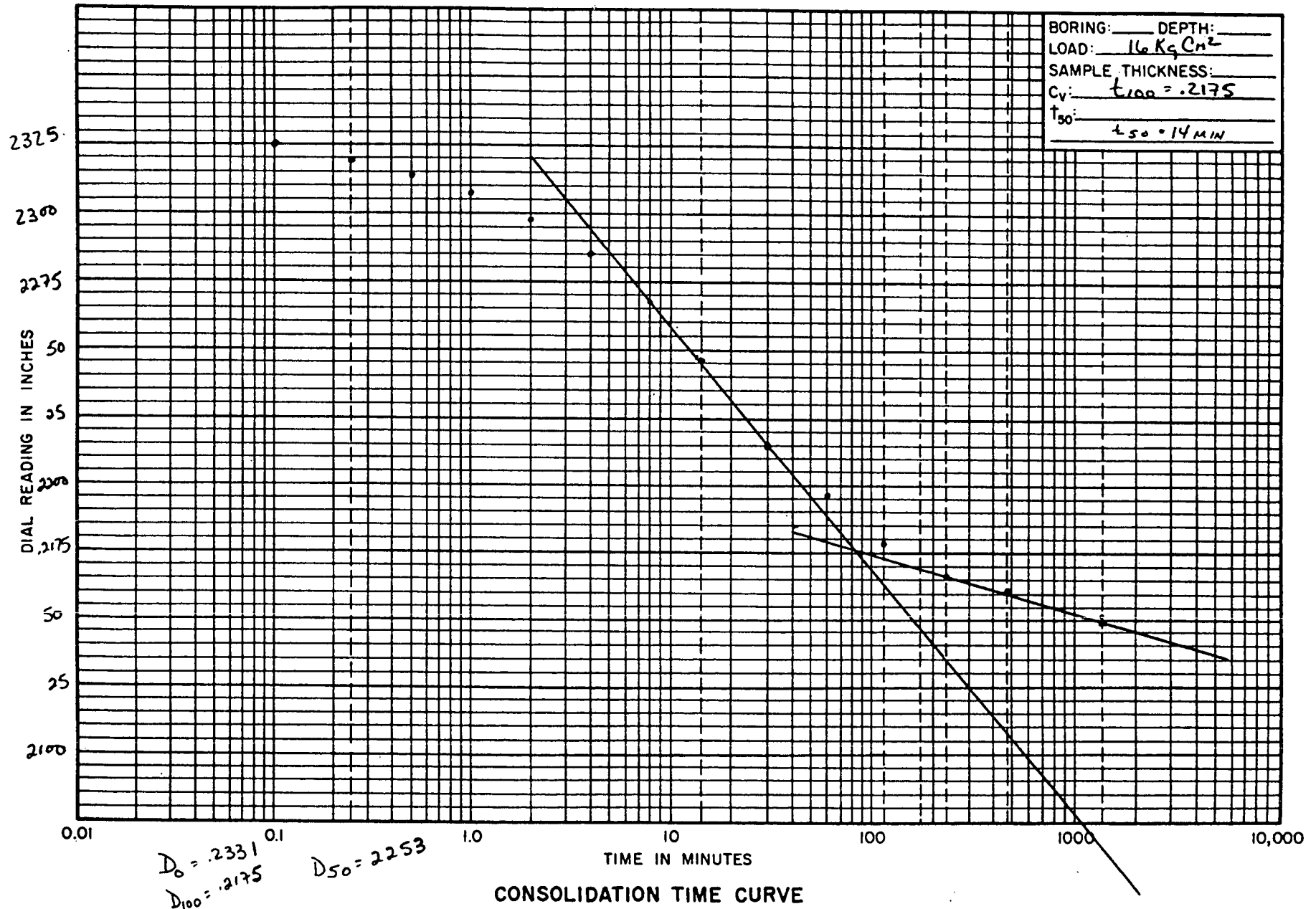




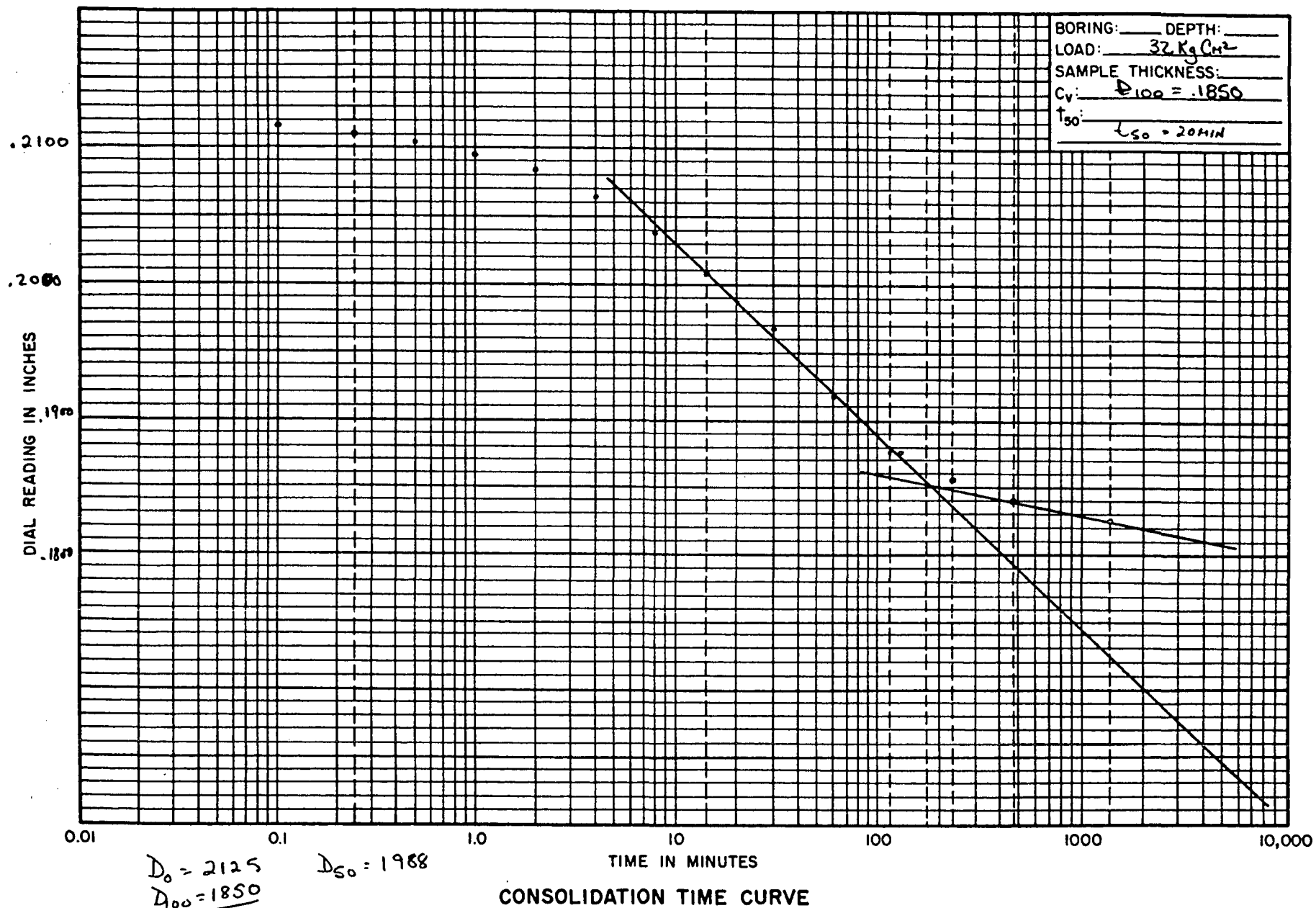
BORING: \_\_\_\_\_ DEPTH: 72-79  
 LOAD: 4 Kg CM<sup>2</sup>  
 SAMPLE THICKNESS: \_\_\_\_\_  
 C<sub>v</sub>: \_\_\_\_\_  
 t<sub>80</sub>: t<sub>100</sub> = 2464  
 L<sub>50</sub> = 3.75

CONSOLIDATION TIME CURVE









# CONSOLIDATION TEST

Version 1.1

=====

JOB NO.:

BORING NO.:

SAMPLE NO.:

DEPTH:

TEST SPECIMEN:

TRIMMINGS:

-----  
 INITIAL FINAL  
 WET WEIGHT + TARE = 133.81 132.94  
 DRY WEIGHT + TARE = 117.09 117.09  
 TARE WEIGHT = 59.38 59.38  
 WATER CONTENT = 29.0% 27.5%

-----  
 WET WEIGHT + TARE = 51.53  
 DRY WEIGHT + TARE = 43.56  
 TARE WEIGHT = 15.49  
 WATER CONTENT = 28.4%

SPECIFIC GRAVITY = 2.8000  
 SAMPLE HEIGHT (IN) = 0.7500  
 SAMPLE DIAMETER (IN) = 1.9700  
 SAMPLE VOLUME (CC) = 37.4681  
 HEIGHT OF SOLIDS (IN) = 0.4126  
 INITIAL VOID RATIO = 0.8179

DEGREE OF SATURATION:

INITIAL = 99.2%

FINAL = 99.6%

UNIT WEIGHT OF SPECIMEN:

WET (PCF) = 124.0

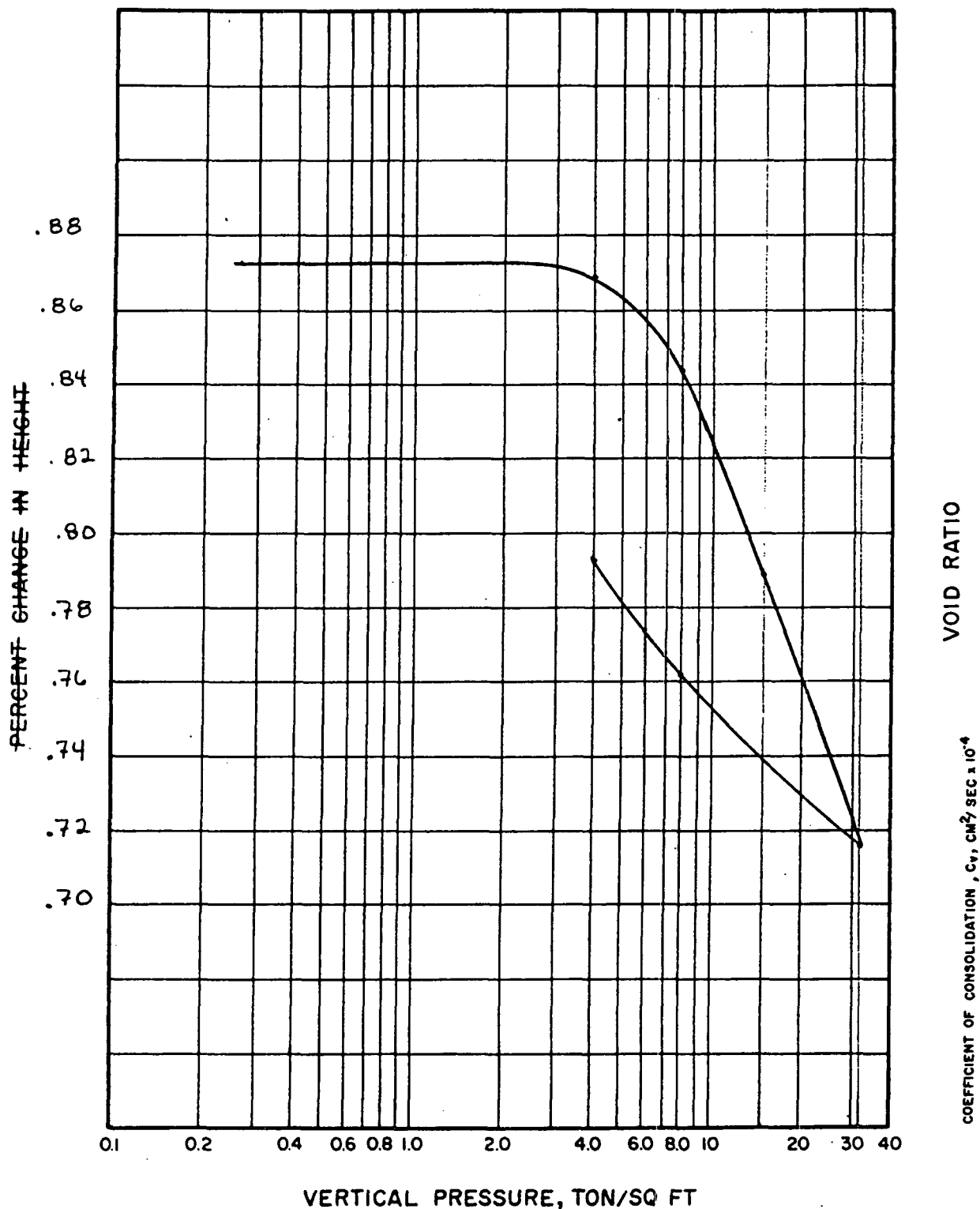
DRY (PCF) = 96.1

MACHINE READING	PRESSURE KG/CM <sup>2</sup>	DIAL READING	CUM. CHANGE	CORR. CHANGE	VOID RATIO	COEFF. IN <sup>2</sup> /DAY
-----	-----	-----	-----	-----	-----	-----
-0.0049	4.000	0.2464	0.0036	0.0007	0.816	10.615
-0.0070	8.000	0.2368	0.0152	0.0082	0.798	6.502
-0.0091	16.000	0.2173	0.0345	0.0254	0.756	2.659
-0.0115	32.000	0.1850	0.0670	0.0553	0.683	1.710
-0.0090	8.000	0.2026	0.0494	0.0404	0.720	0.000
-0.0069	2.000	0.2263	0.0257	0.0188	0.772	0.000

Job No. \_\_\_\_\_

BORING NO:      SAMPLE NO:  
DEPTH, FT: 80-81  
DESCRIPTION: Hard red clay with  
                  calcareous nodules, slickensided

UNIT DRY WEIGHT: 93.3 PCF  
WATER CONTENT: 27.7 %  
LIQUID LIMIT:  
PLASTIC LIMIT:



### CONSOLIDATION TEST RESULTS

## CONSOLIDATION TEST

Date: \_\_\_\_\_ Project: REI PID-4 Job No. \_\_\_\_\_  
Boring No. \_\_\_\_\_ Sample No. \_\_\_\_\_ Depth: 80-81 Ring No. 3  
Description: 1st. red clay w/ calc nodds, Liquid Limit \_\_\_\_\_  
SUCKER SIDED Plastic Limit \_\_\_\_\_

Test Specimen	Initial	Final
Wet wt sple + ring	143.75	142.50
Dry wt sple + ring	126.28	126.28
Wt of ring	70.50	70.50
Dry wt of sple		
Wt of water		
Water content, %		

Trimming, Can No. 605	
Wet wt + tare	64.37
Dry wt - tare	53.67
Tare wt	15.09
Dry wt	
Wt of water	
Water content, %	

A. Specific Gravity \_\_\_\_\_ B. Volume of Spile 37.318 c.c. C. Initial Ht of Spile 0.747 in.  
D. Final Ht of Spile \_\_\_\_\_ in. E. Unit Wet Wt \_\_\_\_\_ lb/ft<sup>3</sup> F. Unit Dry Wt \_\_\_\_\_ lb/ft<sup>3</sup>  
G. Ht of Solids =  $\frac{\text{Final Dry Wt Spile}}{A} \times \frac{C}{B} =$  \_\_\_\_\_ in.  $\frac{1}{G} =$  \_\_\_\_\_  
H. Initial Void Ratio: =  $\frac{C - G}{G} =$  \_\_\_\_\_

**Percent Saturation:**

$$\text{Before Test} = \frac{\text{Initial Wt Water}}{\text{B} - \frac{\text{Dry Wt Sple}}{\text{A}}} \times 100 = \text{_____} \%$$

$$\text{After Test} = \frac{\text{Final Wt Water}}{B \times \frac{D}{C} - \frac{\text{Dry Wt Sple}}{A}} \times 100 = \underline{\hspace{2cm}} \%$$

**Consolidometer No:**

$$* P = 70.9(C-J)^2/N$$

[illegible]

Tested By: QAN  
Computed By: QAN  
Checked By: RY

## CONSOLIDATION TEST DATA SHEET

Job No. \_\_\_\_\_ Boring No. P10-4 Depth 80-81 Consol. No. 3

Observ. By	Date	Time	Elapsed Time min.	Dial Reading in.	Load No.
(P.N.)	15 Aug	1308	0	.2500	.25 Kg/cm <sup>2</sup>
			.1	.2508	
			.25	.2509	
			.5	.2510	
		add H <sub>2</sub> O →	1	.2510	
			2	.2500	(SWELL)
			4		
(P.N.)		1310	0	.2500	15 Kg/cm <sup>2</sup>
			.1	.2504	
			.25	.2505	
			.5	.2504	
			1	.2503	
			2	.2501	(SWELL)
		1313	0	.2501	10 Kg/cm <sup>2</sup>
			.1	.2510	
			.25	.2511	
			.5	.2511½	
			1	.2511½	
			2	.2511	
			4	.2510	(SWELL)
(P.N.)	15 Aug	1315	0	.2510	2.0 Kg/cm <sup>2</sup>
			.1	.2525½	
			.25	.2527	
			.5	.2528½	
			1	.2529½	
			2	.2530½	
			4	.2531	
			8	.2530	(SWELL)
			15		

Observ. By	Date	Time	Elapsed Time min.	Dial Reading in.	Load No.
(P.N.)	15 Aug	1330	0	.2520	4.0 Kg/cm <sup>2</sup>
			.1	.2551	
			.25	.2553½	
			.5	.2556	
			1	.2558½	
			2	.2561	
			4	.2564	
			8	.2568½	
			15	.2571	
			40	.2574½	
		1430	60	.2575½	
		1530	120	.2577	
		1730	240	.2578	
	16 Aug	0800	1110	.2580	
	16 Aug	0910	0	.2580	8 Kg/cm <sup>2</sup>
			.1	.2609	
			.25	.2612	
			.5	.2616	
			1	.2620½	
			2	.2626	
			4	.2633½	
			8	.2649	
			15	.2654	
			30	.2667	
			60	.2682	
			130	.2699	
			240		
			480	.2709	
			1440	.2714	
	17 Aug	0810	0	.2714	16 Kg/cm <sup>2</sup>
			.1	.2748	
			.25	.2752	
			.5	.2757	
			1	.2763	
			2	.2772	
			4	.2784	
			8	.2800	
			15	.2821	
			30	.2850	
			60	.2884	
			120	.2915	
			240	.2938	
			480	.2952	
		0830	1460	.2963	

## CONSOLIDATION TEST

Date: \_\_\_\_\_ Project: \_\_\_\_\_ Job No. \_\_\_\_\_

Boring No. \_\_\_\_\_ Sample No. \_\_\_\_\_ Depth: \_\_\_\_\_ Ring No. \_\_\_\_\_

**Description:** \_\_\_\_\_ **Liquid Limit** \_\_\_\_\_

Plastic Limit \_\_\_\_\_

Test Specimen	Initial	Final
Wet wt sple + ring		
Dry wt sple + ring		
Wt of ring		
Dry wt of sple		
Wt of water		
Water content, %		

Trimblings, Can No.	
Wet wt + tare	
Dry wt - tare	
Tare wt	
Dry wt	
Wt of water	
Water content, %	

**A. Specific Gravity**\_\_\_\_\_ **B. Volume of Sple**\_\_\_\_\_ c. c. **C. Initial Ht of Sple**\_\_\_\_\_ in.

D. Final Ht of Sple\_\_\_\_\_in.    E. Unit Wet Wt\_\_\_\_\_lb/ft<sup>3</sup>    F. Unit Dry Wt\_\_\_\_\_lb/ft<sup>3</sup>

G. Ht of Solids =  $\frac{\text{Final Dry Wt Spie}}{A} \times \frac{C}{B} = \underline{\hspace{2cm}}$  in.  $\frac{1}{G} = \underline{\hspace{2cm}}$

H. Initial Void Ratio:  $= \frac{C - G}{G} = \underline{\hspace{2cm}}$

**Percent Saturation:**

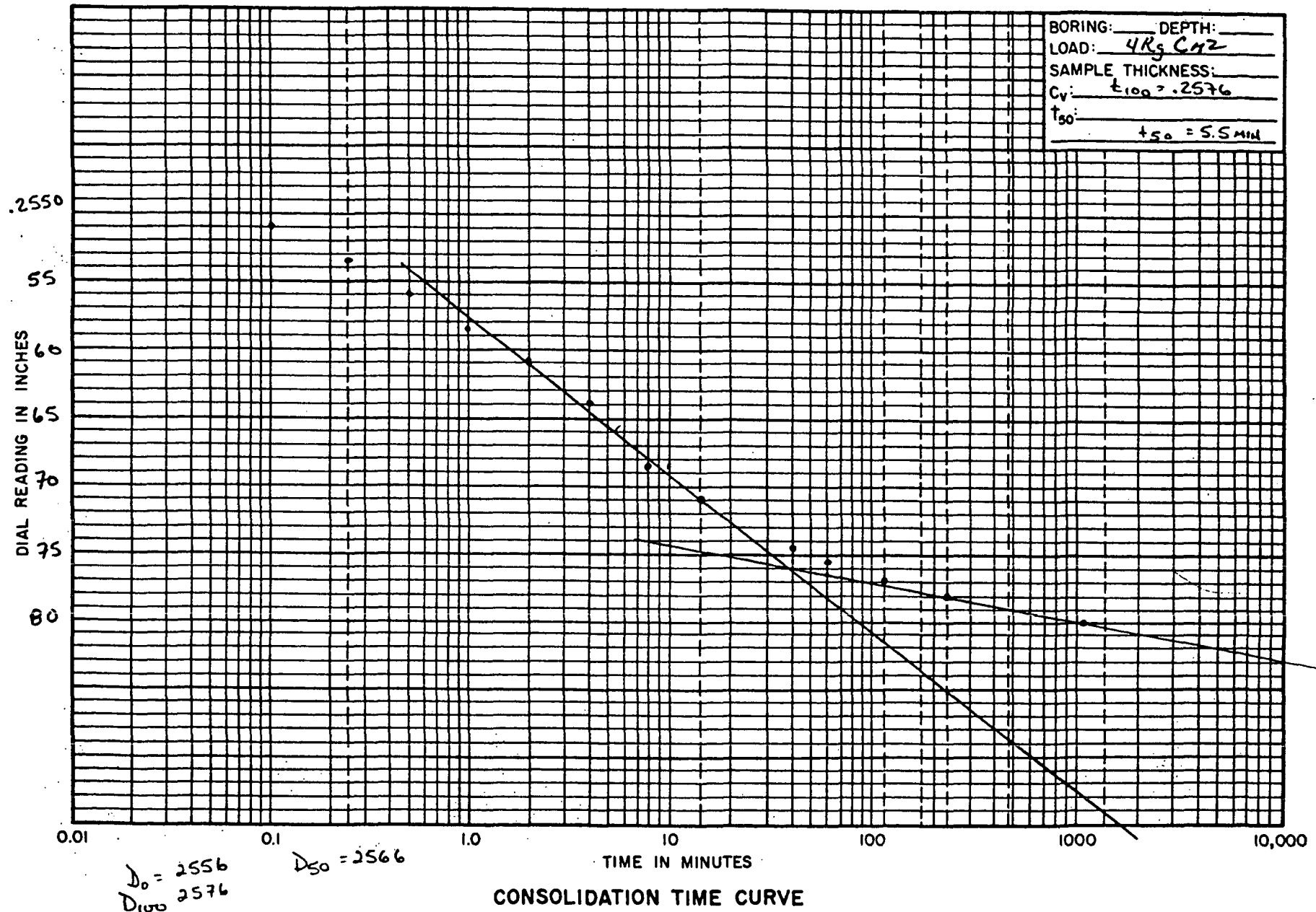
$$\text{Before Test} = \frac{\text{Initial Wt Water}}{\text{B} - \text{Dry Wt Sple}} \times 100 = \underline{\hspace{2cm}} \%$$
$$\text{After Test} = \frac{\text{Final Wt Water}}{\frac{B \times D}{C} - \frac{\text{Dry Wt Sple}}{A}} \times 100 = \text{-----} \%$$

**Consolidometer No:**

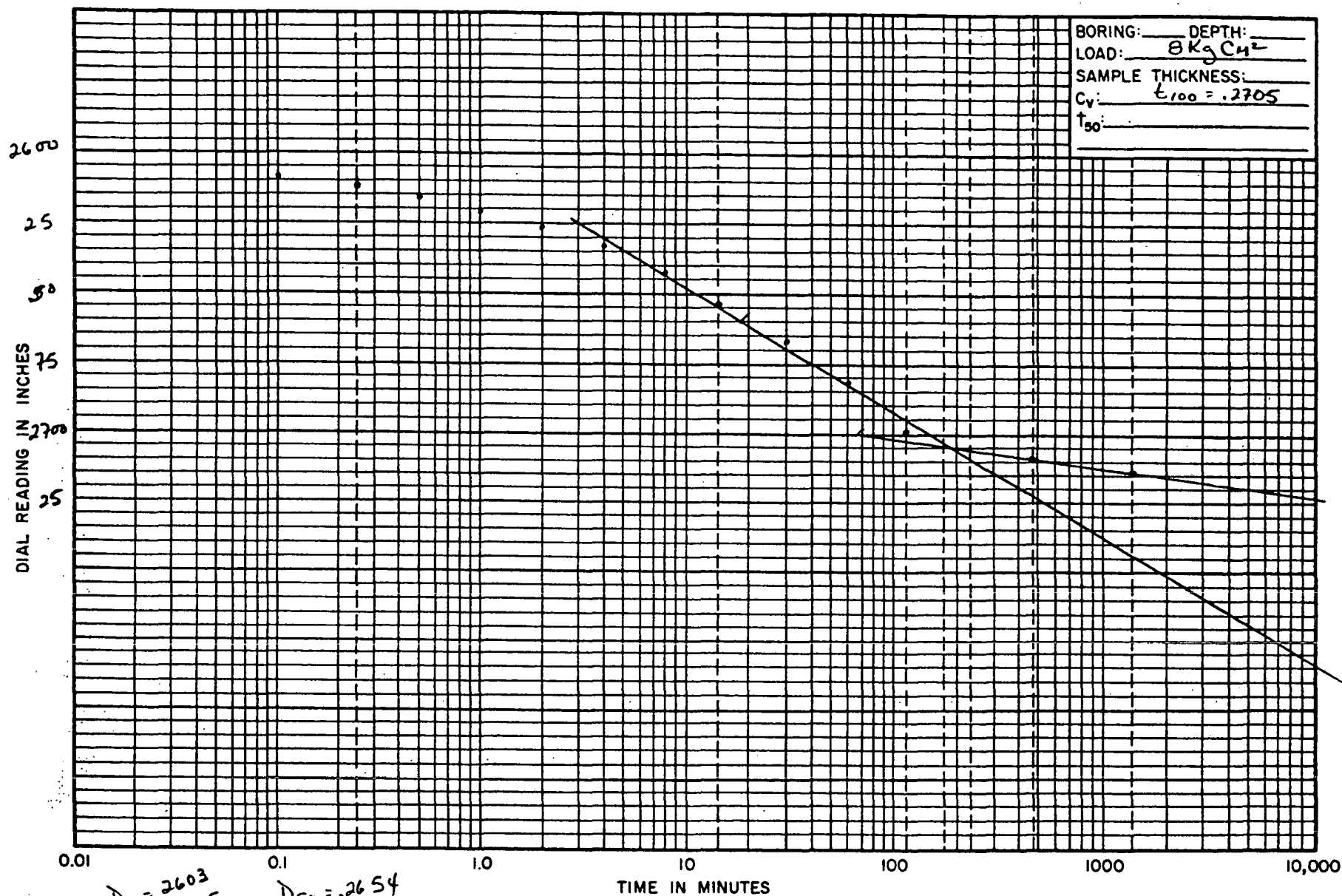
$$* P = 70.9(C-J)^2/N$$

[illegible]

Tested By: \_\_\_\_\_  
Computed By: \_\_\_\_\_  
Checked By: \_\_\_\_\_



BORING: \_\_\_\_\_ DEPTH: \_\_\_\_\_  
LOAD: 8 Kg/cm<sup>2</sup>  
SAMPLE THICKNESS: \_\_\_\_\_  
C<sub>v</sub>: t<sub>100</sub> = .2705  
t<sub>50</sub>: \_\_\_\_\_

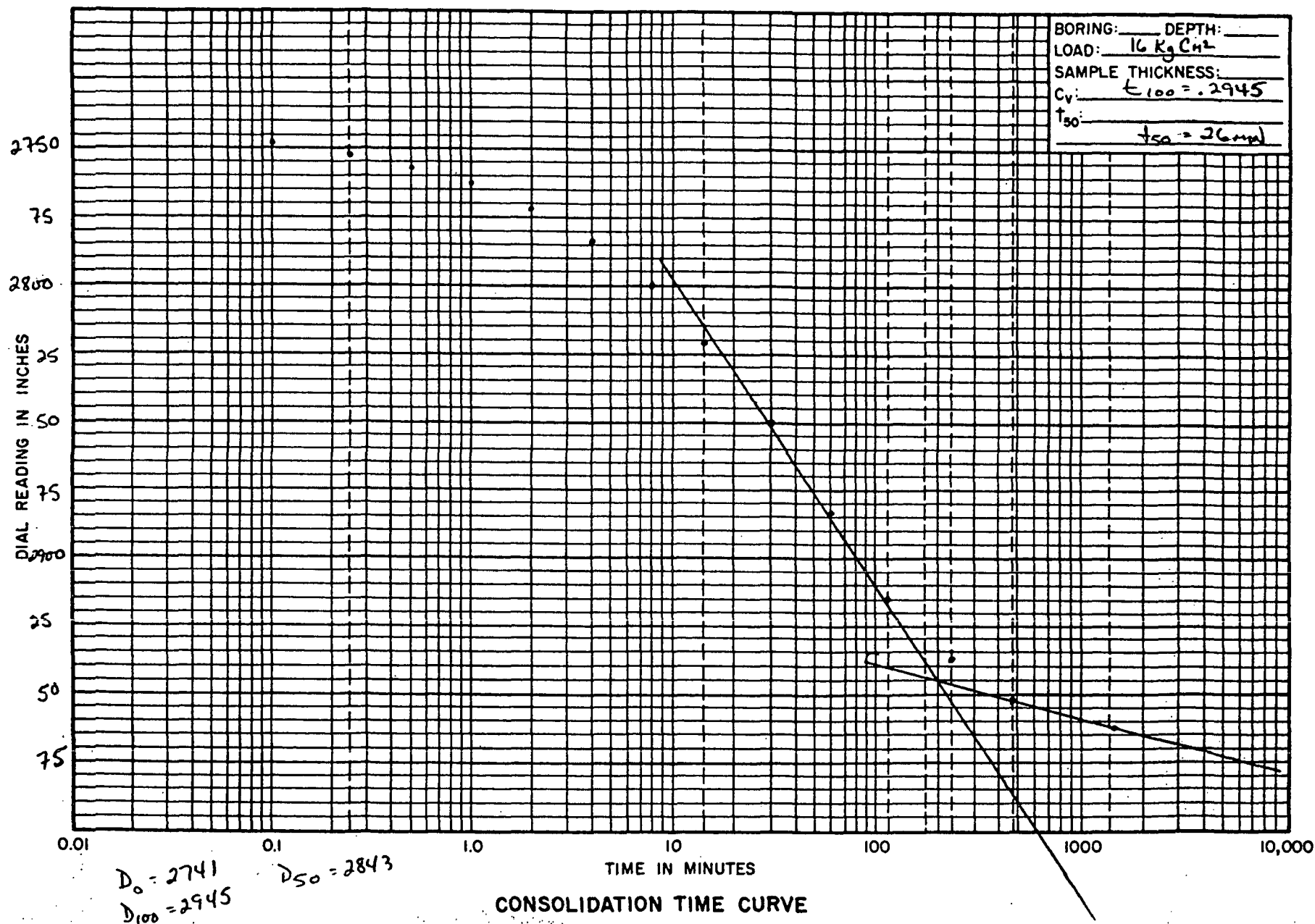


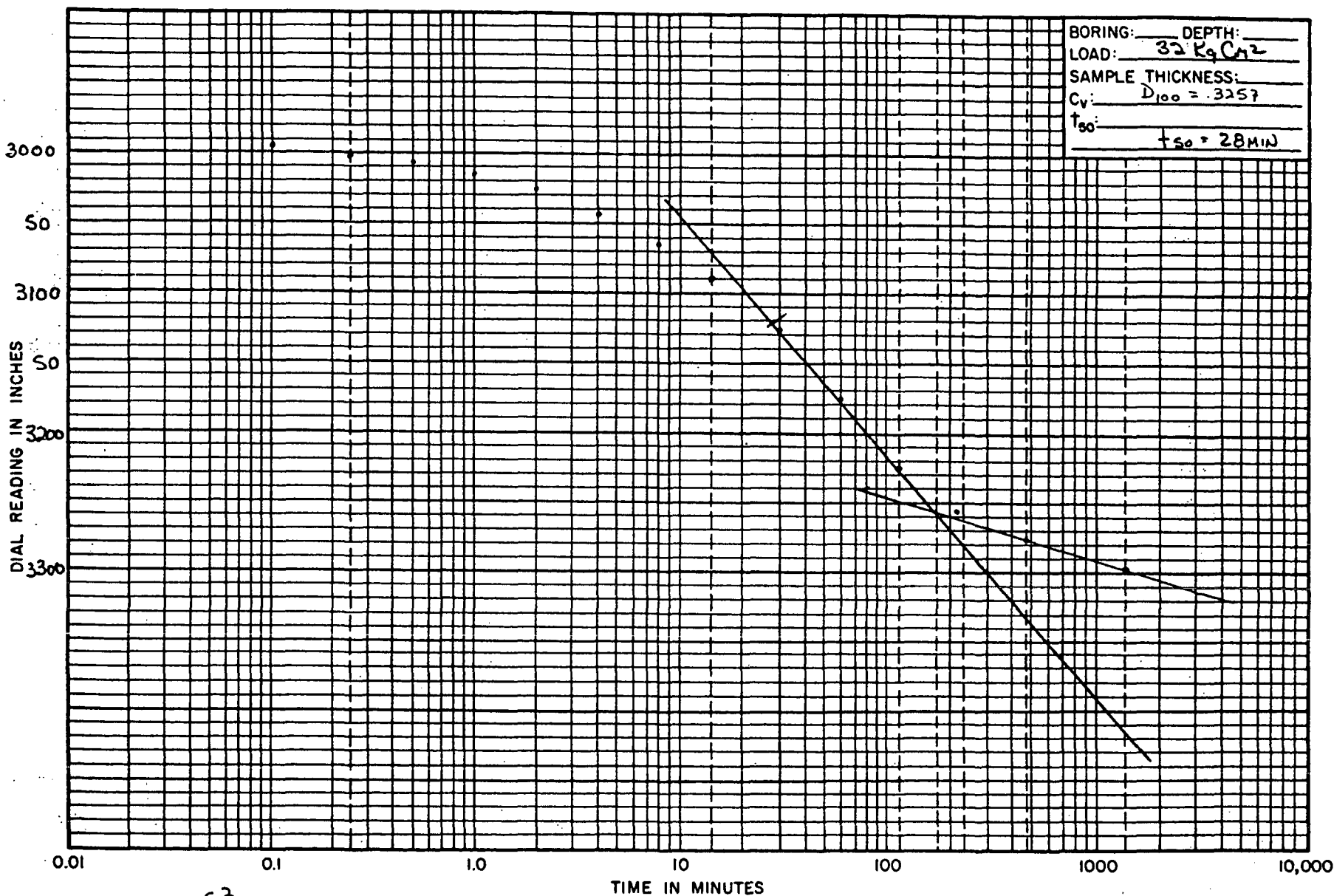
CONSOLIDATION TIME CURVE

D<sub>0</sub> = 26.03  
D<sub>100</sub> = 27.05

D<sub>50</sub> = 26.54







CONSOLIDATION TIME CURVE

CONSOLIDATION TEST  
Version 1.1  
=====

JOB NO.:                      BORING NO.:                      SAMPLE NO.:                      DEPTH:

TEST SPECIMEN:  
-----

	INITIAL	FINAL
WET WEIGHT + TARE =	143.75	142.50
DRY WEIGHT + TARE =	126.28	126.28
TARE WEIGHT =	70.50	70.50
WATER CONTENT =	31.3%	29.1%

SPECIFIC GRAVITY                =    2.8000  
SAMPLE HEIGHT (IN)            =    0.7470  
SAMPLE DIAMETER (IN)        =    1.9700  
SAMPLE VOLUME (CC)          =    37.3183  
HEIGHT OF SOLIDS (IN)       =    0.3988  
INITIAL VOID RATIO           =    0.8733

DEGREE OF SATURATION:

INITIAL = 100.4%  
FINAL = 102.7%

UNIT WEIGHT OF SPECIMEN:

WET (PCF) = 122.5  
DRY (PCF) = 93.3

TRIMMINGS:  
-----

WET WEIGHT + TARE =	64.37
DRY WEIGHT + TARE =	53.67
TARE WEIGHT =	15.09
WATER CONTENT =	27.7%

MACHINE READING	PRESSURE KG/CN <sup>2</sup>	DIAL READING	CUM. CHANGE	CORR. CHANGE	VOID RATIO	COEFF. IN <sup>2</sup> /DAY
-----	-----	-----	-----	-----	-----	-----
-0.0060	4.000	0.2424	0.0076	0.0016	0.869	7.162
-0.0087	8.000	0.2295	0.0205	0.0118	0.844	2.129
-0.0110	16.000	0.2055	0.0445	0.0335	0.789	1.388
-0.0134	32.000	0.1740	0.0760	0.0626	0.716	1.186
-0.0107	8.000	0.1948	0.0552	0.0445	0.762	0.000
-0.0090	4.000	0.2089	0.0411	0.0321	0.793	0.000

Job No. \_\_\_\_\_

BORING NO: SAMPLE NO:

DEPTH, FT: 81-82

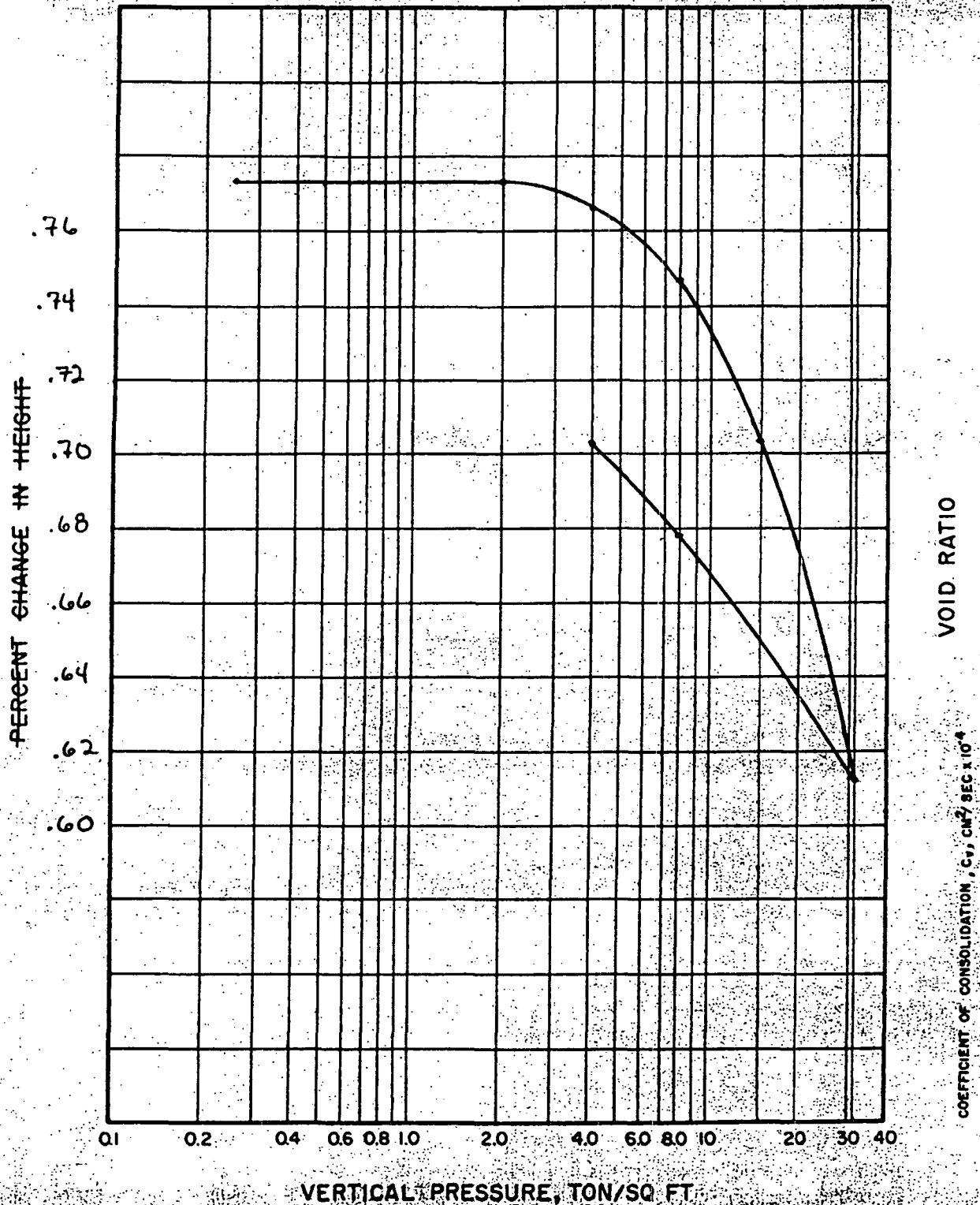
DESCRIPTION: Hard red clay with  
calcareous nodules, slickensided

UNIT DRY WEIGHT: 98.5 PCF

WATER CONTENT: 25.8 %

LIQUID LIMIT:

PLASTIC LIMIT:



VERTICAL PRESSURE, TON/SQ FT  
CONSOLIDATION TEST RESULTS

## CONSOLIDATION TEST

Date: 15 AUG 85

Project: REI P.10-4

**Job No.**

**Boring No.**

**Sample No.:**

**Depth:**

Ring No.

**Description:** Hard red clay w/ calc. material  
slickensided

### Liquid Limit

### Plastic Limit

Test Specimen	Initial	Final
Wet wt sple + ring	146.39	145.42
Dry wt sple + ring	130.43	130.43
Wt of ring	71.27	71.27
Dry wt of sple		
Wt of water		
Water content, %	27.0	25.3

Trimming, Can No. 400	
Wet wt + tare	57.19
Dry wt - tare	48.65
Tare wt	15.54
Dry wt	
Wt of water	
Water content, %	25.8

A. Specific Gravity 2.80

B. Volume of Sple 37.468 c.c.

C. Initial Ht of Sple. 0.750 in.

D. Final Ht of Sple\_\_\_\_\_ in.

E. Unit Wet Wt. 125.1 lb/ft<sup>3</sup>

F. Unit Dry Wt 98.5 lb/ft<sup>3</sup>

$$G. \text{ Ht of Solids} = \frac{\text{Final Dry Wt Sple}}{A} \times \frac{C}{B} = \frac{.4229}{1} \text{ in.}$$

1/5 = \_\_\_\_\_

H. Initial Void Ratio:  $= \frac{C - G}{G} = \underline{0.7733}$

**Percent Saturation:**

$$d = 1.97$$
$$\text{Before Test} = \frac{\text{Initial Wt Water}}{\text{B} - \frac{\text{Dry Wt Sple}}{\text{A}}} \times 100 = \underline{97.7} \%$$
$$\text{After Test} = \frac{\text{Final Wt Water}}{B \times \frac{D}{C} - \frac{\text{Dry Wt Spile}}{A}} \times 100 = \frac{101.0}{\phantom{0000}} \%$$

**Consolidometer No:**

$$* P = 70.9(C-J)^2/N$$
[illegible]

Tested By: \_\_\_\_\_  
Computed By: \_\_\_\_\_  
Checked By: \_\_\_\_\_

## CONSOLIDATION TEST DATA SHEET

Job No. \_\_\_\_\_ Boring No. P10-4 Depth 81-82 Consol. No. 2

Observ. By	Date	Time	Elapsed Time min.	Dial Reading in.	Load No.
QJN	15Aug	1250	0	.2500	.25Kg/cm <sup>2</sup>
			.1	.2508	
			.25	.2509	
			.5	.2510	
		add H <sub>2</sub> O →	1	.2511	
			2	.2500	(SWELL)
		1253	0	.2500	.5Kg/cm <sup>2</sup>
			.1	.2504	
			.25	.2504½	
			.5	.2504	
			1	.2503	
			2	.2501	(SWELL)
QJV	15Aug	1255	0	.2501	1.0Kg/cm <sup>2</sup>
			.1	.2511	
			.25	.2512	
			.5	.2512½	
			1	.2513	
			2	.2512	
			4	.2511	(SWELL)
QJN	15Aug	1300	0	.2511	2.0Kg/cm <sup>2</sup>
			.1	.2525	
			.25	.2527	
			.5	.2528½	
			1	.2529½	
			2	.2530½	
			4	.2531	
			8	.2531	
			15	.2529½	(SWELL)
Observ. By	Date	Time	Elapsed Time min.	Dial Reading in.	Load No.
QJN	15Aug86	1320	0	.2529	4Kg/cm <sup>2</sup>
			.1	.2551	
			.25	.2554	
			.5	.2556½	
			1	.2559	
			2	.2562	
			4	.2565	
			8	.2568	
			15	.2571	
			30	.2573½	
		1420	60	.2575½	
		1520	120	.2577	
		1720	240	.2578	
	16Aug	0800	1120	.2580	
QJN	16Aug	0905	0	.2580	8Kg/cm <sup>2</sup>
			.1	.2610	
			.25	.2613½	
			.5	.2617½	
			1	.2623	
			2	.2629	
			4	.2636½	
			8	.2646	
			15	.2656	
			30	.2668½	
			60	.2678	
			120	.2687	
			240	.2693	
			480	.2698	
	17Aug	0800	1380	.2698	
	17Aug	0805	0	.2698	16Kg/cm <sup>2</sup>
			.1	.2735	
			.25	.2741	
			.5	.2747½	
			1	.2755	
			2	.2763	
			4	.2775	
			8	.2791	
			15	.2810	
			30	.2837	
			60	.2862	
			120	.2880	
			240	.2892	
			480	.2900	
	18Aug	0835		.2909	

## CONSOLIDATION TEST

**Date:** \_\_\_\_\_ **Project:** \_\_\_\_\_ **Job No.** \_\_\_\_\_

**Boring No.**\_\_\_\_\_ **Sample No.**\_\_\_\_\_ **Depth:**\_\_\_\_\_ **Ring No.**\_\_\_\_\_

Description: \_\_\_\_\_ Liquid Limit \_\_\_\_\_

Plastic Limit \_\_\_\_\_

Test Specimen	Initial	Final
Wet wt sple + ring		
Dry wt sple + ring		
Wt of ring		
Dry wt of sple		
Wt of water		
Water content, %		

Trimming, Can No.	
Wet wt + tare	
Dry wt - tare	
Tare wt	
Dry wt	
Wt of water	
Water content, %	

A. Specific Gravity\_\_\_\_\_ B. Volume of Sple\_\_\_\_\_ c. c. C. Initial Ht of Sple\_\_\_\_\_ in.

D. Final Ht of Sple\_\_\_\_\_ in.    E. Unit Wet Wt\_\_\_\_\_ lb/ft<sup>3</sup>    F. Unit Dry Wt\_\_\_\_\_ lb/ft<sup>3</sup>

G. Ht of Solids =  $\frac{\text{Final Dry Wt Sple}}{A} \times \frac{C}{B} = \underline{\hspace{2cm}} \text{ in.}$        $\frac{1}{G} = \underline{\hspace{2cm}}$

H. Initial Void Ratio:  $= \frac{C - G}{G} = \underline{\hspace{2cm}}$

**Percent Saturation:**

$$\text{Before Test} = \frac{\text{Initial Wt Water}}{\text{B} - \frac{\text{Dry Wt Sple}}{\text{A}}} \times 100 = \text{_____} \%$$
$$\text{After Test} = \frac{\text{Final Wt Water}}{B \times \frac{D}{C} - \frac{\text{Dry Wt Sple}}{A}} \times 100 = \underline{\hspace{2cm}} \%$$

**Consolidometer No:**

$$* P = 70.9(C-J)^2/N$$

[illegible]

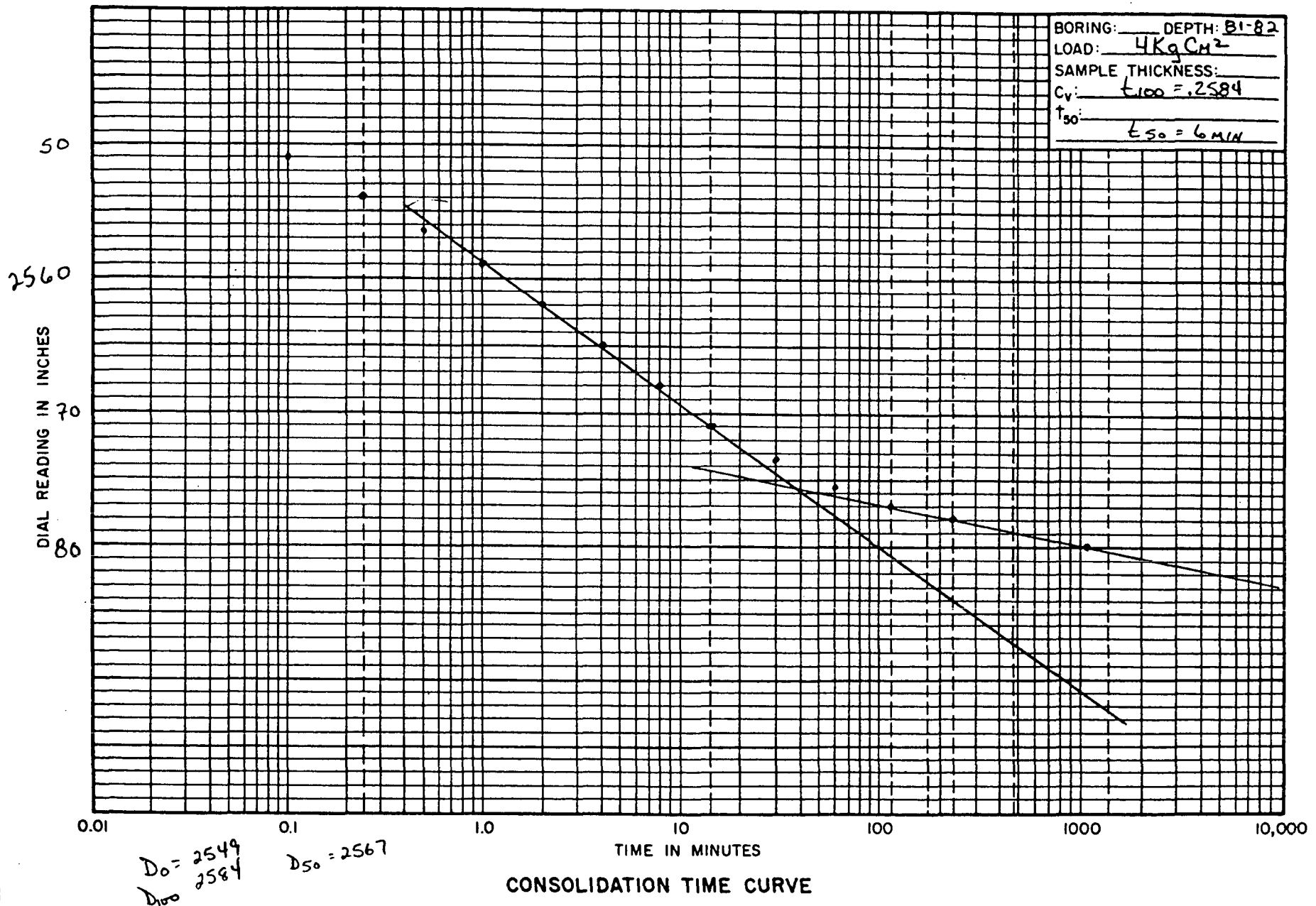
Tested By: \_\_\_\_\_  
Computed By: \_\_\_\_\_  
Checked By: \_\_\_\_\_

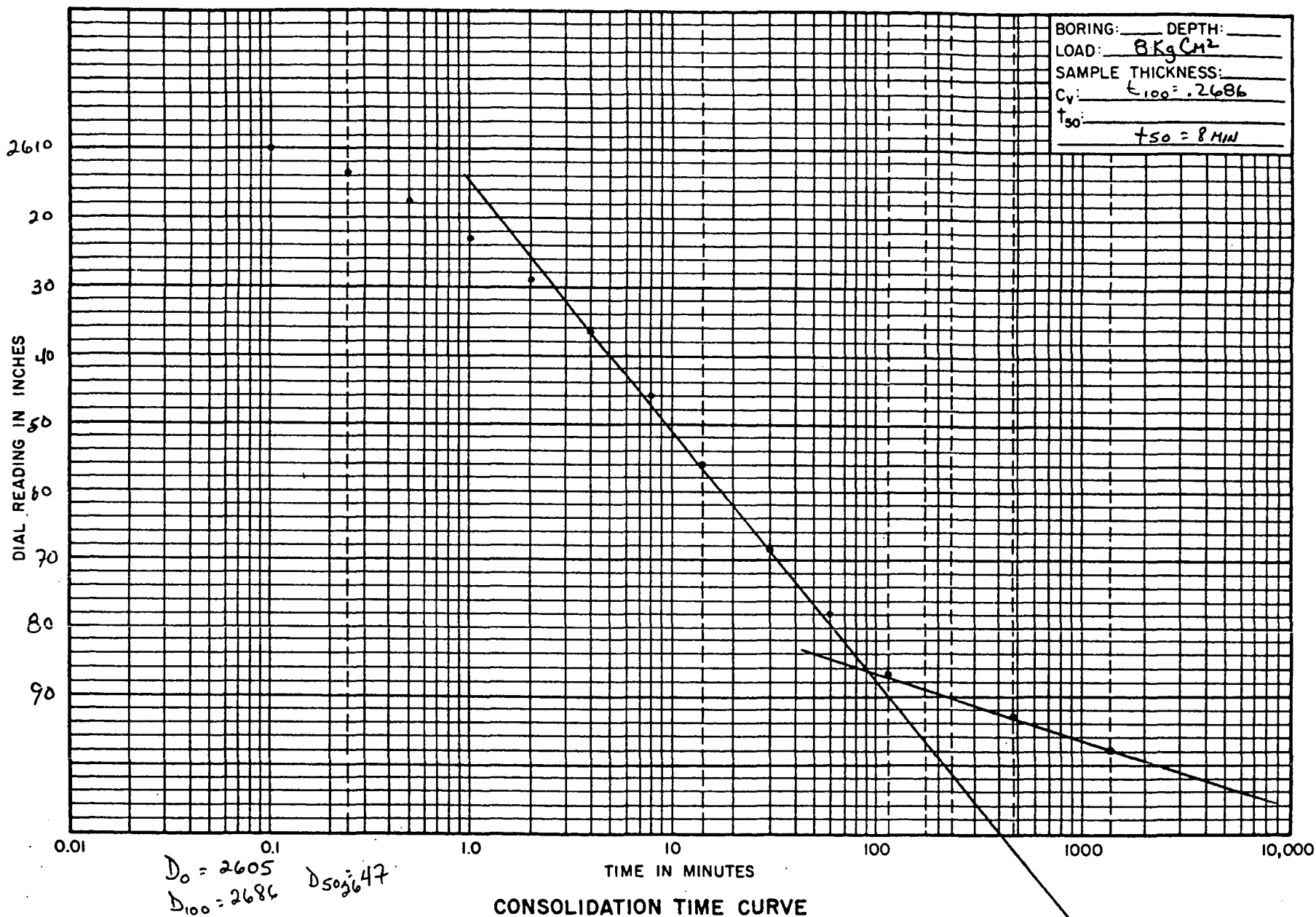
## CONSOLIDATION TEST DATA SHEET

Job No. \_\_\_\_\_ Boring No. \_\_\_\_\_ Depth \_\_\_\_\_ Consol. No. \_\_\_\_\_

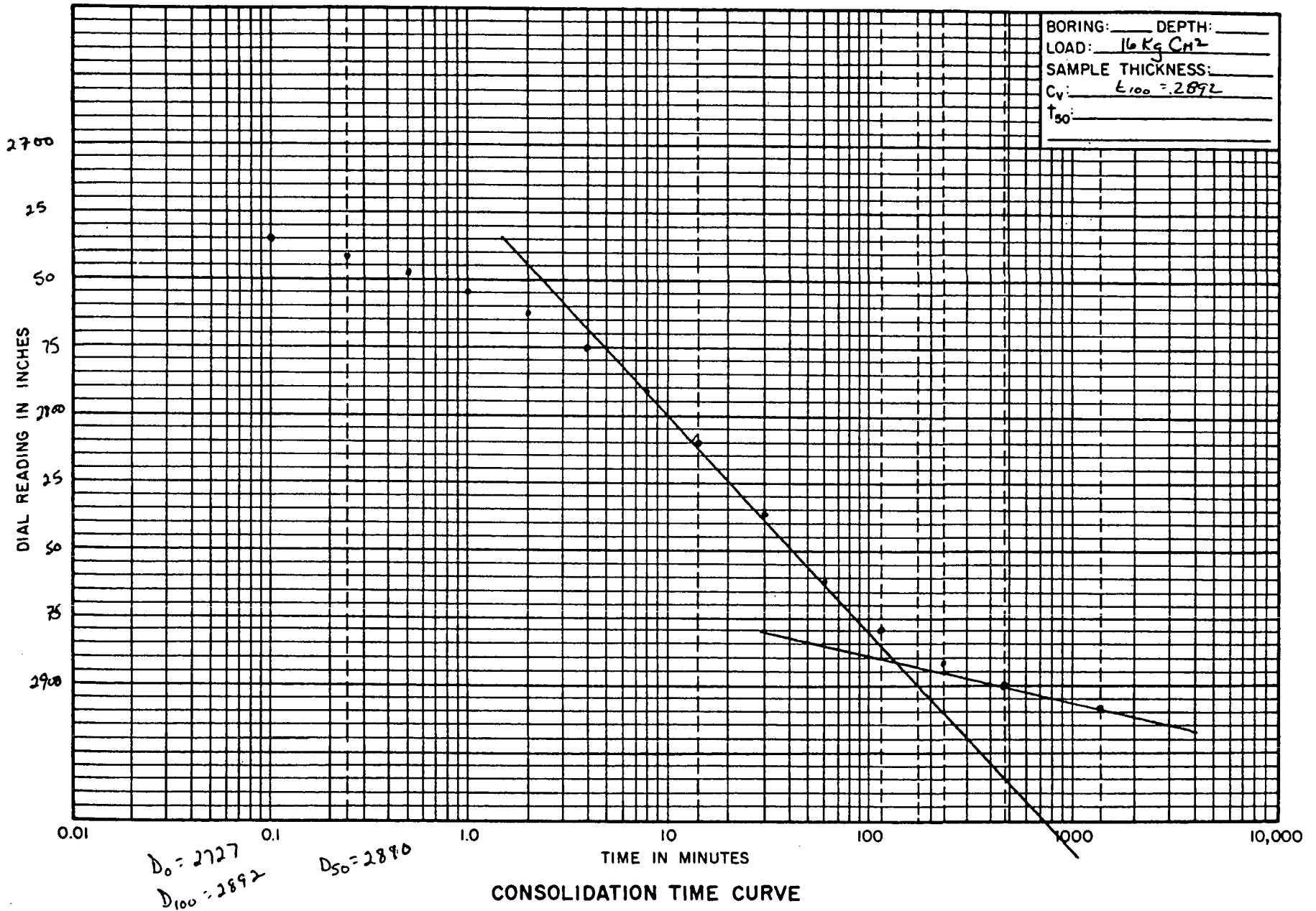
Observ. By	Date	Time	Elapsed Time min.	Dial Reading in.	Load No.
B.T.	19 Aug	0935	0	2945	32 Kg/cm <sup>2</sup>
			.1	2952	
			.25	2958	
			.5	2966	
			1	2971	
			2	2980	
			4	2997 1/2	
			8	3021 1/2	
			15	3051	
			30	3091	
			60	3132	
		1135	120	3162 1/2	
			240	3180	
		1645	430	3191	
		0810		3204	
Rebound					
B.T.	20 Aug	0810	0	3204	32 Kg/cm <sup>2</sup>
B.T.	21 Aug	0820	1450	3005	
Rebound					
	21 Aug	0835	0	3005	4 Kg/cm <sup>2</sup>
	22 Aug	1130		2888	

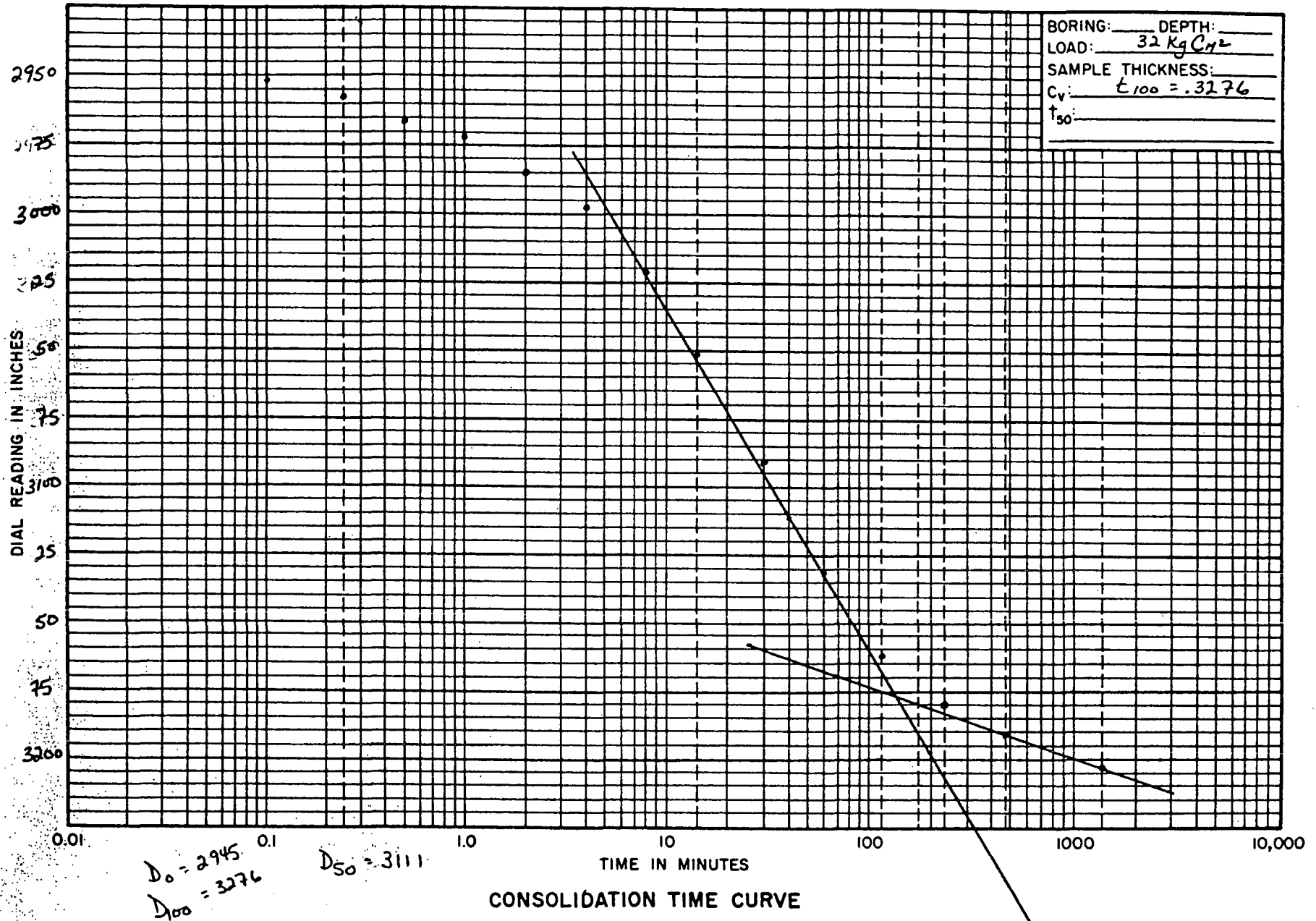






BORING: \_\_\_\_\_ DEPTH: \_\_\_\_\_  
 LOAD: 16 Kg Cm<sup>2</sup>  
 SAMPLE THICKNESS: \_\_\_\_\_  
 $C_v$ :  $E_{100} = 2.892$   
 $t_{50}$ : \_\_\_\_\_





BORING: \_\_\_\_\_ DEPTH: \_\_\_\_\_  
 LOAD: 32 Kg  $C_{H2}$  \_\_\_\_\_  
 SAMPLE THICKNESS: \_\_\_\_\_  
 $C_v$ :  $t_{100} = .3276$  \_\_\_\_\_  
 $t_{50}$ : \_\_\_\_\_

CONSOLIDATION TIME CURVE

# CONSOLIDATION TEST

Version 1.1

=====

JOB NO.:

BORING NO.:

SAMPLE NO.:

DEPTH:

TEST SPECIMEN:

TRIMMINGS:

-----  
                     INITIAL    FINAL  
 WET WEIGHT + TARE = 146.39    145.42  
 DRY WEIGHT + TARE = 130.43    130.43  
           TARE WEIGHT = 71.27    71.27  
           WATER CONTENT = 27.0%    25.3%

-----  
 WET WEIGHT + TARE = 57.19  
 DRY WEIGHT + TARE = 48.65  
           TARE WEIGHT = 15.54  
           WATER CONTENT = 25.8%

SPECIFIC GRAVITY = 2.8000  
 SAMPLE HEIGHT (IN) = 0.7500  
 SAMPLE DIAMETER (IN) = 1.9700  
 SAMPLE VOLUME (CC) = 37.4681  
 HEIGHT OF SOLIDS (IN) = 0.4229  
 INITIAL VOID RATIO = 0.7733

DEGREE OF SATURATION:

          INITIAL = 97.7%  
           FINAL = 101.0%

UNIT WEIGHT OF SPECIMEN:

          WET (PCF) = 125.1  
           DRY (PCF) = 98.5

MACHINE READING	PRESSURE KG/CM <sup>2</sup>	DIAL READING	CUM. CHANGE	CORR. CHANGE	VOID RATIO	COEFF. IN <sup>2</sup> /DAY
-----	-----	-----	-----	-----	-----	-----
-0.0054	4.000	0.2416	0.0084	0.0030	0.766	6.594
-0.0073	8.000	0.2314	0.0186	0.0113	0.747	4.836
-0.0095	16.000	0.2108	0.0392	0.0297	0.703	2.452
-0.0093	32.000	0.1724	0.0776	0.0683	0.612	0.824
-0.0100	8.000	0.1995	0.0505	0.0405	0.678	0.000
-0.0087	4.000	0.2112	0.0388	0.0301	0.702	0.000

Appendix 11

Alluvial Remnant Piezometer Construction Logs



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF MR-1

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. MR-1  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By GCC

DRILLING AND SAMPLING INFORMATION  
 Date Started 8/11/86 Date Completed 8/11/86  
 Method CFA Total Depth 7.76'  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 5.30'  
 Slot Size 0.010" Type PVC  
 Casing Dia. 4" Length 4.61'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 16.60							
	SAND - NOTED IN CUTTINGS, AND LOGS OF R-1 (30' SW) CPT-10 (20's), GW02, and GW07							
10	TD 7.76'. BORING (8") ADVANCED TO 7.0', WELL SUNK .76' WHEN PLACED IN SOFT SAND. SET WITH FLUSH VALVE, 4" SCH 40 PVC FLUSH JOINTED CASING, AND 0.010" SLOT SCREEN. #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL. GROUTED WITH CEMENT CAP. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.	8.84						

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF MR-2

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. MR-2  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By GCC

DRILLING AND SAMPLING INFORMATION  
 Date Started 8/18/86 Date Completed 8/18/86  
 Method MR Total Depth 20.0 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 17.98'  
 Slot Size 0.010" Type PVC  
 Casing Dia. 4" Length 5.00'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
	SURFACE ELEVATION 10.30							
0	TOPSOIL, black, root fragments, sandy clay	8.3	1	ST	20			
	SLIGHTLY SILTY SAND, gray, medium to fine grained, damp		2	SS	20			
			3	SS	53			
		2.3	4	SS	67			
	VERY SANDY CLAY, gray and ocre, medium grains	3	5	SS	73			
10	SAND, tan to pale gray, fine to medium grained quartz, multicolored pebbles, wet		6	SS	33			
		-3.7	7	SS	60			
			8	SS	27			
	VERY SILTY SAND, gray, very fine grained, wet		9	SS	67			
20		-7.7	10	ST	NR			
	SILTY CLAY, red, some black pinpoints, calcareous pebbles	-9.7	11	ST	80			
	T.D. 20.0'. BORING (3-7/8") ADVANCED TO 20.', SAMPLE PUSHED 20-22' BORING (8") OVERREAMED TO 20.0. MONITOR WELL SET WITH FLUSH VALVE, 4" SCH 40 PVC FLUSH JOINTED CASING AND 0.010" SLOT SCREEN. #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL. GROUTED WITH CEMENT CAP. WELL CAPPED AND VENTED. LOCKING PROTECTIVE CASING SET IN GROUT. ELEVATION OF TOP OF CASING SURVEYED.							

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING





# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF MR-3

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.L.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. MR-3  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By GCC

DRILLING AND SAMPLING INFORMATION  
 Date Started 8/18/86 Date Completed 8/18/86  
 Method MR Total Depth 20.0 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 17.49'  
 Slot Size 0.010" Type PVC  
 Casing Dia. 4" Length 5.00'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 9.20							
10	SAND-NOTED IN CUTTINGS, DRILLING RATE, AND CPT-5, APPROXIMATELY 30' SOUTH OF R-3							
20	SILTY CLAY, brown, some gray pockets	-10.6	1	ST	NR			
	T.D. 20.0'. BORING (3-7/8") ADVANCED TO 18', SAMPLES PUSHED 18-22'. BORING (8") OVERREAMED TO 20.0'. MONITOR WELL SET WITH FLUSH VALVE, 4" SCH 40 PVC FLUSH JOINTED CASING, AND 0.010" SLOT SCREEN. #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL. GROUTED WITH CEMENT CAP. LOCKING PROTECTIVE CASING SET IN GROUT. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.	-12.8	2	ST	85			

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF MR-4

Client FRENCH TASK GROUP  
Project Name French Ltd. 1986 F.I.  
Project Location Crosby, Texas  
Job No. 275-14 Boring No. MR-4  
Logged By S. L. Baird  
Approved By \_\_\_\_\_  
Drilled By GCC

DRILLING AND SAMPLING INFORMATION  
Date Started 8/18/86 Date Completed 8/18/86  
Method MR Total Depth 20.0 FEET  
WELL COMPLETION INFORMATION  
Screen Dia. 4" Length 18.45'  
Slot Size 0.010" Type PVC  
Casing Dia. 4" Length 5.00'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 9.50							
10	SAND - NOTED IN CUTTING, DRILLING RATE, AND CPT-8, APPROXIMATELY 30' SOUTH OF R-4							
20	VERY SILTY CLAY, reddish brown, some gray mottling and black pinpoints	-10.5						
	T.D. 20.5'. BORING (3-7/8") ADVANCED TO 20', SAMPLE PUSHED 20-22'. BORING (8") OVERREAMED TO 20.5'. MONITOR WELL SET WITH FLUSH VALVE, 4" SCH 40 PVC FLUSH JOINTED CASING, AND 0.010" SLOT SCREEN. #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL. GROUTED WITH CEMENT CAP. LOCKING PROTECTIVE CASING SET IN GROUT. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.	-12.3	1	ST	80			

SAMPLER TYPE  
SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING

Appendix 12

Monitor Wells and Piezometer Construction Logs

WELL ELEVATION SURVEY  
FRENCH LIMITED WASTE HAZARD SITE  
JOB NO. 86.055

AUGUST 22, 1986

WELL SITE	EASTING	NORTHING	ELEVATION
TBM "C" 11,363.16 10,056.05 14.64 (ER SPIKE GOLF PUMP RD. APPROX 200' E. MAPLE ST.)			
REI-10-1 (16)	12,102.42	10,108.71	12.8 (N.G.) S.O. 14.40 (top PVC @ bottom notch) 1.60
REI-10-2 (15)	12,109.56	10,084.34	11.9 (N.G.) 14.26 (top PVC @ bottom notch) 2.36
REI-10-3 (18)	12,047.35	10,141.01	13.8 (N.G.) 15.76 (top PVC @ bottom notch) 1.96
REI-10-4 (19)	12,120.28	10,138.40	14.4 (N.G.) 16.19 (top PVC @ bottom notch) 1.79
REI-3-5 (26)	12,598.86	9,495.79	10.0 (N.G.) 11.76 (top PVC @ bottom notch) 1.76 12.13 (top casing)
REI-#1 (12)	11,611.15	9,745.75	16.6 (N.G.) 18.75 (top PVC @ bottom notch) 2.15
REI-#2 (13)	11,633.32	10,094.03	10.3 (N.G.) 13.28 (top PVC @ bottom notch) 2.98
REI-#3 (14)	11,722.56	10,086.34	9.2 (N.G.) 11.69 (top PVC @ bottom notch) 2.49
REI-#4 (22)	11,943.57	10,094.28	9.5 (N.G.) 12.45 (top PVC @ bottom notch) 2.95
REI-12-1 (10)	10,739.44	10,715.92	10.5 (N.G.) 12.52 (top PVC @ bottom notch) 2.02
REI-12-2 (11)	10,732.74	10,733.19	10.4 (N.G.) 12.26 (top PVC @ bottom notch) 1.86
REI-11 (25)	12,503.10	9,958.88	9.9 (N.G.) 11.79 (top PVC @ bottom notch) 1.89
P-10-2 (20)	12,116.62	10,123.96	13.8 (N.G.) 15.76 (top PVC @ paint mark) 1.96
P-10-3 (17)	12,094.04	10,127.11	13.4 (N.G.) 15.44 (top PVC @ bottom notch) 2.04
P-10-4 (21)	12,120.51	10,117.36	13.7 (N.G.) 15.22 (top PVC @ bottom notch) 1.52

JWM: bgb  
86.055bm



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF REI 3-5

Client FRENCH LTD.  
 Project Name French Ltd.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. REI 3-5  
 Logged By P. Mann, Hydrogeologist  
 Approved By \_\_\_\_\_  
 Drilled By Southwest Labs/Gulf Coast Coring

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/15/86 Date Completed 7/18/86  
 Method Rotary Wash Total Depth 23.0'  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4 in Length 15.75'  
 Slot Size .010 in Type PVC Schedule 40  
 Casing Dia. 4 in Length 8.85'

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION							
0	TOPSOIL, CLAYEY SILT TO SILTY CLAY, brown and gray, mottled, with roots		0-2	ST	1.10			
		4.0	2-4	ST	1.10			
5	CLAYEY SAND, brown and gray, mottled, moderately soft, moist	6.0	4-6	ST	1.40			
	SANDY CLAY WITH SILT, brown and gray, mottled, firm	7.1	6-8	ST	1.25			
	SILTY SAND TO SAND, fine to coarse grained, gray, wet		8-10	SS	1.60			
10	12.0 to 14.5' with pebbles (fine gravel), subrounded		10-12	SS	1.50			
	below 14.5' brown to grayish brown, mostly medium grained		12-14	SS	1.50			
15	at 16-18' interval caving sands making continuous sampling difficult, drilled to 21.0' and then sampled		14-16	SS	1.60?			
			16-18	SS	1.60?			
20		22.3						
	SILTY CLAY, brown and gray, mottled, moderately firm	23.0	21-23	ST	1.90			
25	BORING COMPLETED TO 23.0' DEPTH USING 3-1/2" BIT ON 7/15/86. ON 7/18/86, BOREHOLE WAS REAMED OUT USING 7-7/8" BIT AND THEN THE MONITOR WELL WAS INSTALLED							

W. L. Collected 8-11-86

#### SAMPLER TYPE

SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

#### BORING METHOD

HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 2

### LITHOLOGIC LOG AND CONSTRUCTION OF REI 10-1

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. 10-1  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By SWL & GCC

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/21/86 Date Completed 7/28/86  
 Method MR Total Depth 153.5' FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 25.3'  
 Slot Size 0.010" Type PVC  
 Casing Dia. 4" & 8" Length 124.3/56

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 12.80							
	SURFACE FILL, gravel, asphalt, rubber							
		7.8	1	PT	NR			
	SAND AND GRAVEL, brown, medium grained, 10% fines, wet, odor		2	SS	33			
		4.5	3	SS	53			
10	SLIGHTLY CLAYEY SAND, olive, fine grained		4	SS	53			
	SILTY SAND, medium to dark gray, fine to medium grained, odor, wet		5	PT	37			
			6	PT	47			
20			7	PT	NR			
			8	SS	60			
			9	SS	60			
			10	SS	67			
			11	SS	73			
			12	SS	67			
30	VERY SANDY SILT, tan, some dark staining, odor	-20.2	13	SS	67			
	CLAYEY SILT, dark gray	-23.1	14	SS	80			
	SILTY SAND, dark gray, wet, odor		15	SS	80			
			16	SS	80			
40			17	SS	80			
			18	SS	47			
		-29.7	19	SS	100			
	VERY SILTY CLAY, grayish green, some brown lenses of clayey sand		20	PT	13			
	SILTY SAND/SANDY SILT, olive gray, odor	-33.5	21	PT	17			
50			22	PT	33			
	SILTY CLAY, olive, blue, red mottles, gray silty sand lenses, odor	-38.7	23	PT	57			
			24	PT	50			
60	EIGHT INCH SURFACE CASING SET @ 56.0'							
	calcareous nodules and clayey silt with depth							
70								
		-64.2						
80	CLAY, very stiff, red							
90	SANDY SILT, grayish green	-75.7						
100	SANDY SILT/SILTY SAND	-87.2						
	CLAY	-91.7						
110	INTERBEDDED CLAY AND SAND	-97.2						
120								

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING

# RESOURCE ENGINEERING

Sheet 2 of 2

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. 10-1

## CONTINUATION OF REI 10-1

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
120		-109.7						
130	SAND, SILTY SAND AND GRAVELS							
140								
150	GRAVELLY CLAY, blue green	-139.7 -140.7	25	SS	53			
160	TD 153.5 BORING (3-7/8") ADVANCED TO 152', SAMPLE PUSHED 152-153.5. BORING (7-1/2") OVER REAMED TO 148.0'. EIGHT INCH PVC CASING (COUPLED WITH STAINLESS STEEL SCREWS) SET AT 56 FEET. FOUR INCH MONITOR WELL SET WITH FLUSH VALVE, 4" PVC FLUSH JOINTED CASING AND 0.010" SLOT SCREEN. #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL, GROUTED TO SURFACE WITH CEMENT/BENTONITE SLURRY. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.							



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF REI 10-2

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. 10-2  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By GCC

DRILLING AND SAMPLING INFORMATION  
 Date Started 8/8/86 Date Completed 8/8/86  
 Method MR Total Depth 48.0 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 13.75'  
 Slot Size 0.010" Type PVC  
 Casing Dia. 4" Length 36.61

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 11.90							
0	SAND AND GRAVEL							
10	SLIGHTLY CLAYEY SAND	2.9						
	SILTY SAND	.9						
20								
30	SILTY CLAY	-16.1						
		-20.1						
	SILTY SAND, gray green, strong odor, wet							
40			1	SS	67			
			2	SS	40			
			3	SS	80			
	SLIGHTLY CLAYEY SAND, gray with yellowish brown stain, some lignite chips	-30.1	4	SS	47			
			5	SS	27			
	SILTY CLAY	-35.1	6	SS	67			
		-36.1	7	SS	100			
50	TD 48.0 BORING (8") DRILLED TO 36'. CONTINUOUSLY SAMPLED IN 3-7/8" BORING TO 49.5. UPPER HOLE COMPARED WITH CONTINUOUS SAMPLE LOG FROM ADJACENT 10-1. ELECTRIC LOGGED. FOUR INCH MONITOR WELL SET WITH FLUSH VALVE, 4" SCH 40 PVC FLUSH JOINTED CASING, AND 0.010" SLOT SCREEN #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL GROUTED TO SURFACE WITH CEMENT/BENTONITE SLURRY. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.							

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING





# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF REI 10-3

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.L.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. 10-3  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By SWL

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/27/86 Date Completed 7/27/86  
 Method MR Total Depth 48.0 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 10.30'  
 Slot Size 0.010" Type PVC  
 Casing Dia. 4" Length 39.66

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 13.80							
	SURFACE FILL AND GRAVEL	10.7						
	SAND AND GRAVEL							
10		4.3						
	SLIGHTLY CLAYEY SAND	2.6						
	SILTY SAND							
20								
30		-18.6						
	SANDY SILT/CLAYEY SILT							
		-24.2						
40	SILTY SAND/SANDY SILT							
	VERY SILTY CLAY, reddish brown	-33.7	1	SS	53			
50	TD 48.0 BORING (8") DRILLED TO 48'. ELECTRIC LOGGED AND COMPARED WITH CONTINUOUS SAMPLE LOG FROM ADJACENT 10-1. FOUR INCH MONITOR WELL SET WITH FLUSH VALVE, 4" SCH 40 PVC FLUSH JOINTED CASING, AND 0.010" SLOT SCREEN #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL. GROUTED TO SURFACE WITH CEMENT/BENTONITE SLURRY. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.	-34.2						

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF REI 10-4

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. 10-4  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By SWL

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/28/86 Date Completed 7/28/86  
 Method MR Total Depth 46.0 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 12.80'  
 Slot Size 0.010" Type PVC  
 Casing Dia. 4" Length 36.99

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 14.40							
	SURFACE FILL, rubber							
		8.4						
	SAND AND GRAVEL	5.9						
10	CLAYEY SAND	1.9						
	SILTY SAND							
20								
		-14.1						
30	SANDY SILT	-7.1						
	CLAYEY SILT	-20.6						
	SLIGHTLY SILTY CLAY	-22.6						
40	SILTY SAND/SANDY SILT							
		-33.6						
50	TD 48.0 BORING (8") DRILLED TO 48.0'. ELECTRIC LOGGED AND COMPARED WITH CONTINUOUS SAMPLE LOG FROM ADJACENT 10-1. FOUR INCH MONITOR WELL SET WITH FLUSH VALVE, 4" SCH 40 PVC FLUSH JOINTED CASING AND 0.010" SLOT SCREEN #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL. GROUTED TO SURFACE WITH CEMENT/BENTONITE SLURRY. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.							

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF REI P10-2

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. P10-2  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By GCC

DRILLING AND SAMPLING INFORMATION  
 Date Started 8/8/86 Date Completed 8/9/86  
 Method MR Total Depth 92.0 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 2.01  
 Slot Size 0.010" Type PVC  
 Casing Dia. 14" & 16" Length 91.95

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 13.80							
10	BORING ADVANCED TO 75' BEFORE TAKING SAMPLES							
20								
30								
40								
50								
60								
70								
		-61.2	1	ST	50			
	SILT AND SILTY CLAY, blue and red, calcareous nodules	-64.2	2	SS	NR			
80	SILTY CLAY, red with blue veining, same calcareous chips in isolated pockets		3	SS	75			
			4	ST	50			
			5	ST	100			
	increasing silt		6	ST	75			
			7	ST	50			
90		-76.7	8	SS	100			
	CLAYEY SILT, dark green, damp	-78.7	9	SS	100			
	TD 92.0. SIX INCH CASING SET TO 80'. TWO INCH SCREEN SET WITH CAP ON BOTTOM COUPLED WITH SLIP COUPLINGS AND STAINLESS STEEL SCREENS TO 1-1/4" FLUSH JOINTED RISER PIPE. #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL. GROUTED WITH CEMENT/BENTONITE SLURRY. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.							

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF REI P10-3

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. P10-3  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By GCC

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/29/86 Date Completed 7/31/86  
 Method MR Total Depth 84.0 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 2" Length 2.00  
 Slot Size 0.010" Type PVC  
 Casing Dia. 2" & 6" Length 82.04

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 13.40							
	ASPHALT AND RUBBER FILL, black, gray and white		1	ST	40			
		8.4	2	ST	60			
	VERY SILTY SAND, gray, fine grained, saturated		3	SS	80			
10								
		.4						
	SLIGHTLY SILTY SAND, orange and dark gray, black staining, medium to fine grain		4	ST	65			
20			5	ST	45			
	SAMPLING DISCONTINUED DUE TO EXCESSIVE SLOUGHING OF SIDE WALL AND CIRCULATION LOSS PROBLEMS							
30								
40								
	SANDY CLAY, gray	-34.6	6	ST	--			
50	SILTY CLAY, gray and brown		7	ST	--			
		-40.6	8	ST	75			
	SANDY CLAY, brown		9	ST	75			
		-44.1	10	ST	50			
60	SILTY CLAY, red and brown horizontal bands with gray silt partings. Some ferrous stains, black staining, odor		11	ST	50			
			12	ST	95			
			13	ST	100			
			14	ST	75			
			15	ST	60			
	VERY SILTY CLAY, blue and red mottles	-53.9	16	ST	60			
70	SLIGHTLY SILTY CLAY, dark brownish red	-56.6	17	ST	65			
		-59.6	18	ST	75			
	SANDY CLAY, blue and red, strong odor		19	ST	25			
		-63.6	20	ST	75			
80	SILTY CLAY, dark red, calcareous nodules, stiff		21	ST	75			
			22	ST	75			
		-70.6	23	ST	75			
90	TD 84.0'. SIX INCH CASING SET TO 80.0'. TWO INCH, 0.010" SLOT SCREEN SET WITH CAP ON BOTTOM. FLUSH JOINTED TRILOC PVC RISER PIPE. #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL. GROUTED WITH CEMENT/BENTONITE SLURRY. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.							

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF REI P10-4

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. P10-4  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By GCC

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/31/86 Date Completed 8/1/86  
 Method MR Total Depth 82.2 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 2" Length 2.0  
 Slot Size 0.010" Type PVC  
 Casing Dia. 2" & 6" Length 81.2

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 13.70							
10								
20	BORING ADVANCED TO 60' BEFORE TAKING SAMPLES							
30								
40								
50								
60		-46.3						
	SILTY CLAY, brown, gray and yellow horizontal bands with gray silt partings		1	ST	80			
		-51.8	2	ST	75			
	SILTY SAND, brown	-53.3	3	ST	80			
	SILTY CLAY, blue with brown mottles, very stiff	-55.1	4	ST	65			
70	VERY CLAYEY SILT, brown, blue, soft	-57.1	5	ST	70			
	CALCAREOUS NODULES, white with 20% blue silty clay	-60.1	6	ST	45			
	SANDY SILT, blue, brown, damp and loose	-62.1	7	ST	60			
	SILTY SAND, brown, some gray mottles, wet	-63.5	8	ST	50			
80	SLIGHTLY SILTY CLAY, red		9	ST	55			
		-69.1	10	ST	80			
			11	ST	80			
90	TD 82.2. SIX INCH CASING SET TO 80.0'. TWO INCH, 0.010" SLOT SCREEN SET WITH CAP ON BOTTOM. FLUSH JOINTED TRILOC PVC RISER PIPE. #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL. GROUTED WITH CEMENT/BENTONITE SLURRY. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.							

SAMPLER TYPE BORING METHOD  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 2

### LITHOLOGIC LOG AND CONSTRUCTION OF REI 11

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. 11  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By SWL

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/17/86 Date Completed 7/31/86  
 Method MR Total Depth 152.5 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 16.56  
 Slot Size 0.010" Type PVC  
 Casing Dia. 4" & 8" Length 137.81

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 9.90							
	CLAYEY SAND, dark gray		1	ST	47			
	SILTY SAND, brown to dark gray, medium to coarse grained, saturated, some gravels and pebbles		2	ST	40			
			3	ST	37			
10			4	ST	NR			
			5	ST	27			
			6	ST	10			
20			7	ST	NR			
	SAND, white, coarse to medium, angular to subrounded, multicolored gravels, odor		8	SS	73			
	SANDY CLAY, gray		9	SS	73			
	SILTY CLAY, tan, odor		10	SS	100			
30			11	SS	100			
	SANDY CLAY, gray, damp, odor		12	SS	73			
			13	SS	73			
	CLAYEY SAND, tan, damp		14	SS	73			
			15	SS	73			
40			16	SS	93			
			17	SS	80			
			18	ST	67			
	SILTY SAND, gray and red, medium to fine grained, saturated		19	ST	93			
	SLIGHTLY SILTY CLAY, reddish brown, gray veining, blocky texture		20	ST	67			
50			21	ST	78			
	SLIGHTLY SILTY CLAY EIGHT INCH SURFACE CASING SET TO 50.5							
60								
	CLAYEY SILT, many calcareous nodules, some sand seams							
70								
	CLAY, less than 10% silt							
80								
90	SANDY SILT							
100								
	SILTY CLAY							
110								
	SILTY SAND/SANDY SILT							
120								
	SILTY CLAY							

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING

# RESOURCE ENGINEERING

Sheet 2 of 2

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. 11

## CONTINUATION OF REI-11

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
120								
130								
140	SILTY SAND/SANDY SILT							
150	SANDY SILT, dark green, damp		27	SS	87			
155	SILTY CLAY, grayish green with red mottles							
	T.D. 155.0 BORING (3 5/8") ADVANCED TO 155; SAMPLE PUSHED 155-156.5: BORING (7 5/8") OVERREAMED TO 152.5. FOUR INCH FLUSH JOINTED PVC SET TO 152.5 AND FOUR INCH 0.010" SLOT SCREEN WITH FLUSH VALVE. #3 SAND USED IN SAND PACK, 75 GALLONS OF BENTONITE GEL TRIMMED 120-134'. BORING CAPPED 3 HOURS LATER WITH CEMENT/BENTONITE SLURRY. WELL CAPPED AND VENTED. TOP OF CASING ELEVATION SURVEYED.		28	SS	55			



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 2

### LITHOLOGIC LOG AND CONSTRUCTION OF REI 12-1

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.L.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. 12-1  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By SWL

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/24/86 Date Completed 8/2/86  
 Method MR Total Depth 151.0 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 36.50  
 Slot Size 0.010" Type PVC  
 Casing Dia. 4" & 8" Length 116.52

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 10.50							
0	SAND, medium to fine grained, angular, wet							
10								
20	CLAYEY SILT/SILTY CLAY							
30	CLAYEY SAND							
30	SILTY CLAY							
40	CLAYEY SILT/SANDY SILT, red							
40	EIGHT INCH CASING, SET TO 33.35							
50	CLAYEY SAND, white, damp		1	SS	75			
50	CLAYEY SAND, white to tan, damp		2	ST	30			
50	SANDY CLAY, tan		3	ST	85			
60	SLIGHTLY SILTY CLAY, multicolored red, brown, green and blue, firm to very stiff, calcareous nodules and specks		4	ST	80			
70			5	ST	50			
70			6	ST	45			
80	CLAY, red, stiff, occasional calcareous specks		7	ST	60			
80			8	ST	45			
90			9	ST	95			
90	SANDY SILT, medium gray with yellowish brown sand lenses		10	ST	70			
100			11	SS	NR			
100	PEAT/SILTY CLAY, dark gray, interbedded		12	SS	100			
100	SILTY CLAY, bluish gray		13	SS	80			
110	SANDY SILT, bluish gray		14	SS	100			
110			15	SS	100			
120	SILTY CLAY/CLAYEY SILT, grayish green							
120	SILTY SAND, gray and green, fine grained, damp, 20% fines		16	SS	NR			

SAMPLER TYPE  
 SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

BORING METHOD  
 HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING



# RESOURCE ENGINEERING

Sheet 2 of 2

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. 12-1

## CONTINUATION OF REI 12-1

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
120	saturated, less than 5% fines		17	SS	27			
130			18	SS	40			
			19	SS	27			
140			20	SS	60			
	VERY SANDY SILT, dark olive		21	SS	NR			
150	SILTY CLAY, grayish green with red		22	SS	67			
	T.D. 153.5. BORING (3 5/8") ADVANCED TO 153.5; SAMPLE PUSHED 153.5-155. BORING (7 5/8") OVERREAMED TO 151.0 FOUR INCH FLUSH JOINTED PVC SET, FOUR INCH 0.010" SLOT SCREEN WITH FLUSH VALVE. #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS USED IN SEAL, CAPPED WITH CEMENT/BENTONITE SLURRY. STAINLESS STEEL CENTRALIZERS @ 110', 80' and 40'. WELL CAPPED AND VENTED. TOP OF CASING ELEVATION SURVEYED.		23	SS	80			



# RESOURCE ENGINEERING

## SUBSURFACE EXPLORATION

Sheet 1 of 1

### LITHOLOGIC LOG AND CONSTRUCTION OF REI 12-2

Client FRENCH LTD. TASK GROUP  
 Project Name French Ltd. 1986 F.I.  
 Project Location Crosby, Texas  
 Job No. 275-14 Boring No. 12-2  
 Logged By S. L. Baird  
 Approved By \_\_\_\_\_  
 Drilled By SWL

DRILLING AND SAMPLING INFORMATION  
 Date Started 7/29/86 Date Completed 7/29/86  
 Method MR Total Depth 50.0 FEET  
 WELL COMPLETION INFORMATION  
 Screen Dia. 4" Length 15.17  
 Slot Size 0.010" Type PVC  
 Casing Dia. 4" Length 36.69

DEPTH IN FEET	DESCRIPTION	STRATUM ELEVATION IN FEET	SAMPLE NO.	SAMPLE TYPE	% RECOVERY	GRAPHIC LOG	WELL COMPLETION	WATER LEVEL
0	SURFACE ELEVATION 10.40							
	SURFACE FILL, SAND, RAILROAD TIES							
10	SILTY SAND/SAND							
20	SILTY CLAY							
30	SILTY SAND							
	VERY SANDY CLAY, red							
40	SILTY SAND, red and gray		1	SS	93			
			2	SS	65			
			3	SS	37			
			4	SS	50			
			5	SS	67			
			6	SS	87			
	CLAYEY SAND, grayish blue		7	SS	100			
50	SILTY CLAY, gray		8	SS	100			
	T.D. 50.5. BORING (3 7/8") ADVANCED TO 49, SAMPLE PUSHED 49-50.5. BORING (8") OVERREAMED TO 50. FOUR INCH MONITOR WELL SET WITH FLUSH VALVE, 4" SCH 40 PVC FLUSH JOINTED CASING AND 0.010" SLOT SCREEN. #3 SAND USED IN SAND PACK, 1/2" BENTONITE PELLETS IN SEAL. GROUTED WITH CEMENT/BENTONITE SLURRY. WELL CAPPED AND VENTED. ELEVATION OF TOP OF CASING SURVEYED.							

#### SAMPLER TYPE

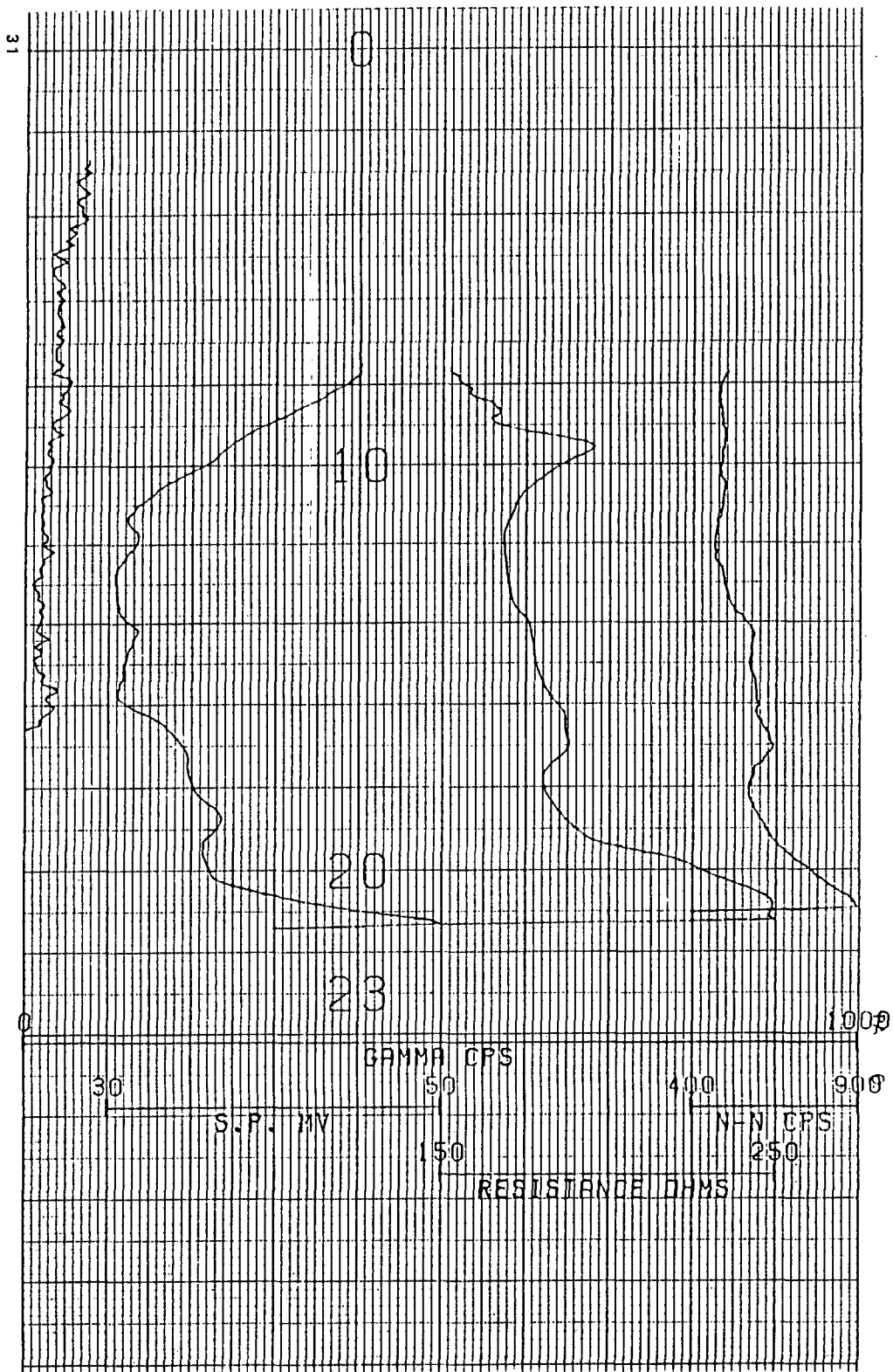
SS - DRIVEN SPLIT SPOON CA - CONTINUOUS FLIGHT AUGER  
 ST - PRESSED SHELBY TUBE RC - ROCK CORE

#### BORING METHOD

HSA - HOLLOW STEM AUGERS DC - DRIVING CASING  
 CFA - CONTINUOUS FLIGHT AUGERS MD - MUD DRILLING

Appendix 13

Monitor Well and Piezometer Geophysical (E-Logs) Logs



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**

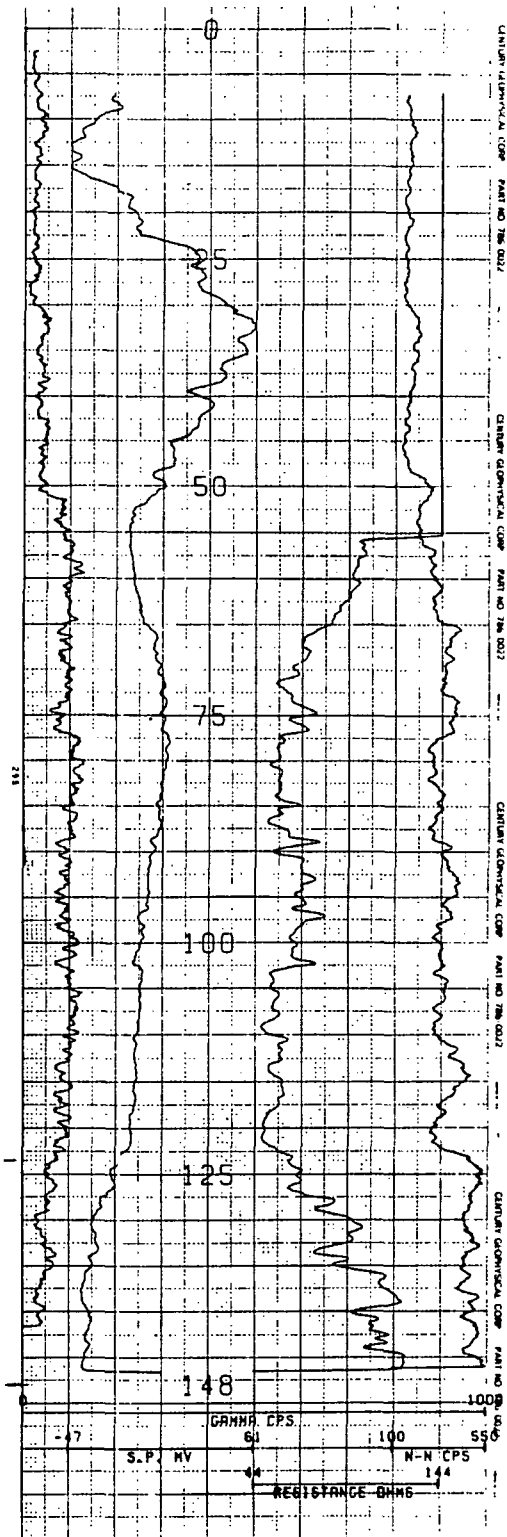
**REI 3-5**

**FRENCH LIMITED**

DRAWN BY:

DATE: 11-22-86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

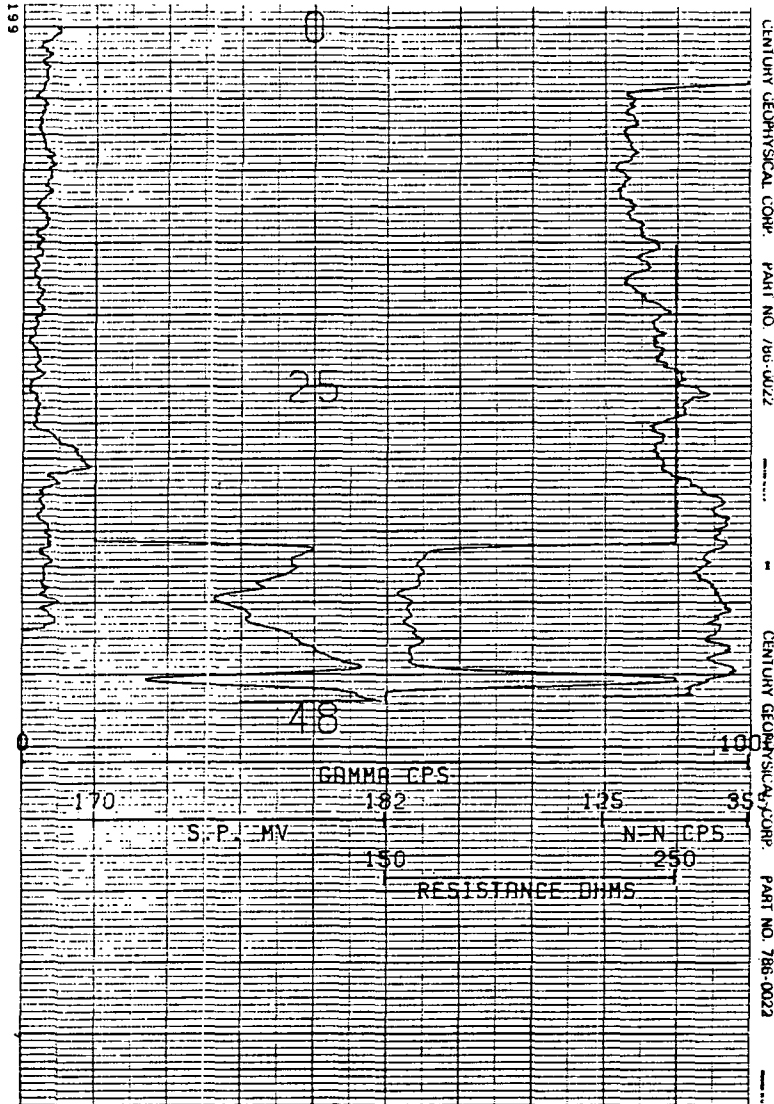
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG  
REI 10-1  
FRENCH LIMITED**

DRAWN BY: L.M.G.

DATE: 11-20-86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

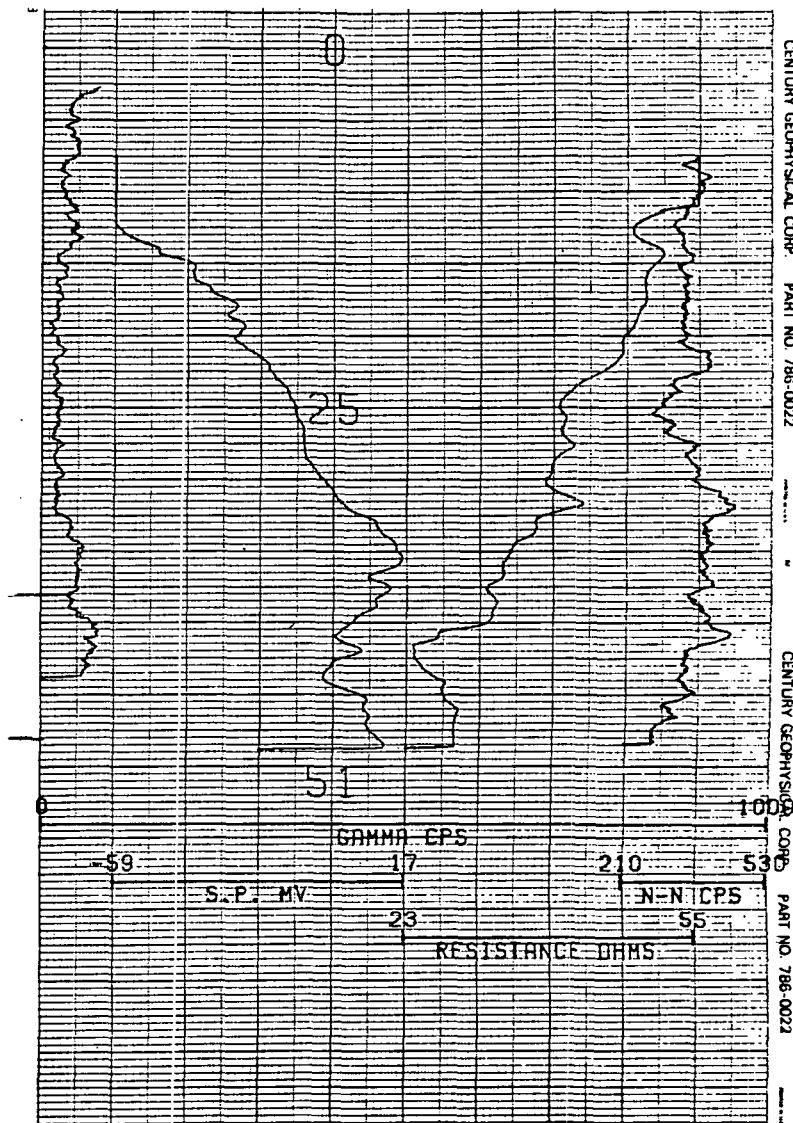
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**  
**REI 10-2**  
**FRENCH LIMITED**

DRAWN BY: L.M.G.

DATE: 11-20-86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

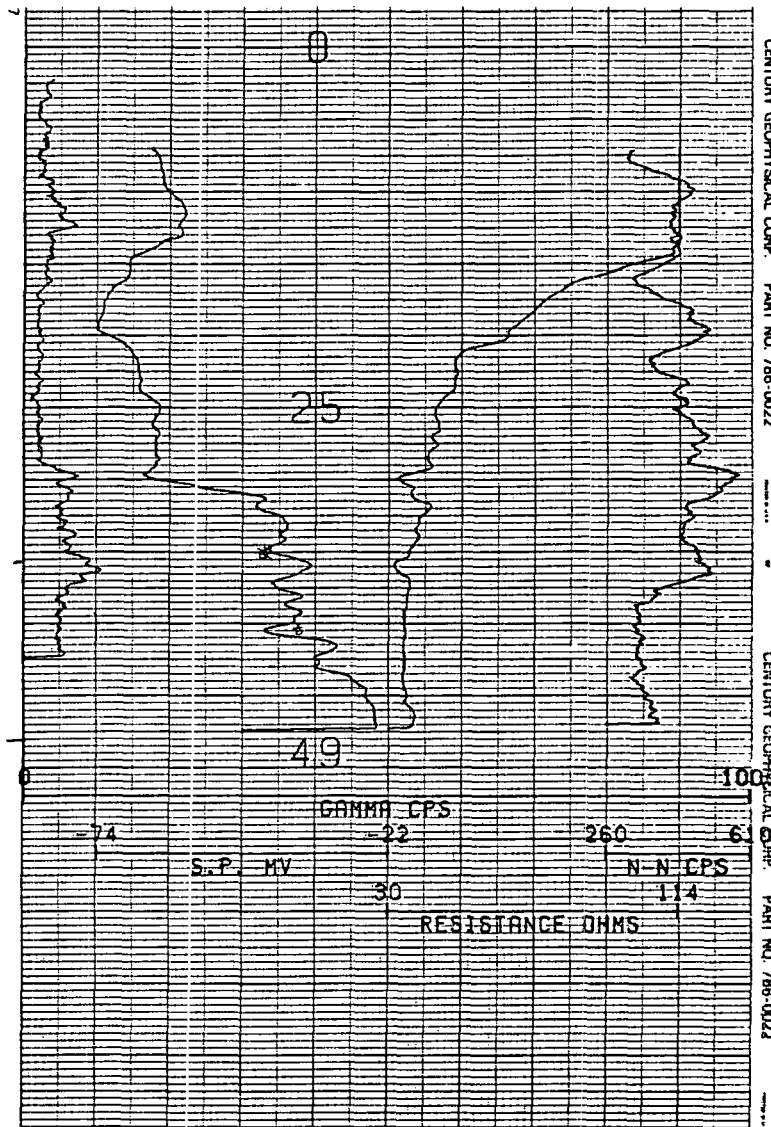
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**  
**REI 10-3**  
**FRENCH LIMITED**

DRAWN BY: L.M.G.

DATE: 11-20-86

PROJECT NO. 275-14



CENTURY GEOPHYSICAL CORP. PART NO. 786-0022

CENTURY GEOPHYSICAL CORP. PART NO. 786-0022



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG  
REI 10-4  
FRENCH LIMITED**

DRAWN BY:

L.M.G.

DATE:

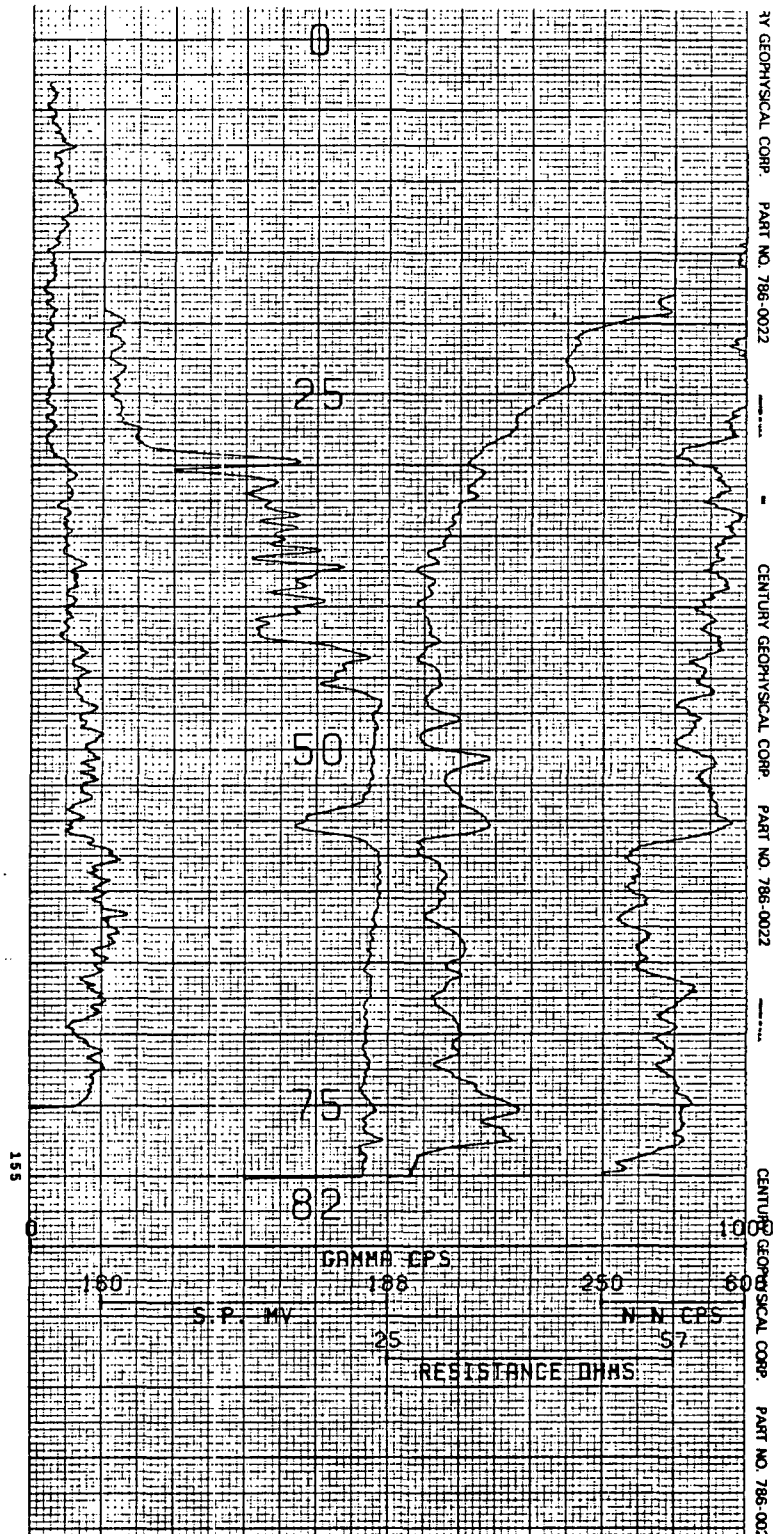
11-20-86

PROJECT NO.

275-14







**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG**  
**REI P10-4**  
**FRENCH LIMITED**

DRAWN BY: L.M.G.

DATE: 11-20-86

PROJECT NO. 275-14



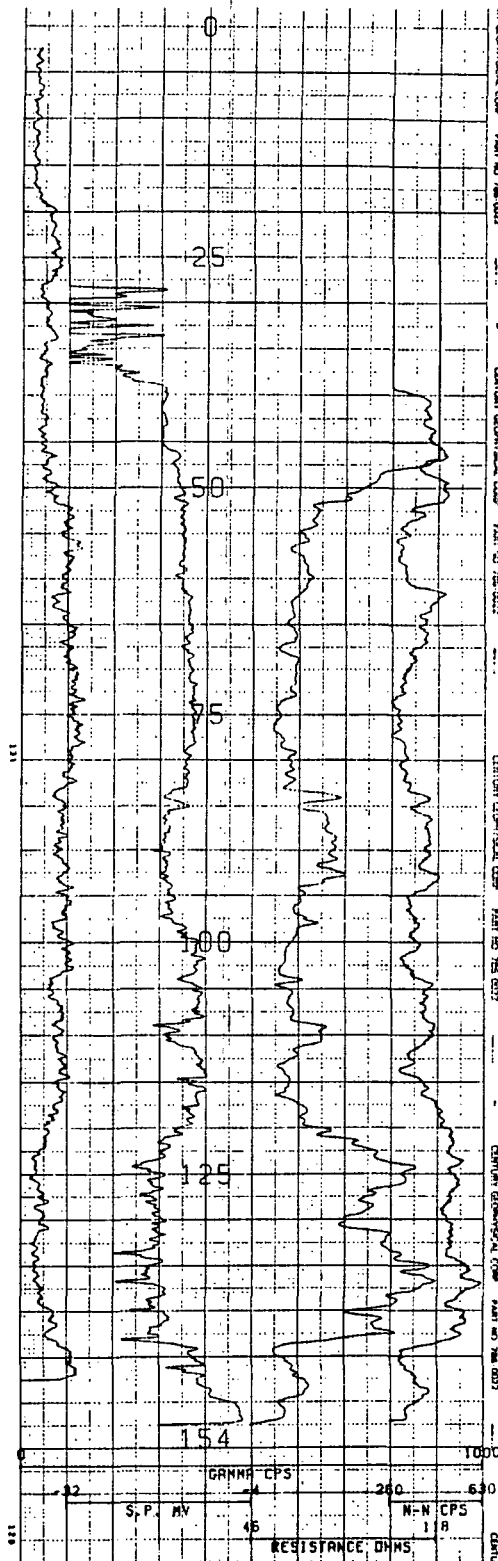
**ENVIRONMENTAL CONSULTANTS**  
**HOUSTON, TEXAS**

**DRAWN BY:**

DATE:

PROJECT NO.

275-14



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

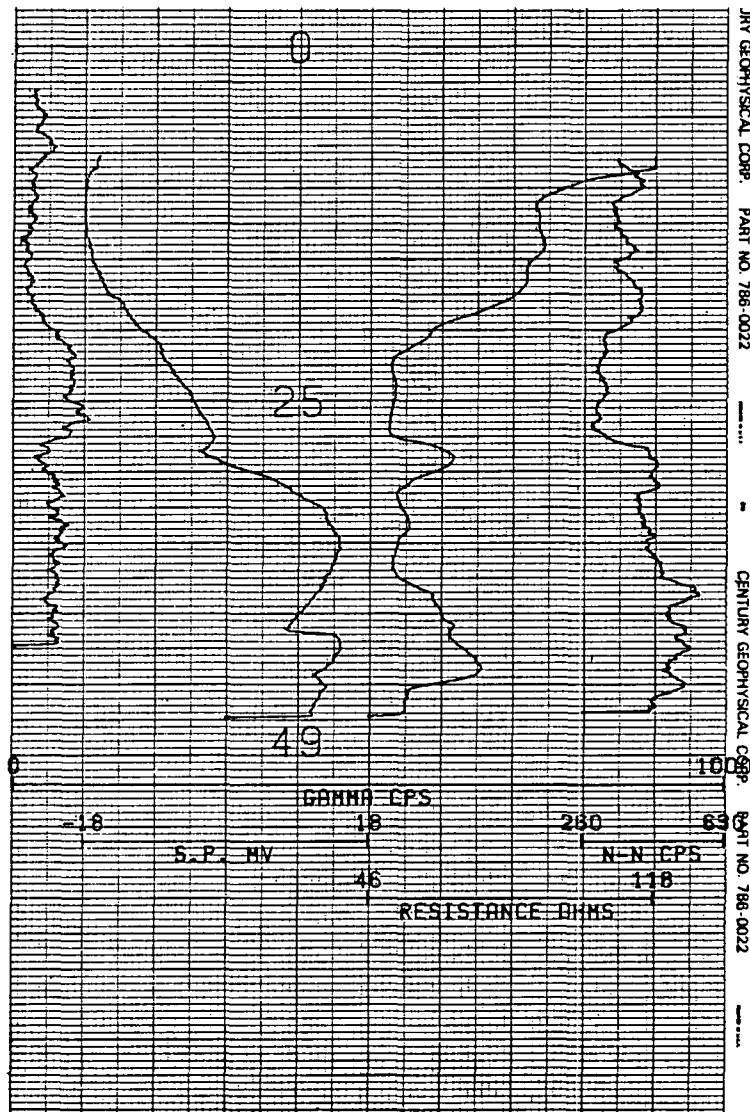
**GEOPHYSICAL LOG  
REI 12-1**

**FRENCH LIMITED**

DRAWN BY: L.M.G.

DATE: 11-20-86

PROJECT NO. 275-14



JRY GEOPHYSICAL CORP. PART NO. 786-0022  
CENTURY GEOPHYSICAL CORP. PART NO. 786-0022



**RESOURCE ENGINEERING INC.**

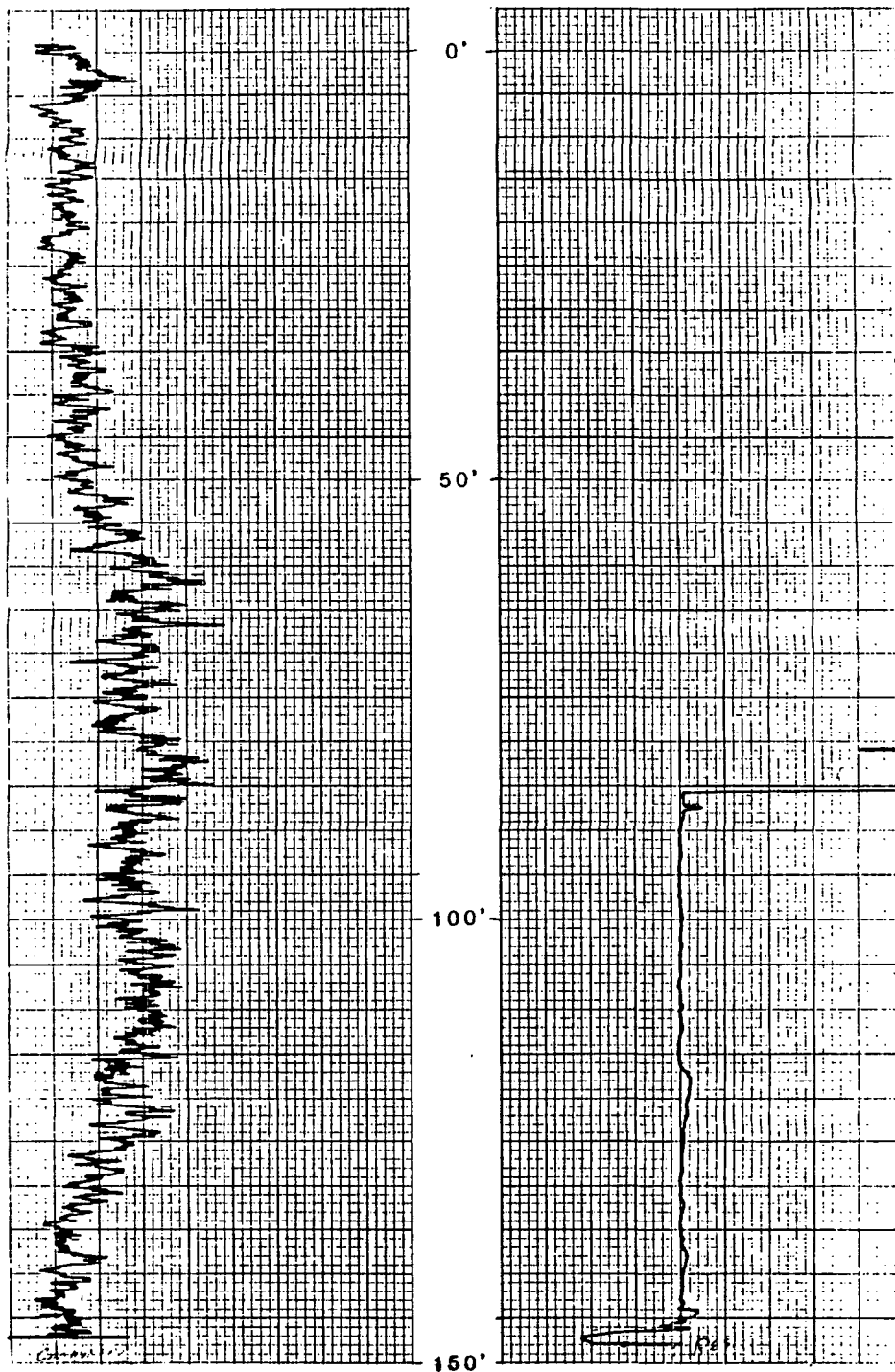
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG  
REI 12-2  
FRENCH LIMITED**

DRAWN BY: L.M.G.

DATE: 11-20-86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

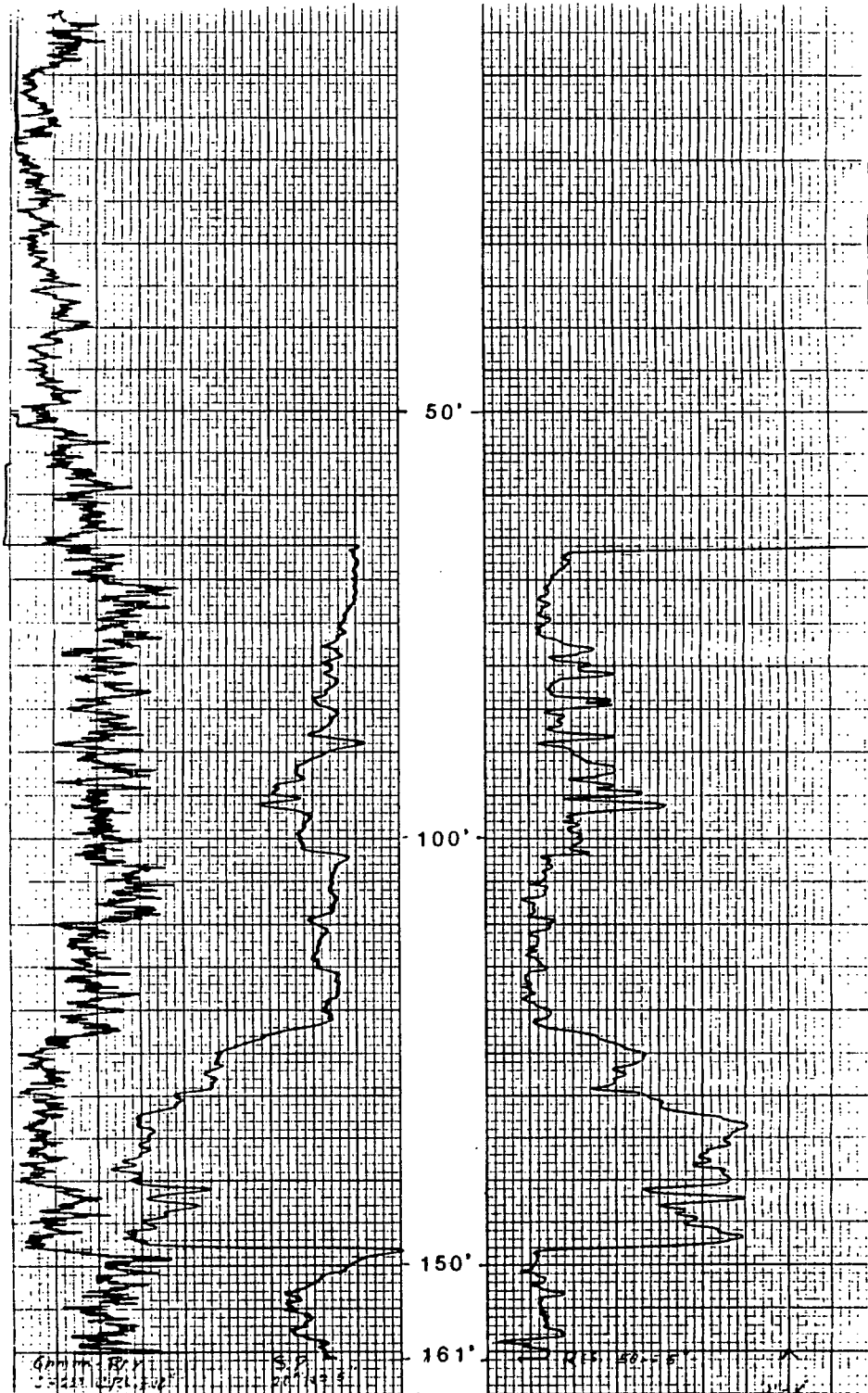
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

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GW-25  
FRENCH LIMITED**

DRAWN BY: L.C.S.

DATE: 12/12/86

PROJECT NO. 275-14

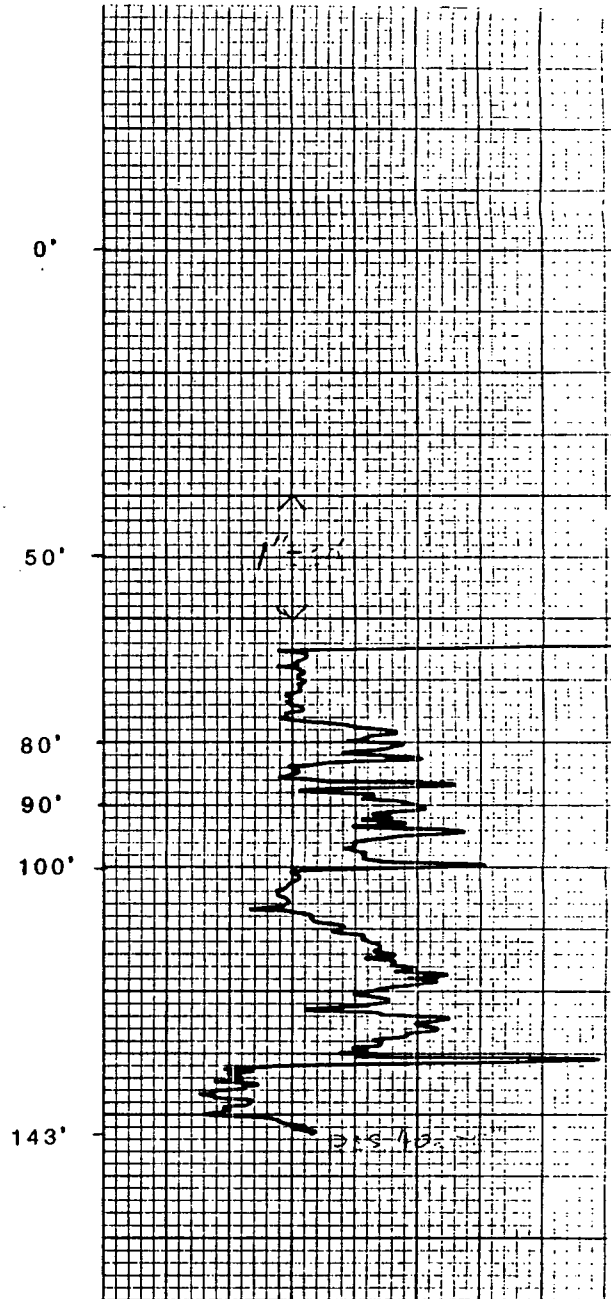
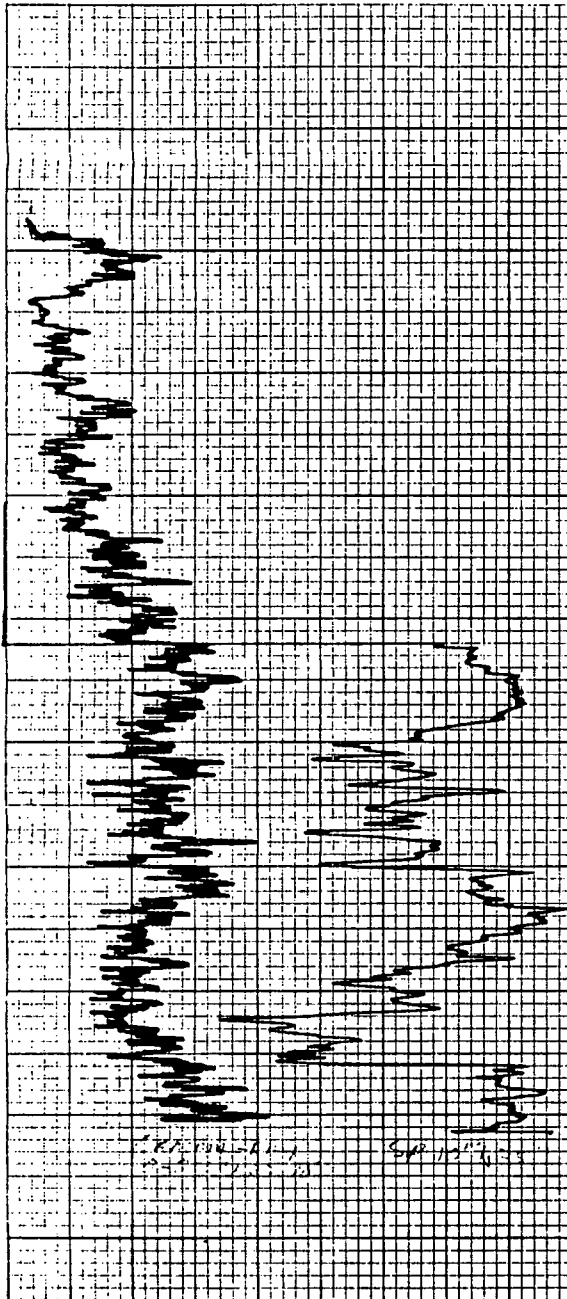


**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG  
REI 3-4  
FRENCH LIMITED**

DRAWN BY: L.C.S.	DATE: 12/12/86	PROJECT NO. 275-14
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**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

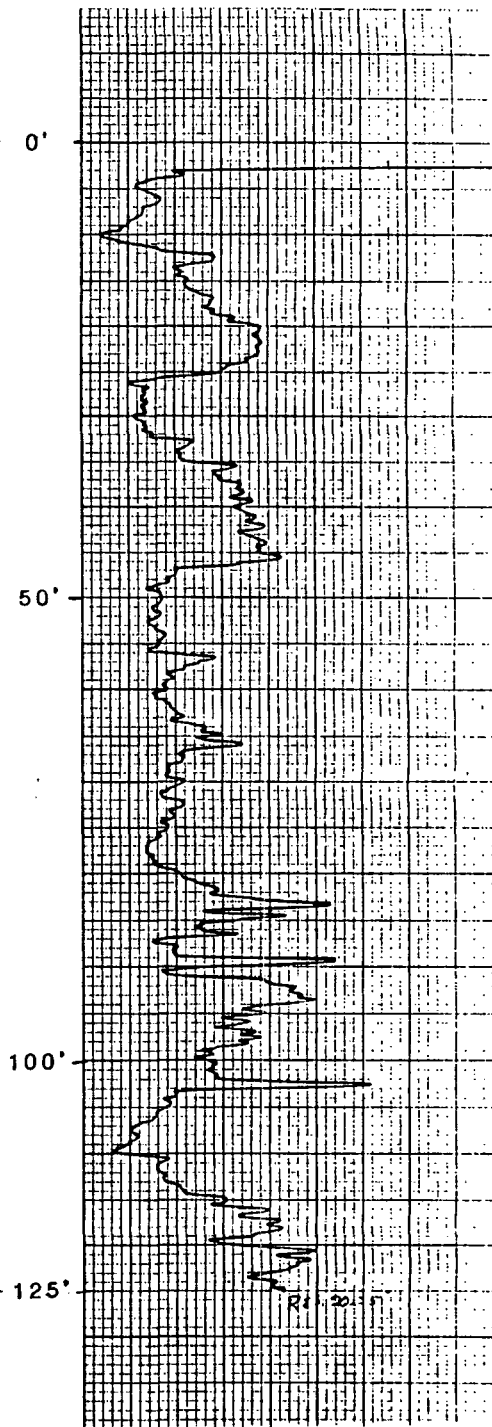
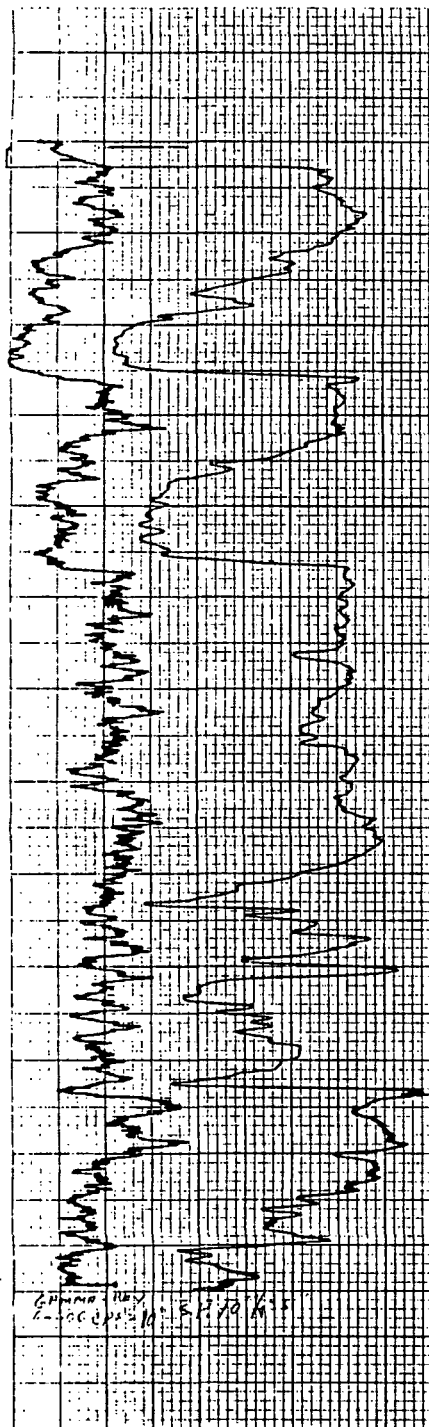
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REI-7  
FRENCH LIMITED**

DRAWN BY: L.C.S.

DATE: 12/12/86

PROJECT NO. 275-14





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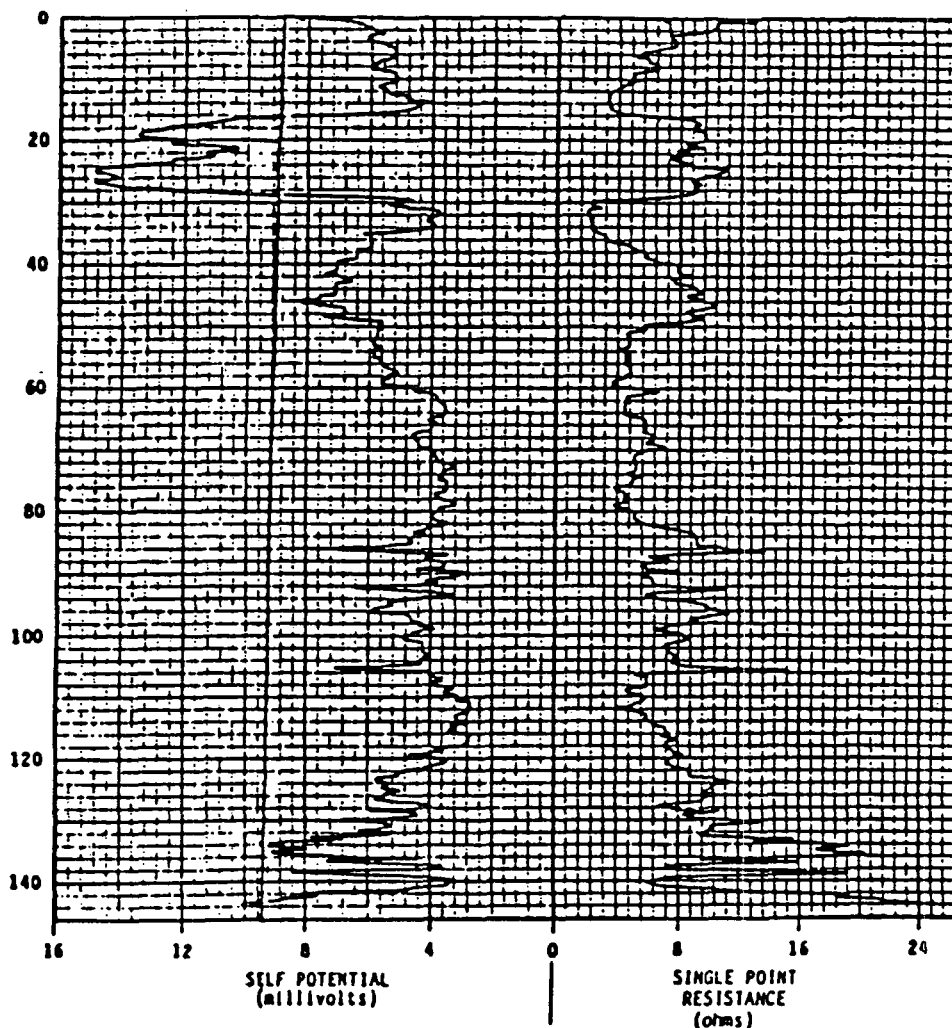
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HOUSTON, TEXAS

**GEOPHYSICAL LOG  
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FRENCH LIMITED**

DRAWN BY: L.C.S.

DATE: 12/12/86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**GEOPHYSICAL LOG  
GW-06  
FRENCH LIMITED**

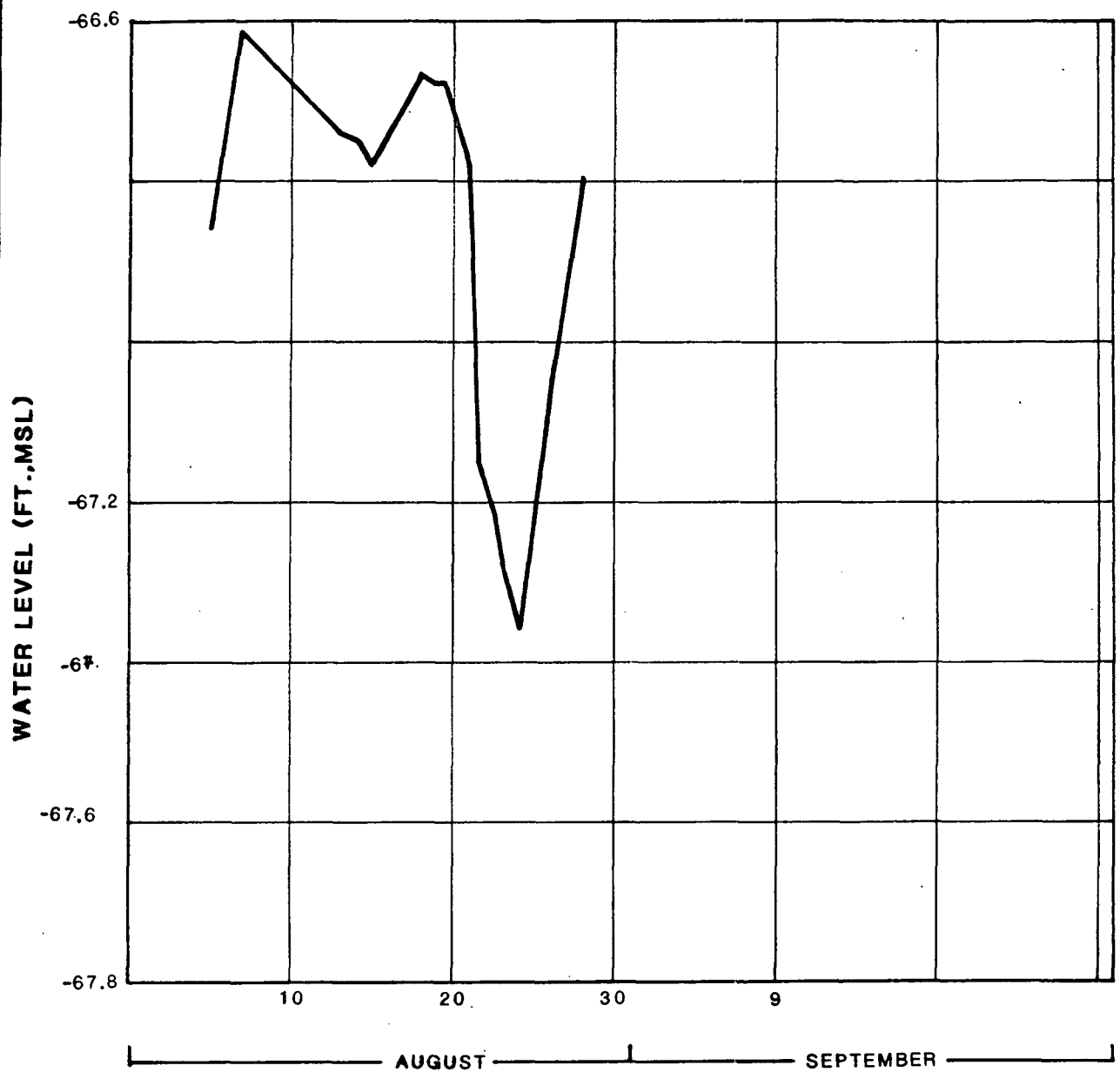
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DATE: 12/12/86

PROJECT NO. 275-14

Appendix 14

Monitor Well and Piezometer Geophysical (E-Logs) Logs



NOTE: SCALE DIFFERS FROM OTHER HYDROGRAPHS



**RESOURCE ENGINEERING INC.**

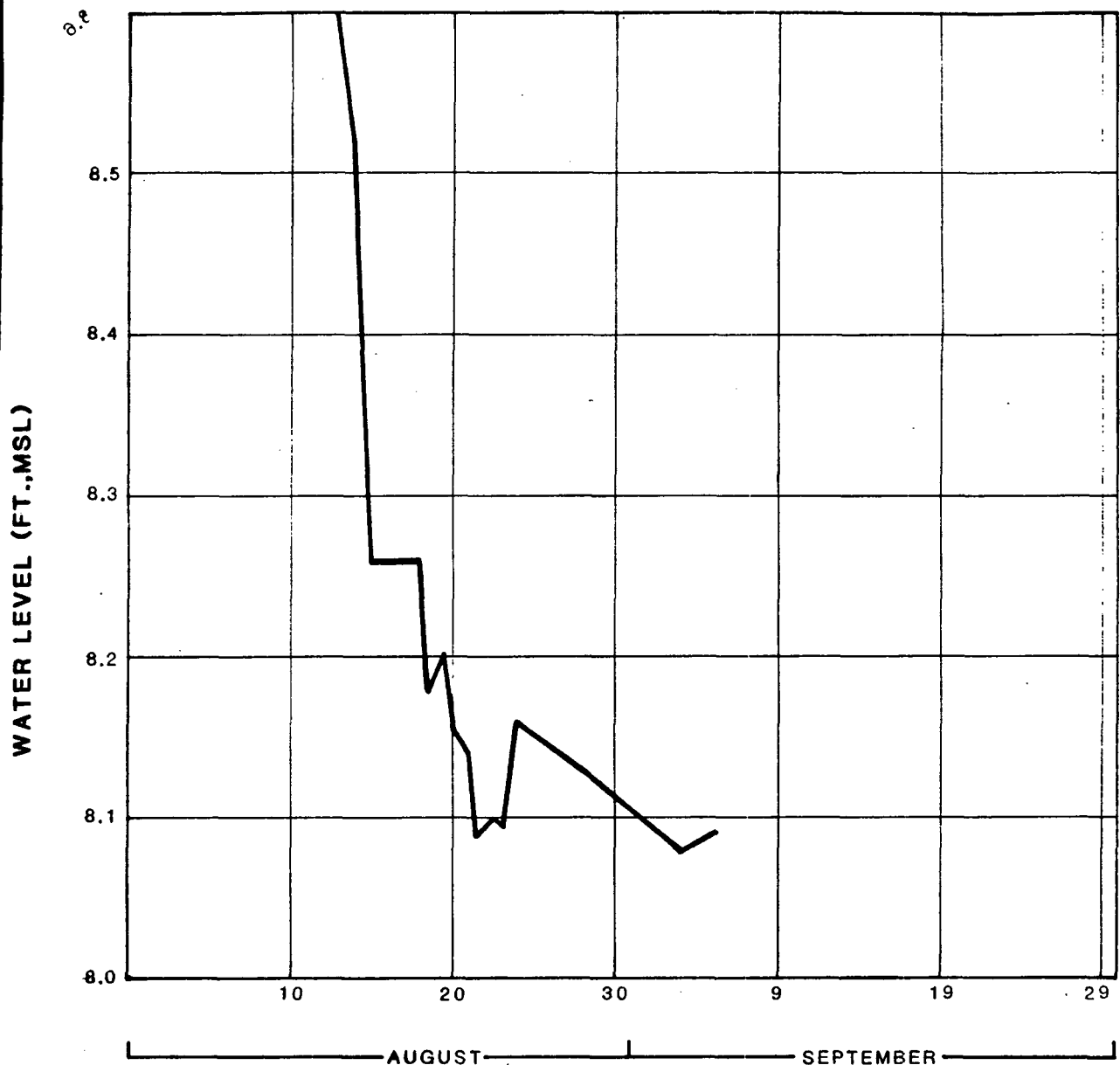
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HOUSTON, TEXAS

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REI 10-1  
FRENCH LIMITED**

DRAWN BY:

DATE:

PROJECT NO.



**RESOURCE ENGINEERING INC.**

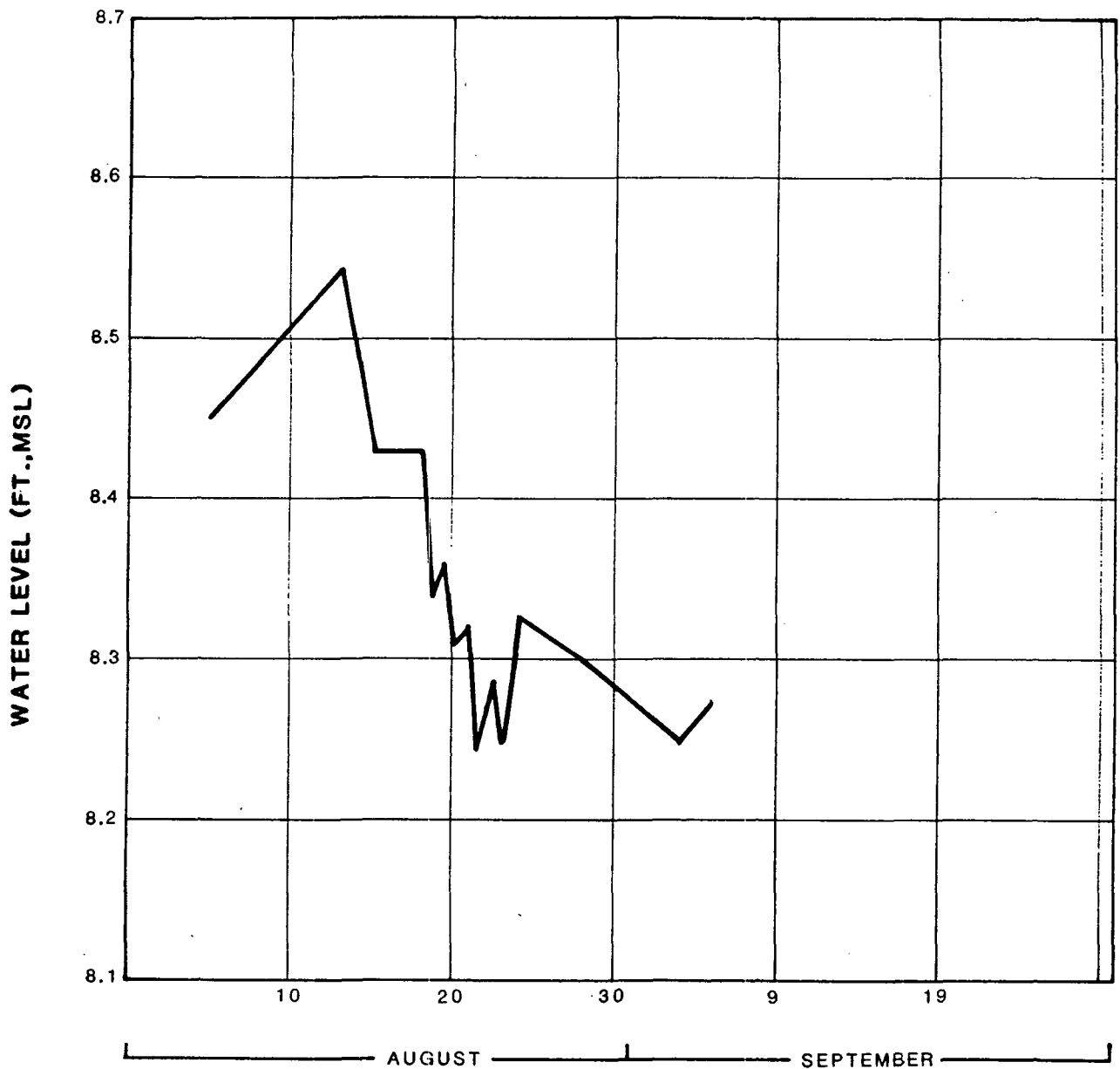
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HOUSTON, TEXAS

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FRENCH LIMITED**

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DATE: 9-15-86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

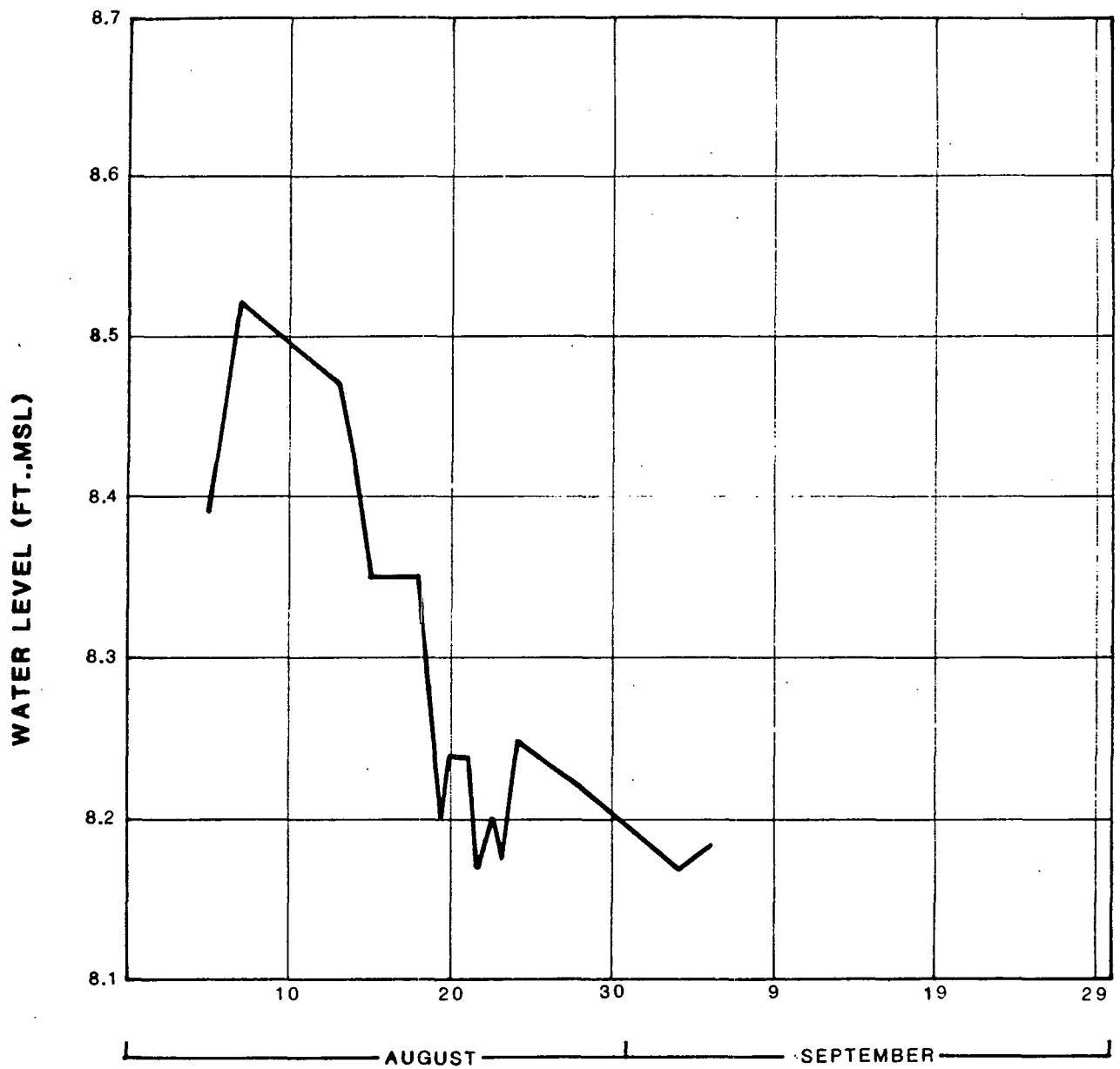
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**HYDROGRAPH**  
**REI 10-3**  
**FRENCH LIMITED**

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DATE: 9-15-86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

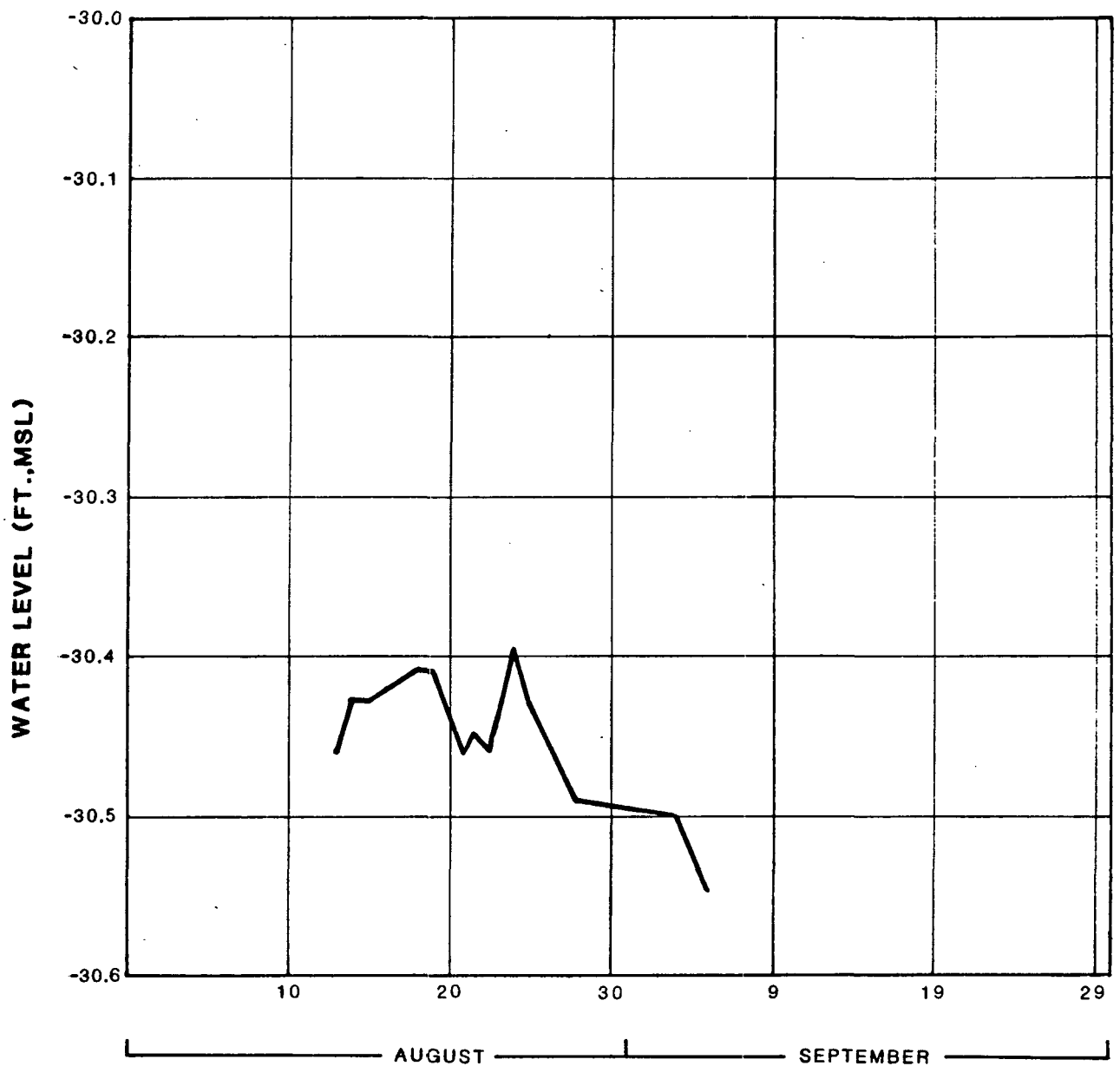
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

HYDROGRAPH  
REI 10-4  
FRENCH LIMITED

DRAWN BY:

DATE: 9-15-86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

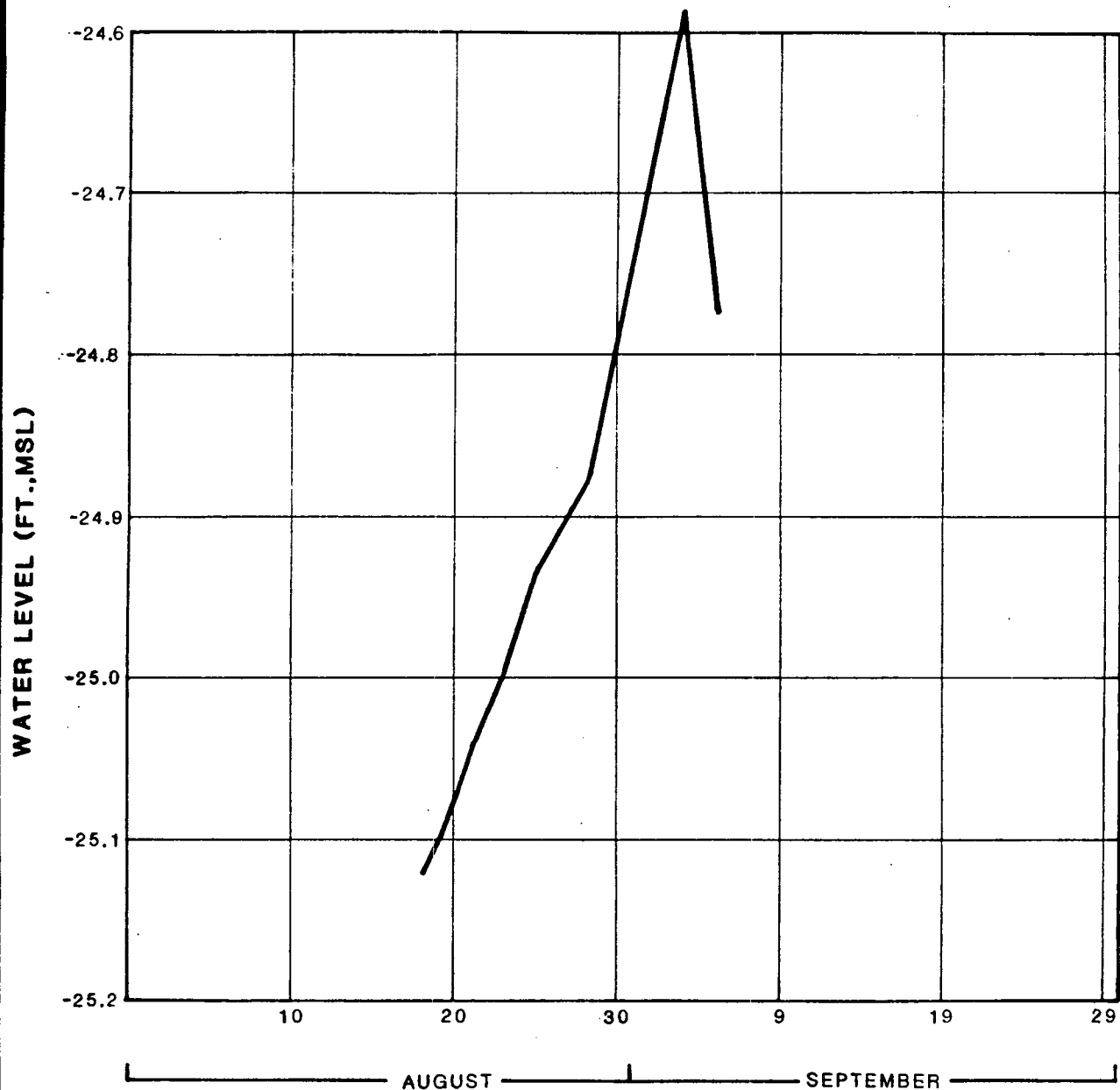
**FIGURE  
HYDROGRAPH  
P 10-2 (SILT SUBCLAY)  
FRENCH LIMITED**

DRAWN BY:

DATE: 9-15-86

PROJECT NO. 275-14





**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

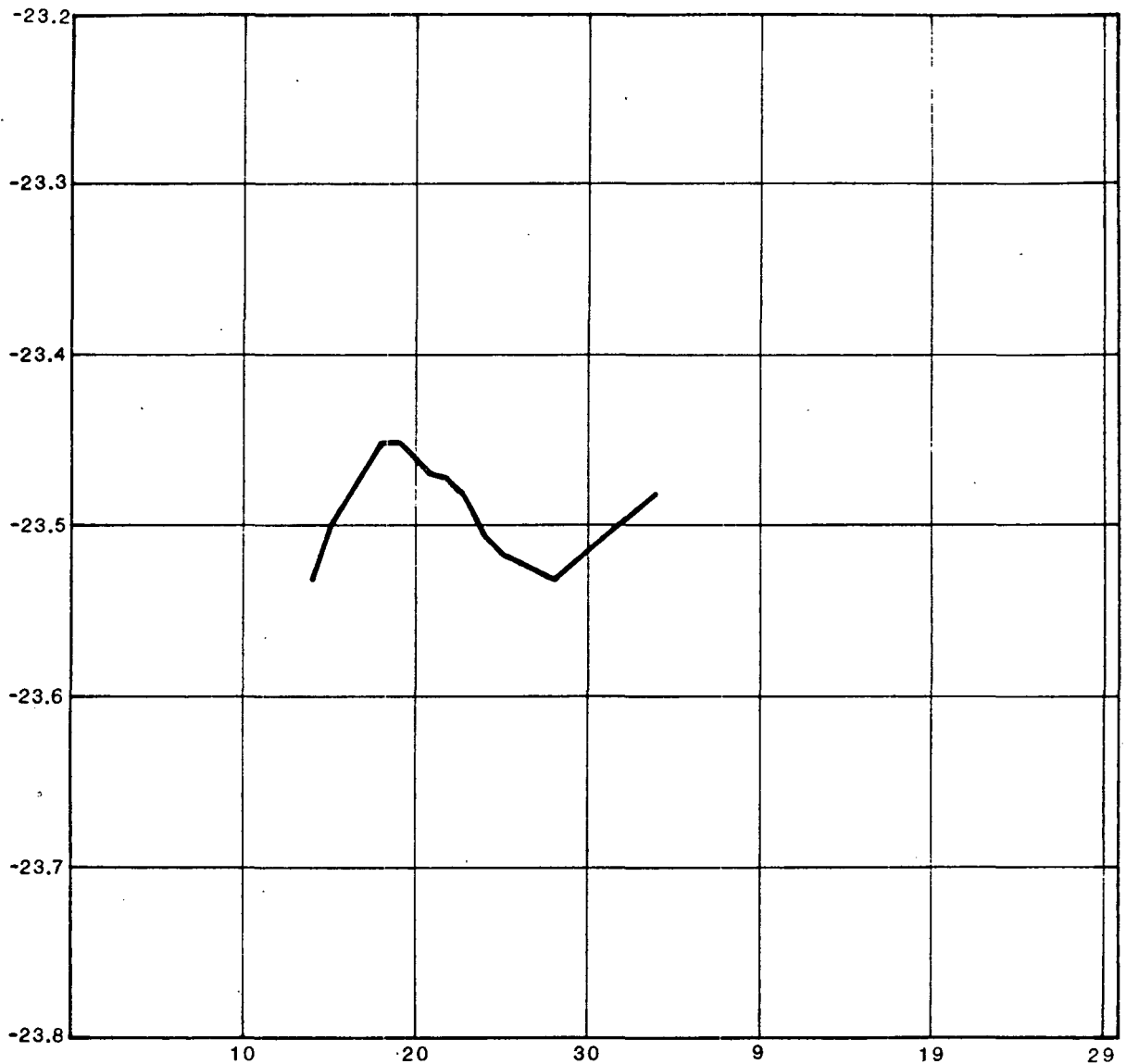
**HYDROGRAPH  
P 10-3 (DEEP CLAY)  
FRENCH LIMITED**

DRAWN BY:

DATE: 9-15-86

PROJECT NO. 275-14

WATER LEVEL (FT.,MSL)



AUGUST

SEPTEMBER



**RESOURCE ENGINEERING INC.**

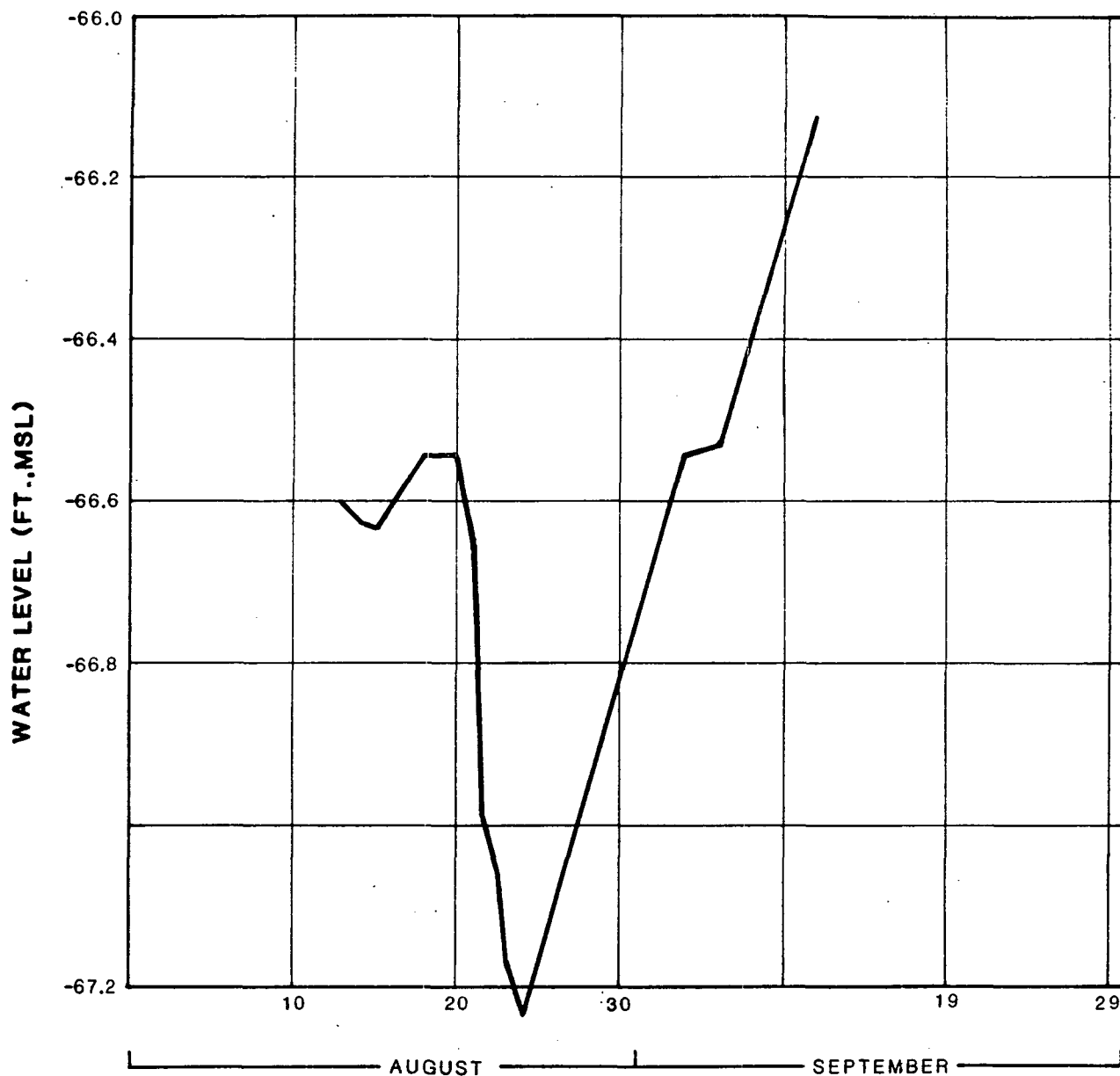
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**HYDROGRAPH  
P 10-4 (SHALLOW CLAY)  
FRENCH LIMITED**

DRAWN BY:

DATE: 9-15-86

PROJECT NO. 275-14



NOTE: SCALE DIFFERS FROM OTHER HYDROGRAPHS



**RESOURCE ENGINEERING INC.**

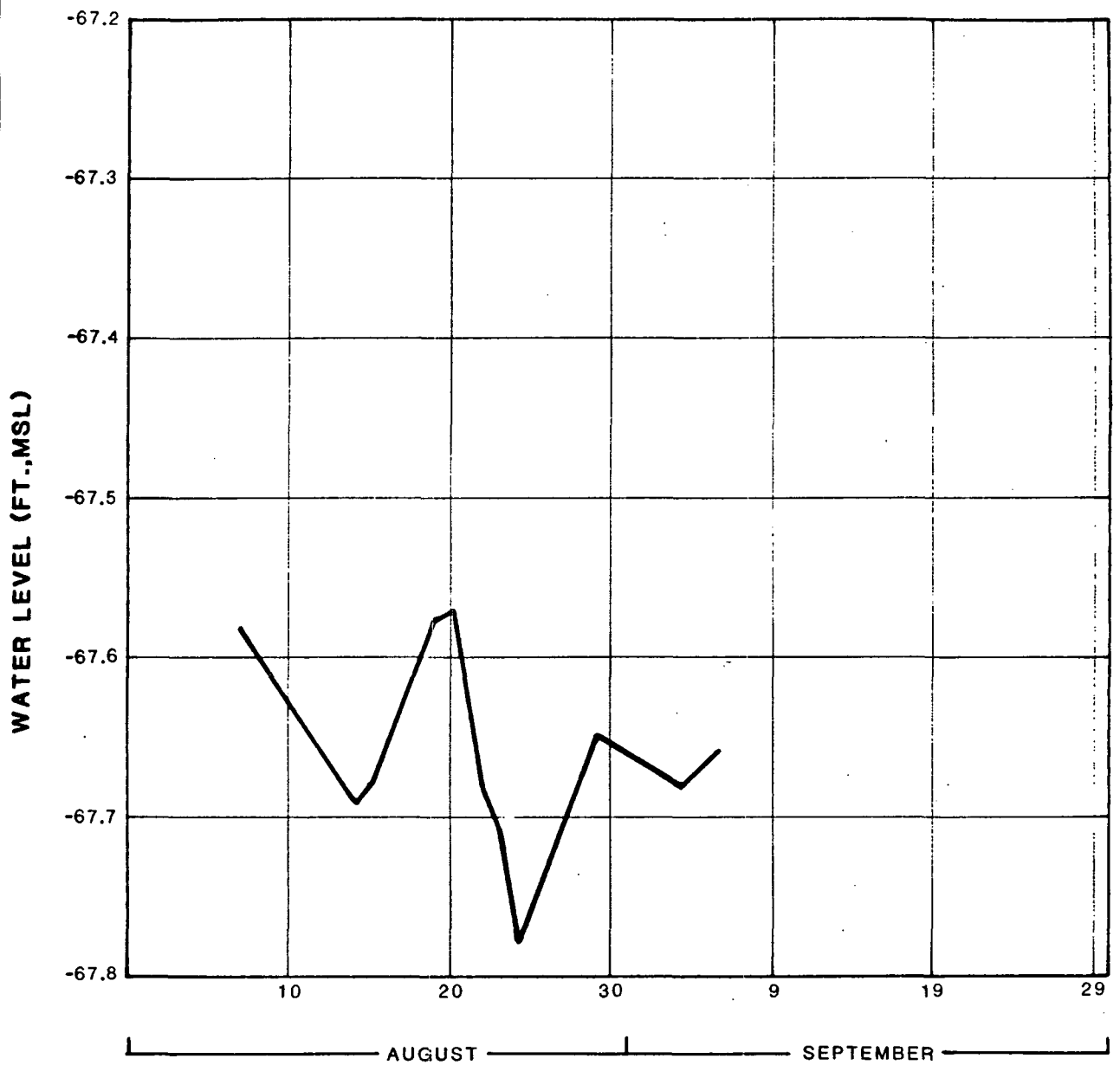
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

HYDROGRAPH  
GW 25  
FRENCH LIMITED

DRAWN BY:

DATE: 9-15-86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

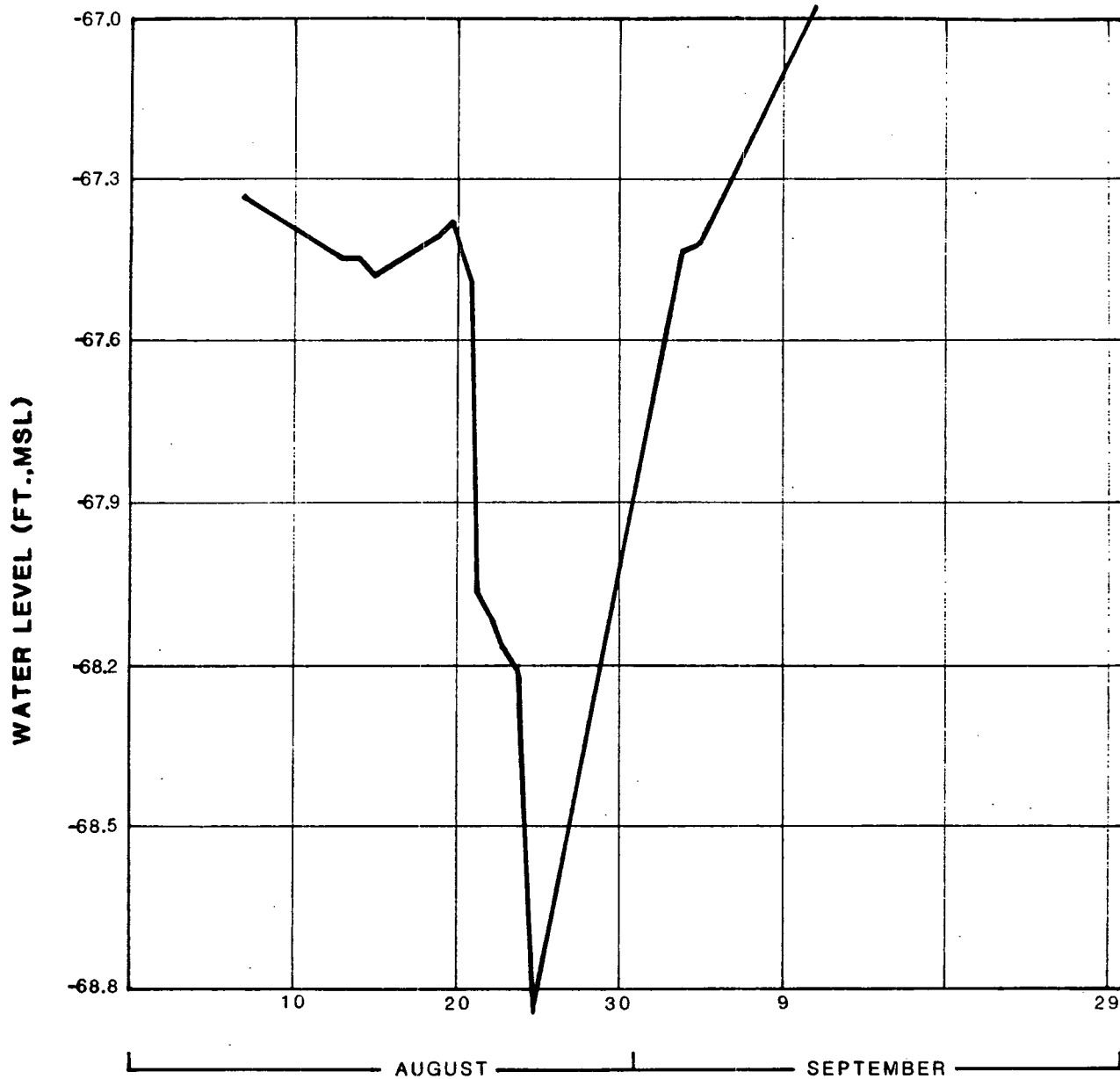
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**HYDROGRAPH  
REI 7  
FRENCH LIMITED**

DRAWN BY:

DATE: 9-15-86

PROJECT NO. 275-14



NOTE: SCALE DIFFERS FROM OTHER HYDROGRAPHS



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

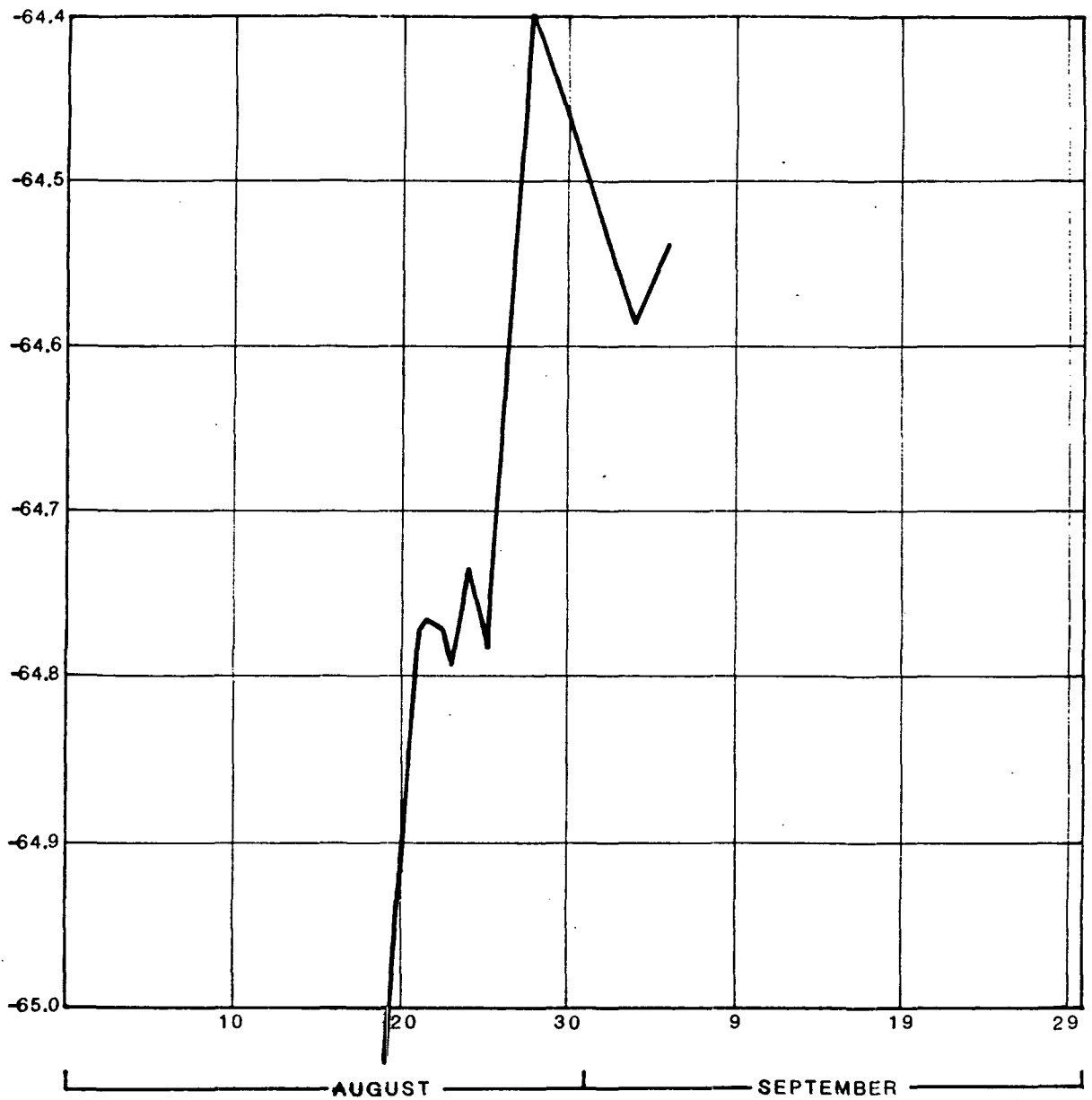
**HYDROGRAPH  
REI 11  
FRENCH LIMITED**

DRAWN BY:

DATE: 9-15-86

PROJECT NO. 275-14

WATER LEVEL (FT.,MSL)



**RESOURCE ENGINEERING INC.**

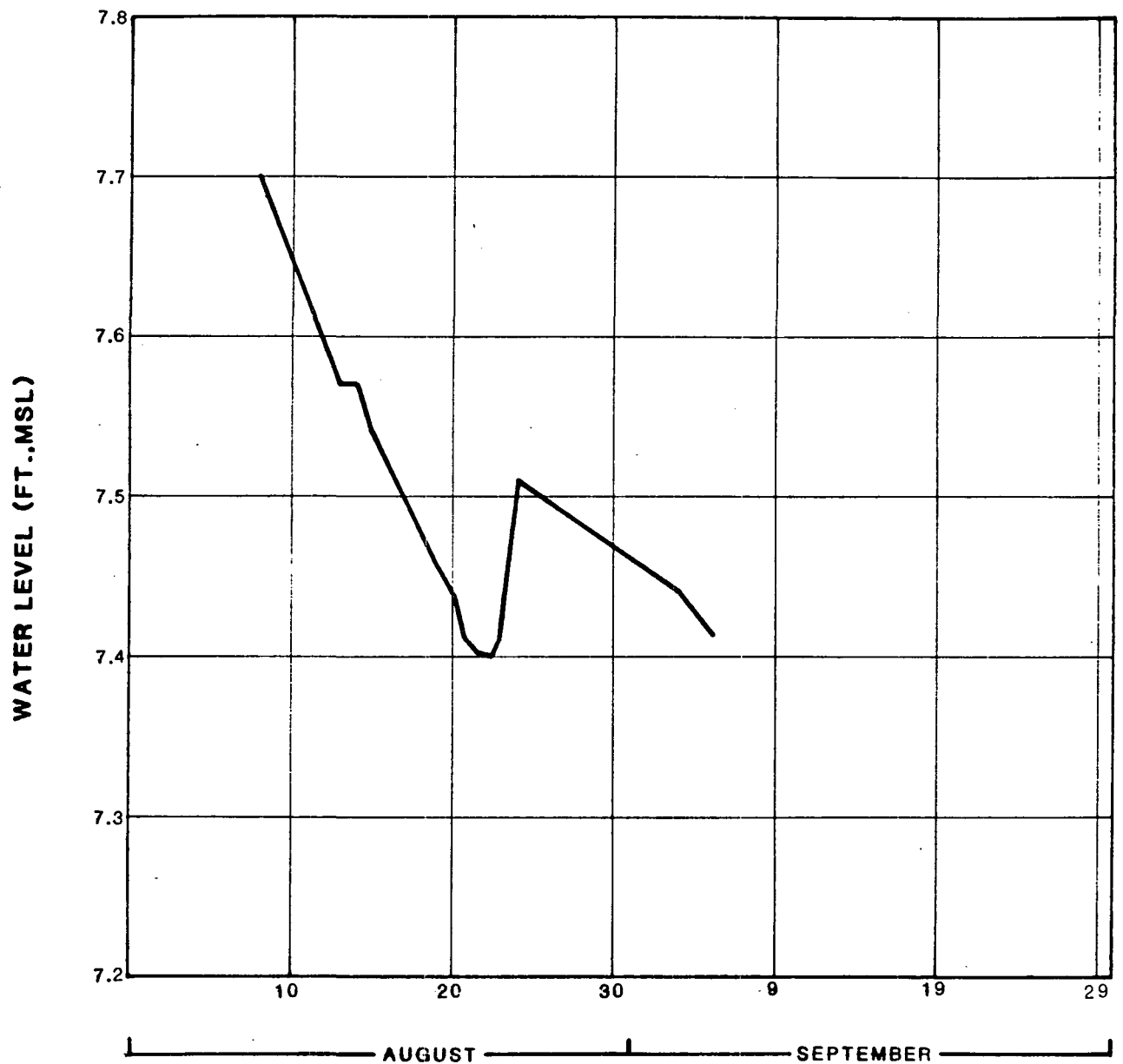
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**HYDROGRAPH  
12-1  
FRENCH LIMITED**

DRAWN BY:

DATE: 9-15-86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

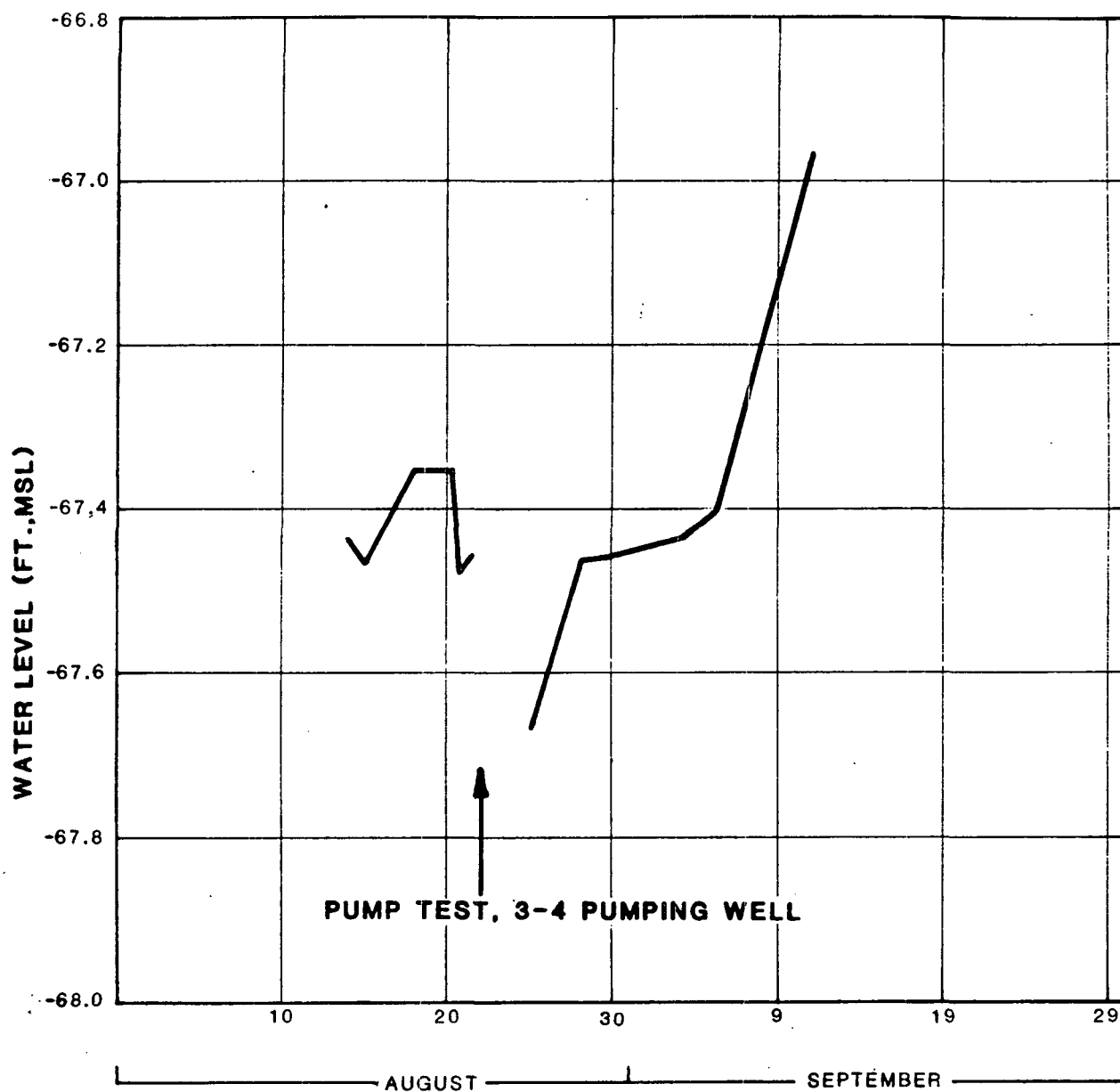
ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**HYDROGRAPH  
12-2  
FRENCH LIMITED**

DRAWN BY:

DATE: 9-15-86

PROJECT NO. 275-14



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**HYDROGRAPH  
REI 3-4  
FRENCH LIMITED**

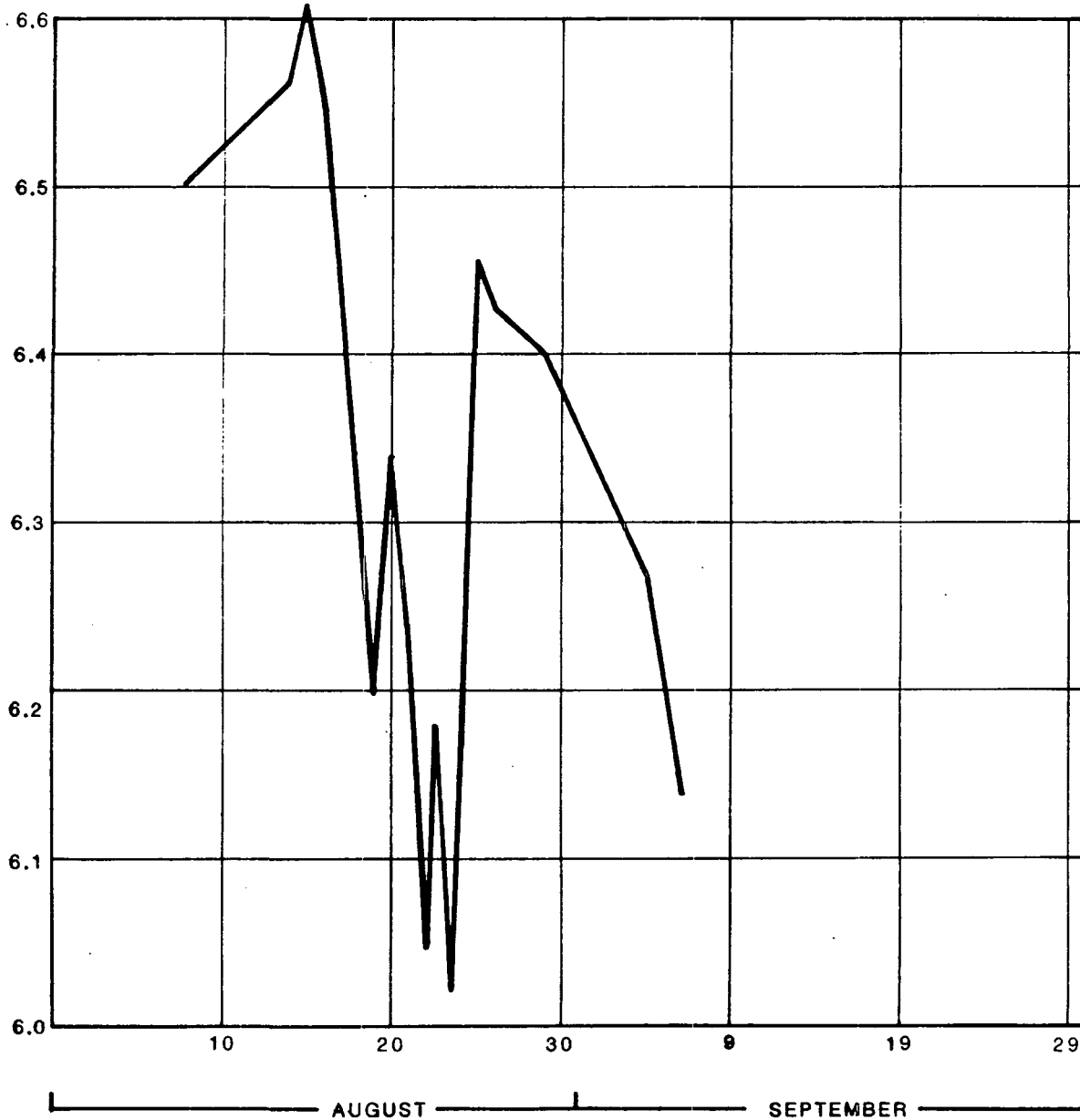
DRAWN BY:

DATE: 9-15-86

PROJECT NO. 275-14



WATER LEVEL (FT., MSL)



**RESOURCE ENGINEERING INC.**

ENVIRONMENTAL CONSULTANTS  
HOUSTON, TEXAS

**HYDROGRAPH  
REI 3-5**

**FRENCH LIMITED**

DRAWN BY:

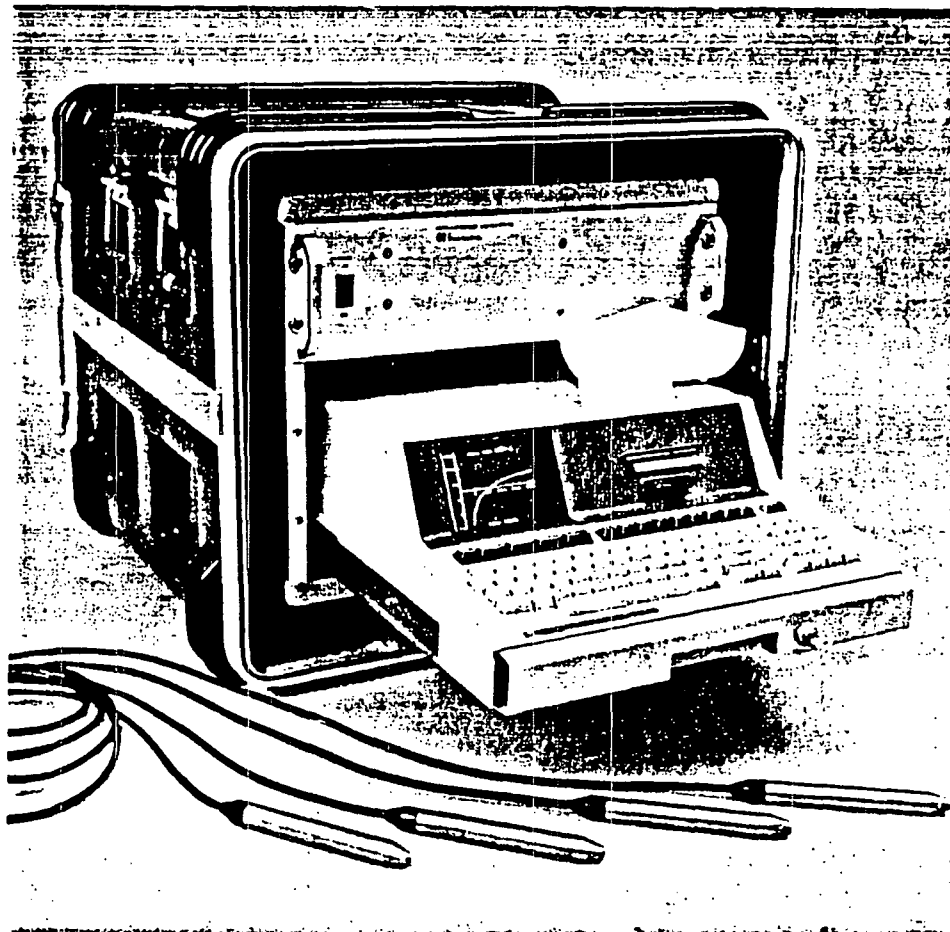
DATE: 9-15-86

PROJECT NO. 275-14

Appendix 15

In-Situ SE-200 Computer System Operating  
Instruction

# HYDROLOGIC ANALYSIS SYSTEM



SE200

**OWNER'S MANUAL: HYDROLOGIC ANALYSIS SYSTEM**

**MODEL SE200**

• **In-Situ Inc.**

1982  
Revised 4/84

## GENERAL DESCRIPTION

The Hydrologic Analysis System Model SE200 is a computer based, automated, water level data acquisition and reduction system. It consists of four basic units: the data acquisition unit, the computer, the environmental enclosure, and water level transducers.

The data acquisition unit can excite and provide signal conditioning for up to 16 individual transducers. It also performs switching and interface functions, enabling the computer to read water level data from each transducer.

The computer (through the data acquisition unit) reads measurements from each transducer, controls the timing of each measurement, records each measurement (and the time it was taken), and permanently stores this data on magnetic tape. In addition, the computer reduces all data, providing plots and tables of real-time data during a test; the permanently recorded data can produce a complete report of the test at any time after test completion. In conjunction with the data acquisition unit and applicable accessories, the computer is capable of automatically controlling start and stop of one pump and automatically regulating discharge rate.

The environmental enclosure is a weather-proof container that holds the data acquisition unit and the computer; it provides shock mounting for these units, a sliding carriage for the computer, and complete protection during transportation and unattended operation.

Water level transducers measure hydrostatic pressure (which is a function of water level).

Three of the basic units of the SE200 are described in greater detail in the following sections.

### 1 Data Acquisition Unit

The data acquisition unit operates on 115/230 VAC, 47 to 440 Hz. Together with plug-in printed circuit boards, the data acquisition unit performs interface functions between the computer and transducers, as well as providing excitation and signal conditioning for the transducers. One data acquisition unit will support a maximum of 16 transducers; up to 13 additional data acquisition units can be connected, enabling the SE200 to support a maximum of 224 transducers.

The data acquisition unit supports four types of plug-in modules.

- 1.1 Control Module. The control module is an IEEE 488 interface that formats digital data for transfer to and from the computer.
- 1.2 A to D Module. The A to D module scans the analog transducer measurements on command from the computer and converts them to digital data.
- 1.3 Pump Module. The pump module automatically controls pump start and stop on command from the computer and processes valve control signals from the computer for transfer to the valve actuator for automatic adjustment of discharge rate.
- 1.4 4-20 mA Module. The 4-20 mA module excites the transducers and measures their output. Each 4-20 mA module can accept 4 transducers.

## 2 Computer

The computer used with the Hydrologic Analysis System is the Hewlett-Packard HP-85 with accessories.

1. the basic HP-85 desktop computer
2. two (optional) 128K modules, providing additional memory to expand the basic computer memory to a total of 288K. Full system performance is provided with the basic 32K memory. However, additional memory automatically loads all subprograms which would normally require manual reinsertion of the system software tape.
3. an HP-IB interface (IEEE 488), interfacing the HP-85 with peripheral equipment

The computer has a CRT display for real-time presentation of system activities and plots of data, a thermal printer for hard copy of plots and data tables, and a tape drive for mass data storage on data cartridges.

### 3 Transducers

The body of the transducer is labelled as follows:

In-Situ Inc.  
SF: --

Druck Ltd.  
PTX 160 D  
-- psig  
S/N --

SF is the abbreviation for scale factor. The value printed after this indicates the exact range of the transducer in psig. The scale factor is entered into the test program as one of the test specifications for each transducer.

PTX 160 D is the transducer model number.

-- psig indicates the design range of the transducer, which is also the limit of accurate measurement for the particular transducer. Water levels in excess of this value will produce an over-range indication (see Appendix C, p. 46).

The label on the transducer reel displays the following information:

Model No.: PTX 160/D  
Serial No.: -----  
Scale Factor: --  
Range --- meters  
Do not exceed ---- m

This gives the transducer range in approximate meters and warns the user not to exceed two times the full range.

3.1 Current Transmitter. Each water level transducer contains a 4-20 mA current transmitter and a strain gauge pressure sensor. The current transmitter prevents measurement sensitivity from being affected by cable length. Since all sensitive electronics are in the transducer and, thus, isolated in the constant temperature environment of the groundwater, errors due to variations in temperature are negligible. Very shallow water tables, however, can produce errors in data due to temperature variations. In such conditions the transducer may be subject to sensitivity and zero offset variations as a

result of the temperature gradient imposed on near-surface water; since the temperature error band is  $\pm 0.3\%$  very shallow applications that may subject the transducer to very wide temperature variations have the potential for the following maximum errors:

Temperature Error Band ( $-2$  to  $30^{\circ}$  C)

XD Range	Maximum Temperature Error
10 psi (6 m) (10 ft)	$\pm 0.03$ psi (0.02 m) (0.07 ft)
50 psi (30 m) (100 ft)	$\pm 0.15$ psi (0.1 m) (0.35 ft)
100 psi (60 m) (200 ft)	$\pm 0.3$ psi (0.2 m) (0.7 ft)

- 3.2 Pressure Sensor. The pressure sensor is specifically designed to be insensitive to barometric pressure changes. By incorporating a vent tube into the transducer cable, atmospheric pressure is the reference pressure to the sensor diaphragm. With this design it is absolutely essential the vent tube not be obstructed; if it is, temperature variations of the transducer cable will result in pressure variations of the air within the vent tube. These pressure changes will be reflected as errors in water level measurements.

The pressure sensor will tolerate an over pressure of twice the full range, but will not tolerate negative pressures.

- 3.3 Pressure Port. The pressure port of the transducer is protected by a guard. If necessary, the guard may be unscrewed. If the guard is removed, the sensor diaphragm must be protected; any object contacting the unprotected sensor diaphragm may destroy the transducer.
- 3.4 Transducer Cable. The jacket of the standard transducer cable is polyurethane. This polymer has been specially selected for its toughness, abrasion resistance, and flexibility at low temperatures, but it is important not to expose the cable to the sharp edges common to well casings. Strong solvents such as acetone and methyl ethyl ketone (MEK) will also destroy the cable.

The cable is blocked at the transducer connection to prevent entry of water. However, if the cable jacket is pierced and this damaged site is then submerged, water will enter the cable and then flow downward, with the potential for filling and destroying the transducer.



Transducer extension cable is available as a system option. Extension cables are vented at each connector. Consequently, extreme care must be taken to prevent water from entering these vents. If water does enter a vent it will cause data errors due to obstruction of air flow through the vent tube.

3.5 Cable Connectors. Cable connectors (with the exception noted above) are waterproof and will withstand normal environmental conditions. When not assembled in the system, the connectors of the cable must be protected.

3.6 Scale Factor. The SF (scale factor) value is equal to the transducer true full range sensitivity in PSIG. For example; A 10 PSIG transducer may have an actual calibration sensitivity of 9.38 PSIG over the operating range of 4 to 20 ma. This value must be entered when preparing test specifications (refer to Software Operation). The scale factor may be verified in the field by the following procedure:

A. Scale Factor Check

Using the system tape, set up the transducers as for normal water level measurement. Set up for the pre-run check option (see Appendix C, p. 28) and proceed as follows.

B. Pre-run Check

1. submerge transducer at a water level below the seasonal temperature variation.
2. accurately measure off and mark a known length on the transducer cable. For maximum accuracy, this length should approximate the transducer range minus the hydrostatic head of the initial transducer setting. For example, if the transducer range is 60 meters and the initial transducer setting submerges the transducer 2 meters below the water level, the measured length should be approximately 58 meters (units of measurement need not be metric).
3. record the water level indicated by the computer.

4. lower the transducer the measured distance of step 2 to its second setting.
5. record the water level indication for this second transducer setting.
6. calculate the transducer scale factor using the following equation:

$$SF2 = SF1 \cdot \frac{L}{\Delta W} ,$$

where SF2 = new scale factor

L = length measured in step 2

$\Delta W$  = difference between water level indications of steps 3 and 5

SF1 = old scale factor.

If the old scale factor (SF1) is unknown, substitute K from table 2.

Table 2

Scale Factor Verification

transducer range (meters)	K
6	10
30	50
60	100

**Note:**

The following factors will introduce errors when performing calibration by this technique.

1. Extreme temperature gradients related to shallow water tables, geothermal sites, etc.
2. Thermal expansion and contraction of air within the transducer cable vent tube as the cable passes between warmer and cooler environments outside and inside the well (transient error).
3. Slug effect caused by volumetric displacement of the transducer and cable in a low permeability situation.

### 3.7 Druck Pressure Transducer Specifications

Excitation Voltage	9 to 30 VDC
Output	4 to 20 mA
Setting Accuracies:	
Zero	4 mA, +0.5% FS
Full Scale	20 mA, -1% FS
Non-Linearity	+0.1% FS
Hysteresis	+0.02% FS
Repeatability	+0.02% FS
Self Noise	Nominal 0.05% FS Pk to Pk with 2.5 KHz cutoff
Long Term Stability	0.2% FS per year
Warm Up	Nominally 0.05% FS, 30 to 60 secs
Accuracy	
At Constant Temp:	+0.1% of Range
Temperature Error Band (TEB) at Constant Pressure	+0.3% of range over a temperature range of -2°C to 30°C; 28°F to 86°F -20°C to 80°C; -4°F to 176°F -55°C to 95°C; -67°F to 203°F
Operating Temperature Range	-20°C to 80°C; -4°F to 176°F
Storage Temperature Range	-55°C to 95°C; -67°F to 203°F
Overpressure Capability	2X Full Range
Media Compatibility	Groundwater with dissolved H <sub>2</sub> S, seawater, salt brine
Size	0.59" dia. X $\approx$ 8.5" long
Pressure Connection	0.58" X 32 TPI 55 DEG (Witworth form)
Wetted Materials	Titanium, Quartz, Polyure- thane, Delrin, Silicone, Grease, Silicone RTV, Stainless Steel

3.8 Transducer Installation. When a transducer is installed in a well with a pump, it is important to install an access tube with the pump column. This will prevent the transducer cable from becoming entangled with the pump column. A tubing ID of one-inch minimum is recommended.

Appendix 16

REI 3-4 Run #2 Pumping Test Data Sheets

117.64  
81/69  
26.00

# CALCULATIONS AND COMPUTATIONS

SHEET 1 OF

PROJECT: French LTD REI 3-4 Pump test

JOB NO.: \_\_\_\_\_

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Run #2 Well 3-4

81.69  
12.5.84

8-21-86

FLOW RATE	TIME (400)	MONITOR INITIALS
START PUMP	16:30	RR
1.6	16:32	RR
1.6	16:33	RR
1.6	16:40	RR
1.6	16:44	RR
1.6	16:50	RR
1.6	16:59	RR
1.6	17:05	GOT
1.6	17:11	D.D
1.6	17:20	D.D
1.6	17:30	D.D
1.6	17:29	Arri
1.6	17:35	Arri
1.6	17:47	D.D
1.6	18:05	D.D
1.6	18:11	D.D
1.6	18:20	RR
1.6	18:27	RR
1.6	18:38	D.D
1.6	18:44	D.D
1.6	18:58	DD
1.6	19:07	DD
1922 - flow fluctuates 0.2 gpm		
1.6	19:28	P.D
1.6	19:49	D.D
1.6	20:03	DD
1.6	20:15	DD

8-22-86

FLOW RATE	TIME (400)	MONITOR INITIALS
1.6	20:26	DD
1.6	20:45	DD
1.6	21:03	D.D
1.6	21:27	DD
1.6	21:44	Arri
1.6	22:07	D.D
1.6	22:20	D.D
1.6	22:56	CWA
1.6	23:11	D.D
1.6	23:32	D.D
1.6	23:50	D.D
1.6	00:11	CWA
1.6	00:29	D.D
1.6	00:50	D.D
1.6	01:13	D.D
1.6	01:35	D.D
1.6	01:48	D.D
1.6	02:15	D.D
1.6	02:44	D.D
1.55	03:02	D.D
1.6	03:10	D.D
1.55	03:19	D.D
1.5	03:31	D.D
1.55	03:45	D.D
1.6	03:59	D.D
1.6	04:17	D.D
1.6	04:30	D.D

117.64

# CALCULATIONS AND COMPUTATIONS

SHEET 2 OF       

PROJECT: FRENCH LTD. REI 3-Y Pump Test

JOB NO.:                     

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY:            DATE:           

French Well 3-4, 8/22/86 RUN #2

CHECKED BY:            DATE:           

FLOW RATE	DME (2400)	MONITORS INITIALS		FLOW RATE	TIME (2400)	MONITORS INITIALS
1.6	0445	D.D.		1.6	1333	RSA
1.6	0459	D. Dad		1.6	1407	RSA
1.6	0515	D. Dad		1.6	1432	RSA
1.6	0530	D. Dad		1.6	1456	RSA
1.6	0545	D. Dad		1.6	1534	RSA
1.6	0559	D. Dad		1.6	1558	RSA
1.6	0615	D. Dad		1.6	1607	RSA
1.6	0630	D. Dad		1.5	1621	RSA
1.6	0646	D. Dad		1.6	1637	RSA
1.6	0713	D. Dad		1.5-1.6	1643	RSA
1.6	0733	D. Dad		1.5	1700	RSA
<del>1.6</del> 1.6	0743	RSA		1.5 ± 0.2	1738	D.D
1.6	0756	RSA		1.5	1753	D.D
1.6	0817	RSA	Fluctuate betw. 1.5-1.6 RSA	1.5 ± 0.1	1815	D.D
1.6	0830	RSA		1.55	1838	D.D
1.6	0830	RSA		1.5	1857	D.D
1.6	0900	RSA		1.55	1926	D.D
1.6	0915	RSA	Discharge changed to new tanker →	1.5 ± .2	1947	D.D
1.6	0929	RSA	Fluctuating betw. 1.4-1.7 RSA	1.65	1956	D.D
1.6	1000	RSA	unstable -	1.65	2007	D.D
1.6	1023	RSA	unstable -	1.5	2028	D.D
1.6-1.7	1038	RSA	unstable -	1.6 ± 0.1	2049	D.D
1.6	1118	RSA	Fluctuations start at this time *	1.1 → 1.9	2111	D.D
1.6	1132	RSA	Flow adjusted down to 1.4 gpm →	1.4	2115	D.D
1.6	1146	RSA				
1.6	1202	RSA				
1.6	1251	RSA				
1.6	1315	RSA				

Fluctuating betw. 1.8 and 1.3 RSA

Fluctuations dropping to 1.5 consistently

Fluctuate betw. 1.5-1.6 RSA

Discharge changed to new tanker →

Fluctuating betw. 1.4-1.7 RSA

unstable -

unstable -

unstable -

Fluctuations start at this time \*

Flow adjusted down to 1.4 gpm →

From 2111 to 2115, the flow rate had oscillated from 1.1 → 1.9 - with occasional bubbles - perhaps indicating breaking of suction. Flow rate adjusted to 1.4 without turning off pump.

**ARPI**

# CALCULATIONS AND COMPUTATIONS

SHEET 3 OF       

PROJECT: FRENCH LTD KEY 3-4 Pump Test JOB NO. 275-14

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY:        DATE:       

CHECKED BY:        DATE:       

French well 3-4 8/22/81

Run #2

	FLOW RATE	DME (2400)	MONITOR INITIALS		FLOW RATE	TIME (2400)	MONITOR INITIALS
stable -	1.4	2123	DD		1.4	0724	DD
stable -	1.4	2129	DD		1.4	0745	OCM
stable -	1.4	2140	DD	Shift	1.4	0813	OCM
stable -	1.4	2156	DD	Time	1.4	0830	OCM
stable -	1.4	2214	DD	"	1.4	0857	OCM
stable -	1.4	2222	DD	"	1.4	926	OCM
stable -	1.4	2234	DD		1.4	10:04	Ami
" " -	1.4	2247	DD		1.4	10:34	Ami
	1.4	2300	OCM		1.4	11:30	Ami
	1.4	2319	DD		1.4	12:15	Ami
	1.4	2341	CWA		1.4	13:20	Ami
steady 8-23	1.4	0004	DD		1.4	13:40	Ami
"	1.4	0029	DD		1.4	14:30	Ami
"	1.4	0105	DD		1.4	14:55	Ami
	1.4	0128	DD		1.4	15:10	PR
	1.4	0205	DD		1.4	15:35	PR
steady	1.4	0239	DD		1.4	16:00	PR
"	1.4	0300	DD		1.4	16:23	PR
"	1.4	0328	DD		1.4	16:46	PR
	1.4	0346	CWA		1.4	17:05	PR
	1.4	0408	CWA		1.4	17:24	PR
	1.4	0432	DD		1.4	18:06	PR
	1.4	0457	DD		1.4	18:30	PR
steady	1.4	0533	DD		1.4	18:52	PR
	1.4	0609	DD		1.4	19:14	PR
	1.4	0634	DD		1.4	19:30	PR
	1.4	0704	DD		1.4	20:17	PR

**ARFI**

# CALCULATIONS AND COMPUTATIONS

SHEET 4 OF 4

PROJECT: FRENCH LTD RET 3-Y Pump TEST JOB NO.: 275-14

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

FLOW RATE	TIME (2400)	MONITOR'S INITIALS	FLOW RATE	TIME (2400)	MONITOR'S INITIALS
1.4	20:27	RK	1.45	1150	DD
1.4	20:49	DRG	1.4	1221	DD
1.4	21:24	DRG	1.43	1252	DD
1.4	21:54	RK	1.45	<del>1300</del> 1300	DD
1.4	22:07	RK	1.45	1324	DD
1.4	22:47	DRG	1.45	1358	DD
1.4	23:39	SCZ	1.45	1424	DD
1.4	00:22	SCZ	1.45	1445	DD
1.4	01:44	SCI	1.45	1509	RK
1.4	02:11	SCZ	1.45	1534	SCM
1.4	02:40	SCZ	1.45	1547	CWA
1.4	03:27	SCZ	1.45	16:14	CWA
1.4	04:01	SCZ	1.45	16:24	RK
1.4	04:38	SCZ	1.40	16:44	RK
1.4	05:30	SCZ			
1.4	06:26	SCI			
1.4	06:39	SCZ			
1.4	06:52	RSA			
1.45	07:18	Nin			
1.45	07:34	D. D.			
1.45	08:07	D. D.			
1.45	08:40	DD			
1.45	09:36	DD			
1.45	10:05	DD			
1.45	10:28	Nin			
1.45	10:43	DD			
1.45	11:21	DD			

B-24-86 →



This is a detailed black and white map of the Hawaiian Islands, including the main islands and surrounding reefs, plotted on a grid of latitude and longitude. The map shows the islands' positions relative to the equator and the Prime Meridian. The grid lines are labeled with latitude (from 10°N to 20°N) and longitude (from 150°W to 160°W). The islands are shown in silhouette, with the main islands (Hawaii, Maui, Oahu, Kauai, and the Line Islands) clearly visible. The map is oriented with North at the top.

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 3-4 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 3-4 INPUT 1  
 RADIUS: 0.166 FEET  
 START DATE : 21-Aug-86  
 START TIME : 16:30  
 WATER START LEVEL: 81.69 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
16:30	0.000	81.69	0.00	0.00E+00
16:30	0.084	82.11	-0.42	2.12E-03
16:30	0.167	82.51	-0.82	4.21E-03
16:30	0.251	82.81	-1.12	6.33E-03
16:30	0.334	83.04	-1.35	8.42E-03
16:30	0.417	83.21	-1.52	1.05E-02
16:30	0.501	83.40	-1.71	1.26E-02
16:30	0.584	83.57	-1.88	1.47E-02
16:30	0.667	83.72	-2.03	1.68E-02
16:30	0.751	84.00	-2.31	1.89E-02
16:30	0.834	84.11	-2.42	2.10E-02
16:30	0.917	84.34	-2.65	2.31E-02
16:31	1.001	84.48	-2.79	2.52E-02
16:31	1.391	85.18	-3.49	3.51E-02
16:31	1.724	85.73	-4.04	4.34E-02
16:32	2.058	86.41	-4.72	5.19E-02
16:32	2.391	87.07	-5.38	6.03E-02
16:32	2.724	87.61	-5.92	6.86E-02
16:33	3.058	88.23	-6.54	7.71E-02
16:33	3.391	88.79	-7.10	8.55E-02
16:33	3.724	89.40	-7.71	9.38E-02
16:34	4.058	89.94	-8.25	1.02E-01
16:34	4.391	90.49	-8.80	1.11E-01
16:34	4.724	90.99	-9.30	1.19E-01
16:35	5.058	91.56	-9.87	1.27E-01
16:35	5.391	91.96	-10.27	1.36E-01
16:35	5.724	92.62	-10.93	1.44E-01
16:36	6.058	92.98	-11.29	1.53E-01
16:36	6.391	93.51	-11.82	1.61E-01
16:36	6.724	93.93	-12.24	1.69E-01
16:37	7.058	94.36	-12.67	1.78E-01
16:37	7.391	94.74	-13.05	1.86E-01
16:37	7.724	95.21	-13.52	1.95E-01
16:38	8.058	95.61	-13.92	2.03E-01
16:38	8.391	95.99	-14.30	2.11E-01
16:38	8.724	96.39	-14.70	2.20E-01
16:39	9.058	96.78	-15.09	2.28E-01
16:39	9.391	97.15	-15.46	2.37E-01
16:39	9.724	97.49	-15.80	2.45E-01
16:40	10.058	98.00	-16.31	2.53E-01

16:42	12.153	100.01	-18.32	3.06E-01
16:44	14.153	101.84	-20.15	3.57E-01
16:46	16.423	103.71	-22.02	4.14E-01
16:48	18.762	105.40	-23.71	4.73E-01
16:50	20.193	106.32	-24.63	5.09E-01
16:52	22.193	107.70	-26.01	5.59E-01
16:54	24.193	108.89	-27.20	6.10E-01
16:56	26.193	109.82	-28.13	6.60E-01
16:58	28.193	110.79	-29.10	7.10E-01
17:00	30.193	111.62	-29.93	7.61E-01
17:02	32.193	112.19	-30.50	8.11E-01
17:04	34.158	112.86	-31.17	8.61E-01
17:06	36.158	113.42	-31.73	9.11E-01
17:08	38.158	113.87	-32.18	9.62E-01
17:10	40.158	114.42	-32.73	1.01E+00
17:12	42.158	114.75	-33.06	1.06E+00
17:14	44.158	115.10	-33.41	1.11E+00
17:16	46.158	115.54	-33.85	1.16E+00
17:18	48.158	115.90	-34.21	1.21E+00
17:20	50.158	116.27	-34.58	1.26E+00
17:22	52.158	116.51	-34.82	1.31E+00
17:24	54.158	116.63	-34.94	1.36E+00
17:26	56.158	116.86	-35.17	1.42E+00
17:28	58.158	117.10	-35.41	1.47E+00
17:30	60.158	117.13	-35.44	1.52E+00
17:32	62.247	117.17	-35.48	1.57E+00
17:34	64.135	117.25	-35.56	1.62E+00
17:36	66.135	117.27	-35.58	1.67E+00
17:38	68.135	117.14	-35.45	1.72E+00
17:40	70.135	117.27	-35.58	1.77E+00
17:42	72.135	117.44	-35.75	1.82E+00
17:44	74.135	117.83	-36.14	1.87E+00
17:46	76.135	118.21	-36.52	1.92E+00
17:48	78.135	118.50	-36.81	1.97E+00
17:50	80.782	118.79	-37.10	2.04E+00
17:52	82.182	118.86	-37.17	2.07E+00
17:54	84.070	119.18	-37.49	2.12E+00
17:56	86.070	119.48	-37.79	2.17E+00
17:58	88.070	119.70	-38.01	2.22E+00
18:00	90.070	120.06	-38.37	2.27E+00
18:02	92.070	120.33	-38.64	2.32E+00
18:04	94.070	120.47	-38.78	2.37E+00
18:06	96.070	120.73	-39.04	2.42E+00
18:08	98.115	120.96	-39.27	2.47E+00
18:10	100.120	121.14	-39.45	2.52E+00
18:30	120.280	122.94	-41.25	3.03E+00
18:50	140.220	122.69	-41.00	3.53E+00
19:10	160.220	123.35	-41.66	4.04E+00
19:30	180.220	123.45	-41.76	4.54E+00
20:10	220.500	123.66	-41.97	5.56E+00
20:30	240.270	123.52	-41.83	6.06E+00
20:50	260.330	123.72	-42.03	6.56E+00
21:10	280.330	123.69	-42.00	7.06E+00
21:30	300.230	123.69	-42.00	7.57E+00
21:50	320.280	123.70	-42.01	8.07E+00
22:10	340.320	123.69	-42.00	8.58E+00

22:30	360.300	123.69	-42.00	9.08E+00
22:50	380.270	123.70	-42.01	9.58E+00
23:10	400.270	123.70	-42.01	1.01E+01
23:30	420.270	123.70	-42.01	1.06E+01
23:50	440.270	123.70	-42.01	1.11E+01
00:10	460.270	123.70	-42.01	1.16E+01
00:30	480.270	123.70	-42.01	1.21E+01
00:50	500.270	123.70	-42.01	1.26E+01
01:10	520.270	123.70	-42.01	1.31E+01
01:30	540.220	123.72	-42.03	1.36E+01
01:50	560.230	123.72	-42.03	1.41E+01
02:10	580.230	123.72	-42.03	1.46E+01
02:30	600.230	123.72	-42.03	1.51E+01
02:50	620.230	123.72	-42.03	1.56E+01
03:10	640.230	123.72	-42.03	1.61E+01
03:30	660.230	123.73	-42.04	1.66E+01
03:50	680.230	123.72	-42.03	1.71E+01
04:10	700.180	123.72	-42.03	1.76E+01
04:30	720.320	123.72	-42.03	1.82E+01
04:50	740.280	123.72	-42.03	1.87E+01
05:10	760.280	123.72	-42.03	1.92E+01
05:30	780.280	123.70	-42.01	1.97E+01
05:50	800.320	123.70	-42.01	2.02E+01
06:10	820.320	123.72	-42.03	2.07E+01
06:30	840.320	123.72	-42.03	2.12E+01
06:50	860.320	123.72	-42.03	2.17E+01
07:10	880.320	123.72	-42.03	2.22E+01
07:30	900.320	123.70	-42.01	2.27E+01
07:50	920.320	123.72	-42.03	2.32E+01
08:10	940.320	123.70	-42.01	2.37E+01
08:30	960.320	123.70	-42.01	2.42E+01
08:50	980.320	123.70	-42.01	2.47E+01
10:10	1060.500	123.70	-42.01	2.67E+01
11:10	1120.200	123.68	-41.99	2.82E+01
12:10	1180.200	123.68	-41.99	2.97E+01
13:10	1240.200	123.66	-41.97	3.13E+01
14:10	1300.200	123.68	-41.99	3.28E+01
15:10	1360.200	123.68	-41.99	3.43E+01
16:10	1420.200	123.68	-41.99	3.58E+01
17:10	1480.200	123.68	-41.99	3.73E+01
18:10	1540.100	123.68	-41.99	3.88E+01
19:10	1600.300	123.68	-41.99	4.03E+01
20:10	1660.300	123.68	-41.99	4.18E+01
21:10	1720.300	123.68	-41.99	4.34E+01
22:10	1780.200	123.68	-41.99	4.49E+01
23:10	1840.200	123.68	-41.99	4.64E+01
00:10	1900.200	123.66	-41.97	4.79E+01
01:10	1960.300	123.68	-41.99	4.94E+01
02:10	2020.300	123.68	-41.99	5.09E+01
03:10	2080.200	123.68	-41.99	5.24E+01
04:10	2140.200	123.68	-41.99	5.39E+01
05:10	2200.200	123.69	-42.00	5.54E+01
06:10	2260.200	123.69	-42.00	5.70E+01
07:10	2320.200	123.69	-42.00	5.85E+01
08:10	2380.300	123.72	-42.03	6.00E+01
09:10	2440.200	123.68	-41.99	6.15E+01

10:10	2500.300	122.72	-41.03	6.30E+01
11:10	2560.300	123.66	-41.97	6.45E+01
12:10	2620.300	123.68	-41.99	6.60E+01
13:10	2680.300	122.55	-40.86	6.75E+01
14:10	2740.200	123.68	-41.99	6.91E+01
15:10	2800.200	123.66	-41.97	7.06E+01
16:10	2860.300	123.57	-41.88	7.21E+01
17:10	2920.200	123.68	-41.99	7.36E+01
18:10	2980.200	123.68	-41.99	7.51E+01
19:10	3040.200	123.49	-41.80	7.66E+01
20:10	3100.200	123.68	-41.99	7.81E+01
21:10	3160.200	123.68	-41.99	7.96E+01
22:10	3220.200	123.68	-41.99	8.12E+01
23:10	3280.200	123.68	-41.99	8.27E+01
00:10	3340.200	123.22	-41.53	8.42E+01
01:10	3400.200	123.39	-41.70	8.57E+01
02:10	3460.200	123.66	-41.97	8.72E+01
03:10	3520.200	123.66	-41.97	8.87E+01
04:10	3580.200	123.66	-41.97	9.02E+01
05:10	3640.200	123.66	-41.97	9.17E+01
06:10	3700.200	123.09	-41.40	9.32E+01
07:10	3760.400	121.10	-39.41	9.48E+01
08:10	3820.200	121.89	-40.20	9.63E+01
09:10	3880.200	122.43	-40.74	9.78E+01
10:10	3940.200	122.12	-40.43	9.93E+01
11:10	4000.200	121.73	-40.04	1.01E+02
12:10	4060.300	123.05	-41.36	1.02E+02
13:10	4120.200	121.57	-39.88	1.04E+02
14:10	4180.200	122.67	-40.98	1.05E+02
15:10	4240.300	122.44	-40.75	1.07E+02
16:10	4300.200	122.44	-40.75	1.08E+02
16:59	4349.700	122.67	-40.98	1.10E+02

PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 3-4 (INPUT 1)  
 WELL MATERIAL: PVC  
 RADIUS: 0.166 FEET  
 STARTING WATER LEVEL: 81.690 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 122.680 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r2	RESIDUAL DRAWDOWN (FEET)	t/t'
0.084	122.46	0.22	2.12E-03	40.77	5.18E+04
0.167	122.29	0.39	4.21E-03	40.60	2.60E+04
0.251	122.10	0.58	6.33E-03	40.41	1.73E+04
0.334	121.92	0.76	8.42E-03	40.23	1.30E+04
0.417	121.72	0.96	1.05E-02	40.03	1.04E+04
0.501	121.52	1.16	1.26E-02	39.83	8.68E+03
0.584	121.30	1.38	1.47E-02	39.61	7.45E+03
0.667	121.10	1.58	1.68E-02	39.41	6.52E+03
0.751	120.90	1.78	1.89E-02	39.21	5.79E+03
0.834	120.70	1.98	2.10E-02	39.01	5.22E+03
0.917	120.50	2.18	2.31E-02	38.81	4.74E+03
1.001	120.30	2.38	2.52E-02	38.61	4.35E+03
1.389	119.37	3.31	3.50E-02	37.68	3.13E+03
1.723	118.59	4.09	4.34E-02	36.90	2.53E+03
2.056	117.81	4.87	5.18E-02	36.12	2.12E+03
2.389	117.06	5.62	6.02E-02	35.37	1.82E+03
2.723	116.31	6.37	6.86E-02	34.62	1.60E+03
3.056	115.57	7.11	7.70E-02	33.88	1.42E+03
3.389	114.85	7.83	8.54E-02	33.16	1.28E+03
3.723	114.14	8.54	9.38E-02	32.45	1.17E+03
4.056	113.45	9.23	1.02E-01	31.76	1.07E+03
4.389	112.77	9.91	1.11E-01	31.08	9.92E+02
4.723	112.09	10.59	1.19E-01	30.40	9.22E+02
5.056	111.43	11.25	1.27E-01	29.74	8.61E+02
5.389	110.79	11.89	1.36E-01	29.10	8.08E+02
5.723	110.15	12.53	1.44E-01	28.46	7.61E+02
6.056	109.52	13.16	1.53E-01	27.83	7.19E+02
6.389	108.90	13.78	1.61E-01	27.21	6.82E+02
6.723	108.30	14.38	1.69E-01	26.61	6.48E+02
7.056	107.72	14.96	1.78E-01	26.03	6.17E+02
7.389	107.13	15.55	1.86E-01	25.44	5.90E+02
7.723	106.57	16.11	1.95E-01	24.88	5.64E+02
8.056	106.00	16.68	2.03E-01	24.31	5.41E+02
8.389	105.46	17.22	2.11E-01	23.77	5.20E+02

PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 3-4 (INPUT 1)  
 WELL MATERIAL: PVC  
 RADIUS: 0.166 FEET  
 STARTING WATER LEVEL: 81.690 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 122.680 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r <sup>2</sup>	RESIDUAL DRAWDOWN (FEET)	t/t'
8.723	104.92	17.76	2.20E-01	23.23	5.00E+02
9.056	104.39	18.29	2.28E-01	22.70	4.81E+02
9.389	103.87	18.81	2.37E-01	22.18	4.64E+02
9.723	103.36	19.32	2.45E-01	21.67	4.48E+02
10.056	102.86	19.82	2.53E-01	21.17	4.34E+02
12.165	99.90	22.78	3.07E-01	18.21	3.59E+02
14.495	97.07	25.61	3.65E-01	15.38	3.01E+02
16.165	95.26	27.42	4.07E-01	13.57	2.70E+02
18.165	93.35	29.33	4.58E-01	11.66	2.40E+02
20.203	91.66	31.02	5.09E-01	9.97	2.16E+02
22.203	90.20	32.48	5.60E-01	8.51	1.97E+02
24.225	88.92	33.76	6.10E-01	7.23	1.81E+02
26.225	87.81	34.87	6.61E-01	6.12	1.67E+02
28.225	86.83	35.85	7.11E-01	5.14	1.55E+02
30.225	86.01	36.67	7.62E-01	4.32	1.45E+02
32.225	85.31	37.37	8.12E-01	3.62	1.36E+02
34.225	84.73	37.95	8.63E-01	3.04	1.28E+02
36.225	84.23	38.45	9.13E-01	2.54	1.21E+02
38.225	83.83	38.85	9.63E-01	2.14	1.15E+02
40.225	83.50	39.18	1.01E+00	1.81	1.09E+02
42.225	83.24	39.44	1.06E+00	1.55	1.04E+02
44.225	83.04	39.64	1.11E+00	1.35	9.94E+01
46.225	82.90	39.78	1.16E+00	1.21	9.51E+01
48.225	82.78	39.90	1.22E+00	1.09	9.12E+01
50.225	82.70	39.98	1.27E+00	1.01	8.76E+01
52.225	82.65	40.03	1.32E+00	0.96	8.43E+01
54.225	82.62	40.06	1.37E+00	0.93	8.12E+01
56.225	82.58	40.10	1.42E+00	0.89	7.84E+01
58.225	82.55	40.13	1.47E+00	0.86	7.57E+01
60.225	82.54	40.14	1.52E+00	0.85	7.32E+01
62.225	82.52	40.16	1.57E+00	0.83	7.09E+01
64.225	82.52	40.16	1.62E+00	0.83	6.87E+01
66.225	82.51	40.17	1.67E+00	0.82	6.67E+01
68.225	82.51	40.17	1.72E+00	0.82	6.48E+01

PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 3-4 (INPUT 1)  
 WELL MATERIAL: PVC  
 RADIUS: 0.166 FEET  
 STARTING WATER LEVEL: 81.690 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 122.680 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r2	RESIDUAL DRAWDOWN (FEET)	t/t'
70.225	82.50	40.18	1.77E+00	0.81	6.29E+01
72.225	82.50	40.18	1.82E+00	0.81	6.12E+01
74.225	82.48	40.20	1.87E+00	0.79	5.96E+01
76.225	82.48	40.20	1.92E+00	0.79	5.81E+01
78.225	82.47	40.21	1.97E+00	0.78	5.66E+01
80.225	82.47	40.21	2.02E+00	0.78	5.52E+01
82.225	82.45	40.23	2.07E+00	0.76	5.39E+01
84.225	82.45	40.23	2.12E+00	0.76	5.26E+01
86.225	82.45	40.23	2.17E+00	0.76	5.14E+01
88.225	82.45	40.23	2.22E+00	0.76	5.03E+01
90.225	82.44	40.24	2.27E+00	0.75	4.92E+01
92.225	82.44	40.24	2.32E+00	0.75	4.82E+01
94.225	82.44	40.24	2.37E+00	0.75	4.72E+01
96.225	82.42	40.26	2.42E+00	0.73	4.62E+01
98.225	82.42	40.26	2.48E+00	0.73	4.53E+01
100.230	82.41	40.27	2.53E+00	0.72	4.44E+01
120.230	82.37	40.31	3.03E+00	0.68	3.72E+01
140.230	82.34	40.34	3.53E+00	0.65	3.20E+01
160.230	82.30	40.38	4.04E+00	0.61	2.81E+01
180.220	82.28	40.40	4.54E+00	0.59	2.51E+01
200.220	82.25	40.43	5.05E+00	0.56	2.27E+01
220.220	82.22	40.46	5.55E+00	0.53	2.08E+01
240.220	82.21	40.47	6.05E+00	0.52	1.91E+01
260.220	82.20	40.48	6.56E+00	0.51	1.77E+01
280.120	82.18	40.50	7.06E+00	0.49	1.65E+01
300.120	82.17	40.51	7.56E+00	0.48	1.55E+01
320.120	82.15	40.53	8.07E+00	0.46	1.46E+01
340.200	82.12	40.56	8.57E+00	0.43	1.38E+01
360.220	82.12	40.56	9.08E+00	0.43	1.31E+01
380.220	82.11	40.57	9.58E+00	0.42	1.24E+01
400.220	82.09	40.59	1.01E+01	0.40	1.19E+01
420.220	82.08	40.60	1.06E+01	0.39	1.14E+01
440.220	82.07	40.61	1.11E+01	0.38	1.09E+01
460.220	82.05	40.63	1.16E+01	0.36	1.05E+01



PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 3-4 (INPUT 1)  
 WELL MATERIAL: PVC  
 RADIUS: 0.165 FEET  
 STARTING WATER LEVEL: 81.690 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 122.680 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r <sup>2</sup>	RESIDUAL DRAWDOWN (FEET)	t/t'
480.220	82.04	40.64	1.21E+01	0.35	1.01E+01
500.220	82.04	40.64	1.26E+01	0.35	9.70E+00
520.220	82.02	40.66	1.31E+01	0.33	9.36E+00
540.220	82.01	40.67	1.36E+01	0.32	9.05E+00
560.200	82.01	40.67	1.41E+01	0.32	8.76E+00
580.200	81.99	40.69	1.46E+01	0.30	8.50E+00
600.200	81.99	40.69	1.51E+01	0.30	8.25E+00
620.200	81.98	40.70	1.56E+01	0.29	8.01E+00
640.200	81.97	40.71	1.61E+01	0.28	7.79E+00
660.200	81.97	40.71	1.66E+01	0.28	7.59E+00
680.220	81.95	40.73	1.71E+01	0.26	7.39E+00
700.220	81.95	40.73	1.76E+01	0.26	7.21E+00
720.220	81.95	40.73	1.82E+01	0.26	7.04E+00
740.220	81.94	40.74	1.87E+01	0.25	6.88E+00
760.170	81.92	40.76	1.92E+01	0.23	6.72E+00

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 3-4 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 11 INPUT 2  
 RADIUS: 446.391 FEET  
 START DATE : 21-Aug-86  
 START TIME : 16:30  
 WATER START LEVEL: 79.28 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
16:30	0.000	79.28	0.00	0.00E+00
16:30	0.084	79.28	0.00	2.93E-10
16:30	0.167	79.28	0.00	5.82E-10
16:30	0.251	79.28	0.00	8.75E-10
16:30	0.334	79.28	0.00	1.16E-09
16:30	0.417	79.28	0.00	1.45E-09
16:30	0.501	79.28	0.00	1.75E-09
16:30	0.584	79.28	0.00	2.04E-09
16:30	0.667	79.28	0.00	2.32E-09
16:30	0.751	79.28	0.00	2.62E-09
16:30	0.834	79.28	0.00	2.91E-09
16:30	0.917	79.28	0.00	3.20E-09
16:31	1.001	79.28	0.00	3.49E-09
16:31	1.391	79.28	0.00	4.85E-09
16:31	1.724	79.28	0.00	6.01E-09
16:32	2.058	79.28	0.00	7.17E-09
16:32	2.391	79.28	0.00	8.33E-09
16:32	2.724	79.28	0.00	9.49E-09
16:33	3.058	79.28	0.00	1.07E-08
16:33	3.391	79.28	0.00	1.18E-08
16:33	3.724	79.28	0.00	1.30E-08
16:34	4.058	79.28	0.00	1.41E-08
16:34	4.391	79.28	0.00	1.53E-08
16:34	4.724	79.28	0.00	1.65E-08
16:35	5.058	79.28	0.00	1.76E-08
16:35	5.391	79.28	0.00	1.88E-08
16:35	5.724	79.28	0.00	1.99E-08
16:36	6.058	79.28	0.00	2.11E-08
16:36	6.391	79.28	0.00	2.23E-08
16:36	6.724	79.28	0.00	2.34E-08
16:37	7.058	79.28	0.00	2.46E-08
16:37	7.391	79.28	0.00	2.58E-08
16:37	7.724	79.28	0.00	2.69E-08
16:38	8.058	79.28	0.00	2.81E-08
16:38	8.391	79.28	0.00	2.92E-08
16:38	8.724	79.28	0.00	3.04E-08
16:39	9.058	79.28	0.00	3.16E-08
16:39	9.391	79.28	0.00	3.27E-08
16:39	9.724	79.28	0.00	3.39E-08
16:40	10.058	79.28	0.00	3.51E-08

16:42	12.153	79.28	0.00	4.24E-08
16:44	14.153	79.28	0.00	4.93E-08
16:46	16.423	79.28	0.00	5.72E-08
16:48	18.762	79.28	0.00	6.54E-08
16:50	20.193	79.28	0.00	7.04E-08
16:52	22.193	79.28	0.00	7.73E-08
16:54	24.193	79.26	0.02	8.43E-08
16:56	26.193	79.28	0.00	9.13E-08
16:58	28.193	79.28	0.00	9.83E-08
17:00	30.193	79.28	0.00	1.05E-07
17:02	32.193	79.28	0.00	1.12E-07
17:04	34.158	79.29	-0.01	1.19E-07
17:06	36.158	79.28	0.00	1.26E-07
17:08	38.158	79.28	0.00	1.33E-07
17:10	40.158	79.28	0.00	1.40E-07
17:12	42.158	79.28	0.00	1.47E-07
17:14	44.158	79.28	0.00	1.54E-07
17:16	46.158	79.28	0.00	1.61E-07
17:18	48.158	79.29	-0.01	1.68E-07
17:20	50.158	79.29	-0.01	1.75E-07
17:22	52.158	79.29	-0.01	1.82E-07
17:24	54.158	79.29	-0.01	1.89E-07
17:26	56.158	79.29	-0.01	1.96E-07
17:28	58.158	79.29	-0.01	2.03E-07
17:30	60.158	79.29	-0.01	2.10E-07
17:32	62.247	79.29	-0.01	2.17E-07
17:34	64.135	79.29	-0.01	2.24E-07
17:36	66.135	79.31	-0.03	2.30E-07
17:38	68.135	79.31	-0.03	2.37E-07
17:40	70.135	79.31	-0.03	2.44E-07
17:42	72.135	79.31	-0.03	2.51E-07
17:44	74.135	79.31	-0.03	2.58E-07
17:46	76.135	79.31	-0.03	2.65E-07
17:48	78.135	79.31	-0.03	2.72E-07
17:50	80.782	79.31	-0.03	2.82E-07
17:52	82.182	79.32	-0.04	2.86E-07
17:54	84.070	79.32	-0.04	2.93E-07
17:56	86.070	79.32	-0.04	3.00E-07
17:58	88.070	79.32	-0.04	3.07E-07
18:00	90.070	79.34	-0.06	3.14E-07
18:02	92.070	79.34	-0.06	3.21E-07
18:04	94.070	79.34	-0.06	3.28E-07
18:06	96.070	79.34	-0.06	3.35E-07
18:08	98.115	79.35	-0.07	3.42E-07
18:10	100.120	79.35	-0.07	3.49E-07
18:30	120.280	79.37	-0.09	4.19E-07
18:50	140.220	79.37	-0.09	4.89E-07
19:10	160.220	79.38	-0.10	5.58E-07
19:30	180.220	79.41	-0.13	6.28E-07
20:10	220.500	79.45	-0.17	7.68E-07
20:30	240.270	79.48	-0.20	8.37E-07
20:50	260.330	79.50	-0.22	9.07E-07
21:10	280.330	79.51	-0.23	9.77E-07
21:30	300.230	79.53	-0.25	1.05E-06
21:50	320.280	79.56	-0.28	1.12E-06
22:10	340.320	79.56	-0.28	1.19E-06

22:30	360.300	79.57	-0.29	1.26E-06
22:50	380.270	79.58	-0.30	1.33E-06
23:10	400.270	79.58	-0.30	1.39E-06
23:30	420.270	79.60	-0.32	1.46E-06
23:50	440.270	79.60	-0.32	1.53E-06
00:10	460.270	79.60	-0.32	1.60E-06
00:30	480.270	79.61	-0.33	1.67E-06
00:50	500.270	79.61	-0.33	1.74E-06
01:10	520.270	79.63	-0.35	1.81E-06
01:30	540.220	79.63	-0.35	1.88E-06
01:50	560.230	79.64	-0.36	1.95E-06
02:10	580.230	79.64	-0.36	2.02E-06
02:30	600.230	79.64	-0.36	2.09E-06
02:50	620.230	79.66	-0.38	2.16E-06
03:10	640.230	79.66	-0.38	2.23E-06
03:30	660.230	79.66	-0.38	2.30E-06
03:50	680.230	79.67	-0.39	2.37E-06
04:10	700.180	79.67	-0.39	2.44E-06
04:30	720.320	79.67	-0.39	2.51E-06
04:50	740.280	79.69	-0.41	2.58E-06
05:10	760.280	79.69	-0.41	2.65E-06
05:30	780.280	79.69	-0.41	2.72E-06
05:50	800.320	79.70	-0.42	2.79E-06
06:10	820.320	79.70	-0.42	2.86E-06
06:30	840.320	79.70	-0.42	2.93E-06
06:50	860.320	79.70	-0.42	3.00E-06
07:10	880.320	79.72	-0.44	3.07E-06
07:30	900.320	79.72	-0.44	3.14E-06
07:50	920.320	79.72	-0.44	3.21E-06
08:10	940.320	79.73	-0.45	3.28E-06
08:30	960.320	79.73	-0.45	3.35E-06
08:50	980.320	79.74	-0.46	3.42E-06
10:10	1060.500	79.76	-0.48	3.70E-06
11:10	1120.200	79.77	-0.49	3.90E-06
12:10	1180.200	79.77	-0.49	4.11E-06
13:10	1240.200	79.77	-0.49	4.32E-06
14:10	1300.200	79.79	-0.51	4.53E-06
15:10	1360.200	79.80	-0.52	4.74E-06
16:10	1420.200	79.80	-0.52	4.95E-06
17:10	1480.200	79.80	-0.52	5.16E-06
18:10	1540.100	79.80	-0.52	5.37E-06
19:10	1600.300	79.79	-0.51	5.58E-06
20:10	1660.300	79.79	-0.51	5.79E-06
21:10	1720.300	79.80	-0.52	6.00E-06
22:10	1780.200	79.82	-0.54	6.20E-06
23:10	1840.200	79.80	-0.52	6.41E-06
00:10	1900.200	79.82	-0.54	6.62E-06
01:10	1960.300	79.82	-0.54	6.83E-06
02:10	2020.300	79.82	-0.54	7.04E-06
03:10	2080.200	79.82	-0.54	7.25E-06
04:10	2140.200	79.83	-0.55	7.46E-06
05:10	2200.200	79.83	-0.55	7.67E-06
06:10	2260.200	79.83	-0.55	7.88E-06
07:10	2320.200	79.83	-0.55	8.09E-06
08:10	2380.300	79.83	-0.55	8.30E-06
09:10	2440.200	79.83	-0.55	8.50E-06

10:10	2500.300	79.85	-0.57	8.71E-06
11:10	2560.300	79.85	-0.57	8.92E-06
12:10	2620.300	79.85	-0.57	9.13E-06
13:10	2680.300	79.83	-0.55	9.34E-06
14:10	2740.200	79.83	-0.55	9.55E-06
15:10	2800.200	79.83	-0.55	9.76E-06
16:10	2860.300	79.82	-0.54	9.97E-06
17:10	2920.200	79.82	-0.54	1.02E-05
18:10	2980.200	79.80	-0.52	1.04E-05
19:10	3040.200	79.80	-0.52	1.06E-05
20:10	3100.200	79.80	-0.52	1.08E-05
21:10	3160.200	79.80	-0.52	1.10E-05
22:10	3220.200	79.82	-0.54	1.12E-05
23:10	3280.200	79.82	-0.54	1.14E-05
00:10	3340.200	79.83	-0.55	1.16E-05
01:10	3400.200	79.83	-0.55	1.18E-05
02:10	3460.200	79.83	-0.55	1.21E-05
03:10	3520.200	79.85	-0.57	1.23E-05
04:10	3580.200	79.85	-0.57	1.25E-05
05:10	3640.200	79.85	-0.57	1.27E-05
06:10	3700.200	79.85	-0.57	1.29E-05
07:10	3760.400	79.85	-0.57	1.31E-05
08:10	3820.200	79.86	-0.58	1.33E-05
09:10	3880.200	79.86	-0.58	1.35E-05
10:10	3940.200	79.88	-0.60	1.37E-05
11:10	4000.200	79.89	-0.61	1.39E-05
12:10	4060.300	79.90	-0.62	1.42E-05
13:10	4120.200	79.90	-0.62	1.44E-05
14:10	4180.200	79.92	-0.64	1.46E-05
15:10	4240.300	79.92	-0.64	1.48E-05
16:10	4300.200	79.92	-0.64	1.50E-05
16:59	4349.700	79.95	-0.67	1.52E-05

PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 11 (INPUT 2)  
 WELL MATERIAL: PVC  
 RADIUS: 446.391 FEET  
 STARTING WATER LEVEL: 79.280 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 79.950 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r2	RESIDUAL DRAWDOWN (FEET)	t/t'
0.084	79.95	0.00	2.93E-10	0.67	5.18E+04
0.167	79.95	0.00	5.82E-10	0.67	2.60E+04
0.251	79.95	0.00	8.75E-10	0.67	1.73E+04
0.334	79.95	0.00	1.16E-09	0.67	1.30E+04
0.417	79.95	0.00	1.45E-09	0.67	1.04E+04
0.501	79.95	0.00	1.75E-09	0.67	8.68E+03
0.584	79.95	0.00	2.04E-09	0.67	7.45E+03
0.667	79.95	0.00	2.32E-09	0.67	6.52E+03
0.751	79.93	0.02	2.62E-09	0.65	5.79E+03
0.834	79.93	0.02	2.91E-09	0.65	5.22E+03
0.917	79.95	0.00	3.20E-09	0.67	4.74E+03
1.001	79.93	0.02	3.49E-09	0.65	4.35E+03
1.389	79.93	0.02	4.84E-09	0.65	3.13E+03
1.723	79.95	0.00	6.00E-09	0.67	2.53E+03
2.056	79.95	0.00	7.17E-09	0.67	2.12E+03
2.389	79.95	0.00	8.33E-09	0.67	1.82E+03
2.723	79.95	0.00	9.49E-09	0.67	1.60E+03
3.056	79.95	0.00	1.07E-08	0.67	1.42E+03
3.389	79.95	0.00	1.18E-08	0.67	1.28E+03
3.723	79.95	0.00	1.30E-08	0.67	1.17E+03
4.056	79.95	0.00	1.41E-08	0.67	1.07E+03
4.389	79.95	0.00	1.53E-08	0.67	9.92E+02
4.723	79.95	0.00	1.65E-08	0.67	9.22E+02
5.056	79.95	0.00	1.76E-08	0.67	8.61E+02
5.389	79.95	0.00	1.88E-08	0.67	8.08E+02
5.723	79.93	0.02	1.99E-08	0.65	7.61E+02
6.056	79.93	0.02	2.11E-08	0.65	7.19E+02
6.389	79.93	0.02	2.23E-08	0.65	6.82E+02
6.723	79.93	0.02	2.34E-08	0.65	6.48E+02
7.056	79.95	0.00	2.46E-08	0.67	6.17E+02
7.389	79.93	0.02	2.58E-08	0.65	5.90E+02
7.723	79.95	0.00	2.69E-08	0.67	5.64E+02
8.056	79.95	0.00	2.81E-08	0.67	5.41E+02
8.389	79.95	0.00	2.92E-08	0.67	5.20E+02

PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 11 (INPUT 2)  
 WELL MATERIAL: PVC  
 RADIUS: 446.391 FEET  
 STARTING WATER LEVEL: 79.280 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 79.950 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r <sup>2</sup>	RESIDUAL DRAWDOWN (FEET)	t/t'
8.723	79.95	0.00	3.04E-08	0.67	5.00E+02
9.056	79.95	0.00	3.16E-08	0.67	4.81E+02
9.389	79.93	0.02	3.27E-08	0.65	4.64E+02
9.723	79.95	0.00	3.39E-08	0.67	4.48E+02
10.056	79.93	0.02	3.50E-08	0.65	4.34E+02
12.165	79.95	0.00	4.24E-08	0.67	3.59E+02
14.495	79.95	0.00	5.05E-08	0.67	3.01E+02
16.165	79.93	0.02	5.63E-08	0.65	2.70E+02
18.165	79.95	0.00	6.33E-08	0.67	2.40E+02
20.203	79.93	0.02	7.04E-08	0.65	2.16E+02
22.203	79.93	0.02	7.74E-08	0.65	1.97E+02
24.225	79.93	0.02	8.44E-08	0.65	1.81E+02
26.225	79.93	0.02	9.14E-08	0.65	1.67E+02
28.225	79.93	0.02	9.84E-08	0.65	1.55E+02
30.225	79.93	0.02	1.05E-07	0.65	1.45E+02
32.225	79.93	0.02	1.12E-07	0.65	1.36E+02
34.225	79.93	0.02	1.19E-07	0.65	1.28E+02
36.225	79.93	0.02	1.26E-07	0.65	1.21E+02
38.225	79.93	0.02	1.33E-07	0.65	1.15E+02
40.225	79.93	0.02	1.40E-07	0.65	1.09E+02
42.225	79.93	0.02	1.47E-07	0.65	1.04E+02
44.225	79.93	0.02	1.54E-07	0.65	9.94E+01
46.225	79.93	0.02	1.61E-07	0.65	9.51E+01
48.225	79.93	0.02	1.68E-07	0.65	9.12E+01
50.225	79.93	0.02	1.75E-07	0.65	8.76E+01
52.225	79.92	0.03	1.82E-07	0.64	8.43E+01
54.225	79.93	0.02	1.89E-07	0.65	8.12E+01
56.225	79.92	0.03	1.96E-07	0.64	7.84E+01
58.225	79.92	0.03	2.03E-07	0.64	7.57E+01
60.225	79.92	0.03	2.10E-07	0.64	7.32E+01
62.225	79.92	0.03	2.17E-07	0.64	7.09E+01
64.225	79.92	0.03	2.24E-07	0.64	6.87E+01
66.225	79.92	0.03	2.31E-07	0.64	6.67E+01
68.225	79.90	0.05	2.38E-07	0.62	6.48E+01

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 3-4 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 7 INPUT 3  
 RADIUS: 682.670 FEET  
 START DATE : 21-Aug-86  
 START TIME : 16:30  
 WATER START LEVEL: 81.17 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
16:30	0.000	81.17	0.00	0.00E+00
16:30	0.084	81.17	0.00	1.25E-10
16:30	0.167	81.17	0.00	2.49E-10
16:30	0.251	81.17	0.00	3.74E-10
16:30	0.334	81.17	0.00	4.98E-10
16:30	0.417	81.17	0.00	6.21E-10
16:30	0.501	81.17	0.00	7.47E-10
16:30	0.584	81.17	0.00	8.70E-10
16:30	0.667	81.17	0.00	9.94E-10
16:30	0.751	81.17	0.00	1.12E-09
16:30	0.834	81.17	0.00	1.24E-09
16:30	0.917	81.17	0.00	1.37E-09
16:31	1.001	81.17	0.00	1.49E-09
16:31	1.391	81.17	0.00	2.07E-09
16:31	1.724	81.17	0.00	2.57E-09
16:32	2.058	81.17	0.00	3.07E-09
16:32	2.391	81.17	0.00	3.56E-09
16:32	2.724	81.17	0.00	4.06E-09
16:33	3.058	81.17	0.00	4.56E-09
16:33	3.391	81.17	0.00	5.05E-09
16:33	3.724	81.17	0.00	5.55E-09
16:34	4.058	81.17	0.00	6.05E-09
16:34	4.391	81.17	0.00	6.54E-09
16:34	4.724	81.17	0.00	7.04E-09
16:35	5.058	81.17	0.00	7.54E-09
16:35	5.391	81.17	0.00	8.03E-09
16:35	5.724	81.17	0.00	8.53E-09
16:36	6.058	81.17	0.00	9.03E-09
16:36	6.391	81.18	-0.01	9.52E-09
16:36	6.724	81.17	0.00	1.00E-08
16:37	7.058	81.17	0.00	1.05E-08
16:37	7.391	81.17	0.00	1.10E-08
16:37	7.724	81.17	0.00	1.15E-08
16:38	8.058	81.17	0.00	1.20E-08
16:38	8.391	81.16	0.01	1.25E-08
16:38	8.724	81.16	0.01	1.30E-08
16:39	9.058	81.16	0.01	1.35E-08
16:39	9.391	81.17	0.00	1.40E-08
16:39	9.724	81.18	-0.01	1.45E-08
16:40	10.058	81.17	0.00	1.50E-08



PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 11 (INPUT 2)  
 WELL MATERIAL: PVC  
 RADIUS: 446.391 FEET  
 STARTING WATER LEVEL: 79.280 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 79.950 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r <sup>2</sup>	RESIDUAL DRAWDOWN (FEET)	t/t'
70.225	79.90	0.05	2.45E-07	0.62	6.29E+01
72.225	79.90	0.05	2.52E-07	0.62	6.12E+01
74.225	79.90	0.05	2.59E-07	0.62	5.96E+01
76.225	79.90	0.05	2.66E-07	0.62	5.81E+01
78.225	79.89	0.06	2.73E-07	0.61	5.66E+01
80.225	79.89	0.06	2.80E-07	0.61	5.52E+01
82.225	79.89	0.06	2.87E-07	0.61	5.39E+01
84.225	79.89	0.06	2.94E-07	0.61	5.26E+01
86.225	79.89	0.06	3.00E-07	0.61	5.14E+01
88.225	79.89	0.06	3.07E-07	0.61	5.03E+01
90.225	79.88	0.07	3.14E-07	0.60	4.92E+01
92.225	79.88	0.07	3.21E-07	0.60	4.82E+01
94.225	79.88	0.07	3.28E-07	0.60	4.72E+01
96.225	79.88	0.07	3.35E-07	0.60	4.62E+01
98.225	79.88	0.07	3.42E-07	0.60	4.53E+01
100.230	79.88	0.07	3.49E-07	0.60	4.44E+01
120.230	79.85	0.10	4.19E-07	0.57	3.72E+01
140.230	79.82	0.13	4.89E-07	0.54	3.20E+01
160.230	79.79	0.16	5.58E-07	0.51	2.81E+01
180.220	79.77	0.18	6.28E-07	0.49	2.51E+01
200.220	79.74	0.21	6.98E-07	0.46	2.27E+01
220.220	79.73	0.22	7.67E-07	0.45	2.08E+01
240.220	79.72	0.23	8.37E-07	0.44	1.91E+01
260.220	79.70	0.25	9.07E-07	0.42	1.77E+01
280.120	79.69	0.26	9.76E-07	0.41	1.65E+01
300.120	79.67	0.28	1.05E-06	0.39	1.55E+01
320.120	79.66	0.29	1.12E-06	0.38	1.46E+01
340.200	79.64	0.31	1.19E-06	0.36	1.38E+01
360.220	79.63	0.32	1.26E-06	0.35	1.31E+01
380.220	79.61	0.34	1.33E-06	0.33	1.24E+01
400.220	79.60	0.35	1.39E-06	0.32	1.19E+01
420.220	79.58	0.37	1.46E-06	0.30	1.14E+01
440.220	79.58	0.37	1.53E-06	0.30	1.09E+01
460.220	79.57	0.38	1.60E-06	0.29	1.05E+01

PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 11 (INPUT 2)  
 WELL MATERIAL: PVC  
 RADIUS: 446.391 FEET  
 STARTING WATER LEVEL: 79.280 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 79.950 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r <sup>2</sup>	RESIDUAL DRAWDOWN (FEET)	t/t'
480.220	79.56	0.39	1.67E-06	0.28	1.01E+01
500.220	79.56	0.39	1.74E-06	0.28	9.70E+00
520.220	79.54	0.41	1.81E-06	0.26	9.36E+00
540.220	79.54	0.41	1.88E-06	0.26	9.05E+00
560.200	79.53	0.42	1.95E-06	0.25	8.76E+00
580.200	79.53	0.42	2.02E-06	0.25	8.50E+00
600.200	79.51	0.44	2.09E-06	0.23	8.25E+00
620.200	79.51	0.44	2.16E-06	0.23	8.01E+00
640.200	79.51	0.44	2.23E-06	0.23	7.79E+00
660.200	79.50	0.45	2.30E-06	0.22	7.59E+00
680.220	79.50	0.45	2.37E-06	0.22	7.39E+00
700.220	79.48	0.47	2.44E-06	0.20	7.21E+00
720.220	79.48	0.47	2.51E-06	0.20	7.04E+00
740.220	79.47	0.48	2.58E-06	0.19	6.88E+00
760.170	79.47	0.48	2.65E-06	0.19	6.72E+00
780.080	79.45	0.50	2.72E-06	0.17	6.58E+00
800.080	79.45	0.50	2.79E-06	0.17	6.44E+00
820.080	79.45	0.50	2.86E-06	0.17	6.30E+00
840.080	79.45	0.50	2.93E-06	0.17	6.18E+00
860.070	79.45	0.50	3.00E-06	0.17	6.06E+00
880.170	79.44	0.51	3.07E-06	0.16	5.94E+00
900.170	79.44	0.51	3.14E-06	0.16	5.83E+00
920.170	79.44	0.51	3.21E-06	0.16	5.73E+00
940.130	79.45	0.50	3.28E-06	0.17	5.63E+00
954.580	79.44	0.51	3.33E-06	0.16	5.56E+00

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 3-4 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 7 INPUT 3  
 RADIUS: 682.670 FEET  
 START DATE : 21-Aug-86  
 START TIME : 16:30  
 WATER START LEVEL: 81.17 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
16:30	0.000	81.17	0.00	0.00E+00
16:30	0.084	81.17	0.00	1.25E-10
16:30	0.167	81.17	0.00	2.49E-10
16:30	0.251	81.17	0.00	3.74E-10
16:30	0.334	81.17	0.00	4.98E-10
16:30	0.417	81.17	0.00	6.21E-10
16:30	0.501	81.17	0.00	7.47E-10
16:30	0.584	81.17	0.00	8.70E-10
16:30	0.667	81.17	0.00	9.94E-10
16:30	0.751	81.17	0.00	1.12E-09
16:30	0.834	81.17	0.00	1.24E-09
16:30	0.917	81.17	0.00	1.37E-09
16:31	1.001	81.17	0.00	1.49E-09
16:31	1.391	81.17	0.00	2.07E-09
16:31	1.724	81.17	0.00	2.57E-09
16:32	2.058	81.17	0.00	3.07E-09
16:32	2.391	81.17	0.00	3.56E-09
16:32	2.724	81.17	0.00	4.06E-09
16:33	3.058	81.17	0.00	4.56E-09
16:33	3.391	81.17	0.00	5.05E-09
16:33	3.724	81.17	0.00	5.55E-09
16:34	4.058	81.17	0.00	6.05E-09
16:34	4.391	81.17	0.00	6.54E-09
16:34	4.724	81.17	0.00	7.04E-09
16:35	5.058	81.17	0.00	7.54E-09
16:35	5.391	81.17	0.00	8.03E-09
16:35	5.724	81.17	0.00	8.53E-09
16:36	6.058	81.17	0.00	9.03E-09
16:36	6.391	81.18	-0.01	9.52E-09
16:36	6.724	81.17	0.00	1.00E-08
16:37	7.058	81.17	0.00	1.05E-08
16:37	7.391	81.17	0.00	1.10E-08
16:37	7.724	81.17	0.00	1.15E-08
16:38	8.058	81.17	0.00	1.20E-08
16:38	8.391	81.16	0.01	1.25E-08
16:38	8.724	81.16	0.01	1.30E-08
16:39	9.058	81.16	0.01	1.35E-08
16:39	9.391	81.17	0.00	1.40E-08
16:39	9.724	81.18	-0.01	1.45E-08
16:40	10.058	81.17	0.00	1.50E-08

16:42	12.153	81.18	-0.01	1.81E-08
16:44	14.153	81.17	0.00	2.11E-08
16:46	16.423	81.17	0.00	2.45E-08
16:48	18.762	81.17	0.00	2.80E-08
16:50	20.193	81.17	0.00	3.01E-08
16:52	22.193	81.17	0.00	3.31E-08
16:54	24.193	81.17	0.00	3.61E-08
16:56	26.193	81.17	0.00	3.90E-08
16:58	28.193	81.17	0.00	4.20E-08
17:00	30.193	81.18	-0.01	4.50E-08
17:02	32.193	81.17	0.00	4.80E-08
17:04	34.158	81.17	0.00	5.09E-08
17:06	36.158	81.17	0.00	5.39E-08
17:08	38.158	81.17	0.00	5.69E-08
17:10	40.158	81.17	0.00	5.98E-08
17:12	42.158	81.17	0.00	6.28E-08
17:14	44.158	81.17	0.00	6.58E-08
17:16	46.158	81.17	0.00	6.88E-08
17:18	48.158	81.17	0.00	7.18E-08
17:20	50.158	81.17	0.00	7.47E-08
17:22	52.158	81.17	0.00	7.77E-08
17:24	54.158	81.17	0.00	8.07E-08
17:26	56.158	81.17	0.00	8.37E-08
17:28	58.158	81.17	0.00	8.67E-08
17:30	60.158	81.17	0.00	8.96E-08
17:32	62.247	81.17	0.00	9.28E-08
17:34	64.135	81.17	0.00	9.56E-08
17:36	66.135	81.17	0.00	9.85E-08
17:38	68.135	81.17	0.00	1.02E-07
17:40	70.135	81.17	0.00	1.05E-07
17:42	72.135	81.17	0.00	1.07E-07
17:44	74.135	81.17	0.00	1.10E-07
17:46	76.135	81.17	0.00	1.13E-07
17:48	78.135	81.17	0.00	1.16E-07
17:50	80.782	81.17	0.00	1.20E-07
17:52	82.182	81.17	0.00	1.22E-07
17:54	84.070	81.17	0.00	1.25E-07
17:56	86.070	81.17	0.00	1.28E-07
17:58	88.070	81.17	0.00	1.31E-07
18:00	90.070	81.17	0.00	1.34E-07
18:02	92.070	81.17	0.00	1.37E-07
18:04	94.070	81.17	0.00	1.40E-07
18:06	96.070	81.17	0.00	1.43E-07
18:08	98.115	81.17	0.00	1.46E-07
18:10	100.120	81.17	0.00	1.49E-07
18:30	120.280	81.17	0.00	1.79E-07
18:50	140.220	81.17	0.00	2.09E-07
19:10	160.220	81.15	0.02	2.39E-07
19:30	180.220	81.15	0.02	2.69E-07
20:10	220.500	81.16	0.01	3.29E-07
20:30	240.270	81.16	0.01	3.58E-07
20:50	260.330	81.16	0.01	3.88E-07
21:10	280.330	81.16	0.01	4.18E-07
21:30	300.230	81.16	0.01	4.47E-07
21:50	320.280	81.16	0.01	4.77E-07
22:10	340.320	81.17	0.00	5.07E-07

22:30	360.300	81.17	0.00	5.37E-07
22:50	380.270	81.17	0.00	5.67E-07
23:10	400.270	81.17	0.00	5.96E-07
23:30	420.270	81.17	0.00	6.26E-07
23:50	440.270	81.17	0.00	6.56E-07
00:10	460.270	81.17	0.00	6.86E-07
00:30	480.270	81.17	0.00	7.16E-07
00:50	500.270	81.18	-0.01	7.45E-07
01:10	520.270	81.18	-0.01	7.75E-07
01:30	540.220	81.18	-0.01	8.05E-07
01:50	560.230	81.18	-0.01	8.35E-07
02:10	580.230	81.18	-0.01	8.65E-07
02:30	600.230	81.19	-0.02	8.94E-07
02:50	620.230	81.19	-0.02	9.24E-07
03:10	640.230	81.19	-0.02	9.54E-07
03:30	660.230	81.19	-0.02	9.84E-07
03:50	680.230	81.19	-0.02	1.01E-06
04:10	700.180	81.19	-0.02	1.04E-06
04:30	720.320	81.19	-0.02	1.07E-06
04:50	740.280	81.19	-0.02	1.10E-06
05:10	760.280	81.19	-0.02	1.13E-06
05:30	780.280	81.19	-0.02	1.16E-06
05:50	800.320	81.20	-0.03	1.19E-06
06:10	820.320	81.19	-0.02	1.22E-06
06:30	840.320	81.20	-0.03	1.25E-06
06:50	860.320	81.20	-0.03	1.28E-06
07:10	880.320	81.20	-0.03	1.31E-06
07:30	900.320	81.20	-0.03	1.34E-06
07:50	920.320	81.20	-0.03	1.37E-06
08:10	940.320	81.21	-0.04	1.40E-06
08:30	960.320	81.21	-0.04	1.43E-06
08:50	980.320	81.21	-0.04	1.46E-06
10:10	1060.500	81.22	-0.05	1.58E-06
11:10	1120.200	81.23	-0.06	1.67E-06
12:10	1180.200	81.23	-0.06	1.76E-06
13:10	1240.200	81.23	-0.06	1.85E-06
14:10	1300.200	81.24	-0.07	1.94E-06
15:10	1360.200	81.24	-0.07	2.03E-06
16:10	1420.200	81.24	-0.07	2.12E-06
17:10	1480.200	81.24	-0.07	2.21E-06
18:10	1540.100	81.25	-0.08	2.29E-06
19:10	1600.300	81.25	-0.08	2.38E-06
20:10	1660.300	81.25	-0.08	2.47E-06
21:10	1720.300	81.26	-0.09	2.56E-06
22:10	1780.200	81.26	-0.09	2.65E-06
23:10	1840.200	81.27	-0.10	2.74E-06
00:10	1900.200	81.27	-0.10	2.83E-06
01:10	1960.300	81.28	-0.11	2.92E-06
02:10	2020.300	81.28	-0.11	3.01E-06
03:10	2080.200	81.29	-0.12	3.10E-06
04:10	2140.200	81.29	-0.12	3.19E-06
05:10	2200.200	81.28	-0.11	3.28E-06
06:10	2260.200	81.28	-0.11	3.37E-06
07:10	2320.200	81.28	-0.11	3.46E-06
08:10	2380.300	81.27	-0.10	3.55E-06
09:10	2440.200	81.26	-0.09	3.64E-06

10:10	2500.300	81.26	-0.09	3.73E-06
11:10	2560.300	81.26	-0.09	3.82E-06
12:10	2620.300	81.25	-0.08	3.90E-06
13:10	2680.300	81.23	-0.06	3.99E-06
14:10	2740.200	81.23	-0.06	4.08E-06
15:10	2800.200	81.23	-0.06	4.17E-06
16:10	2860.300	81.23	-0.06	4.26E-06
17:10	2920.200	81.23	-0.06	4.35E-06
18:10	2980.200	81.23	-0.06	4.44E-06
19:10	3040.200	81.23	-0.06	4.53E-06
20:10	3100.200	81.23	-0.06	4.62E-06
21:10	3160.200	81.24	-0.07	4.71E-06
22:10	3220.200	81.24	-0.07	4.80E-06
23:10	3280.200	81.24	-0.07	4.89E-06
00:10	3340.200	81.24	-0.07	4.98E-06
01:10	3400.200	81.24	-0.07	5.07E-06
02:10	3460.200	81.24	-0.07	5.16E-06
03:10	3520.200	81.24	-0.07	5.25E-06
04:10	3580.200	81.24	-0.07	5.33E-06
05:10	3640.200	81.25	-0.08	5.42E-06
06:10	3700.200	81.25	-0.08	5.51E-06
07:10	3760.400	81.25	-0.08	5.60E-06
08:10	3820.200	81.25	-0.08	5.69E-06
09:10	3880.200	81.25	-0.08	5.78E-06
10:10	3940.200	81.25	-0.08	5.87E-06
11:10	4000.200	81.26	-0.09	5.96E-06
12:10	4060.300	81.26	-0.09	6.05E-06
13:10	4120.200	81.26	-0.09	6.14E-06
14:10	4180.200	81.27	-0.10	6.23E-06
15:10	4240.300	81.27	-0.10	6.32E-06
16:10	4300.200	81.27	-0.10	6.41E-06
16:59	4349.700	81.27	-0.10	6.48E-06

PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 7 (INPUT 3)  
 WELL MATERIAL: PVC  
 RADIUS: 682.670 FEET  
 STARTING WATER LEVEL: 81.170 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 81.270 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r2	RESIDUAL DRAWDOWN (FEET)	t/t'
0.084	81.28	-0.01	1.25E-10	0.11	5.18E+04
0.167	81.27	0.00	2.49E-10	0.10	2.60E+04
0.251	81.27	0.00	3.74E-10	0.10	1.73E+04
0.334	81.27	0.00	4.98E-10	0.10	1.30E+04
0.417	81.27	0.00	6.21E-10	0.10	1.04E+04
0.501	81.28	-0.01	7.47E-10	0.11	8.68E+03
0.584	81.28	-0.01	8.70E-10	0.11	7.45E+03
0.667	81.28	-0.01	9.94E-10	0.11	6.52E+03
0.751	81.27	0.00	1.12E-09	0.10	5.79E+03
0.834	81.27	0.00	1.24E-09	0.10	5.22E+03
0.917	81.27	0.00	1.37E-09	0.10	4.74E+03
1.001	81.27	0.00	1.49E-09	0.10	4.35E+03
1.389	81.27	0.00	2.07E-09	0.10	3.13E+03
1.723	81.27	0.00	2.57E-09	0.10	2.53E+03
2.056	81.27	0.00	3.06E-09	0.10	2.12E+03
2.389	81.27	0.00	3.56E-09	0.10	1.82E+03
2.723	81.27	0.00	4.06E-09	0.10	1.60E+03
3.056	81.27	0.00	4.55E-09	0.10	1.42E+03
3.389	81.27	0.00	5.05E-09	0.10	1.28E+03
3.723	81.27	0.00	5.55E-09	0.10	1.17E+03
4.056	81.28	-0.01	6.04E-09	0.11	1.07E+03
4.389	81.27	0.00	6.54E-09	0.10	9.92E+02
4.723	81.27	0.00	7.04E-09	0.10	9.22E+02
5.056	81.27	0.00	7.53E-09	0.10	8.61E+02
5.389	81.27	0.00	8.03E-09	0.10	8.08E+02
5.723	81.27	0.00	8.53E-09	0.10	7.61E+02
6.056	81.27	0.00	9.02E-09	0.10	7.19E+02
6.389	81.27	0.00	9.52E-09	0.10	6.82E+02
6.723	81.27	0.00	1.00E-08	0.10	6.48E+02
7.056	81.27	0.00	1.05E-08	0.10	6.17E+02
7.389	81.27	0.00	1.10E-08	0.10	5.90E+02
7.723	81.27	0.00	1.15E-08	0.10	5.64E+02
8.056	81.27	0.00	1.20E-08	0.10	5.41E+02
8.389	81.27	0.00	1.25E-08	0.10	5.20E+02

PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: RE1 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: RE1 7 (INPUT 3)  
 WELL MATERIAL: PVC  
 RADIUS: 682.670 FEET  
 STARTING WATER LEVEL: 81.170 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 81.270 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r2	RESIDUAL DRAWDOWN (FEET)	t/t'
8.723	81.27	0.00	1.30E-08	0.10	5.00E+02
9.056	81.27	0.00	1.35E-08	0.10	4.81E+02
9.389	81.27	0.00	1.40E-08	0.10	4.64E+02
9.723	81.27	0.00	1.45E-08	0.10	4.48E+02
10.056	81.27	0.00	1.50E-08	0.10	4.34E+02
12.165	81.27	0.00	1.81E-08	0.10	3.59E+02
14.495	81.27	0.00	2.16E-08	0.10	3.01E+02
16.165	81.27	0.00	2.41E-08	0.10	2.70E+02
18.165	81.27	0.00	2.71E-08	0.10	2.40E+02
20.203	81.27	0.00	3.01E-08	0.10	2.16E+02
22.203	81.27	0.00	3.31E-08	0.10	1.97E+02
24.225	81.27	0.00	3.61E-08	0.10	1.81E+02
26.225	81.28	-0.01	3.91E-08	0.11	1.67E+02
28.225	81.27	0.00	4.21E-08	0.10	1.55E+02
30.225	81.27	0.00	4.50E-08	0.10	1.45E+02
32.225	81.27	0.00	4.80E-08	0.10	1.36E+02
34.225	81.28	-0.01	5.10E-08	0.11	1.28E+02
36.225	81.27	0.00	5.40E-08	0.10	1.21E+02
38.225	81.27	0.00	5.70E-08	0.10	1.15E+02
40.225	81.27	0.00	5.99E-08	0.10	1.09E+02
42.225	81.27	0.00	6.29E-08	0.10	1.04E+02
44.225	81.27	0.00	6.59E-08	0.10	9.94E+01
46.225	81.27	0.00	6.89E-08	0.10	9.51E+01
48.225	81.27	0.00	7.19E-08	0.10	9.12E+01
50.225	81.27	0.00	7.48E-08	0.10	8.76E+01
52.225	81.27	0.00	7.78E-08	0.10	8.43E+01
54.225	81.27	0.00	8.08E-08	0.10	8.12E+01
56.225	81.27	0.00	8.38E-08	0.10	7.84E+01
58.225	81.27	0.00	8.68E-08	0.10	7.57E+01
60.225	81.27	0.00	8.97E-08	0.10	7.32E+01
62.225	81.27	0.00	9.27E-08	0.10	7.09E+01
64.225	81.27	0.00	9.57E-08	0.10	6.87E+01
66.225	81.27	0.00	9.87E-08	0.10	6.67E+01
68.225	81.27	0.00	1.02E-07	0.10	6.48E+01



PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 7 (INPUT 3)  
 WELL MATERIAL: PVC  
 RADIUS: 682.670 FEET  
 STARTING WATER LEVEL: 81.170 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 81.270 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r2	RESIDUAL DRAWDOWN (FEET)	t/t'
70.225	81.27	0.00	1.05E-07	0.10	6.29E+01
72.225	81.27	0.00	1.08E-07	0.10	6.12E+01
74.225	81.27	0.00	1.11E-07	0.10	5.96E+01
76.225	81.27	0.00	1.14E-07	0.10	5.81E+01
78.225	81.27	0.00	1.17E-07	0.10	5.66E+01
80.225	81.27	0.00	1.20E-07	0.10	5.52E+01
82.225	81.27	0.00	1.23E-07	0.10	5.39E+01
84.225	81.27	0.00	1.26E-07	0.10	5.26E+01
86.225	81.27	0.00	1.28E-07	0.10	5.14E+01
88.225	81.27	0.00	1.31E-07	0.10	5.03E+01
90.225	*	*	1.34E-07	*	4.92E+01
92.225	*	*	1.37E-07	*	4.82E+01
94.225	*	*	1.40E-07	*	4.72E+01
96.225	*	*	1.43E-07	*	4.62E+01
98.225	*	*	1.46E-07	*	4.53E+01
100.230	*	*	1.49E-07	*	4.44E+01
120.230	*	*	1.79E-07	*	3.72E+01
140.230	*	*	2.09E-07	*	3.20E+01
160.230	*	*	2.39E-07	*	2.81E+01
180.220	*	*	2.69E-07	*	2.51E+01
200.220	*	*	2.98E-07	*	2.27E+01
220.220	91.02	-9.75	3.28E-07	9.85	2.08E+01
240.220	91.03	-9.76	3.58E-07	9.86	1.91E+01
260.220	91.03	-9.76	3.88E-07	9.86	1.77E+01
280.120	91.03	-9.76	4.17E-07	9.86	1.65E+01
300.120	91.03	-9.76	4.47E-07	9.86	1.55E+01
320.120	91.03	-9.76	4.77E-07	9.86	1.46E+01
340.200	91.03	-9.76	5.07E-07	9.86	1.38E+01
360.220	91.03	-9.76	5.37E-07	9.86	1.31E+01
380.220	91.03	-9.76	5.67E-07	9.86	1.24E+01
400.220	91.03	-9.76	5.96E-07	9.86	1.19E+01
420.220	91.03	-9.76	6.26E-07	9.86	1.14E+01
440.220	91.03	-9.76	6.56E-07	9.86	1.09E+01
460.220	91.03	-9.76	6.86E-07	9.86	1.05E+01

PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 3-4 RUN #2  
 TEST DATE: 8/21/86  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 7 (INPUT 3)  
 WELL MATERIAL: PVC  
 RADIUS: 682.670 FEET  
 STARTING WATER LEVEL: 81.170 FEET  
 PUMPING TIME: 4349.7 MIN  
 STOPPING WATER LEVEL: 81.270 FEET

ELAPSED TIME (MIN)	WATER LEVEL (FEET)	HEAD RECOVERY (FEET)	t/r2	RESIDUAL DRAWDOWN (FEET)	t/t'
480.220	91.03	-9.76	7.16E-07	9.86	1.01E+01
500.220	91.03	-9.76	7.45E-07	9.86	9.70E+00
520.220	91.03	-9.76	7.75E-07	9.86	9.36E+00
540.220	91.03	-9.76	8.05E-07	9.86	9.05E+00
560.200	91.03	-9.76	8.35E-07	9.86	8.76E+00
580.200	91.03	-9.76	8.65E-07	9.86	8.50E+00
600.200	91.03	-9.76	8.94E-07	9.86	8.25E+00
620.200	91.03	-9.76	9.24E-07	9.86	8.01E+00
640.200	91.03	-9.76	9.54E-07	9.86	7.79E+00
660.200	91.03	-9.76	9.84E-07	9.86	7.59E+00
680.220	91.03	-9.76	1.01E-06	9.86	7.39E+00
700.220	91.03	-9.76	1.04E-06	9.86	7.21E+00
720.220	91.03	-9.76	1.07E-06	9.86	7.04E+00
740.220	91.03	-9.76	1.10E-06	9.86	6.88E+00
760.170	91.03	-9.76	1.13E-06	9.86	6.72E+00
780.080	91.03	-9.76	1.16E-06	9.86	6.58E+00
800.080	91.03	-9.76	1.19E-06	9.86	6.44E+00
820.080	91.03	-9.76	1.22E-06	9.86	6.30E+00
840.080	91.03	-9.76	1.25E-06	9.86	6.18E+00
860.070	91.03	-9.76	1.28E-06	9.86	6.06E+00
880.170	91.03	-9.76	1.31E-06	9.86	5.94E+00
900.170	91.03	-9.76	1.34E-06	9.86	5.83E+00
920.170	91.02	-9.75	1.37E-06	9.85	5.73E+00
940.130	90.96	-9.69	1.40E-06	9.79	5.63E+00
954.580	91.03	-9.76	1.42E-06	9.86	5.56E+00

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 3-4 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 10-1 INPUT 4  
 RADIUS: 784.360 FEET  
 START DATE : 21-Aug-86  
 START TIME : 16:30  
 WATER START LEVEL: 81.18 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
16:30	0.000	81.18	0.00	0.00E+00
16:30	0.084	81.19	-0.01	9.48E-11
16:30	0.167	81.19	-0.01	1.89E-10
16:30	0.251	81.19	-0.01	2.83E-10
16:30	0.334	81.19	-0.01	3.77E-10
16:30	0.417	81.19	-0.01	4.71E-10
16:30	0.501	81.19	-0.01	5.66E-10
16:30	0.584	81.19	-0.01	6.59E-10
16:30	0.667	81.19	-0.01	7.53E-10
16:30	0.751	81.18	0.00	8.48E-10
16:30	0.834	81.19	-0.01	9.41E-10
16:30	0.917	81.19	-0.01	1.04E-09
16:31	1.001	81.19	-0.01	1.13E-09
16:31	1.391	81.19	-0.01	1.57E-09
16:31	1.724	81.18	0.00	1.95E-09
16:32	2.058	81.18	0.00	2.32E-09
16:32	2.391	81.18	0.00	2.70E-09
16:32	2.724	81.18	0.00	3.07E-09
16:33	3.058	81.18	0.00	3.45E-09
16:33	3.391	81.17	0.01	3.83E-09
16:33	3.724	81.17	0.01	4.20E-09
16:34	4.058	81.17	0.01	4.58E-09
16:34	4.391	81.17	0.01	4.96E-09
16:34	4.724	81.18	0.00	5.33E-09
16:35	5.058	81.17	0.01	5.71E-09
16:35	5.391	81.17	0.01	6.09E-09
16:35	5.724	81.18	0.00	6.46E-09
16:36	6.058	81.18	0.00	6.84E-09
16:36	6.391	81.18	0.00	7.21E-09
16:36	6.724	81.18	0.00	7.59E-09
16:37	7.058	81.17	0.01	7.97E-09
16:37	7.391	81.17	0.01	8.34E-09
16:37	7.724	81.18	0.00	8.72E-09
16:38	8.058	81.17	0.01	9.10E-09
16:38	8.391	81.17	0.01	9.47E-09
16:38	8.724	81.17	0.01	9.85E-09
16:39	9.058	81.17	0.01	1.02E-08
16:39	9.391	81.17	0.01	1.06E-08
16:39	9.724	81.17	0.01	1.10E-08
16:40	10.058	81.17	0.01	1.14E-08

16:42	12.153	81.18	0.00	1.37E-08
16:44	14.153	81.17	0.01	1.60E-08
16:46	16.423	81.17	0.01	1.85E-08
16:48	18.762	81.17	0.01	2.12E-08
16:50	20.193	81.18	0.00	2.28E-08
16:52	22.193	81.17	0.01	2.51E-08
16:54	24.193	81.17	0.01	2.73E-08
16:56	26.193	81.17	0.01	2.96E-08
16:58	28.193	81.17	0.01	3.18E-08
17:00	30.193	81.18	0.00	3.41E-08
17:02	32.193	81.17	0.01	3.63E-08
17:04	34.158	81.18	0.00	3.86E-08
17:06	36.158	81.17	0.01	4.08E-08
17:08	38.158	81.18	0.00	4.31E-08
17:10	40.158	81.17	0.01	4.53E-08
17:12	42.158	81.17	0.01	4.76E-08
17:14	44.158	81.18	0.00	4.98E-08
17:16	46.158	81.17	0.01	5.21E-08
17:18	48.158	81.17	0.01	5.44E-08
17:20	50.158	81.17	0.01	5.66E-08
17:22	52.158	81.17	0.01	5.89E-08
17:24	54.158	81.17	0.01	6.11E-08
17:26	56.158	81.17	0.01	6.34E-08
17:28	58.158	81.16	0.02	6.56E-08
17:30	60.158	81.17	0.01	6.79E-08
17:32	62.247	81.17	0.01	7.03E-08
17:34	64.135	81.17	0.01	7.24E-08
17:36	66.135	81.18	0.00	7.47E-08
17:38	68.135	81.17	0.01	7.69E-08
17:40	70.135	81.17	0.01	7.92E-08
17:42	72.135	81.18	0.00	8.14E-08
17:44	74.135	81.17	0.01	8.37E-08
17:46	76.135	81.17	0.01	8.59E-08
17:48	78.135	81.18	0.00	8.82E-08
17:50	80.782	81.19	-0.01	9.12E-08
17:52	82.182	81.18	0.00	9.28E-08
17:54	84.070	81.18	0.00	9.49E-08
17:56	86.070	81.18	0.00	9.72E-08
17:58	88.070	81.19	-0.01	9.94E-08
18:00	90.070	81.19	-0.01	1.02E-07
18:02	92.070	81.17	0.01	1.04E-07
18:04	94.070	81.19	-0.01	1.06E-07
18:06	96.070	81.19	-0.01	1.08E-07
18:08	98.115	81.19	-0.01	1.11E-07
18:10	100.120	81.19	-0.01	1.13E-07
18:30	120.280	81.20	-0.02	1.36E-07
18:50	140.220	81.22	-0.04	1.58E-07
19:10	160.220	81.22	-0.04	1.81E-07
19:30	180.220	81.23	-0.05	2.03E-07
20:10	220.500	81.26	-0.08	2.49E-07
20:30	240.270	81.28	-0.10	2.71E-07
20:50	260.330	81.29	-0.11	2.94E-07
21:10	280.330	81.30	-0.12	3.16E-07
21:30	300.230	81.32	-0.14	3.39E-07
21:50	320.280	81.31	-0.13	3.62E-07
22:10	340.320	81.31	-0.13	3.84E-07

22:30	360.300	81.32	-0.14	4.07E-07
22:50	380.270	81.32	-0.14	4.29E-07
23:10	400.270	81.33	-0.15	4.52E-07
23:30	420.270	81.33	-0.15	4.74E-07
23:50	440.270	81.33	-0.15	4.97E-07
00:10	460.270	81.34	-0.16	5.20E-07
00:30	480.270	81.34	-0.16	5.42E-07
00:50	500.270	81.35	-0.17	5.65E-07
01:10	520.270	81.35	-0.17	5.87E-07
01:30	540.220	81.36	-0.18	6.10E-07
01:50	560.230	81.36	-0.18	6.32E-07
02:10	580.230	81.36	-0.18	6.55E-07
02:30	600.230	81.36	-0.18	6.78E-07
02:50	620.230	81.37	-0.19	7.00E-07
03:10	640.230	81.38	-0.20	7.23E-07
03:30	660.230	81.38	-0.20	7.45E-07
03:50	680.230	81.38	-0.20	7.68E-07
04:10	700.180	81.38	-0.20	7.90E-07
04:30	720.320	81.40	-0.22	8.13E-07
04:50	740.280	81.39	-0.21	8.36E-07
05:10	760.280	81.39	-0.21	8.58E-07
05:30	780.280	81.40	-0.22	8.81E-07
05:50	800.320	81.40	-0.22	9.03E-07
06:10	820.320	81.40	-0.22	9.26E-07
06:30	840.320	81.40	-0.22	9.49E-07
06:50	860.320	81.41	-0.23	9.71E-07
07:10	880.320	81.42	-0.24	9.94E-07
07:30	900.320	81.42	-0.24	1.02E-06
07:50	920.320	81.42	-0.24	1.04E-06
08:10	940.320	81.43	-0.25	1.06E-06
08:30	960.320	81.43	-0.25	1.08E-06
08:50	980.320	81.44	-0.26	1.11E-06
10:10	1060.500	81.45	-0.27	1.20E-06
11:10	1120.200	81.46	-0.28	1.26E-06
12:10	1180.200	81.47	-0.29	1.33E-06
13:10	1240.200	81.47	-0.29	1.40E-06
14:10	1300.200	81.49	-0.31	1.47E-06
15:10	1360.200	81.49	-0.31	1.54E-06
16:10	1420.200	81.50	-0.32	1.60E-06
17:10	1480.200	81.51	-0.33	1.67E-06
18:10	1540.100	81.51	-0.33	1.74E-06
19:10	1600.300	81.52	-0.34	1.81E-06
20:10	1660.300	81.52	-0.34	1.87E-06
21:10	1720.300	81.54	-0.36	1.94E-06
22:10	1780.200	81.55	-0.37	2.01E-06
23:10	1840.200	81.56	-0.38	2.08E-06
00:10	1900.200	81.57	-0.39	2.14E-06
01:10	1960.300	81.58	-0.40	2.21E-06
02:10	2020.300	81.59	-0.41	2.28E-06
03:10	2080.200	81.60	-0.42	2.35E-06
04:10	2140.200	81.61	-0.43	2.42E-06
05:10	2200.200	81.62	-0.44	2.48E-06
06:10	2260.200	81.63	-0.45	2.55E-06
07:10	2320.200	81.64	-0.46	2.62E-06
08:10	2380.300	81.65	-0.47	2.69E-06
09:10	2440.200	81.67	-0.49	2.75E-06

10:10	2500.300	81.68	-0.50	2.82E-06
11:10	2560.300	81.68	-0.50	2.89E-06
12:10	2620.300	81.69	-0.51	2.96E-06
13:10	2680.300	81.67	-0.49	3.03E-06
14:10	2740.200	81.66	-0.48	3.09E-06
15:10	2800.200	81.66	-0.48	3.16E-06
16:10	2860.300	81.64	-0.46	3.23E-06
17:10	2920.200	81.64	-0.46	3.30E-06
18:10	2980.200	81.62	-0.44	3.36E-06
19:10	3040.200	81.61	-0.43	3.43E-06
20:10	3100.200	81.60	-0.42	3.50E-06
21:10	3160.200	81.58	-0.40	3.57E-06
22:10	3220.200	81.58	-0.40	3.63E-06
23:10	3280.200	81.57	-0.39	3.70E-06
00:10	3340.200	81.57	-0.39	3.77E-06
01:10	3400.200	81.57	-0.39	3.84E-06
02:10	3460.200	81.57	-0.39	3.91E-06
03:10	3520.200	81.57	-0.39	3.97E-06
04:10	3580.200	81.58	-0.40	4.04E-06
05:10	3640.200	81.58	-0.40	4.11E-06
06:10	3700.200	81.59	-0.41	4.18E-06
07:10	3760.400	81.59	-0.41	4.24E-06
08:10	3820.200	81.59	-0.41	4.31E-06
09:10	3880.200	81.60	-0.42	4.38E-06
10:10	3940.200	81.63	-0.45	4.45E-06
11:10	4000.200	81.65	-0.47	4.52E-06
12:10	4060.300	81.65	-0.47	4.58E-06
13:10	4120.200	81.68	-0.50	4.65E-06
14:10	4180.200	81.69	-0.51	4.72E-06
15:10	4240.300	81.72	-0.54	4.79E-06
16:10	4300.200	81.75	-0.57	4.85E-06
16:59	4349.700	81.75	-0.57	4.91E-06

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 3-4 Run #2  
 TEST TYPE : RECOVERY  
 WELL NUMBER : REI 10-1 INPUT 4  
 RADIUS: 784.360 FEET  
 START DATE : 21-Aug-86  
 START TIME : 16:59  
 WATER START LEVEL: 81.18 FEET  
 WATER STOP LEVEL: 81.75 FEET  
 TOTAL PUMPING TIME: 4349.7 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)	t/r2	t/t'
16:59	0.084	81.75	0.00	0.57	9.48E-11	5.18E+04
16:59	0.167	81.75	0.00	0.57	1.89E-10	2.60E+04
16:59	0.251	81.75	0.00	0.57	2.83E-10	1.73E+04
16:59	0.334	81.75	0.00	0.57	3.77E-10	1.30E+04
16:59	0.417	81.75	0.00	0.57	4.71E-10	1.04E+04
16:59	0.501	81.75	0.00	0.57	5.66E-10	8.68E+03
16:59	0.584	81.75	0.00	0.57	6.59E-10	7.45E+03
16:59	0.667	81.75	0.00	0.57	7.53E-10	6.52E+03
16:59	0.751	81.76	-0.01	0.58	8.48E-10	5.79E+03
16:59	0.834	81.76	-0.01	0.58	9.41E-10	5.22E+03
16:59	0.917	81.76	-0.01	0.58	1.04E-09	4.74E+03
17:00	1.001	81.76	-0.01	0.58	1.13E-09	4.35E+03
17:00	1.389	81.75	0.00	0.57	1.57E-09	3.13E+03
17:00	1.723	81.75	0.00	0.57	1.94E-09	2.53E+03
17:01	2.056	81.75	0.00	0.57	2.32E-09	2.12E+03
17:01	2.389	81.75	0.00	0.57	2.70E-09	1.82E+03
17:01	2.723	81.75	0.00	0.57	3.07E-09	1.60E+03
17:02	3.056	81.75	0.00	0.57	3.45E-09	1.42E+03
17:02	3.389	81.75	0.00	0.57	3.83E-09	1.28E+03
17:02	3.723	81.75	0.00	0.57	4.20E-09	1.17E+03
17:03	4.056	81.75	0.00	0.57	4.58E-09	1.07E+03
17:03	4.389	81.74	0.01	0.56	4.95E-09	9.92E+02
17:03	4.723	81.75	0.00	0.57	5.33E-09	9.22E+02
17:04	5.056	81.76	-0.01	0.58	5.71E-09	8.61E+02
17:04	5.389	81.75	0.00	0.57	6.08E-09	8.08E+02
17:04	5.723	81.75	0.00	0.57	6.46E-09	7.61E+02
17:05	6.056	81.75	0.00	0.57	6.84E-09	7.19E+02
17:05	6.389	81.75	0.00	0.57	7.21E-09	6.82E+02
17:05	6.723	81.75	0.00	0.57	7.59E-09	6.48E+02
17:06	7.056	81.75	0.00	0.57	7.96E-09	6.17E+02
17:06	7.389	81.75	0.00	0.57	8.34E-09	5.90E+02
17:06	7.723	81.75	0.00	0.57	8.72E-09	5.64E+02
17:07	8.056	81.75	0.00	0.57	9.09E-09	5.41E+02
17:07	8.389	81.75	0.00	0.57	9.47E-09	5.20E+02
17:07	8.723	81.75	0.00	0.57	9.85E-09	5.00E+02
17:08	9.056	81.75	0.00	0.57	1.02E-08	4.81E+02
17:08	9.389	81.74	0.01	0.56	1.06E-08	4.64E+02
17:08	9.723	81.75	0.00	0.57	1.10E-08	4.48E+02

17:09	10.056	81.75	0.00	0.57	1.14E-08	4.34E+02
17:11	12.165	81.75	0.00	0.57	1.37E-08	3.59E+02
17:13	14.495	81.75	0.00	0.57	1.64E-08	3.01E+02
17:15	16.165	81.75	0.00	0.57	1.82E-08	2.70E+02
17:17	18.165	81.74	0.01	0.56	2.05E-08	2.40E+02
17:19	20.203	81.75	0.00	0.57	2.28E-08	2.16E+02
17:21	22.203	81.75	0.00	0.57	2.51E-08	1.97E+02
17:23	24.225	81.75	0.00	0.57	2.73E-08	1.81E+02
17:25	26.225	81.76	-0.01	0.58	2.96E-08	1.67E+02
17:27	28.225	81.75	0.00	0.57	3.19E-08	1.55E+02
17:29	30.225	81.75	0.00	0.57	3.41E-08	1.45E+02
17:31	32.225	81.76	-0.01	0.58	3.64E-08	1.36E+02
17:33	34.225	81.76	-0.01	0.58	3.86E-08	1.28E+02
17:35	36.225	81.76	-0.01	0.58	4.09E-08	1.21E+02
17:37	38.225	81.76	-0.01	0.58	4.31E-08	1.15E+02
17:39	40.225	81.76	-0.01	0.58	4.54E-08	1.09E+02
17:41	42.225	81.75	0.00	0.57	4.77E-08	1.04E+02
17:43	44.225	81.75	0.00	0.57	4.99E-08	9.94E+01
17:45	46.225	81.75	0.00	0.57	5.22E-08	9.51E+01
17:47	48.225	81.75	0.00	0.57	5.44E-08	9.12E+01
17:49	50.225	81.74	0.01	0.56	5.67E-08	8.76E+01
17:51	52.225	81.74	0.01	0.56	5.90E-08	8.43E+01
17:53	54.225	81.75	0.00	0.57	6.12E-08	8.12E+01
17:55	56.225	81.75	0.00	0.57	6.35E-08	7.84E+01
17:57	58.225	81.74	0.01	0.56	6.57E-08	7.57E+01
17:59	60.225	81.74	0.01	0.56	6.80E-08	7.32E+01
18:01	62.225	81.74	0.01	0.56	7.02E-08	7.09E+01
18:03	64.225	81.74	0.01	0.56	7.25E-08	6.87E+01
18:05	66.225	81.73	0.02	0.55	7.48E-08	6.67E+01
18:07	68.225	81.74	0.01	0.56	7.70E-08	6.48E+01
18:09	70.225	81.74	0.01	0.56	7.93E-08	6.29E+01
18:11	72.225	81.73	0.02	0.55	8.15E-08	6.12E+01
18:13	74.225	81.73	0.02	0.55	8.38E-08	5.96E+01
18:15	76.225	81.73	0.02	0.55	8.60E-08	5.81E+01
18:17	78.225	81.73	0.02	0.55	8.83E-08	5.66E+01
18:19	80.225	81.72	0.03	0.54	9.06E-08	5.52E+01
18:21	82.225	81.72	0.03	0.54	9.28E-08	5.39E+01
18:23	84.225	81.72	0.03	0.54	9.51E-08	5.26E+01
18:25	86.225	81.72	0.03	0.54	9.73E-08	5.14E+01
18:27	88.225	81.72	0.03	0.54	9.96E-08	5.03E+01
18:29	90.225	81.72	0.03	0.54	1.02E-07	4.92E+01
18:31	92.225	81.72	0.03	0.54	1.04E-07	4.82E+01
18:33	94.225	81.72	0.03	0.54	1.06E-07	4.72E+01
18:35	96.225	81.72	0.03	0.54	1.09E-07	4.62E+01
18:37	98.225	81.72	0.03	0.54	1.11E-07	4.53E+01
18:39	100.230	81.71	0.04	0.53	1.13E-07	4.44E+01
18:59	120.230	81.71	0.04	0.53	1.36E-07	3.72E+01
19:19	140.230	81.70	0.05	0.52	1.58E-07	3.20E+01
19:39	160.230	81.67	0.08	0.49	1.81E-07	2.81E+01
19:59	180.220	81.66	0.09	0.48	2.03E-07	2.51E+01
20:19	200.220	81.64	0.11	0.46	2.26E-07	2.27E+01
20:39	220.220	81.63	0.12	0.45	2.49E-07	2.08E+01
20:59	240.220	81.61	0.14	0.43	2.71E-07	1.91E+01
21:19	260.220	81.60	0.15	0.42	2.94E-07	1.77E+01
21:39	280.120	81.59	0.16	0.41	3.16E-07	1.65E+01
21:59	300.120	81.58	0.17	0.40	3.39E-07	1.55E+01



22:19	320.120	81.56	0.19	0.38	3.61E-07	1.46E+01
22:39	340.200	81.55	0.20	0.37	3.84E-07	1.38E+01
22:59	360.220	81.54	0.21	0.36	4.07E-07	1.31E+01
23:19	380.220	81.53	0.22	0.35	4.29E-07	1.24E+01
23:39	400.220	81.51	0.24	0.33	4.52E-07	1.19E+01
23:59	420.220	81.50	0.25	0.32	4.74E-07	1.14E+01
00:19	440.220	81.50	0.25	0.32	4.97E-07	1.09E+01
00:39	460.220	81.49	0.26	0.31	5.19E-07	1.05E+01
00:59	480.220	81.48	0.27	0.30	5.42E-07	1.01E+01
01:19	500.220	81.47	0.28	0.29	5.65E-07	9.70E+00
01:39	520.220	81.46	0.29	0.28	5.87E-07	9.36E+00
01:59	540.220	81.45	0.30	0.27	6.10E-07	9.05E+00
02:19	560.200	81.44	0.31	0.26	6.32E-07	8.76E+00
02:39	580.200	81.43	0.32	0.25	6.55E-07	8.50E+00
02:59	600.200	81.42	0.33	0.24	6.77E-07	8.25E+00
03:19	620.200	81.42	0.33	0.24	7.00E-07	8.01E+00
03:39	640.200	81.41	0.34	0.23	7.23E-07	7.79E+00
03:59	660.220	81.39	0.36	0.21	7.45E-07	7.59E+00
04:19	680.220	81.39	0.36	0.21	7.68E-07	7.39E+00
04:39	700.220	81.38	0.37	0.20	7.90E-07	7.21E+00
04:59	720.220	81.38	0.37	0.20	8.13E-07	7.04E+00
05:19	740.220	81.37	0.38	0.19	8.36E-07	6.88E+00
05:39	760.170	81.36	0.39	0.18	8.58E-07	6.72E+00
05:59	780.080	81.36	0.39	0.18	8.81E-07	6.58E+00
06:19	800.080	81.35	0.40	0.17	9.03E-07	6.44E+00
06:39	820.080	81.35	0.40	0.17	9.26E-07	6.30E+00
06:59	840.080	81.35	0.40	0.17	9.48E-07	6.18E+00
07:19	860.070	81.34	0.41	0.16	9.71E-07	6.06E+00
07:39	880.170	81.34	0.41	0.16	9.94E-07	5.94E+00
07:59	900.170	81.33	0.42	0.15	1.02E-06	5.83E+00
08:19	920.170	81.34	0.41	0.16	1.04E-06	5.73E+00
08:39	940.130	81.33	0.42	0.15	1.06E-06	5.63E+00
08:53	954.580	81.33	0.42	0.15	1.08E-06	5.56E+00

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 3-4 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : REI 3-1 INPUT 5  
RADIUS: NOT AVAILABLE  
START DATE : 21-Aug-86  
START TIME : 16:30  
WATER START LEVEL: 6.29 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
16:30	0.000	6.29	0.00
16:30	0.084	6.29	0.00
16:30	0.167	6.29	0.00
16:30	0.251	6.29	0.00
16:30	0.334	6.29	0.00
16:30	0.417	6.29	0.00
16:30	0.501	6.29	0.00
16:30	0.584	6.29	0.00
16:30	0.667	6.30	-0.01
16:30	0.751	6.30	-0.01
16:30	0.834	6.30	-0.01
16:30	0.917	6.29	0.00
16:31	1.001	6.29	0.00
16:31	1.391	6.29	0.00
16:31	1.724	6.29	0.00
16:32	2.058	6.29	0.00
16:32	2.391	6.29	0.00
16:32	2.724	6.29	0.00
16:33	3.058	6.29	0.00
16:33	3.391	6.28	0.01
16:33	3.724	6.28	0.01
16:34	4.058	6.29	0.00
16:34	4.391	6.29	0.00
16:34	4.724	6.29	0.00
16:35	5.058	6.29	0.00
16:35	5.391	6.29	0.00
16:35	5.724	6.28	0.01
16:36	6.058	6.29	0.00
16:36	6.391	6.29	0.00
16:36	6.724	6.29	0.00
16:37	7.058	6.29	0.00
16:37	7.391	6.29	0.00
16:37	7.724	6.29	0.00
16:38	8.058	6.29	0.00
16:38	8.391	6.29	0.00
16:38	8.724	6.30	-0.01
16:39	9.058	6.29	0.00
16:39	9.391	6.29	0.00
16:39	9.724	6.29	0.00
16:40	10.058	6.29	0.00

16:42	12.153	6.29	0.00
16:44	14.153	6.28	0.01
16:46	16.423	6.29	0.00
16:48	18.762	6.29	0.00
16:50	20.193	6.28	0.01
16:52	22.193	6.29	0.00
16:54	24.193	6.28	0.01
16:56	26.193	6.28	0.01
16:58	28.193	6.28	0.01
17:00	30.193	6.30	-0.01
17:02	32.193	6.28	0.01
17:04	34.158	6.28	0.01
17:06	36.158	6.29	0.00
17:08	38.158	6.28	0.01
17:10	40.158	6.27	0.02
17:12	42.158	6.27	0.02
17:14	44.158	6.28	0.01
17:16	46.158	6.28	0.01
17:18	48.158	6.28	0.01
17:20	50.158	6.28	0.01
17:22	52.158	6.27	0.02
17:24	54.158	6.27	0.02
17:26	56.158	6.27	0.02
17:28	58.158	6.27	0.02
17:30	60.158	6.28	0.01
17:32	62.247	6.27	0.02
17:34	64.135	6.27	0.02
17:36	66.135	6.28	0.01
17:38	68.135	6.28	0.01
17:40	70.135	6.27	0.02
17:42	72.135	6.27	0.02
17:44	74.135	6.27	0.02
17:46	76.135	6.27	0.02
17:48	78.135	6.26	0.03
17:50	80.782	6.26	0.03
17:52	82.182	6.26	0.03
17:54	84.070	6.26	0.03
17:56	86.070	6.26	0.03
17:58	88.070	6.26	0.03
18:00	90.070	6.27	0.02
18:02	92.070	6.26	0.03
18:04	94.070	6.27	0.02
18:06	96.070	6.28	0.01
18:08	98.115	6.28	0.01
18:10	100.120	6.27	0.02
18:30	120.280	6.26	0.03
18:50	140.220	6.24	0.05
19:10	160.220	6.25	0.04
19:30	180.220	6.25	0.04
20:10	220.500	6.28	0.01
20:30	240.270	6.28	0.01
20:50	260.330	6.29	0.00
21:10	280.330	6.27	0.02
21:30	300.230	6.27	0.02
21:50	320.280	6.26	0.03
22:10	340.320	6.26	0.03

22:30	360.300	6.26	0.03
22:50	380.270	6.26	0.03
23:10	400.270	6.26	0.03
23:30	420.270	6.26	0.03
23:50	440.270	6.26	0.03
00:10	460.270	6.25	0.04
00:30	480.270	6.25	0.04
00:50	500.270	6.24	0.05
01:10	520.270	6.24	0.05
01:30	540.220	6.25	0.04
01:50	560.230	6.25	0.04
02:10	580.230	6.24	0.05
02:30	600.230	6.24	0.05
02:50	620.230	6.24	0.05
03:10	640.230	6.24	0.05
03:30	660.230	6.24	0.05
03:50	680.230	6.24	0.05
04:10	700.180	6.23	0.06
04:30	720.320	6.23	0.06
04:50	740.280	6.23	0.06
05:10	760.280	6.24	0.05
05:30	780.280	6.24	0.05
05:50	800.320	6.24	0.05
06:10	820.320	6.24	0.05
06:30	840.320	6.24	0.05
06:50	860.320	6.24	0.05
07:10	880.320	6.23	0.06
07:30	900.320	6.23	0.06
07:50	920.320	6.23	0.06
08:10	940.320	6.22	0.07
08:30	960.320	6.22	0.07
08:50	980.320	6.23	0.06
10:10	1060.500	6.23	0.06
11:10	1120.200	6.24	0.05
12:10	1180.200	6.23	0.06
13:10	1240.200	6.24	0.05
14:10	1300.200	6.26	0.03
15:10	1360.200	6.28	0.01
16:10	1420.200	6.27	0.02
17:10	1480.200	6.29	0.00
18:10	1540.100	6.30	-0.01
19:10	1600.300	6.31	-0.02
20:10	1660.300	6.32	-0.03
21:10	1720.300	6.33	-0.04
22:10	1780.200	6.34	-0.05
23:10	1840.200	6.34	-0.05
00:10	1900.200	6.33	-0.04
01:10	1960.300	6.33	-0.04
02:10	2020.300	6.33	-0.04
03:10	2080.200	6.33	-0.04
04:10	2140.200	6.31	-0.02
05:10	2200.200	6.31	-0.02
06:10	2260.200	6.30	-0.01
07:10	2320.200	6.29	0.00
08:10	2380.300	6.29	0.00
09:10	2440.200	6.26	0.03

10:10	2500.300	6.25	0.04
11:10	2560.300	6.25	0.04
12:10	2620.300	6.23	0.06
13:10	2680.300	6.20	0.09
14:10	2740.200	6.18	0.11
15:10	2800.200	6.18	0.11
16:10	2860.300	6.15	0.14
17:10	2920.200	6.14	0.15
18:10	2980.200	6.14	0.15
19:10	3040.200	6.13	0.16
20:10	3100.200	6.12	0.17
21:10	3160.200	6.12	0.17
22:10	3220.200	6.13	0.16
23:10	3280.200	6.13	0.16
00:10	3340.200	6.12	0.17
01:10	3400.200	6.12	0.17
02:10	3460.200	6.11	0.18
03:10	3520.200	6.11	0.18
04:10	3580.200	6.11	0.18
05:10	3640.200	6.11	0.18
06:10	3700.200	6.10	0.19
07:10	3760.400	6.10	0.19
08:10	3820.200	6.10	0.19
09:10	3880.200	6.10	0.19
10:10	3940.200	6.11	0.18
11:10	4000.200	6.12	0.17
12:10	4060.300	6.12	0.17
13:10	4120.200	6.07	0.22
14:10	4180.200	6.13	0.16
15:10	4240.300	6.14	0.15
16:10	4300.200	6.14	0.15
16:59	4349.700	6.17	0.12

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 3-4 Run #2  
 TEST TYPE : RECOVERY  
 WELL NUMBER : REI 3-1 INPUT 5  
 RADIUS: NOT AVAILABLE  
 START DATE : 21-Aug-86  
 START TIME : 16:59  
 WATER START LEVEL: 6.29 FEET  
 WATER STOP LEVEL: 6.17 FEET  
 TOTAL PUMPING TIME: 4349.7 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
16:59	0.084	6.17	0.00	0.12
16:59	0.167	6.17	0.00	0.12
16:59	0.251	6.16	0.01	0.13
16:59	0.334	6.16	0.01	0.13
16:59	0.417	6.16	0.01	0.13
16:59	0.501	6.17	0.00	0.12
16:59	0.584	6.17	0.00	0.12
16:59	0.667	6.17	0.00	0.12
16:59	0.751	6.18	-0.01	0.11
16:59	0.834	6.17	0.00	0.12
16:59	0.917	6.16	0.01	0.13
17:00	1.001	6.17	0.00	0.12
17:00	1.389	6.16	0.01	0.13
17:00	1.723	6.16	0.01	0.13
17:01	2.056	6.16	0.01	0.13
17:01	2.389	6.16	0.01	0.13
17:01	2.723	6.17	0.00	0.12
17:02	3.056	6.17	0.00	0.12
17:02	3.389	6.16	0.01	0.13
17:02	3.723	6.17	0.00	0.12
17:03	4.056	6.17	0.00	0.12
17:03	4.389	6.16	0.01	0.13
17:03	4.723	6.16	0.01	0.13
17:04	5.056	6.17	0.00	0.12
17:04	5.389	6.16	0.01	0.13
17:04	5.723	6.16	0.01	0.13
17:05	6.056	6.16	0.01	0.13
17:05	6.389	6.16	0.01	0.13
17:05	6.723	6.16	0.01	0.13
17:06	7.056	6.16	0.01	0.13
17:06	7.389	6.16	0.01	0.13
17:06	7.723	6.16	0.01	0.13
17:07	8.056	6.17	0.00	0.12
17:07	8.389	6.16	0.01	0.13
17:07	8.723	6.17	0.00	0.12
17:08	9.056	6.16	0.01	0.13
17:08	9.389	6.16	0.01	0.13
17:08	9.723	6.17	0.00	0.12

17:09	10.056	6.16	0.01	0.13
17:11	12.165	6.16	0.01	0.13
17:13	14.495	6.17	0.00	0.12
17:15	16.165	6.16	0.01	0.13
17:17	18.165	6.16	0.01	0.13
17:19	20.203	6.17	0.00	0.12
17:21	22.203	6.16	0.01	0.13
17:23	24.225	6.16	0.01	0.13
17:25	26.225	6.18	-0.01	0.11
17:27	28.225	6.16	0.01	0.13
17:29	30.225	6.16	0.01	0.13
17:31	32.225	6.16	0.01	0.13
17:33	34.225	6.16	0.01	0.13
17:35	36.225	6.16	0.01	0.13
17:37	38.225	6.16	0.01	0.13
17:39	40.225	6.16	0.01	0.13
17:41	42.225	6.16	0.01	0.13
17:43	44.225	6.16	0.01	0.13
17:45	46.225	6.16	0.01	0.13
17:47	48.225	6.16	0.01	0.13
17:49	50.225	6.16	0.01	0.13
17:51	52.225	6.16	0.01	0.13
17:53	54.225	6.16	0.01	0.13
17:55	56.225	6.16	0.01	0.13
17:57	58.225	6.17	0.00	0.12
17:59	60.225	6.16	0.01	0.13
18:01	62.225	6.15	0.02	0.14
18:03	64.225	6.15	0.02	0.14
18:05	66.225	6.15	0.02	0.14
18:07	68.225	6.15	0.02	0.14
18:09	70.225	6.15	0.02	0.14
18:11	72.225	6.15	0.02	0.14
18:13	74.225	6.15	0.02	0.14
18:15	76.225	6.15	0.02	0.14
18:17	78.225	6.15	0.02	0.14
18:19	80.225	6.15	0.02	0.14
18:21	82.225	6.15	0.02	0.14
18:23	84.225	6.15	0.02	0.14
18:25	86.225	6.15	0.02	0.14
18:27	88.225	6.14	0.03	0.15
18:29	90.225	6.14	0.03	0.15
18:31	92.225	6.14	0.03	0.15
18:33	94.225	6.14	0.03	0.15
18:35	96.225	6.14	0.03	0.15
18:37	98.225	6.14	0.03	0.15
18:39	100.230	6.14	0.03	0.15
18:59	120.230	6.13	0.04	0.16
19:19	140.230	6.13	0.04	0.16
19:39	160.230	6.12	0.05	0.17
19:59	180.220	6.12	0.05	0.17
20:19	200.220	6.12	0.05	0.17
20:39	220.220	6.12	0.05	0.17
20:59	240.220	6.12	0.05	0.17
21:19	260.220	15.96	-9.79	9.67
21:39	280.120	15.96	-9.79	9.67
21:59	300.120	15.96	-9.79	9.67

22:19	320.120	15.97	-9.80	9.68
22:39	340.200	15.97	-9.80	9.68
22:59	360.220	15.98	-9.81	9.69
23:19	380.220	15.98	-9.81	9.69
23:39	400.220	15.98	-9.81	9.69
23:59	420.220	15.98	-9.81	9.69
00:19	440.220	15.98	-9.81	9.69
00:39	460.220	15.98	-9.81	9.69
00:59	480.220	15.98	-9.81	9.69
01:19	500.220	15.98	-9.81	9.69
01:39	520.220	15.98	-9.81	9.69
01:59	540.220	15.98	-9.81	9.69
02:19	560.200	15.98	-9.81	9.69
02:39	580.200	15.99	-9.82	9.70
02:59	600.200	15.99	-9.82	9.70
03:19	620.200	15.99	-9.82	9.70
03:39	640.200	15.99	-9.82	9.70
03:59	660.220	15.99	-9.82	9.70
04:19	680.220	15.99	-9.82	9.70
04:39	700.220	16.00	-9.83	9.71
04:59	720.220	16.00	-9.83	9.71
05:19	740.220	16.00	-9.83	9.71
05:39	760.170	16.00	-9.83	9.71
05:59	780.080	15.95	-9.78	9.66
06:19	800.080	15.95	-9.78	9.66
06:39	820.080	15.95	-9.78	9.66
06:59	840.080	15.95	-9.78	9.66
07:19	860.070	15.95	-9.78	9.66
07:39	880.170	15.95	-9.78	9.66
07:59	900.170	15.95	-9.78	9.66
08:19	920.170	15.96	-9.79	9.67
08:39	940.130	15.98	-9.81	9.69
08:53	954.580	15.96	-9.79	9.67



PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 3-4 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : REI 3-2 INPUT 6  
RADIUS: NOT AVAILABLE  
START DATE : 21-Aug-86  
START TIME : 16:30  
WATER START LEVEL: 5.87 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
16:30	0.000	5.87	0.00
16:30	0.084	5.87	0.00
16:30	0.167	5.87	0.00
16:30	0.251	5.87	0.00
16:30	0.334	5.87	0.00
16:30	0.417	5.87	0.00
16:30	0.501	5.87	0.00
16:30	0.584	5.87	0.00
16:30	0.667	5.87	0.00
16:30	0.751	5.87	0.00
16:30	0.834	5.87	0.00
16:30	0.917	5.87	0.00
16:31	1.001	5.87	0.00
16:31	1.391	5.87	0.00
16:31	1.724	5.87	0.00
16:32	2.058	5.87	0.00
16:32	2.391	5.87	0.00
16:32	2.724	5.87	0.00
16:33	3.058	5.87	0.00
16:33	3.391	5.87	0.00
16:33	3.724	5.87	0.00
16:34	4.058	5.87	0.00
16:34	4.391	5.87	0.00
16:34	4.724	5.87	0.00
16:35	5.058	5.87	0.00
16:35	5.391	5.87	0.00
16:35	5.724	5.87	0.00
16:36	6.058	5.87	0.00
16:36	6.391	5.87	0.00
16:36	6.724	5.87	0.00
16:37	7.058	5.87	0.00
16:37	7.391	5.87	0.00
16:37	7.724	5.87	0.00
16:38	8.058	5.87	0.00
16:38	8.391	5.87	0.00
16:38	8.724	5.88	-0.01
16:39	9.058	5.87	0.00
16:39	9.391	5.87	0.00
16:39	9.724	5.87	0.00
16:40	10.058	5.88	-0.01

16:42	12.153	5.87	0.00
16:44	14.153	5.87	0.00
16:46	16.423	5.87	0.00
16:48	18.762	5.87	0.00
16:50	20.193	5.87	0.00
16:52	22.193	5.87	0.00
16:54	24.193	5.87	0.00
16:56	26.193	5.87	0.00
16:58	28.193	5.87	0.00
17:00	30.193	5.88	-0.01
17:02	32.193	5.87	0.00
17:04	34.158	5.88	-0.01
17:06	36.158	5.88	-0.01
17:08	38.158	5.87	0.00
17:10	40.158	5.87	0.00
17:12	42.158	5.87	0.00
17:14	44.158	5.88	-0.01
17:16	46.158	5.88	-0.01
17:18	48.158	5.88	-0.01
17:20	50.158	5.88	-0.01
17:22	52.158	5.87	0.00
17:24	54.158	5.88	-0.01
17:26	56.158	5.87	0.00
17:28	58.158	5.88	-0.01
17:30	60.158	5.88	-0.01
17:32	62.247	5.87	0.00
17:34	64.135	5.88	-0.01
17:36	66.135	5.88	-0.01
17:38	68.135	5.88	-0.01
17:40	70.135	5.88	-0.01
17:42	72.135	5.88	-0.01
17:44	74.135	5.88	-0.01
17:46	76.135	5.88	-0.01
17:48	78.135	5.88	-0.01
17:50	80.782	5.88	-0.01
17:52	82.182	5.87	0.00
17:54	84.070	5.88	-0.01
17:56	86.070	5.88	-0.01
17:58	88.070	5.88	-0.01
18:00	90.070	5.88	-0.01
18:02	92.070	5.88	-0.01
18:04	94.070	5.88	-0.01
18:06	96.070	5.89	-0.02
18:08	98.115	5.89	-0.02
18:10	100.120	5.88	-0.01
18:30	120.280	5.88	-0.01
18:50	140.220	5.87	0.00
19:10	160.220	5.88	-0.01
19:30	180.220	5.88	-0.01
20:10	220.500	5.90	-0.03
20:30	240.270	5.90	-0.03
20:50	260.330	5.90	-0.03
21:10	280.330	5.90	-0.03
21:30	300.230	5.89	-0.02
21:50	320.280	5.89	-0.02
22:10	340.320	5.90	-0.03

22:30	360.300	5.89	-0.02
22:50	380.270	5.89	-0.02
23:10	400.270	5.89	-0.02
23:30	420.270	5.88	-0.01
23:50	440.270	5.88	-0.01
00:10	460.270	5.88	-0.01
00:30	480.270	5.87	0.00
00:50	500.270	5.87	0.00
01:10	520.270	5.87	0.00
01:30	540.220	5.86	0.01
01:50	560.230	5.86	0.01
02:10	580.230	5.86	0.01
02:30	600.230	5.85	0.02
02:50	620.230	5.85	0.02
03:10	640.230	5.85	0.02
03:30	660.230	5.84	0.03
03:50	680.230	5.84	0.03
04:10	700.180	5.83	0.04
04:30	720.320	5.83	0.04
04:50	740.280	5.83	0.04
05:10	760.280	5.83	0.04
05:30	780.280	5.83	0.04
05:50	800.320	5.83	0.04
06:10	820.320	5.82	0.05
06:30	840.320	5.82	0.05
06:50	860.320	5.82	0.05
07:10	880.320	5.81	0.06
07:30	900.320	5.81	0.06
07:50	920.320	5.81	0.06
08:10	940.320	5.80	0.07
08:30	960.320	5.80	0.07
08:50	980.320	5.80	0.07
10:10	1060.500	5.79	0.08
11:10	1120.200	5.80	0.07
12:10	1180.200	5.79	0.08
13:10	1240.200	5.81	0.06
14:10	1300.200	5.82	0.05
15:10	1360.200	5.84	0.03
16:10	1420.200	5.83	0.04
17:10	1480.200	5.86	0.01
18:10	1540.100	5.87	0.00
19:10	1600.300	5.88	-0.01
20:10	1660.300	5.88	-0.01
21:10	1720.300	5.89	-0.02
22:10	1780.200	5.89	-0.02
23:10	1840.200	5.89	-0.02
00:10	1900.200	5.88	-0.01
01:10	1960.300	5.88	-0.01
02:10	2020.300	5.87	0.00
03:10	2080.200	5.86	0.01
04:10	2140.200	5.85	0.02
05:10	2200.200	5.85	0.02
06:10	2260.200	5.84	0.03
07:10	2320.200	5.83	0.04
08:10	2380.300	5.81	0.06
09:10	2440.200	5.80	0.07

10:10	2500.300	5.78	0.09
11:10	2560.300	5.78	0.09
12:10	2620.300	5.77	0.10
13:10	2680.300	5.75	0.12
14:10	2740.200	5.74	0.13
15:10	2800.200	5.73	0.14
16:10	2860.300	5.71	0.16
17:10	2920.200	5.70	0.17
18:10	2980.200	5.68	0.19
19:10	3040.200	5.66	0.21
20:10	3100.200	5.65	0.22
21:10	3160.200	5.64	0.23
22:10	3220.200	5.63	0.24
23:10	3280.200	5.62	0.25
00:10	3340.200	5.61	0.26
01:10	3400.200	5.61	0.26
02:10	3460.200	5.60	0.27
03:10	3520.200	5.59	0.28
04:10	3580.200	5.59	0.28
05:10	3640.200	5.58	0.29
06:10	3700.200	5.58	0.29
07:10	3760.400	5.57	0.30
08:10	3820.200	5.57	0.30
09:10	3880.200	5.57	0.30
10:10	3940.200	5.57	0.30
11:10	4000.200	5.57	0.30
12:10	4060.300	5.57	0.30
13:10	4120.200	5.56	0.31
14:10	4180.200	5.59	0.28
15:10	4240.300	5.59	0.28
16:10	4300.200	5.59	0.28
16:59	4349.700	5.62	0.25

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 3-4 Run #2  
TEST TYPE : RECOVERY  
WELL NUMBER : REI 3-2 INPUT 6  
RADIUS: NOT AVAILABLE  
START DATE : 21-Aug-86  
START TIME : 16:59  
WATER START LEVEL: 5.87 FEET  
WATER STOP LEVEL: 5.62 FEET  
TOTAL PUMPING TIME: 4349.7 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
16:59	0.084	5.62	0.00	0.25
16:59	0.167	5.62	0.00	0.25
16:59	0.251	5.62	0.00	0.25
16:59	0.334	5.62	0.00	0.25
16:59	0.417	5.62	0.00	0.25
16:59	0.501	5.62	0.00	0.25
16:59	0.584	5.62	0.00	0.25
16:59	0.667	5.62	0.00	0.25
16:59	0.751	5.62	0.00	0.25
16:59	0.834	5.62	0.00	0.25
16:59	0.917	5.62	0.00	0.25
17:00	1.001	5.62	0.00	0.25
17:00	1.389	5.62	0.00	0.25
17:00	1.723	5.62	0.00	0.25
17:01	2.056	5.62	0.00	0.25
17:01	2.389	5.61	0.01	0.26
17:01	2.723	5.62	0.00	0.25
17:02	3.056	5.61	0.01	0.26
17:02	3.389	5.61	0.01	0.26
17:02	3.723	5.61	0.01	0.26
17:03	4.056	5.62	0.00	0.25
17:03	4.389	5.62	0.00	0.25
17:03	4.723	5.62	0.00	0.25
17:04	5.056	5.62	0.00	0.25
17:04	5.389	5.62	0.00	0.25
17:04	5.723	5.62	0.00	0.25
17:05	6.056	5.62	0.00	0.25
17:05	6.389	5.62	0.00	0.25
17:05	6.723	5.62	0.00	0.25
17:06	7.056	5.62	0.00	0.25
17:06	7.389	5.62	0.00	0.25
17:06	7.723	5.62	0.00	0.25
17:07	8.056	5.62	0.00	0.25
17:07	8.389	5.62	0.00	0.25
17:07	8.723	5.62	0.00	0.25
17:08	9.056	5.62	0.00	0.25
17:08	9.389	5.62	0.00	0.25
17:08	9.723	5.62	0.00	0.25

17:09	10.056	5.62	0.00	0.25
17:11	12.165	5.62	0.00	0.25
17:13	14.495	5.62	0.00	0.25
17:15	16.165	5.62	0.00	0.25
17:17	18.165	5.62	0.00	0.25
17:19	20.203	5.62	0.00	0.25
17:21	22.203	5.62	0.00	0.25
17:23	24.225	5.62	0.00	0.25
17:25	26.225	5.63	-0.01	0.24
17:27	28.225	5.62	0.00	0.25
17:29	30.225	5.62	0.00	0.25
17:31	32.225	5.63	-0.01	0.24
17:33	34.225	5.62	0.00	0.25
17:35	36.225	5.63	-0.01	0.24
17:37	38.225	5.63	-0.01	0.24
17:39	40.225	5.63	-0.01	0.24
17:41	42.225	5.63	-0.01	0.24
17:43	44.225	5.63	-0.01	0.24
17:45	46.225	5.63	-0.01	0.24
17:47	48.225	5.63	-0.01	0.24
17:49	50.225	5.63	-0.01	0.24
17:51	52.225	5.63	-0.01	0.24
17:53	54.225	5.63	-0.01	0.24
17:55	56.225	5.63	-0.01	0.24
17:57	58.225	5.63	-0.01	0.24
17:59	60.225	5.63	-0.01	0.24
18:01	62.225	5.63	-0.01	0.24
18:03	64.225	5.63	-0.01	0.24
18:05	66.225	5.63	-0.01	0.24
18:07	68.225	5.63	-0.01	0.24
18:09	70.225	5.63	-0.01	0.24
18:11	72.225	5.63	-0.01	0.24
18:13	74.225	5.63	-0.01	0.24
18:15	76.225	5.63	-0.01	0.24
18:17	78.225	5.63	-0.01	0.24
18:19	80.225	5.63	-0.01	0.24
18:21	82.225	5.63	-0.01	0.24
18:23	84.225	5.64	-0.02	0.23
18:25	86.225	5.64	-0.02	0.23
18:27	88.225	5.64	-0.02	0.23
18:29	90.225	5.64	-0.02	0.23
18:31	92.225	5.63	-0.01	0.24
18:33	94.225	5.64	-0.02	0.23
18:35	96.225	5.64	-0.02	0.23
18:37	98.225	5.64	-0.02	0.23
18:39	100.230	5.64	-0.02	0.23
18:59	120.230	5.64	-0.02	0.23
19:19	140.230	5.63	-0.01	0.24
19:39	160.230	5.63	-0.01	0.24
19:59	180.220	5.63	-0.01	0.24
20:19	200.220	5.62	0.00	0.25
20:39	220.220	5.62	0.00	0.25
20:59	240.220	-999.99	1005.61	1005.86
21:19	260.220	15.58	-9.96	9.71
21:39	280.120	15.57	-9.95	9.70
21:59	300.120	15.55	-9.93	9.68

22:19	320.120	15.55	-9.93	9.68
22:39	340.200	15.54	-9.92	9.67
22:59	360.220	15.54	-9.92	9.67
23:19	380.220	15.54	-9.92	9.67
23:39	400.220	15.54	-9.92	9.67
23:59	420.220	15.54	-9.92	9.67
00:19	440.220	15.54	-9.92	9.67
00:39	460.220	15.54	-9.92	9.67
00:59	480.220	15.54	-9.92	9.67
01:19	500.220	15.54	-9.92	9.67
01:39	520.220	15.54	-9.92	9.67
01:59	540.220	15.54	-9.92	9.67
02:19	560.200	15.54	-9.92	9.67
02:39	580.200	15.54	-9.92	9.67
02:59	600.200	15.54	-9.92	9.67
03:19	620.200	15.54	-9.92	9.67
03:39	640.200	15.54	-9.92	9.67
03:59	660.220	15.54	-9.92	9.67
04:19	680.220	15.54	-9.92	9.67
04:39	700.220	15.54	-9.92	9.67
04:59	720.220	15.54	-9.92	9.67
05:19	740.220	15.54	-9.92	9.67
05:39	760.170	15.54	-9.92	9.67
05:59	780.080	15.54	-9.92	9.67
06:19	800.080	15.54	-9.92	9.67
06:39	820.080	15.54	-9.92	9.67
06:59	840.080	15.54	-9.92	9.67
07:19	860.070	15.54	-9.92	9.67
07:39	880.170	15.54	-9.92	9.67
07:59	900.170	15.54	-9.92	9.67
08:19	920.170	15.54	-9.92	9.67
08:39	940.130	15.54	-9.92	9.67
08:53	954.580	15.54	-9.92	9.67

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 3-4 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : REI 3-3 INPUT 7  
RADIUS: NOT AVAILABLE  
START DATE : 21-Aug-86  
START TIME : 16:30  
WATER START LEVEL: 7.32 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
16:30	0.000	7.32	0.00
16:30	0.084	7.33	-0.01
16:30	0.167	7.33	-0.01
16:30	0.251	7.33	-0.01
16:30	0.334	7.33	-0.01
16:30	0.417	7.33	-0.01
16:30	0.501	7.33	-0.01
16:30	0.584	7.33	-0.01
16:30	0.667	7.33	-0.01
16:30	0.751	7.33	-0.01
16:30	0.834	7.33	-0.01
16:30	0.917	7.33	-0.01
16:31	1.001	7.33	-0.01
16:31	1.391	7.33	-0.01
16:31	1.724	7.33	-0.01
16:32	2.058	7.33	-0.01
16:32	2.391	7.33	-0.01
16:32	2.724	7.33	-0.01
16:33	3.058	7.33	-0.01
16:33	3.391	7.33	-0.01
16:33	3.724	7.33	-0.01
16:34	4.058	7.33	-0.01
16:34	4.391	7.33	-0.01
16:34	4.724	7.33	-0.01
16:35	5.058	7.33	-0.01
16:35	5.391	7.33	-0.01
16:35	5.724	7.33	-0.01
16:36	6.058	7.33	-0.01
16:36	6.391	7.33	-0.01
16:36	6.724	7.33	-0.01
16:37	7.058	7.33	-0.01
16:37	7.391	7.33	-0.01
16:37	7.724	7.33	-0.01
16:38	8.058	7.33	-0.01
16:38	8.391	7.34	-0.02
16:38	8.724	7.34	-0.02
16:39	9.058	7.34	-0.02
16:39	9.391	7.33	-0.01
16:39	9.724	7.34	-0.02
16:40	10.058	7.34	-0.02



16:42	12.153	7.33	-0.01
16:44	14.153	7.33	-0.01
16:46	16.423	7.34	-0.02
16:48	18.762	7.34	-0.02
16:50	20.193	7.34	-0.02
16:52	22.193	7.34	-0.02
16:54	24.193	7.34	-0.02
16:56	26.193	7.34	-0.02
16:58	28.193	7.34	-0.02
17:00	30.193	7.34	-0.02
17:02	32.193	7.34	-0.02
17:04	34.158	7.35	-0.03
17:06	36.158	7.35	-0.03
17:08	38.158	7.35	-0.03
17:10	40.158	7.35	-0.03
17:12	42.158	7.35	-0.03
17:14	44.158	7.35	-0.03
17:16	46.158	7.35	-0.03
17:18	48.158	7.35	-0.03
17:20	50.158	7.35	-0.03
17:22	52.158	7.35	-0.03
17:24	54.158	7.35	-0.03
17:26	56.158	7.35	-0.03
17:28	58.158	7.35	-0.03
17:30	60.158	7.35	-0.03
17:32	62.247	7.35	-0.03
17:34	64.135	7.35	-0.03
17:36	66.135	7.35	-0.03
17:38	68.135	7.35	-0.03
17:40	70.135	7.35	-0.03
17:42	72.135	7.35	-0.03
17:44	74.135	7.35	-0.03
17:46	76.135	7.35	-0.03
17:48	78.135	7.35	-0.03
17:50	80.782	7.35	-0.03
17:52	82.182	7.35	-0.03
17:54	84.070	7.35	-0.03
17:56	86.070	7.36	-0.04
17:58	88.070	7.35	-0.03
18:00	90.070	7.36	-0.04
18:02	92.070	7.36	-0.04
18:04	94.070	7.36	-0.04
18:06	96.070	7.36	-0.04
18:08	98.115	7.36	-0.04
18:10	100.120	7.36	-0.04
18:30	120.280	7.37	-0.05
18:50	140.220	7.37	-0.05
19:10	160.220	7.35	-0.03
19:30	180.220	7.35	-0.03
20:10	220.500	7.34	-0.02
20:30	240.270	7.34	-0.02
20:50	260.330	7.33	-0.01
21:10	280.330	7.32	0.00
21:30	300.230	7.32	0.00
21:50	320.280	7.32	0.00
22:10	340.320	7.30	0.02

22:30	360.300	7.29	0.03
22:50	380.270	7.28	0.04
23:10	400.270	7.27	0.05
23:30	420.270	7.26	0.06
23:50	440.270	7.25	0.07
00:10	460.270	7.24	0.08
00:30	480.270	7.24	0.08
00:50	500.270	7.23	0.09
01:10	520.270	7.22	0.10
01:30	540.220	7.21	0.11
01:50	560.230	7.21	0.11
02:10	580.230	7.21	0.11
02:30	600.230	7.20	0.12
02:50	620.230	7.19	0.13
03:10	640.230	7.20	0.12
03:30	660.230	7.19	0.13
03:50	680.230	7.18	0.14
04:10	700.180	7.17	0.15
04:30	720.320	7.17	0.15
04:50	740.280	7.17	0.15
05:10	760.280	7.16	0.16
05:30	780.280	7.16	0.16
05:50	800.320	7.15	0.17
06:10	820.320	7.15	0.17
06:30	840.320	7.15	0.17
06:50	860.320	7.14	0.18
07:10	880.320	7.14	0.18
07:30	900.320	7.14	0.18
07:50	920.320	7.14	0.18
08:10	940.320	7.14	0.18
08:30	960.320	7.14	0.18
08:50	980.320	7.14	0.18
10:10	1060.500	7.14	0.18
11:10	1120.200	7.15	0.17
12:10	1180.200	7.18	0.14
13:10	1240.200	7.21	0.11
14:10	1300.200	7.26	0.06
15:10	1360.200	7.30	0.02
16:10	1420.200	7.31	0.01
17:10	1480.200	7.35	-0.03
18:10	1540.100	7.37	-0.05
19:10	1600.300	7.37	-0.05
20:10	1660.300	7.37	-0.05
21:10	1720.300	7.36	-0.04
22:10	1780.200	7.35	-0.03
23:10	1840.200	7.32	0.00
00:10	1900.200	7.30	0.02
01:10	1960.300	7.28	0.04
02:10	2020.300	7.27	0.05
03:10	2080.200	7.25	0.07
04:10	2140.200	7.23	0.09
05:10	2200.200	7.22	0.10
06:10	2260.200	7.21	0.11
07:10	2320.200	7.20	0.12
08:10	2380.300	7.19	0.13
09:10	2440.200	7.17	0.15

10:10	2500.300	7.17	0.15
11:10	2560.300	7.17	0.15
12:10	2620.300	7.15	0.17
13:10	2680.300	7.11	0.21
14:10	2740.200	7.08	0.24
15:10	2800.200	7.07	0.25
16:10	2860.300	7.05	0.27
17:10	2920.200	7.02	0.30
18:10	2980.200	7.00	0.32
19:10	3040.200	6.98	0.34
20:10	3100.200	6.98	0.34
21:10	3160.200	6.97	0.35
22:10	3220.200	6.96	0.36
23:10	3280.200	6.95	0.37
00:10	3340.200	6.94	0.38
01:10	3400.200	6.93	0.39
02:10	3460.200	6.92	0.40
03:10	3520.200	6.91	0.41
04:10	3580.200	6.90	0.42
05:10	3640.200	6.89	0.43
06:10	3700.200	6.89	0.43
07:10	3760.400	6.89	0.43
08:10	3820.200	6.89	0.43
09:10	3880.200	6.89	0.43
10:10	3940.200	6.88	0.44
11:10	4000.200	6.88	0.44
12:10	4060.300	6.91	0.41
13:10	4120.200	6.92	0.40
14:10	4180.200	6.95	0.37
15:10	4240.300	6.98	0.34
16:10	4300.200	7.02	0.30
16:59	4349.700	7.02	0.30

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 3-4 Run #2  
TEST TYPE : RECOVERY  
WELL NUMBER : REI 3-3 INPUT 7  
RADIUS: NOT AVAILABLE  
START DATE : 21-Aug-86  
START TIME : 16:59  
WATER START LEVEL: 7.32 FEET  
WATER STOP LEVEL: 7.02 FEET  
TOTAL PUMPING TIME: 4349.7 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
16:59	0.084	7.02	0.00	0.30
16:59	0.167	7.02	0.00	0.30
16:59	0.251	7.02	0.00	0.30
16:59	0.334	7.02	0.00	0.30
16:59	0.417	7.02	0.00	0.30
16:59	0.501	7.02	0.00	0.30
16:59	0.584	7.02	0.00	0.30
16:59	0.667	7.02	0.00	0.30
16:59	0.751	7.02	0.00	0.30
16:59	0.834	7.02	0.00	0.30
16:59	0.917	7.02	0.00	0.30
17:00	1.001	7.02	0.00	0.30
17:00	1.389	7.02	0.00	0.30
17:00	1.723	7.02	0.00	0.30
17:01	2.056	7.02	0.00	0.30
17:01	2.389	7.02	0.00	0.30
17:01	2.723	7.02	0.00	0.30
17:02	3.056	7.02	0.00	0.30
17:02	3.389	7.02	0.00	0.30
17:02	3.723	7.02	0.00	0.30
17:03	4.056	7.02	0.00	0.30
17:03	4.389	7.02	0.00	0.30
17:03	4.723	7.02	0.00	0.30
17:04	5.056	7.02	0.00	0.30
17:04	5.389	7.02	0.00	0.30
17:04	5.723	7.02	0.00	0.30
17:05	6.056	7.02	0.00	0.30
17:05	6.389	7.02	0.00	0.30
17:05	6.723	7.02	0.00	0.30
17:06	7.056	7.02	0.00	0.30
17:06	7.389	7.02	0.00	0.30
17:06	7.723	7.02	0.00	0.30
17:07	8.056	7.02	0.00	0.30
17:07	8.389	7.02	0.00	0.30
17:07	8.723	7.02	0.00	0.30
17:08	9.056	7.02	0.00	0.30
17:08	9.389	7.02	0.00	0.30
17:08	9.723	7.02	0.00	0.30

17:09	10.056	7.02	0.00	0.30
17:11	12.165	7.02	0.00	0.30
17:13	14.495	7.02	0.00	0.30
17:15	16.165	7.02	0.00	0.30
17:17	18.165	7.02	0.00	0.30
17:19	20.203	7.02	0.00	0.30
17:21	22.203	7.02	0.00	0.30
17:23	24.225	7.02	0.00	0.30
17:25	26.225	7.02	0.00	0.30
17:27	28.225	7.02	0.00	0.30
17:29	30.225	7.02	0.00	0.30
17:31	32.225	7.02	0.00	0.30
17:33	34.225	7.02	0.00	0.30
17:35	36.225	7.02	0.00	0.30
17:37	38.225	7.02	0.00	0.30
17:39	40.225	7.01	0.01	0.31
17:41	42.225	7.01	0.01	0.31
17:43	44.225	7.01	0.01	0.31
17:45	46.225	7.02	0.00	0.30
17:47	48.225	7.01	0.01	0.31
17:49	50.225	7.01	0.01	0.31
17:51	52.225	7.01	0.01	0.31
17:53	54.225	7.01	0.01	0.31
17:55	56.225	7.01	0.01	0.31
17:57	58.225	7.01	0.01	0.31
17:59	60.225	7.01	0.01	0.31
18:01	62.225	7.01	0.01	0.31
18:03	64.225	7.01	0.01	0.31
18:05	66.225	7.01	0.01	0.31
18:07	68.225	7.01	0.01	0.31
18:09	70.225	7.01	0.01	0.31
18:11	72.225	7.01	0.01	0.31
18:13	74.225	7.01	0.01	0.31
18:15	76.225	7.01	0.01	0.31
18:17	78.225	7.01	0.01	0.31
18:19	80.225	7.01	0.01	0.31
18:21	82.225	7.01	0.01	0.31
18:23	84.225	7.01	0.01	0.31
18:25	86.225	7.01	0.01	0.31
18:27	88.225	7.01	0.01	0.31
18:29	90.225	7.00	0.02	0.32
18:31	92.225	7.00	0.02	0.32
18:33	94.225	7.00	0.02	0.32
18:35	96.225	7.00	0.02	0.32
18:37	98.225	7.00	0.02	0.32
18:39	100.230	7.00	0.02	0.32
18:59	120.230	6.99	0.03	0.33
19:19	140.230	6.99	0.03	0.33
19:39	160.230	6.98	0.04	0.34
19:59	180.220	6.98	0.04	0.34
20:19	200.220	6.98	0.04	0.34
20:39	220.220	6.98	0.04	0.34
20:59	240.220	16.89	-9.87	9.57
21:19	260.220	16.90	-9.88	9.58
21:39	280.120	16.91	-9.89	9.59
21:59	300.120	16.91	-9.89	9.59

Appendix 17

Neuman and Witherspoon (1972) Method Reference

## Field Determination of the Hydraulic Properties of Leaky Multiple Aquifer Systems

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**Abstract.** A new field method is proposed for determining the hydraulic properties of aquifers and aquitards in leaky systems. Conventional methods of analyzing leaky aquifers usually rely on drawdown data from the pumped aquifer alone. Such an approach is not sufficient to characterize a leaky system; our new method requires observation wells to be placed not only in the aquifer being pumped but also in the confining layers (aquitards) above and/or below. The ratio of the drawdown in the aquitard to that measured in the aquifer at the same time and the same radial distance from the pumping well can be used to evaluate the hydraulic properties of the aquitard. The new method is supported by theory and has been applied to the coastal groundwater basin of Oxnard, California. The field results are in good agreement with laboratory measurements.

Traditionally, groundwater hydrologists have tended to focus their attention on the more permeable aquifer layers of a groundwater basin in developing water supplies. However, sedimentary groundwater basins usually consist of a series of aquifers separated by confining layers of relatively low permeability, which may act as conduits for the vertical migration of water from one aquifer to another. Since fine-grained sediments often tend to be much more compressible than associated coarse-grained aquifer materials, they also can release large quantities of water from storage and thereby increase the supply available to the aquifer. The combined effects of these phenomena are known as leakage.

Usually, when the effects of leakage can be detected by observing drawdown in the aquifer being pumped, the confining beds are called 'aquitards,' and the aquifer is referred to as being 'leaky.' When such effects cannot be easily detected in the aquifer, the confining beds are called 'aquicludes,' and the aquifer is termed 'slightly leaky' [Neuman and Witherspoon, 1968].

Aquitards play an important role in the

hydrology of multiple aquifer systems, and we shall mention here only a few examples. Although groundwater recharge is often believed to occur in areas of aquifer overtopping, Gil [1969] has recently reported that substantial amounts of water produced from the Potomac-Raritan-Magothy aquifer system are coming through the aquitards. Earlier, Walton [1963] had shown how the Maquoketa formation in Illinois, which is essentially a shale bed, serves as an effective transmitter of water between aquifers. Land subsidence in the San Joaquin Valley and other areas in California has been shown to be associated with water withdrawal from multiple aquifer systems and is generally attributed to the resulting compaction of fine-grained aquitard sediments [Poland and Davis, 1969]. Similar situations exist in Venice, Japan, and other parts of the world.

For the past 20 years, aquifers at depths below 500 feet have been used for storing natural gas in the United States and Europe. Where the properties of the aquitards were not properly investigated, the gas industry has on occasion witnessed the spectacular and dangerous effects of gas leakage. The storage of other fluids

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ze. The storage of other fluids,

as well as the disposal of waste products under-  
ground, requires the role of aquitards to be  
thoroughly understood if the degradation of  
groundwater supplies and the pollution of the  
surface environment are to be avoided. The  
role of aquitards may also be important in de-  
termining the rate at which the seawater from  
a degraded aquifer may migrate vertically to an  
uninvaded zone. An interesting situation in  
which the effectiveness of aquitards in prevent-  
ing seawater intrusion is largely unknown occurs  
with the construction of shallow harbors and  
marinas requires the removal of a part of the  
aquitard that normally provides a natural bar-  
rier between the ocean and the freshwater aqui-  
fer beneath [California Department of Water  
Resources, 1971, p. 10].

Although the importance of aquitards is be-  
ing recognized more and more, there is no re-  
liable method for their investigation, and very  
little is known about their hydraulic properties.  
This report describes an improved field method  
for evaluating the hydraulic properties of aqui-  
fers and aquitards in leaky multiple aquifer sys-  
tems. The new approach is simple to use and  
applicable to a wide range of hydrogeological  
situations. We shall describe in detail one par-  
ticular investigation performed in the coastal  
groundwater basin of Oxnard, California.

#### PROBLEMS IN ANALYZING PUMPING TESTS WITH CURRENT METHODS

In analyzing results of water pumping tests  
the well-known Theis [1935] solution is often  
used to determine the permeability and the spe-  
cific storage of the aquifer under investigation.  
As long as the aquitards do not leak significant  
amounts of water into the aquifer, this method  
of analysis produces reliable results.

However, groundwater hydrologists noted  
many years ago that deviations from the aquifer  
behavior, as predicted by the Theis solution,  
are not uncommon. These deviations are often  
caused by water leaking out of the confining  
beds, and this led to the 'leaky aquifer' theory  
of Hantush and Jacob [1955]. This theory and  
its later modifications [Hantush, 1960] relied  
only on an examination of aquifer behavior and  
attempted to relate such behavior to the prop-  
erties of the adjacent aquitards.

Unfortunately, this approach has not been  
entirely satisfactory. As has recently been

pointed out by Neuman and Witherspoon  
[1969b], field methods based on the leaky aquifer  
theory of Hantush and Jacob [1955] may often  
lead to significant errors. These errors are such  
that one tends to overestimate the permeability  
of the aquifer and underestimate the permeabil-  
ity of the confining beds. Under some circum-  
stances, one may also get the false impression  
that the aquifer is inhomogeneous. Further-  
more, the method does not provide a means of  
distinguishing whether the leaking beds lie above  
or below the aquifer being pumped.

A new theory of flow in multiple aquifer sys-  
tems has recently been developed by Neuman  
and Witherspoon [1969a; California Depart-  
ment of Water Resources, 1971, pp. 24-38].  
This theory shows that the behavior of draw-  
down in each layer is a function of several  
dimensionless parameters  $\beta_i$  and  $r/B_i$ , which  
depend on the hydraulic characteristics of the  
aquitards as well as those of the aquifers. The  
new theory clearly indicates that the observa-  
tion of drawdown in the pumped aquifer alone  
is not always sufficient to determine uniquely  
the values of  $\beta$  and  $r/B$ . For example, Han-  
tush's [1960] modified theory of leaky aquifers  
provides an analytical solution in terms of  $\beta$   
that we know is applicable at sufficiently small  
values of time. Nevertheless, since this solution  
relates only to drawdown in the aquifer being  
pumped, its usefulness in determining uniquely  
the properties of each aquitard or even in  
determining a unique value of  $\beta$  is very limited  
[California Department of Water Resources,  
1971, p. 327; Riley and McClelland, 1970]. Our  
theory indicates that one should be able to de-  
velop improved methods of analysis by installing  
observation wells not only in the aquifer being  
pumped but also in the confining layers enclos-  
ing it. Indeed, as will be shown later, a series of  
observation wells in more than one layer is a  
prerequisite for any reliable evaluation of aqui-  
tard characteristics.

The idea of placing observation wells in a  
low permeability layer (aquiclude) overlying a  
slightly leaky aquifer was originally proposed  
by Witherspoon et al. [1962] in connection with  
the underground storage of natural gas in aqui-  
fers. Their purpose was to determine how effec-  
tive a given aquiclude would be in preventing  
gas leakage from the intended underground  
storage reservoir. Using results obtained from a



finite difference simulation model, Witherspoon et al. were able to suggest a method for evaluating the hydraulic diffusivity of an aquiclude by means of a pumping test.

Later, a theoretical analysis of flow in aquicludes adjacent to slightly leaky aquifers was developed by Neuman and Witherspoon [1968]. This theory led to an improved method for determining the hydraulic diffusivity of aquicludes under slightly leaky conditions [Witherspoon and Neuman, 1967; Witherspoon et al., 1967, pp. 72-92]. Since the method relies on the ratio between drawdown in the aquiclude and drawdown in the pumped aquifer, it will henceforth be referred to as the 'ratio method.'

A method for evaluating the hydraulic diffusivity of an aquitard under arbitrary conditions of leakage, which also uses observation wells completed in the confining layer itself, was recently described by Wolff [1970]. In his analysis Wolff assumed that, at any given radial distance from the pumping well and at a sufficiently large value of time, one can represent drawdown in the pumped aquifer by a step function. Assuming also that drawdown in the unpumped aquifer remains 0, Wolff arrived at a set of type curves that he recommended for aquitard evaluation.

Although this method gave satisfactory results for the particular site investigated by Wolff, we think that the step function approach may lead to difficulties when it is applied to arbitrary multiple aquifer systems. Fundamentally, drawdown in the pumped aquifer cannot be reliably represented by a single step function unless a quasi-steady state is reached within a sufficiently short period of time. The quasi-steady state will be reached only if the transmissibility of the aquifer is large and if the observation wells are situated at relatively small radial distances from the pumping well. To minimize the effect of early drawdowns, Wolff's method further requires that the duration of the pumping test be sufficiently long and that the vertical distance between the pumped aquifer and the aquitard observation wells not be too small.

From our new theory of flow in multiple aquifer systems, we now know that at large values of time the results in the aquitard may be affected significantly by the influence of an adjacent unpumped aquifer, especially where the aquitard

observation well has been perforated close to such an aquifer. Thus, although the single step function approach renders the method inapplicable at small values of time, the assumption of zero drawdown in the unpumped aquifer introduces an additional restriction at large values of time.

In the special case where the thickness of the aquitard is known, one can determine its diffusivity directly from the step function type curves without the need for graphical curve matching. Quite often, however, the effective thickness of the aquitard is unknown. For example, the aquitard may contain unidentified or poorly defined layers of highly permeable material that act as a buffer to the pressure transient and also as a source of leakage. Another possibility is that the aquitard is situated below the pumped aquifer and that its lower limit has never been adequately defined. Then the step function approach requires the graphical matching of aquitard drawdown data with Wolff's [1970] type curves.

However, the intermediate parts of these type curves are essentially parallel, and therefore they cannot be matched uniquely with field results. On the other hand, neither the early nor the late parts of the type curves can be used with confidence. Thus there may be a significant element of uncertainty when Wolff's [1970] method is applied to real field situations.

Since the currently available direct field methods appear to be limited in their application, there is an obvious need for a new approach that would enable one to determine the characteristics of multiple aquifer systems under a wide variety of field conditions. We shall attempt to demonstrate that a rational basis for such an approach is provided by our new theory of flow in multiple aquifer systems [Neuman and Witherspoon, 1969a]. We will start by showing that the ratio method, which we originally thought was limited in application only to aquicludes under slightly leaky conditions, can in fact also be used to evaluate the properties of aquitards under very leaky conditions.

#### APPLICABILITY OF THE RATIO METHOD TO LEAKY CONDITIONS

To develop a method for determining the hydraulic properties of aquitards, we shall first

is perforated close to the surface, though the single step method may apply. In time, the assumption of an unpumped aquifer is a restriction at large

the thickness of the aquifer to determine its diffusion step function type for graphical curve fitting. However, the effective permeability is unknown. For example, contain unidentified of highly permeable aquifer to the pressure of leakage. Another aquifer is situated below but its lower limit has not been defined. Then the step function graphical matching data with Wolf's

late parts of these parameters are parallel, and therefore uniquely with field data. Whether the early type curves can be used there may be a difficulty when Wolf's model is used in real field situations. Available direct field data are limited in their application. There is a need for a new model one to determine multiple aquifer systems under field conditions. We note that a rational model is provided by our multiple aquifer systems model (1969a). We will use the ratio method, which is limited in application to slightly leaky conditions to evaluate the effect of very leaky condi-

consider a two-aquifer system (Figure 1). A complete solution for the distribution of drawdown in such a system has been developed by Neuman and Witherspoon [1969a]. In each aquifer the solutions depend on five dimensionless parameters  $\beta_{11}$ ,  $r/B_{11}$ ,  $\beta_{21}$ ,  $r/B_{21}$ , and  $t_{D1}$ . In the aquitard the solution involves one additional parameter  $z/b_1'$ . This large number of dimensionless parameters makes it practically impossible to construct a sufficient number of type curves to cover the entire range of values necessary for field application. For a set of type curves to be useful, they are normally expressed in terms of not more than two independent dimensionless parameters.

One way to significantly reduce the number of parameters is to restrict the analysis of field data to small values of time. In particular, we want to focus our attention on those early effects that occur prior to the time when a discernible pressure transient reaches the unpumped aquifer. At such early times the unpumped aquifer does not exert any influence on the rest of the system, and therefore drawdowns are independent of the parameters  $\beta_{21}$  and  $r/B_{21}$ . Furthermore, the aquitard behaves as if its thickness were infinite, which simply means that the parameters  $r/B_{11}$  and  $z/b_1'$  also have no influence on the drawdown. Thus the resulting equation will depend only on  $\beta_{11}$ ,  $t_{D1}$ , and an additional parameter  $t_{D1}'$ .

In the pumped aquifer, drawdown is then given by Hantush's [1960] asymptotic equation [Neuman and Witherspoon, 1969a],

$$s_1(r, t) = \frac{Q_1}{4\pi t_1} \int_{1/4t_{D1}}^{\infty} \frac{e^{-y}}{y} \cdot \operatorname{erfc} \left( \frac{\beta_{11}}{[y(4t_{D1}y - 1)]^{1/2}} \right) dy \quad (1)$$

In the aquitard the solution is

$$s_1'(r, z, t) = \frac{Q_1}{4\pi T_1} \int_{1/4t_{D1}}^{\infty} \frac{e^{-y}}{y} \cdot \operatorname{erfc} \left( \frac{\beta_{11} + y(t_{D1}'/t_{D1})^{1/2}}{[y(4t_{D1}y - 1)]^{1/2}} \right) dy \quad (2)$$

Theoretically, (1) and (2) are limited to those small values of time that satisfy the criterion

$$t_{D1} \leq 1.6\beta_{11}^2/(r/B_{11})^2 \quad (3)$$

In terms of real time this criterion may also be

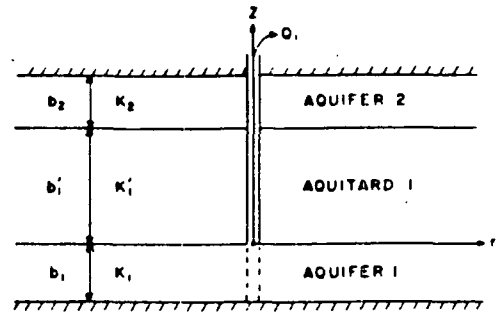


Fig. 1. A schematic diagram of a two-aquifer system.

expressed by

$$t \leq 0.1S_{11}'b_1'^2/K_1' \quad (4)$$

indicating that the limiting value of time is independent of the radial distance from the pumping well.

From a practical standpoint the criterion given by (3) or (4) is overly conservative. For example, Figures 2-8 in Neuman and Witherspoon [1969a] reveal that the effect of the unpumped aquifer is felt in the rest of the system at times that are always greater than those predicted by (3). Note further that in these figures the effects of  $\beta_{21}$  and  $r/B_{21}$  are negligible as long as the log-log curve of drawdown versus time for the unpumped aquifer does not depart from its initial steep slope.

This effect of the unpumped aquifer provides a useful criterion for determining the time limit beyond which the asymptotic solutions may no longer be applicable. If an observation well can be provided in the unpumped aquifer, a log-log plot of drawdown versus time should enable the hydrologist to identify this time limit.

Note that there may be field situations in which the procedure above is not applicable. For example, when the transmissibility of the unpumped aquifer is large in comparison to that of the aquifer being pumped, drawdowns in the unpumped aquifer will be too small to measure, and one would not be able to determine the time limit as outlined above. This procedure may also fail when the water levels in the unpumped aquifer are fluctuating during the pumping test owing to some uncontrolled local or regional effect. Then a more conservative estimate of the time limit can be established from drawdown data observed in one of the

#### RATIO METHOD CONDITIONS

or determining the aquitards, we shall first

aquitard wells. In general, the smaller the vertical distance between the perforated interval in the aquitard well and the boundary of the pumped aquifer is, the more conservative the time indicated by the procedure above is.

Having established a practical method for estimating the time within which (1) and (2) are valid, we can now proceed to show how these equations lead to the ratio method for evaluating aquitards. Remember that Hantush's equation does not by itself lead to a reliable method for determining a unique value of  $\beta_{11}$  from field results. The same can be said of (2), because it involves three independent parameters  $\beta_{11}$ ,  $t_{D1}$ , and  $t_{D1}'$ . However, the usefulness of these two equations becomes immediately evident when one considers  $s_1'/s_1$ , i.e., the ratio of drawdown in the aquitard to that in the pumped aquifer at the same elapsed time and the same radial distance from the pumping well.

In the discussion that follows we shall be dealing with only one aquifer and one aquitard, and for the sake of simplicity we shall omit all subscripts. Figure 2 shows the variation of  $s_1'/s_1$  versus  $t_{D1}'$  for a practical range of  $t_{D1}$  and  $\beta$  values. Note that at  $t_{D1} = 0.2$  changing the

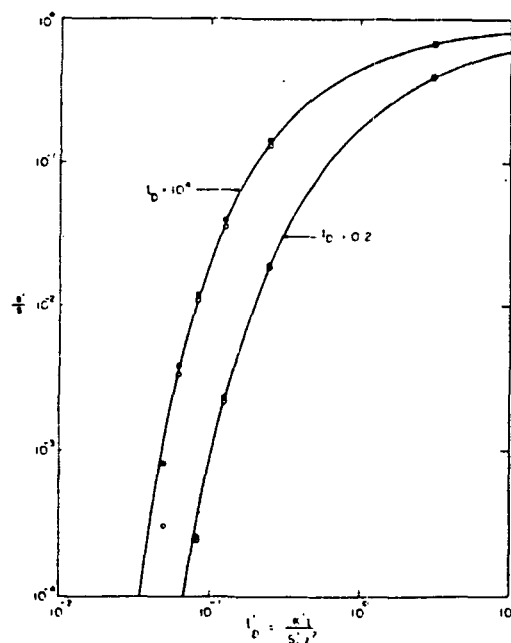


Fig. 2. The variation of  $s_1'/s_1$  with  $t_{D1}'$  for  $\beta = 0.0$  (solid lines),  $\beta = 0.01$  (squares), and  $\beta = 1.0$  (circles).

value of  $\beta$  from 0.01 to 1.0 has practically no effect on the ratio  $s_1'/s_1$ . The same is true as  $t_{D1}$  increases, and this relationship is shown by the additional results for  $t_{D1} = 10'$ .

If we now use our theory for slightly leaky situations [Neuman and Witherspoon, 1968] where  $s'$  is given by

$$s'(r, z, t) = \frac{Q}{4\pi T} \frac{2}{\pi^{1/2}} \int_0^\infty \frac{1}{(4t_{D1}y^2 + 1)^{1/2}} - \text{Ei} \left( -\frac{t_{D1}'y^2}{t_{D1}(4t_{D1}y^2 + 1)} \right) e^{-y^2} dy \quad (5)$$

and  $s$  is obtained from the Theis solution, we have in effect the special case where  $\beta = 0$ . This is represented by the two solid lines in Figure 2.

We also examined the case where  $\beta = 10.0$  and found that the values of  $s_1'/s_1$  deviate significantly from those shown in Figure 2. Thus one may conclude that for all practical values of  $t_{D1}$  the ratio  $s_1'/s_1$  is independent of  $\beta$  as long as  $\beta$  is of order 1.0 or less. Since  $\beta$  is directly proportional to the radial distance from the pumping well, its magnitude can be kept within any prescribed bounds simply by placing the observation wells close enough to the pumping well. A quick calculation will show that distances of the order of a few hundred feet will be satisfactory for most field situations.

Thus we arrive at the very important conclusion that the ratio method, which we originally thought was restricted to only slightly leaky situations, can in effect be used to determine the hydraulic diffusivities of aquitards under arbitrary leaky conditions. We therefore decided to adopt the ratio method as a standard tool for evaluating the properties of aquitards.

#### USE OF THE RATIO METHOD IN AQUITARD EVALUATION

The ratio method can be applied to any aquifer and its adjacent aquitards, above and below, in a multiple aquifer system (see sketch in Figure 3). The method relies on a family of curves of  $s_1'/s_1$  versus  $t_{D1}'$ , each curve corresponding to a different value of  $t_{D1}$  as obtained from (5) and the Theis equation. The curves in Figure 3 have been prepared from tables of values published previously by Witherspoon et al. [1967, Appendix G].

0.01 to 1.0 has practically no effect on  $s'/s$ . The same is true as  $t_b$  relationship is shown by the curves for  $t_b = 10$ .

Our theory for slightly leaky aquifers and Witherspoon, 1968]

$$\frac{2}{\pi^{1/2}} \left( -\frac{t_b' y^2}{t_b (4t_b' y^2 - 1)} \right) \cdot s' dy \quad (5)$$

from the Theis solution, we consider a special case where  $\beta = 0$ , and by the two solid lines in

Figure 2. Thus one can see that for all practical values of  $t_b$ , the values of  $s'/s$  deviate significantly from the case where  $\beta = 10.0$ .

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#### RATIO METHOD IN AQUIFARD EVALUATION

The ratio method can be applied to any leaky aquifer system (see sketch in Figure 3). The method relies on a family of curves of  $s'/s$  versus  $t_b'$ , each curve corresponding to a value of  $t_b$  as obtained from the Theis equation. The curves in Figure 3 were prepared from tables of  $s'/s$  values previously by Witherspoon et al. (1968).

In the ratio method, one first calculates the value of  $s'/s$  at a given radial distance from the pumping well  $r$  and at a given instant of time  $t$ . The next step is to determine the magnitude of  $t_b'$  for the particular values of  $r$  and  $t$  at which  $s'/s$  has been measured. When  $t_b < 100$ , the curves in Figure 3 are sensitive to minor changes in the magnitude of this parameter, and therefore a good estimate of  $t_b$  is desirable. When  $t_b > 100$ , these curves are so close to each other that they can be assumed to be practically independent of  $t_b$ . Then even a crude estimate of  $t_b$  will be sufficient for the ratio method to yield satisfactory results. A procedure for determining the value of  $t_b$  from drawdown data in the aquifer will be discussed later in connection with methods dealing with aquifer characteristics.

Having determined which one of the curves in Figure 3 should be used in a given calculation, one can now read off a value of  $t_b'$  corresponding to the computed ratio of  $s'/s$ . Finally, the diffusivity of the aquitard is determined from the simple formula

$$\alpha' = (z^2/t) t_b' \quad (6)$$

Note in Figure 3 that, when  $s'/s < 0.1$ , the value of  $t_b'$  obtained by the ratio method is not very sensitive to the magnitude of  $s'/s$ . As a result the value of  $\alpha'$  calculated from (6) depends very little on the actual magnitude of the drawdown in the aquitard. Instead, the critical quantity determining the value of  $\alpha'$  at a given elevation  $z$  is the time lag  $t$  between the start of the test and the time when the aquitard observation well begins to respond. The time lag is very important because in using the ratio method one need not worry about having extremely sensitive measurements of drawdown in the aquitard observation wells. A conventional piezometer with a standing water column will usually give sufficiently accurate information for most field situations. The time lag between a change in pressure and the corresponding change in water level in the column is usually so small in comparison to the time lag between the start of the test and this change in pressure that its influence can be safely ignored.

To evaluate the permeability and specific storage of an aquitard from its hydraulic diffusivity, one of these quantities must first be determined by means other than the ratio

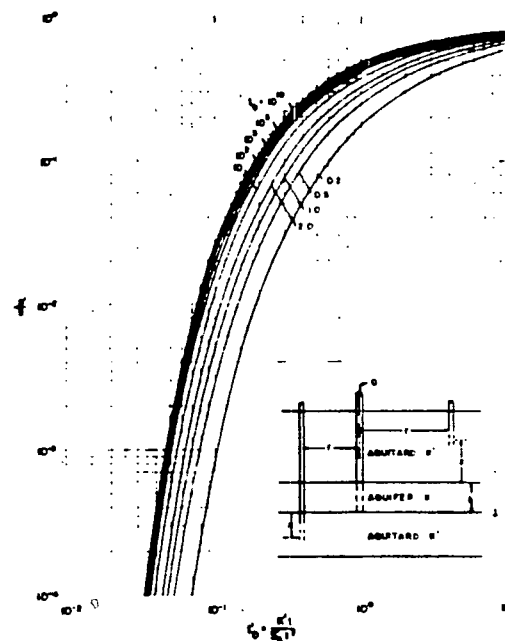


Fig. 3. The variation of  $s'/s$  with  $t_b'$  for a semi-infinite aquitard.

method. Experience indicates that permeability may vary by several orders of magnitude from one aquitard to another and even from one elevation to another in the same aquitard. A much more stable range of values is usually encountered when one is dealing with specific storage.

Recent field measurements in areas of land subsidence (F. S. Riley, personal communication, 1971) have shown that the specific storage of fine-grained sediments depends on the relationship between the load generated by pumping and the past history of loading. When this relationship is such that the sediments react elastically, the value of  $S_s'$  is relatively small. When the sediments are undergoing irreversible consolidation, the value of  $S_s'$  may be larger by 1 or 2 orders of magnitude. Presently, the most reliable measurements of  $S_s'$  are performed in the field by using borehole extensometers. Another way to determine approximate values of  $S_s'$  is to perform standard consolidation tests on core samples in the laboratory. In the total absence of field and laboratory measurements,  $S_s'$  can be estimated by correlating published results on similar sediments. Once the value of

$S_v'$  has been determined,  $K'$  is easily calculated from  $K' = \alpha'S_v'$ .

We also studied the effects of aquitard heterogeneity and anisotropy on the value of  $K'$  obtained by the ratio method at a given elevation  $a$ . In our investigation we used the finite element method to examine the behavior of a two-aquifer system when: (1) the aquitard was a homogeneous anisotropic layer with a horizontal permeability as much as 250 times greater than the vertical and (2) the aquitard consisted of three different layers, each of which was homogeneous and anisotropic. The results of this study indicated that for homogeneous anisotropic aquitards the ratio method will always give a value of  $K'$  that corresponds to the vertical permeability of the aquitard. For a heterogeneous aquitard,  $K'$  is simply the weighted average vertical permeability over the thickness  $z$ . If there are  $N$  layers of thickness  $b^n$  and vertical permeability  $K_v^n$  inside this interval,  $K'$  represents the average value

$$K' = z / \left( \sum_{n=1}^N \frac{b^n}{K_v^n} \right) \quad (7)$$

Boulton [1963] and Neuman [1972] have shown that, at early values of time, drawdown in an unconfined aquifer can safely be approximated by the Theis solution. At later values of time, drawdown is affected by the delayed response of the water table, and the effect is similar to that of leakage in a confined aquifer. Thus, if the ratio method is applicable to aquitards adjacent to confined leaky aquifers, it should also be applicable to situations in which the pumped aquifer is unconfined. This conclusion is further supported by the fact that the ratio method depends less on the actual values of drawdown in the aquifer than on the time lag observed in the aquitard. To test this applicability of the ratio method to an unconfined aquifer, we took data from Wolff [1970] for a pumping test in which observation wells were placed in a confining layer underneath a water table aquifer. We analyzed these data by using the ratio method, and the results are in excellent agreement with those obtained by Wolff.

When we showed that our slightly leaky theory was applicable to the so-called leaky aquifer, our previous discussion was restricted to a two-aquifer system. By now, however, the

reader will recognize that such a restriction is not necessary and that the ratio method is actually applicable to arbitrary multiple aquifer systems. The only requirement is that the sum of the  $\beta_i$  values with respect to the overlying and underlying aquitards be of order 1 or less.

In summary, note once again the following features of the ratio method.

1. The method applies to arbitrary, leaky multiple aquifer situations.
2. The pumped aquifer can be either confined or unconfined.
3. The confining layers can be heterogeneous and anisotropic. Then the ratio method gives the average vertical permeability over the thickness  $z$  of the aquitard being tested.
4. The method relies only on early drawdown data, and therefore the pumping test can be of relatively short duration.
5. The drawdown data in the unpumped aquifer or in the aquitard provide an in situ indication of the time limit at which the ratio method ceases to give reliable results.
6. Since the method is more sensitive to time lag than to the actual magnitude of  $s_v'$ 's, the accuracy with which drawdowns are measured in the aquitard is not overly critical.
7. The method does not require prior knowledge of the aquitard thickness.
8. The ratio method is simple to use and does not involve any graphical curve-matching procedures. This lack of curve-matching procedures is an advantage because curve matching is often prone to errors due to individual judgment and because a more reliable result can be obtained by taking the arithmetic average of results from several values of the ratio  $s_v'$ 's.

#### METHOD FOR EVALUATING AQUIFERS

When the pumped aquifer is slightly leaky, one can evaluate its transmissibility and storage coefficient by the usual procedures based on the Theis equation. When leakage is appreciable, these procedures will not always yield satisfactory results. Alternative methods for analyzing the results of pumping tests in leaky aquifers were proposed by Jacob [1946] and Hantush [1956, 1960]. Still another method based on the  $r/B$  solution has recently been proposed by Narasimhan [1968]. All these methods rely on drawdown data from the pumped aquifer alone.

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#### EVALUATING AQUIFERS

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Their purpose is to determine not only the properties of the aquifer but also the so-called "leakage factors"  $r'B$  and  $\beta$  that depend on the characteristics of the confining layers as well as on those of the aquifer. We have shown earlier that these methods have a limited application and that they can often lead to erroneous results.

Since we have introduced the ratio method as a means for evaluating aquitards, the only remaining unknowns to be determined are the

fer transmissibility  $T$  and the storage coefficient  $S$ . When the aquifer is leaky, the use of methods based on the Theis solution will lead to errors whose magnitudes are a function of  $\beta$  and  $r'B$ . A look at Neuman and Witherspoon [1969a] will reveal that the smaller the values of  $\beta$  and  $r'B$  are, the less the drawdowns in the pumped aquifer deviate from the Theis solution, and therefore the smaller the errors introduced by such methods are. At this point we must recognize that  $\beta$  and  $r'B$  do not necessarily reflect the amount of water that leaks into the aquifer. In fact, both these parameters are directly proportional to  $r$ , which simply means that their magnitude in a given aquifer varies from nearly 0 at the pumping well to relatively large values further away from this well. Thus the extent to which leakage can affect the behavior of the drawdown in any given aquifer

a function of the radial distance from the pumping well. Thus the closer one is to this well, the smaller the deviations of drawdown from the Theis curve are. On the other hand, the rate of leakage is obviously greatest near the pumping well where the vertical gradients in the aquitard are largest and diminishes as the radial distance from this well increases. Therefore, in a given system,  $\beta$  and  $r'B$  increase with radial distance, whereas the actual rate of leakage decreases.

At first glance, we seem to be faced with a paradox: The greater the leakage is, the less the deviations from the nonleaky Theis solution are. However, a closer examination of the flow system will show that there is a simple physical explanation for this phenomenon. The reader will recognize that, although vertical gradients in the aquitard do not vary appreciably with radial distance from the pumping well, the same cannot be said about drawdown in a pumped aquifer. As a result the rate of leakage per unit area relative to this drawdown is negligibly

small in the immediate vicinity of the pumping well but becomes increasingly important at larger values of  $r$ . In addition, the water that leaks into the aquifer at smaller values of  $r$  tends to act as a buffer to the pressure transient. This transient cannot propagate as fast as it otherwise might have had there been no increase in aquifer storage. The effect is to reduce further the drawdown at points farther away from the pumping well. The net result is a situation in which larger values of  $r$  are associated with less leakage but also with greater deviations from the Theis curve.

Thus we arrive at the important conclusion that one can evaluate the transmissibility and storage coefficient of a leaky aquifer by using conventional methods of analysis based on the Theis solution. The errors introduced by these methods will be small if the data are collected close to the pumping well, but they may become significant when the observation well is placed too far away. Therefore a distance drawdown analysis based on the Theis curve is not generally applicable to leaky aquifers and should be avoided whenever possible.

Ideally, the values of  $T$  and  $S$  should be evaluated by using drawdown or buildup data from the pumping well itself because here the effect of leakage is always the smallest. We recommend this approach whenever the effective radius of the pumping well is known (e.g., wells in hard rock formations). However, when a well derives its water from unconsolidated materials, its effective radius usually remains unknown owing to the presence of a gravel pack. In these situations the approach above can still be used to evaluate  $T$  but cannot be used to determine  $S$ .

As a general rule, early drawdown data are affected by leakage to a lesser degree than data taken at a later time are. Therefore we feel that in performing the analysis most of the weight should be given to the earliest data available, if, of course, there is confidence in their reliability.

Once  $S$  and  $T$  have been determined, one can calculate the dimensionless time at any given radial distance from the pumping well by

$$t_D = \bar{T}t/Sr^2 \quad (8)$$

Equation 8 can then be used with the ratio method as we discussed earlier.

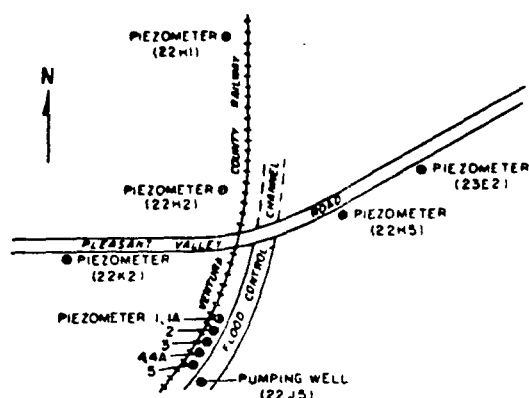


Fig. 4. The locations of the piezometers used in field pumping tests.

#### FIELD PUMPING TESTS IN THE OXNARD, CALIFORNIA, BASIN

The California Department of Water Resources had previously investigated the Oxnard basin in connection with seawater intrusion problems and constructed several wells at various locations in the basin. For our field studies we selected a particular location in the city of Oxnard where a large capacity pumping well (Figure 4, 22J5) was available to produce water from the Oxnard aquifer. Four additional piezometers (22H2, 22H5, 22K2, and 23E2) were available to monitor water levels in the Oxnard aquifer at radial distances of 502-1060 feet.

In addition, seven new piezometers were installed at various elevations relative to that of the Oxnard aquifer. Table 1 summarizes the vertical distances above or below the Oxnard for each piezometer and also gives the radial distances from pumping well 22J5. Ideally, the

seven piezometers should have been arranged along a circular arc with its center at the pumping well so that responses would be given at various elevations but at only one unique value of  $r$ . However, this arrangement was not possible under the local conditions, and we therefore had to design the well field according to the scheme shown in Figure 4. For details of the construction, the completion, and the development methods, the reader is referred to *California Department of Water Resources* [1971, pp. 63-68].

The following is a brief description of the lithology in the vicinity of the test area. The semipерched zone is composed of fine- to medium-grained sand with interbedded silty clay lenses. The upper aquitard is made up of predominantly silty and sandy clays, mainly montmorillonite. The Oxnard aquifer, which is the most important water producer in the Oxnard basin, is composed of fine- to coarse-grained sand and gravel. Silty clay with some interbedded sandy clay lenses makes up the lower aquitard. The material that forms the Mugu aquifer is fine- to coarse-grained sand and gravel with some interbedded silty clay. Figure 5 shows an electric log through this series of sediments.

#### ANALYSIS OF PUMPING TEST RESULTS

Two pumping tests were performed in the field. Their purpose was to determine the hydraulic characteristics of the Oxnard aquifer and the confining layers above and below it and to confirm our theoretical concepts [Neuman and Witherspoon, 1969a] regarding the response of multiple aquifer systems to pumping.

The first pumping test lasted 31 days. Figure 6 shows the response in the Oxnard aquifer at

TABLE 1. Location of Piezometers

Piezometer	Distance from 22J5, feet	Depth, feet	Vertical Distance*, feet	Layer
1	100	120	...	Oxnard aquifer
1A	100	239	...	Mugu aquifer
2	91	225	-26	lower aquitard
3	81	205	-6	lower aquitard
4	72	95	+11	upper aquitard
4A	72	58.5	+50	semipерched aquifer
5	62	84	+22	upper aquitard

\* The vertical distance is the distance above the top of the Oxnard aquifer at a depth of 105 feet or below the bottom at a depth of 198 feet.

† Failed to operate satisfactorily.

various radial distances from the pumping well. Piezometer 1, which is nearest to the pumping well, demonstrated an anomalous behavior during the first 6 min of pumping. This was apparently due to a surging effect in the pumping well. At about 6000 min the entire basin started experiencing a general drop in water levels probably due to the beginning of intermittent pumping for irrigation at this time of the year. Table 2 gives the values of  $T$  and  $S$  as calculated from these data by using Jacob's [1950] semi-logarithmic approach.

Table 2 shows that in general the values of  $T$  become progressively larger as  $r$  increases. This relationship can be explained as follows. Since the Oxnard aquifer is obviously leaky, the actual drawdown curve at any given well will lie below the Theis solution, as is shown diagrammatically in Figure 7. To demonstrate this positioning, we shall choose a particular point on the data curve that corresponds to some given value of  $s$  and  $t$ . If we could match the data to the true type curve where  $\beta$  and  $r/B$  are not 0, we would obtain the true value of  $s_D$  for the point chosen.

However, such type curves were not available for this investigation, and we used a method that is essentially equivalent to matching the field data to the Theis curve. Therefore the field data are being shifted upward from their true position, and our chosen point will now indicate an apparent value of  $s_D$ ,  $> s_D$ .

From the definition of  $s_D$  it is clear that since  $s$  remains unchanged the value of  $T$  is increased. The greater the radial distance  $r$ , the larger  $\beta$  and  $r/B$  become, and therefore the larger the difference between the true type curve and the Theis curve is. In other words, as  $r$  increases, the magnitude of  $T$  should become more and more exaggerated, which is clearly evident in Table 2.

With regard to errors in  $S$ , the shifting of field data as indicated on Figure 7 may be either to the left or to the right. Thus the effect on the calculated values of  $S$  is not predictable (Table 2). With this unpredictability in mind, we decided to select the results from piezometer 1 of  $T = 130,600$  gpd ft and  $S = 1.12 \times 10^{-4}$  as being most representative of the Oxnard aquifer, at least in the area of the pumping test.

Having estimated the properties of the pumped aquifer, we shall now consider the results from other parts of this three-aquifer

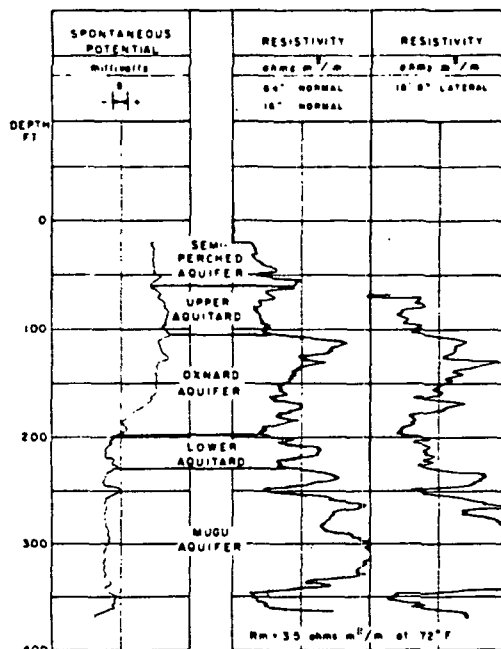


Fig. 5. The electric log from the first exploratory hole.

subsystem. Figure 8 shows the response at one particular point in the lower aquitard (well 3) as well as the responses in the Oxnard above (well 1) and the Mugu below (well 1A). Figure 9 shows the response at two different elevations in the upper aquitard (wells 4 and 5) as well as the response in the overlying semiperched aquifer (well 4A). Since piezometer 1 is located farthest from the pumping well, we do not have the response in the pumped aquifer directly below the piezometers where drawdowns in the upper aquitard were measured. However, from distance-drawdown curves in the Oxnard aquifer and from the behavior of piezometer 4, we concluded that the aquifer response was approximately as shown by the dashed curve in Figure 9. Remember that the ratio method for evaluating aquitards is more sensitive to the time lag than to the actual magnitude of drawdown in the aquifer. Therefore the dashed curve in Figure 9 can be considered sufficiently accurate for our purposes. Note that the shapes of the curves in Figures 8 and 9 are quite similar to those of our theoretical curves [Neuman and Witherspoon, 1969a].

To evaluate the lower aquitard, we shall determine the ratio  $s'/s$  at two early values of



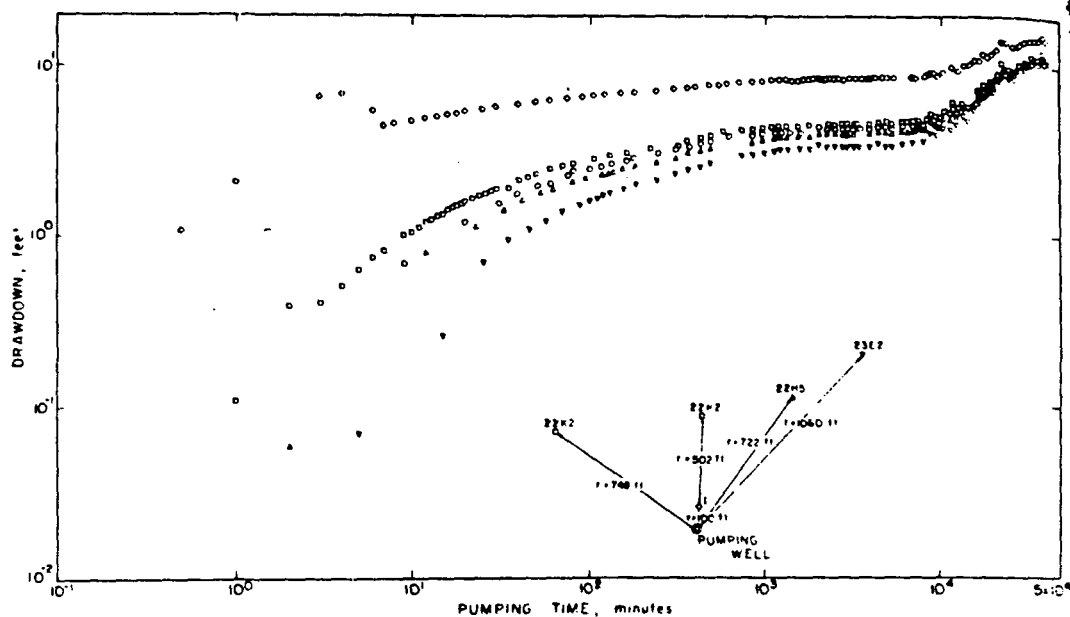


Fig. 6. The fluid levels in the Oxnard piezometers during the first pumping test. The diamonds represent well 1, the squares represent well 22H2, the triangles represent well 22H5, the circles represent well 22K2, and the inverted triangles represent well 23E2.

time,  $t = 80$  min and  $t = 200$  min. At  $t = 80$  min, one can read on Figure 8 that  $s' = 0.078$  and  $s = 6.6$  feet. The ratio is simply  $s'/s = 0.078/6.6 = 1.18 \times 10^{-2}$ . To obtain  $t_D$ , one can use the equation

$$t_D = 9.28 \times 10^{-5} T t / r^2 S \quad (9)$$

where  $T$  is in gallons per day per foot,  $t$  is in minutes, and  $r$  is in feet. Then, using the known values of  $T$  and  $S$  and noting from Table 1 that, at piezometer 3,  $r = 81$  feet, one can calculate

$$t_D = \frac{(9.28 \times 10^{-5})(130,600)(80)}{(81)^2(1.12 \times 10^{-4})} = 1.32 \times 10^3$$

TABLE 2. Results of Oxnard Aquifer Using Jacob's Semilog Method

Well	$r$ , feet	$T$ , gpd/ft	$S$
1	100	130,600	$1.12 \times 10^{-4}$
22H2	502	139,000	$3.22 \times 10^{-4}$
22H5	722	142,600	$3.08 \times 10^{-4}$
22K2	748	136,700	$2.48 \times 10^{-4}$
23E2	1060	157,000	$2.53 \times 10^{-4}$

Referring to Figure 3, one finds that these values of  $s'/s$  and  $t_D$  correspond to  $t_D' = 0.086$ . From the definition of  $t_D'$ , one can verify the formula

$$\alpha' = 1.077 \times 10^4 t_D' z^2 / t \quad (10)$$

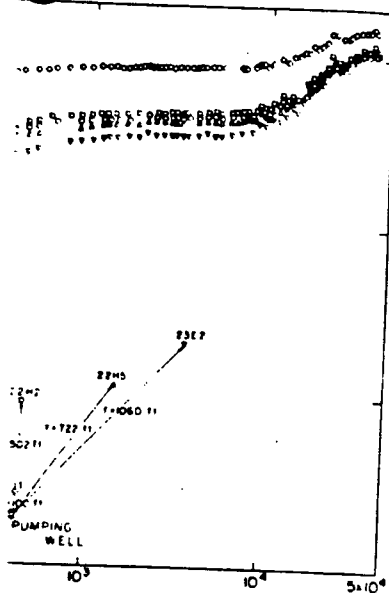
where  $\alpha'$  is in gallons per day per foot,  $z$  is in feet, and  $t$  is in minutes. One notes from Table 1 that, for piezometer 3,  $z = 6$  feet, and therefore

$$\alpha' = \frac{(1.077 \times 10^4)(0.086)(6)^2}{(80)} = 4.17 \times 10^2 \text{ gpd/ft}$$

Similarly, one finds that, at  $t = 200$  min,  $\alpha' = 3.39 \times 10^2$  gpd/ft. Since the method gives more reliable results when  $t$  is small, we adopted  $\alpha' = 4.17 \times 10^2$  gpd/ft as the representative value for the top 6 feet of the lower aquitard. The results of similar calculations for both aquitards are summarized in Table 3. Note that the diffusivity of the Oxnard aquifer is

$$\alpha = \frac{T}{S} = \frac{130,600}{1.12 \times 10^{-4}} = 1.17 \times 10^9 \text{ gpd/ft}$$

which is more than 1 million times the values obtained for the aquitards.



ing the first pumping test. The triangles represent well 22H5, present well 23E2.

Figure 3, one finds that these values correspond to  $t_D' = 0.086$ . From  $t_D'$ , one can verify the formula

$$= 1.077 \times 10^4 t_D' z^2 / t \quad (10)$$

gallons per day per foot,  $z$  is in feet. One notes from Table 1 meter 3,  $z = 6$  feet, and therefore

$$\frac{\times 10^4 (0.086) (6)^2}{(80)}$$

$$= 4.17 \times 10^2 \text{ gpd/ft}$$

finds that, at  $t = 200$  min,  $\alpha' = 1$  ft. Since the method gives more when  $t$  is small, we adopted  $\alpha' = 1$  ft as the representative value of the lower aquitard. The calculations for both aquitards are in Table 3. Note that the diffusive aquifer is

$$\frac{30,600}{\times 10^{-4}} = 1.17 \times 10^9 \text{ gpd/ft}$$

than 1 million times the values of aquitards.

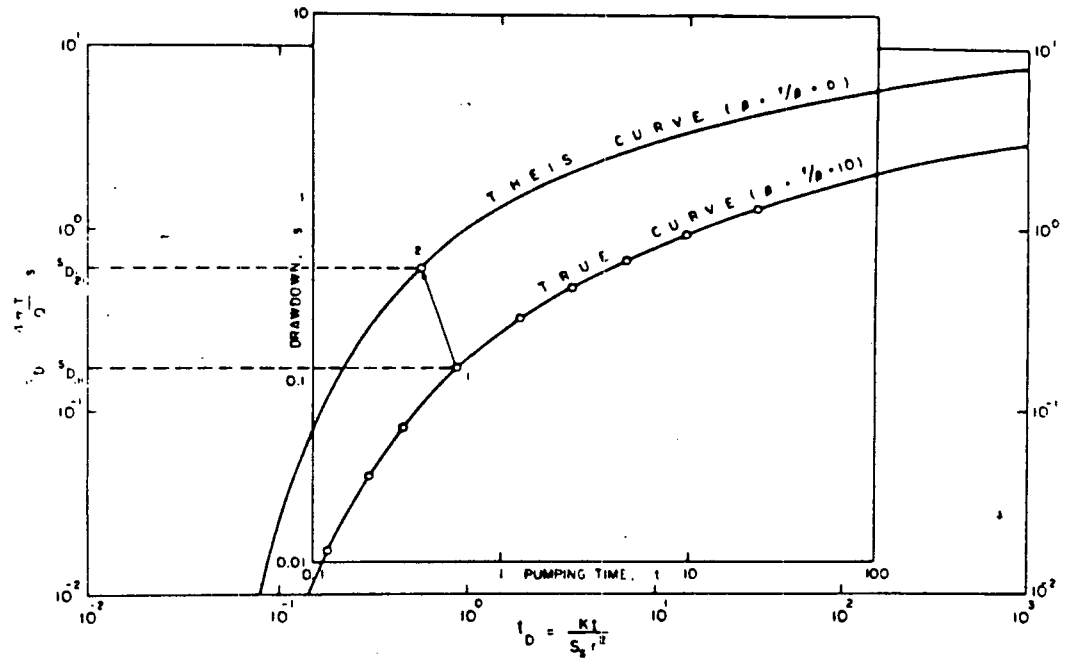


Fig. 7. A comparison of hypothetical field data with leaky and nonleaky type curves.

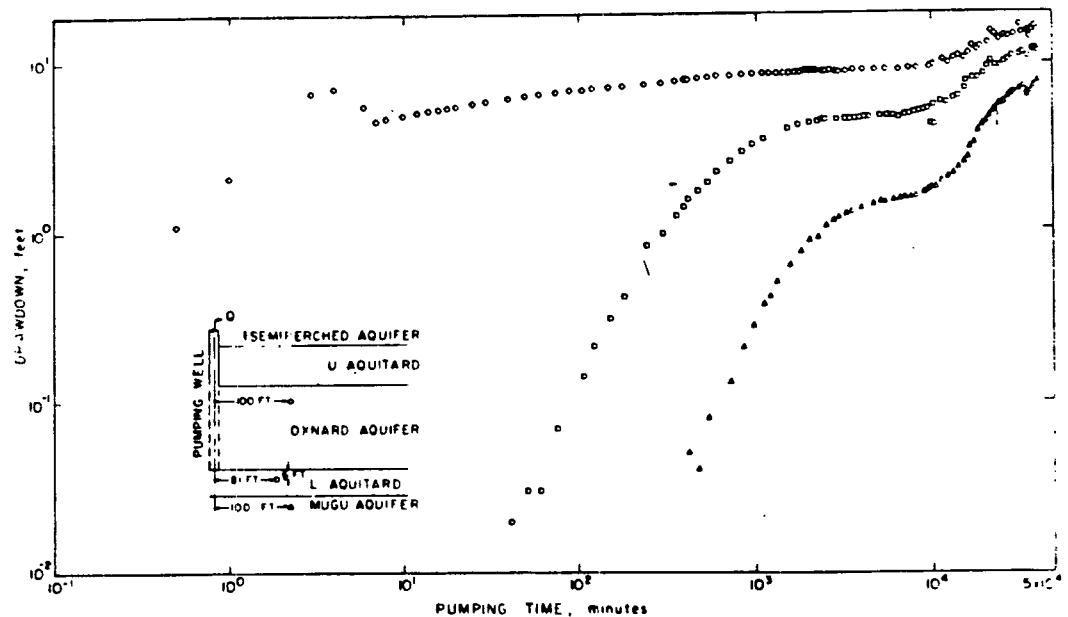


Fig. 8. The response of the piezometers in the lower aquitard (well 3, squares) to that in the Oxnard (well 1, diamonds) and Mugu (well 1A, triangles) aquifers during the first pumping test.

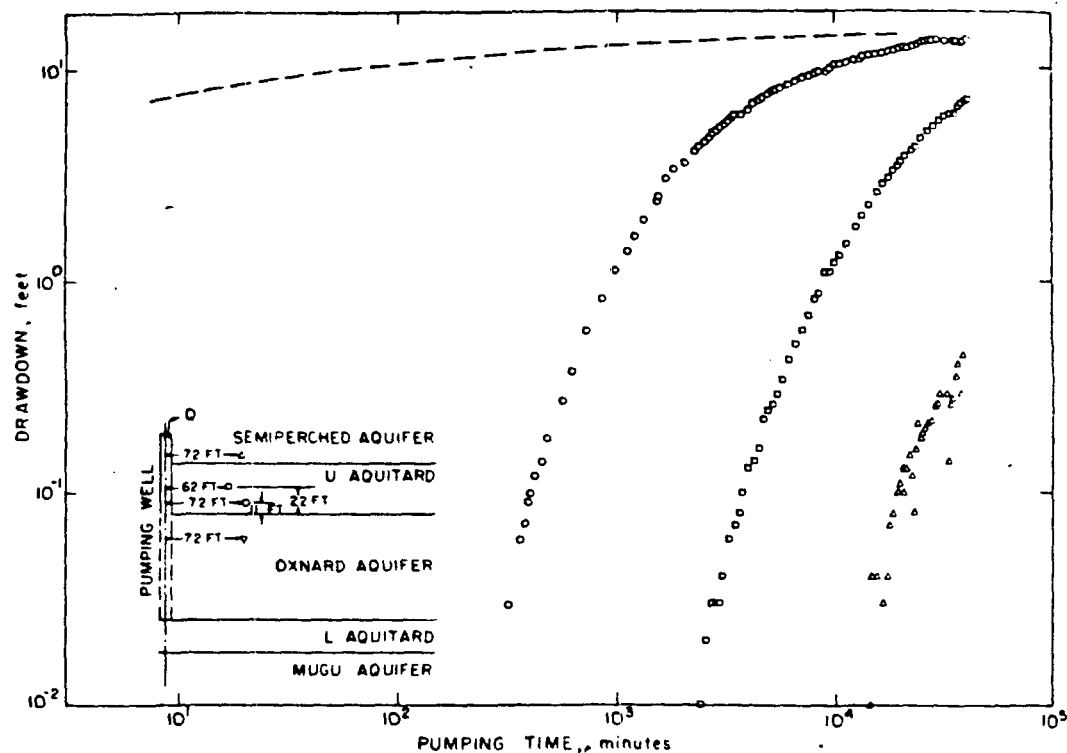


Fig. 9. The response of the piezometers in the upper aquitard (well 4, circles, and well 5, squares) and the semiperched aquifer (well 4A, triangles) during the first pumping test. The broken line indicates the probable response of the Oxnard aquifer at  $r = 72$  feet.

The results of the second pumping test were essentially the same as those of the first test and will therefore not be presented here.

#### DETERMINATION OF AQUITARD PROPERTIES USING FIELD AND LABORATORY RESULTS

Having determined the hydraulic diffusivities, we can evaluate the permeability  $K'$  of each aquitard if the storage factor is known. The values of  $S_s'$  were calculated from consolidation

tests performed in the laboratory [California Department of Water Resources, 1971, pp. 106-110] by using the formula

$$S_s' = a_v \gamma_w / (1 + e) \quad (11)$$

These values were then used to calculate  $K'$  according to

$$K' = \alpha' S_s' \quad (12)$$

and the results are summarized in Table 4.

Direct measurements performed on undisturbed samples in the laboratory indicated that the aquitard permeabilities vary within a range of at least 3 orders of magnitude. The results in Table 4 fall on the high side of this range and thus are an indication that the average permeability in the field cannot always be reliably estimated from laboratory measurements.

It is interesting to compare the specific storage and permeability of the aquitard with those of the Oxnard aquifer. Using an aquifer thickness

TABLE 3. Results for Hydraulic Diffusivity of Aquitards from First Pumping Test

Layer	Section Tested	$K'/S_s'$ , gpd/ft	$K'/S_s'$ , cm <sup>2</sup> /sec
Upper aquitard	bottom 22 feet	$1.02 \times 10^2$	$1.47 \times 10^{-1}$
Upper aquitard	bottom 11 feet	$2.44 \times 10^2$	$3.51 \times 10^{-1}$
Lower aquitard	top 6 feet	$4.17 \times 10^2$	$5.99 \times 10^{-1}$

TABLE 4. Hydraulic Properties of Aquitard Layers

Layer	Section Tested	Specific Storage $S_s'$		Permeability $K'$	
		cm <sup>-1</sup>	ft <sup>-1</sup>	cm/sec	gpd/ft <sup>2</sup>
Upper aquitard	bottom 21 feet	$7.88 \times 10^{-6}$	$2.4 \times 10^{-4}$	$1.11 \times 10^{-6}$	$2.45 \times 10^{-2}$
Upper aquitard	bottom 11 feet	$7.88 \times 10^{-6}$	$2.4 \times 10^{-4}$	$2.66 \times 10^{-6}$	$5.85 \times 10^{-2}$
Lower aquitard	top 6 feet	$3.28 \times 10^{-6}$	$1.0 \times 10^{-4}$	$1.89 \times 10^{-6}$	$4.17 \times 10^{-2}$

of 93 feet, one has

$$K = \frac{T}{b} = \frac{130,600}{93} = 1405 \text{ gpd/ft}^2$$

and

$$s = \frac{S}{b} = \frac{1.12 \times 10^{-4}}{93} = 1.20 \times 10^{-6} \text{ ft}^{-1}$$

Thus the permeability of the aquifer exceeds that of the aquitards by more than 4 orders of magnitude. However, note that the specific storage of the aquifer is less than  $S_s'$  in the aquitards above and below by 2 orders of magnitude. In other words, for the same change in head a unit volume of aquitard material can contribute about 100 times more water from storage than a similar volume of the aquifer can. This statistic confirms our belief that storage in the aquitards must be considered when one deals with leaky aquifer systems.

## NOTATION

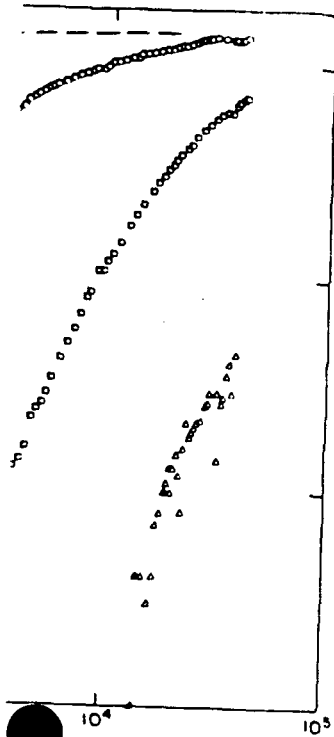
- $\alpha_c$ , coefficient of compressibility, equal to  $-\Delta_c/\Delta p$ ,  $LT^2M^{-1}$ ;  
 $b_i$ , thickness of  $i$ th aquifer,  $L$ ;  
 $b_j'$ , thickness of  $j$ th aquitard,  $L$ ;  
 $c$ , void ratio;  
 $K_i$ , permeability of  $i$ th aquifer,  $LT^{-1}$ ;  
 $K_j'$ , permeability of  $j$ th aquitard,  $LT^{-1}$ ;  
 $p$ , pressure,  $ML^{-1}T^{-2}$ ;  
 $Q_i$ , pumping rate from  $i$ th aquifer,  $L^3T^{-1}$ ;  
 $r$ , radial distance from pumping well,  $L$ ;  
 $r/B_{ij}$ , dimensionless leakage parameter, equal to  $r(K_i'/K_j b_i b_j')^{1/2}$ ;  
 $s_D$ , dimensionless drawdown, equal to  $4\pi T_i s/Q_i$ ;  
 $s_i$ , drawdown in  $i$ th aquifer,  $L$ ;  
 $s_j'$ , drawdown in  $j$ th aquitard,  $L$ ;  
 $S_i$ , storage coefficient of  $i$ th aquifer, equal to  $S_s b_i$ ;  
 $S_{s,i}$ , specific storage of  $i$ th aquifer,  $L^{-1}$ ;  
 $S_{s,j}'$ , specific storage of  $j$ th aquitard,  $L^{-1}$ ;  
 $t$ , pumping time,  $T$ ;

- $t_{D,i}$ , dimensionless time for pumped  $i$ th aquifer, equal to  $K_i t/S_{s,i} r^2$ ;  
 $t_{D,j}'$ , dimensionless time for  $j$ th aquitard, equal to  $K_j' t/S_{s,j}' z^2$ ;  
 $T_i$ , transmissibility of  $i$ th aquifer, equal to  $K_i b_i$ ,  $L^2T^{-1}$ ;  
 $z$ , vertical coordinate,  $L$ ;  
 $\alpha_i$ , hydraulic diffusivity of  $i$ th aquifer, equal to  $K_i/S_{s,i}$ ,  $L^2T^{-1}$ ;  
 $\alpha_j'$ , hydraulic diffusivity of  $j$ th aquitard, equal to  $K_j'/S_{s,j}'$ ,  $L^2T^{-1}$ ;  
 $\beta_{ij}$ , dimensionless leakage parameter, equal to  $r/4b_i(K_i'/S_{s,j}'/K_j b_j')^{1/2}$ ;  
 $\gamma_w$ , specific weight of water,  $ML^{-2}T^{-2}$ .

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well 4, circles, and well 5, triangles, at first pumping test. The data are at  $r = 72$  feet.

the laboratory [California Department of Water Resources, 1971, pp. 106-107].

$$s = \alpha_c \gamma_w / (1 + c) \quad (11)$$

then used to calculate  $K'$

$$S_s' = \alpha' S_s \quad (12)$$

summarized in Table 4.

Experiments performed on undischargeable laboratory indicated that permeabilities vary within a range of 2 orders of magnitude. The results are on the high side of this range and cannot always be reliably compared with laboratory measurements.

To compare the specific storage of the aquitard with those of the aquifer, one uses the formula

Using an aquifer thickness

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(Manuscript received April 20, 1972;  
revised May 5, 1972.)

Appendix 18

REI 10-1 Run #1 Pumping Test Data Sheets

PEI 10-1 LTD PEI 10-1 F-10-1  
Run 1  
09/15/86

SECURE DATA  
constant rate test

TRANSDUCER TABLE

Input (1) PEI 10-1  
Transducer s/n: 139  
Scale factor: 49.53  
Initial level: 81.73 feet

FAST DATA

Input (2) GW-25  
Transducer s/n: 1857/858  
Scale factor: 50.4  
Initial level: 82.22 feet

Input (3) NONE  
Transducer s/n: NONE  
Scale factor: 1

Input (4) PEI 3-4  
Transducer s/n: 1504/854  
Scale factor: 10.03  
Initial level: 81.18 feet

Input (5) PEI-7  
Transducer s/n: 1366/851  
Scale factor: 10.03  
Initial level: 80.77 feet

Input (6) F-10-2  
Transducer s/n: 1634/857  
Scale factor: 10.08  
Initial level: 46.07 feet

Input (7) F-10-3  
Transducer s/n: 1518/854  
Scale factor: 10.06  
Initial level: 40.09 feet

Input (8) F-10-4  
Transducer s/n: 2344/85N  
Scale factor: 10.13  
Initial level: 38.82 feet

Input (9) PEI 10-2  
Transducer s/n: 516/830  
Scale factor: 10.04  
Initial level: 5.68 feet

Input (10) PEI 10-7  
Transducer s/n: 596/841  
Scale factor: 10.03  
Initial level: 7.03 feet

Input (11) PEI 10-4  
Transducer s/n: 1272/84N  
Scale factor: 10.05  
Initial level: 7.52 feet

Input (12) PEI-11  
Transducer s/n: 1076/849  
Scale factor: 10.07  
Initial level: 78.78 feet

# CALCULATIONS AND COMPUTATIONS

SHEET      OF     

PROJECT: FRENCH LTD REI 10-4 Run #1

JOB NO.: 225-14

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY:      DATE: 9-15

CHECKED BY:      DATE:     

Begin pumping at 1300(9-15-86)

FLOW RATE GPM	TIME (2400)	MONITORS INITIALS	FLOW RATE	TIME (2400)	MONITORS INITIALS
20.0	13:00:35	CWA	19.9	17:54	DRG
20.1	13:01	CWA	20.1	17:58	DRG
20.0	13:03	CWA	19.9	18:24	DRG
20.1	13:05	BMB	20.3	18:30	DRG
20.0	13:10	BMB	20.1	18:31	DRG
20.0	13:15	BMB	20.0	19:00	ARI
20.0	13:20	BMB	19.9	19:24	DRG
20.0	13:30	BMB	19.8	19:34	DRG
19.9	13:45	J.A.	20.0	19:35	DRG
20.0	14:00	J.A.	20.0	19:50	ARI
20.0	14:15	BMB	19.8	20:34	DRG
20.0	14:30	BMB	20.1	20:35	DRG
20.0	14:35	PCM	19.8	21:10	DRG
20.8	14:47	PCM	19.9	21:38	DRG
20.1	14:51	PCM	20.0	21:44	DRG
20.0	15:00	J.A.	19.7	22:17	DRG
20.0	15:15	BMB	20.0	22:18	DRG
19.9	15:32	J.A.	19.8	22:28	DRG
20.0	15:35	DG	20.1	22:52	DRG
20.3	15:46	DG	19.6	23:36	DRG
20.1	15:51	DG	19.9	23:38	DRG
19.8	15:57	ARI	19.5	00:54	SC
19.9	16:24	ARI	19.7	00:12	SC
19.9	16:40	ARI	19.1	02:07	SC
19.9	17:14	DRG	19.0	300	SC
19.8	17:28	DRG	18.6	335	SC
20.0	17:34	DRG	18.0	400	SC
19.9-20.9	17:41	PCM			

rechecked  
10-20-86  
to 20.0  
PCM

10-20  
10-20

30-60

**REI**



SHEET \_\_\_\_ OF \_\_\_\_

JOB NO.: \_\_\_\_\_

COMPUTED BY: \_\_\_\_\_ DATE: 6-16

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

# AREN

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: \_\_\_\_\_

JOB NO.: \_\_\_\_\_

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

9-16-86

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

FLOW RATE	TIME (2400)	MONITORS INITIALS		FLOW RATE	TIME (2400)	MONITORS INITIALS
14.7	845	BMB		14.5	1430	BMB
14.5	900	BMB		14.5	1445	BMB
14.3	915	BMB		14.5	1500	BMB
14.4	930	BMB		14.7	1515	BMB
14.4	945	BMB		14.6	1539	DRG
14.8	1000	BMB		14.7	1552	D.W.D
14.9	1015	BMB		14.6	16100	A.T.
15.2	1030	BMB	Δ-51.79'	14.7	16220	A.T.
15.4	1042	BMB				
12.0	1045	BMB				
12.1	1100	BMB	Δ-40.88'			
12.1	1115	BMB				
12.2	1130	BMB				
12.0	1145	BMB				
12.0	1200	BMB	Δ-35.00			
12.0	1215	BMB	At 1303 increase flow to 12.5gpm as per Dave Dorrance.			
12.2	1230	BMB				
12.0	1245	BMB				
12.0	1300	BMB				
12.5	1303	BMB				
13.0	1312	BMB				
13.0	1315	BMB				
13.5	1320	BMB				
13.5	1330	BMB				
14.0	1330	BMB				
14.0	1345	BMB				
14.0	1400	BMB				
14.5	1415	BMB				

At 1043 reduced flow to 12 gpm, as per P. Mann. Pumping well recovered ~ 14' and appears to be stable at Δ-40.87 at 1058. Will maintain flow at 12gpm

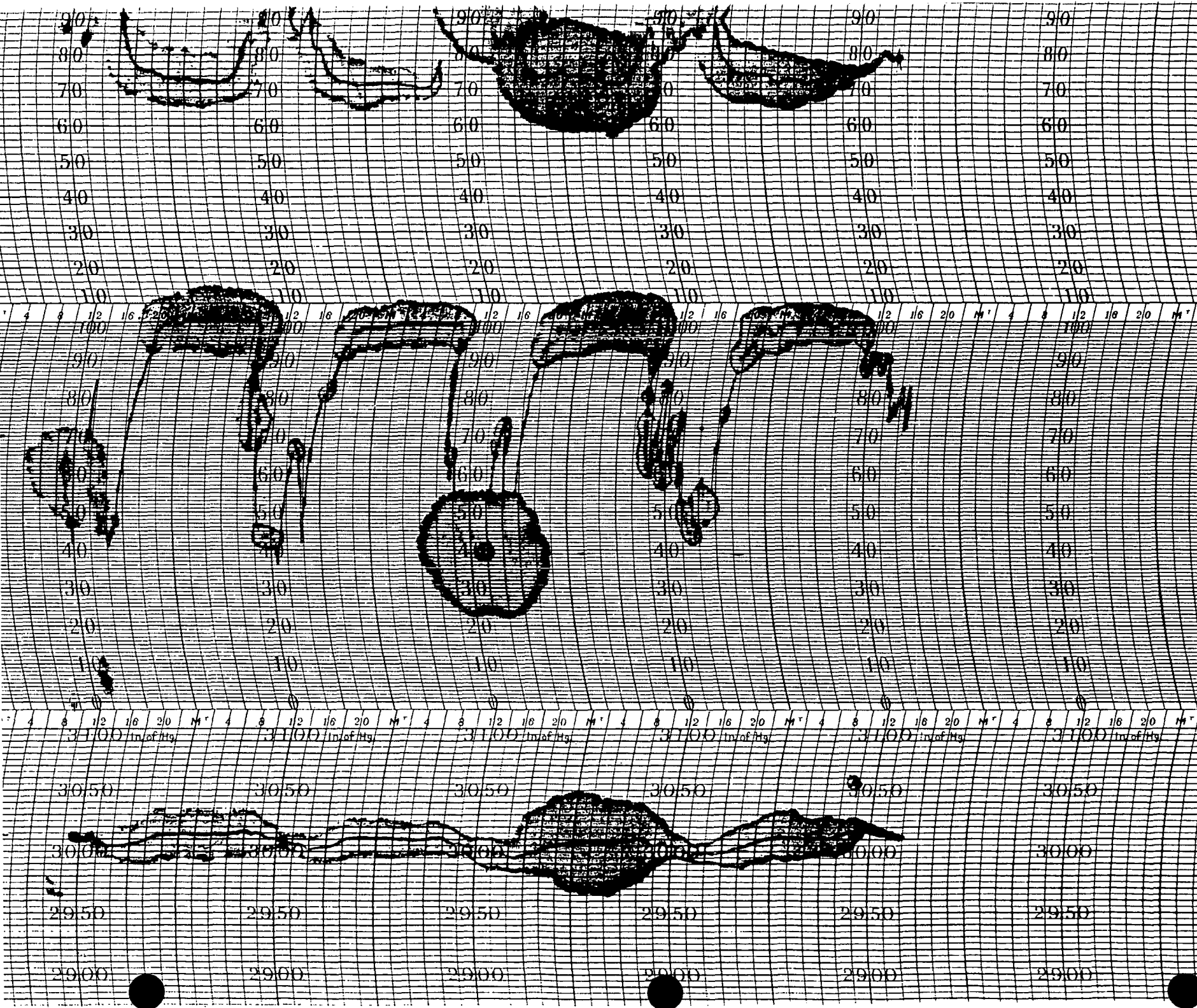
At 1303 increase flow to 12.5gpm as per Dave Dorrance.

**REI**

STATION .....

DATE ON 9-15-86

DATE OFF 9-19-86



PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: REI 10-1 INPUT 1  
 RADIUS: 0.166 FEET  
 START DATE: 15-Sep-86  
 START TIME: 13:00  
 WATER START LEVEL: 81.72 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
13:00	0.000	81.72	0.00	0.00E+00
13:00	0.017	85.92	-4.20	4.28E-04
13:00	0.034	88.15	-6.43	8.57E-04
13:00	0.050	82.53	-0.81	1.26E-03
13:00	0.067	90.27	-8.55	1.69E-03
13:00	0.084	91.43	-9.71	2.12E-03
13:00	0.100	90.74	-9.02	2.52E-03
13:00	0.117	91.03	-9.31	2.95E-03
13:00	0.134	91.10	-9.38	3.38E-03
13:00	0.150	91.04	-9.32	3.78E-03
13:00	0.167	91.54	-9.82	4.21E-03
13:00	0.257	94.20	-12.48	6.48E-03
13:00	0.340	96.32	-14.60	8.57E-03
13:00	0.424	97.98	-16.26	1.07E-02
13:00	0.507	99.19	-17.47	1.28E-02
13:00	0.590	100.42	-18.70	1.49E-02
13:00	0.674	101.48	-19.76	1.70E-02
13:00	0.757	102.35	-20.63	1.91E-02
13:00	0.840	103.12	-21.40	2.12E-02
13:00	0.924	103.98	-22.26	2.33E-02
13:01	1.007	104.86	-23.14	2.54E-02
13:01	1.417	107.93	-26.21	3.57E-02
13:01	1.750	109.30	-27.58	4.41E-02
13:02	2.084	110.53	-28.81	5.25E-02
13:02	2.417	111.40	-29.68	6.09E-02
13:02	2.750	112.00	-30.28	6.93E-02
13:03	3.084	112.48	-30.76	7.77E-02
13:03	3.417	112.90	-31.18	8.61E-02
13:03	3.750	113.39	-31.67	9.45E-02
13:04	4.084	113.73	-32.01	1.03E-01
13:04	4.417	114.09	-32.37	1.11E-01
13:04	4.750	114.31	-32.59	1.20E-01
13:05	5.084	114.44	-32.72	1.28E-01
13:05	5.417	114.69	-32.97	1.37E-01
13:05	5.750	114.78	-33.06	1.45E-01
13:06	6.084	115.08	-33.36	1.53E-01
13:06	6.417	115.13	-33.41	1.62E-01
13:06	6.750	115.41	-33.69	1.70E-01
13:07	7.084	115.58	-33.86	1.79E-01
13:07	7.417	115.61	-33.89	1.87E-01

13:07	7.750	115.63	-33.91	1.95E-01
13:08	8.084	115.71	-33.99	2.04E-01
13:08	8.417	115.71	-33.99	2.12E-01
13:08	8.750	115.75	-34.03	2.21E-01
13:09	9.084	115.92	-34.20	2.29E-01
13:09	9.417	115.98	-34.26	2.37E-01
13:09	9.750	115.96	-34.24	2.46E-01
13:10	10.084	116.12	-34.40	2.54E-01
13:12	12.101	116.45	-34.73	3.05E-01
13:14	14.188	116.77	-35.05	3.58E-01
13:16	16.139	117.02	-35.30	4.07E-01
13:18	18.237	117.31	-35.59	4.60E-01
13:20	20.233	117.60	-35.88	5.10E-01
13:22	22.233	117.69	-35.97	5.60E-01
13:24	24.233	117.99	-36.27	6.11E-01
13:26	26.233	118.18	-36.46	6.61E-01
13:28	28.233	118.41	-36.69	7.12E-01
13:30	30.233	118.68	-36.96	7.62E-01
13:32	32.152	118.72	-37.00	8.10E-01
13:34	34.620	119.01	-37.29	8.72E-01
13:36	36.095	119.08	-37.36	9.10E-01
13:38	38.095	119.11	-37.39	9.60E-01
13:40	40.095	119.37	-37.65	1.01E+00
13:42	42.195	119.42	-37.70	1.06E+00
13:44	44.232	119.48	-37.76	1.11E+00
13:46	46.232	119.64	-37.92	1.17E+00
13:48	48.252	119.74	-38.02	1.22E+00
13:50	50.122	119.90	-38.18	1.26E+00
13:52	52.122	119.97	-38.25	1.31E+00
13:54	54.122	120.00	-38.28	1.36E+00
13:56	56.122	120.17	-38.45	1.41E+00
13:58	58.122	120.28	-38.56	1.46E+00
14:00	60.122	121.10	-39.38	1.52E+00
14:02	62.122	121.43	-39.71	1.57E+00
14:04	64.122	121.64	-39.92	1.62E+00
14:06	66.442	121.94	-40.22	1.67E+00
14:08	68.122	122.21	-40.49	1.72E+00
14:10	70.335	122.44	-40.72	1.77E+00
14:12	72.160	122.76	-41.04	1.82E+00
14:14	74.160	123.51	-41.79	1.87E+00
14:16	76.167	123.81	-42.09	1.92E+00
14:18	78.230	123.92	-42.20	1.97E+00
14:20	80.217	124.46	-42.74	2.02E+00
14:22	82.213	124.84	-43.12	2.07E+00
14:24	84.213	124.97	-43.25	2.12E+00
14:26	86.213	125.10	-43.38	2.17E+00
14:28	88.213	124.52	-42.80	2.22E+00
14:30	90.213	124.22	-42.50	2.27E+00
14:32	92.213	124.20	-42.48	2.32E+00
14:34	94.213	123.83	-42.11	2.37E+00
14:36	96.213	123.72	-42.00	2.42E+00
14:38	98.238	123.59	-41.87	2.48E+00
15:00	120.220	122.04	-40.32	3.03E+00
15:20	140.130	121.51	-39.79	3.53E+00
15:40	160.130	121.96	-40.24	4.04E+00
16:00	180.370	120.64	-38.92	4.55E+00

16:20	200.200	120.73	-39.01	5.05E+00
16:40	220.200	120.77	-39.05	5.55E+00
17:00	240.080	120.87	-39.15	6.05E+00
17:20	260.220	121.24	-39.52	6.56E+00
17:40	280.150	121.43	-39.71	7.06E+00
18:00	300.150	121.73	-40.01	7.56E+00
18:20	320.130	121.67	-39.95	8.07E+00
18:40	340.220	122.23	-40.51	8.57E+00
19:00	360.180	122.20	-40.48	9.08E+00
19:20	380.220	122.34	-40.62	9.58E+00
19:40	400.220	122.66	-40.94	1.01E+01
20:00	420.220	122.73	-41.01	1.06E+01
20:20	440.220	123.00	-41.28	1.11E+01
20:40	460.220	123.59	-41.87	1.16E+01
21:00	480.120	123.79	-42.07	1.21E+01
21:20	500.220	124.24	-42.52	1.26E+01
21:40	520.320	124.41	-42.69	1.31E+01
22:00	540.200	125.62	-43.90	1.36E+01
22:20	560.100	125.90	-44.18	1.41E+01
22:40	580.100	126.64	-44.92	1.46E+01
23:00	600.150	127.25	-45.53	1.51E+01
23:20	620.150	127.60	-45.88	1.56E+01
23:40	640.180	128.32	-46.60	1.61E+01
00:00	660.180	128.61	-46.89	1.66E+01
00:20	680.180	129.38	-47.66	1.71E+01
00:40	700.180	129.26	-47.54	1.76E+01
01:00	720.180	130.71	-48.99	1.81E+01
01:20	740.180	131.74	-50.02	1.87E+01
01:40	760.180	131.52	-49.80	1.92E+01
02:00	780.180	131.31	-49.59	1.97E+01
02:20	800.180	131.48	-49.76	2.02E+01
02:40	820.180	131.91	-50.19	2.07E+01
03:00	840.180	132.15	-50.43	2.12E+01
03:20	860.180	131.92	-50.20	2.17E+01
03:40	880.180	131.36	-49.64	2.22E+01
04:00	900.180	131.49	-49.77	2.27E+01
04:20	920.180	131.64	-49.92	2.32E+01
04:40	940.180	131.75	-50.03	2.37E+01
05:00	960.180	131.98	-50.26	2.42E+01
05:20	980.180	132.07	-50.35	2.47E+01
05:40	1000.200	132.18	-50.46	2.52E+01
06:40	1060.400	132.45	-50.73	2.67E+01
07:40	1120.500	132.67	-50.95	2.82E+01
08:40	1180.300	132.94	-51.22	2.97E+01
09:40	1240.300	133.12	-51.40	3.13E+01
10:40	1300.200	133.44	-51.72	3.28E+01
11:40	1360.300	119.83	-38.11	3.43E+01
12:40	1420.300	115.81	-34.09	3.58E+01
13:40	1480.200	117.78	-36.06	3.73E+01
14:40	1540.300	117.74	-36.02	3.88E+01
15:40	1600.300	118.22	-36.50	4.03E+01
16:30	1650.600	105.33	-23.61	4.16E+01

TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 10-1 INPUT 1  
 RADIUS: 0.166 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 81.72 FEET  
 WATER STOP LEVEL: 105.33 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)	t/r2	t/t'
16:30	0.017	103.91	1.42	22.19	4.28E-04	9.71E+04
16:30	0.034	103.70	1.63	21.98	8.57E-04	4.85E+04
16:30	0.050	103.48	1.85	21.76	1.26E-03	3.30E+04
16:30	0.067	103.28	2.05	21.56	1.69E-03	2.46E+04
16:30	0.084	103.07	2.26	21.35	2.12E-03	1.97E+04
16:30	0.100	102.88	2.45	21.16	2.52E-03	1.65E+04
16:30	0.117	102.68	2.65	20.96	2.95E-03	1.41E+04
16:30	0.134	102.48	2.85	20.76	3.38E-03	1.23E+04
16:30	0.150	102.30	3.03	20.58	3.78E-03	1.10E+04
16:30	0.167	102.10	3.23	20.38	4.21E-03	9.88E+03
16:30	0.257	101.11	4.22	19.39	6.48E-03	6.42E+03
16:30	0.340	100.28	5.05	18.56	8.57E-03	4.86E+03
16:30	0.424	99.52	5.81	17.80	1.07E-02	3.89E+03
16:30	0.507	98.82	6.51	17.10	1.28E-02	3.26E+03
16:30	0.591	98.18	7.15	16.46	1.49E-02	2.79E+03
16:30	0.674	97.59	7.74	15.87	1.70E-02	2.45E+03
16:30	0.757	97.03	8.30	15.31	1.91E-02	2.18E+03
16:30	0.840	96.53	8.80	14.81	2.12E-02	1.97E+03
16:30	0.924	96.06	9.27	14.34	2.33E-02	1.79E+03
16:31	1.007	95.62	9.71	13.90	2.54E-02	1.64E+03
16:31	1.417	93.96	11.37	12.24	3.57E-02	1.17E+03
16:31	1.751	93.00	12.33	11.28	4.41E-02	9.44E+02
16:32	2.084	92.32	13.01	10.60	5.25E-02	7.93E+02
16:32	2.417	91.80	13.53	10.08	6.09E-02	6.84E+02
16:32	2.751	91.43	13.90	9.71	6.93E-02	6.01E+02
16:33	3.084	91.13	14.20	9.41	7.77E-02	5.36E+02
16:33	3.417	90.91	14.42	9.19	8.61E-02	4.84E+02
16:33	3.751	90.74	14.59	9.02	9.45E-02	4.41E+02
16:34	4.084	90.60	14.73	8.88	1.03E-01	4.05E+02
16:34	4.417	90.50	14.83	8.78	1.11E-01	3.75E+02
16:34	4.751	90.40	14.93	8.68	1.20E-01	3.48E+02
16:35	5.084	90.31	15.02	8.59	1.28E-01	3.26E+02
16:35	5.417	90.26	15.07	8.54	1.37E-01	3.06E+02
16:35	5.751	90.18	15.15	8.46	1.45E-01	2.88E+02
16:36	6.084	90.14	15.19	8.42	1.53E-01	2.72E+02
16:36	6.417	90.10	15.23	8.38	1.62E-01	2.58E+02
16:36	6.751	90.06	15.27	8.34	1.70E-01	2.45E+02
16:37	7.084	90.01	15.32	8.29	1.79E-01	2.34E+02
16:37	7.417	89.97	15.36	8.25	1.87E-01	2.24E+02
16:37	7.751	89.94	15.39	8.22	1.95E-01	2.14E+02
16:38	8.084	89.90	15.43	8.18	2.04E-01	2.05E+02
16:38	8.417	89.87	15.46	8.15	2.12E-01	1.97E+02

16:38	8.751	89.84	15.49	8.12	2.21E-01	1.90E+02
16:39	9.084	89.81	15.52	8.09	2.29E-01	1.83E+02
16:39	9.417	89.78	15.55	8.06	2.37E-01	1.76E+02
16:39	9.751	89.76	15.57	8.04	2.46E-01	1.70E+02
16:40	10.084	89.73	15.60	8.01	2.54E-01	1.65E+02
16:42	12.120	89.60	15.73	7.88	3.05E-01	1.37E+02
16:44	14.120	89.48	15.85	7.76	3.56E-01	1.18E+02
16:46	16.120	89.38	15.95	7.66	4.06E-01	1.03E+02
16:48	18.120	89.30	16.03	7.58	4.57E-01	9.21E+01
16:50	20.142	89.23	16.10	7.51	5.08E-01	8.29E+01
16:52	22.225	89.17	16.16	7.45	5.60E-01	7.53E+01
16:54	24.225	89.10	16.23	7.38	6.10E-01	6.91E+01
16:56	26.225	89.04	16.29	7.32	6.61E-01	6.39E+01
16:58	28.225	88.98	16.35	7.26	7.11E-01	5.95E+01
17:00	30.225	88.94	16.39	7.22	7.62E-01	5.56E+01
17:02	32.225	88.90	16.43	7.18	8.12E-01	5.22E+01
17:04	34.225	88.86	16.47	7.14	8.63E-01	4.92E+01
17:06	36.225	88.80	16.53	7.08	9.13E-01	4.66E+01
17:08	38.225	88.77	16.56	7.05	9.63E-01	4.42E+01
17:10	40.225	88.73	16.60	7.01	1.01E+00	4.20E+01
17:12	42.225	88.70	16.63	6.98	1.06E+00	4.01E+01
17:14	44.225	88.65	16.68	6.93	1.11E+00	3.83E+01
17:16	46.225	88.63	16.70	6.91	1.16E+00	3.67E+01
17:18	48.225	88.60	16.73	6.88	1.22E+00	3.52E+01
17:20	50.342	88.55	16.78	6.83	1.27E+00	3.38E+01
17:22	52.220	88.53	16.80	6.81	1.32E+00	3.26E+01
17:24	54.222	88.50	16.83	6.78	1.37E+00	3.14E+01
17:26	56.222	88.48	16.85	6.76	1.42E+00	3.04E+01
17:28	58.220	88.44	16.89	6.72	1.47E+00	2.94E+01
17:30	60.120	88.43	16.90	6.71	1.52E+00	2.85E+01
17:32	62.220	88.38	16.95	6.66	1.57E+00	2.75E+01
17:34	64.222	88.37	16.96	6.65	1.62E+00	2.67E+01
17:36	66.220	88.34	16.99	6.62	1.67E+00	2.59E+01
17:38	68.220	88.31	17.02	6.59	1.72E+00	2.52E+01
17:40	70.220	88.28	17.05	6.56	1.77E+00	2.45E+01
17:42	72.220	88.25	17.08	6.53	1.82E+00	2.39E+01
17:44	74.222	88.24	17.09	6.52	1.87E+00	2.32E+01
17:46	76.095	88.21	17.12	6.49	1.92E+00	2.27E+01
17:48	78.180	88.20	17.13	6.48	1.97E+00	2.21E+01
17:50	80.575	88.17	17.16	6.45	2.03E+00	2.15E+01
17:52	82.215	88.15	17.18	6.43	2.07E+00	2.11E+01
17:54	84.215	88.13	17.20	6.41	2.12E+00	2.06E+01
17:56	86.215	88.11	17.22	6.39	2.17E+00	2.01E+01
17:58	88.215	88.08	17.25	6.36	2.22E+00	1.97E+01
18:00	90.493	88.07	17.26	6.35	2.28E+00	1.92E+01
18:02	92.210	88.04	17.29	6.32	2.32E+00	1.89E+01
18:04	94.248	88.03	17.30	6.31	2.38E+00	1.85E+01
18:06	96.248	88.01	17.32	6.29	2.43E+00	1.81E+01
18:08	98.248	87.98	17.35	6.26	2.48E+00	1.78E+01
18:30	120.250	87.78	17.55	6.06	3.03E+00	1.47E+01
18:50	140.250	87.63	17.70	5.91	3.53E+00	1.28E+01
19:10	160.180	87.48	17.85	5.76	4.04E+00	1.13E+01
19:30	180.170	87.34	17.99	5.62	4.54E+00	1.02E+01
19:50	200.220	87.22	18.11	5.50	5.05E+00	9.24E+00
20:10	220.150	87.11	18.22	5.39	5.55E+00	8.50E+00
20:30	240.150	87.00	18.33	5.28	6.05E+00	7.87E+00



20:50	260.150	86.90	18.43	5.18	6.56E+00	7.34E+00
21:10	280.250	86.80	18.53	5.08	7.06E+00	6.89E+00
21:30	300.250	86.71	18.62	4.99	7.57E+00	6.50E+00
21:50	320.250	86.62	18.71	4.90	8.07E+00	6.15E+00
22:10	340.250	86.54	18.79	4.82	8.57E+00	5.85E+00
22:30	360.220	86.47	18.86	4.75	9.08E+00	5.58E+00
22:50	380.080	86.40	18.93	4.68	9.58E+00	5.34E+00
23:10	400.080	86.32	19.01	4.60	1.01E+01	5.13E+00
23:30	420.150	86.25	19.08	4.53	1.06E+01	4.93E+00
23:50	440.080	86.20	19.13	4.48	1.11E+01	4.75E+00
00:10	460.220	86.12	19.21	4.40	1.16E+01	4.59E+00
00:30	480.220	86.07	19.26	4.35	1.21E+01	4.44E+00
00:50	500.220	86.02	19.31	4.30	1.26E+01	4.30E+00
01:10	520.220	85.95	19.38	4.23	1.31E+01	4.17E+00
01:30	540.220	85.91	19.42	4.19	1.36E+01	4.06E+00
01:50	560.220	85.85	19.48	4.13	1.41E+01	3.95E+00
02:10	580.220	85.79	19.54	4.07	1.46E+01	3.84E+00
02:30	600.220	85.75	19.58	4.03	1.51E+01	3.75E+00
02:50	620.220	85.71	19.62	3.99	1.56E+01	3.66E+00
03:10	640.220	85.65	19.68	3.93	1.61E+01	3.58E+00
03:30	660.220	85.62	19.71	3.90	1.66E+01	3.50E+00
03:50	680.220	85.57	19.76	3.85	1.71E+01	3.43E+00
04:10	700.220	85.52	19.81	3.80	1.76E+01	3.36E+00
04:30	720.220	85.48	19.85	3.76	1.82E+01	3.29E+00
04:50	740.220	85.45	19.88	3.73	1.87E+01	3.23E+00
05:10	760.220	85.41	19.92	3.69	1.92E+01	3.17E+00
05:30	780.220	85.37	19.96	3.65	1.97E+01	3.12E+00
05:50	800.220	85.32	20.01	3.60	2.02E+01	3.06E+00
06:10	820.220	85.29	20.04	3.57	2.07E+01	3.01E+00
06:30	840.220	85.25	20.08	3.53	2.12E+01	2.96E+00
06:50	860.220	85.22	20.11	3.50	2.17E+01	2.92E+00
07:10	880.180	85.18	20.15	3.46	2.22E+01	2.88E+00
07:30	900.180	85.15	20.18	3.43	2.27E+01	2.83E+00
07:50	920.180	85.12	20.21	3.40	2.32E+01	2.79E+00
08:10	940.180	85.08	20.25	3.36	2.37E+01	2.76E+00
08:30	960.180	85.05	20.28	3.33	2.42E+01	2.72E+00
08:50	980.170	85.02	20.31	3.30	2.47E+01	2.68E+00
09:10	1000.200	84.99	20.34	3.27	2.52E+01	2.65E+00
10:10	1060.400	84.92	20.41	3.20	2.67E+01	2.56E+00
11:10	1120.700	84.85	20.48	3.13	2.82E+01	2.47E+00
12:10	1180.300	84.77	20.56	3.05	2.97E+01	2.40E+00
13:10	1240.300	84.69	20.64	2.97	3.13E+01	2.33E+00
14:10	1300.400	84.64	20.69	2.92	3.28E+01	2.27E+00
15:10	1360.300	84.59	20.74	2.87	3.43E+01	2.21E+00
16:10	1420.200	84.52	20.81	2.80	3.58E+01	2.16E+00
17:10	1480.300	84.45	20.88	2.73	3.73E+01	2.12E+00
18:10	1540.300	84.38	20.95	2.66	3.88E+01	2.07E+00
19:10	1600.300	84.31	21.02	2.59	4.03E+01	2.03E+00
20:10	1660.300	84.27	21.06	2.55	4.18E+01	1.99E+00
21:10	1720.300	84.21	21.12	2.49	4.34E+01	1.96E+00
22:10	1780.300	84.17	21.16	2.45	4.49E+01	1.93E+00
23:10	1840.300	84.11	21.22	2.39	4.64E+01	1.90E+00
00:10	1900.300	84.06	21.27	2.34	4.79E+01	1.87E+00
01:10	1960.300	84.01	21.32	2.29	4.94E+01	1.84E+00
02:10	2020.300	83.98	21.35	2.26	5.09E+01	1.82E+00
03:10	2080.300	83.92	21.41	2.20	5.24E+01	1.79E+00

04:10	2140.300	83.88	21.45	2.16	5.39E+01	1.77E+00
05:10	2200.300	83.84	21.49	2.12	5.55E+01	1.75E+00
06:10	2260.300	83.79	21.54	2.07	5.70E+01	1.73E+00
07:10	2320.300	83.75	21.58	2.03	5.85E+01	1.71E+00
08:10	2380.300	83.71	21.62	1.99	6.00E+01	1.69E+00
09:10	2440.300	83.68	21.65	1.96	6.15E+01	1.68E+00
10:10	2500.300	83.65	21.68	1.93	6.30E+01	1.66E+00
11:10	2560.300	83.62	21.71	1.90	6.45E+01	1.64E+00
12:10	2620.400	83.59	21.74	1.87	6.60E+01	1.63E+00
13:10	2680.400	83.56	21.77	1.84	6.75E+01	1.62E+00
14:10	2740.400	83.52	21.81	1.80	6.91E+01	1.60E+00
15:10	2800.400	83.52	21.81	1.80	7.06E+01	1.59E+00
16:10	2860.400	83.49	21.84	1.77	7.21E+01	1.58E+00
17:10	2920.400	83.45	21.88	1.73	7.36E+01	1.57E+00
18:10	2980.400	83.44	21.89	1.72	7.51E+01	1.55E+00
19:10	3040.200	83.38	21.95	1.66	7.66E+01	1.54E+00
20:10	3100.200	83.35	21.98	1.63	7.81E+01	1.53E+00
21:10	3160.200	83.32	22.01	1.60	7.96E+01	1.52E+00
22:10	3220.200	83.31	22.02	1.59	8.12E+01	1.51E+00
23:10	3280.200	83.28	22.05	1.56	8.27E+01	1.50E+00
00:10	3340.200	83.29	22.04	1.57	8.42E+01	1.49E+00
01:10	3400.200	83.24	22.09	1.52	8.57E+01	1.49E+00
02:10	3460.200	83.24	22.09	1.52	8.72E+01	1.48E+00
03:10	3520.200	83.19	22.14	1.47	8.87E+01	1.47E+00
04:10	3580.300	83.16	22.17	1.44	9.02E+01	1.46E+00
05:10	3640.300	83.21	22.12	1.49	9.17E+01	1.45E+00
06:10	3700.300	83.14	22.19	1.42	9.33E+01	1.45E+00
07:10	3760.300	83.08	22.25	1.36	9.48E+01	1.44E+00
07:36	3786.600	83.06	22.27	1.34	9.54E+01	1.44E+00

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: GW-25 INPUT 2  
 RADIUS: 66.670 FEET  
 START DATE: 15-Sep-86  
 START TIME: 13:00  
 WATER START LEVEL: 82.22 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
13:00	0.000	82.22	0.00	0.00E+00
13:00	0.017	-999.99	1082.21	2.66E-09
13:00	0.034	-999.99	1082.21	5.31E-09
13:00	0.050	-999.99	1082.21	7.81E-09
13:00	0.067	-999.99	1082.21	1.05E-08
13:00	0.084	-999.99	1082.21	1.31E-08
13:00	0.100	-999.99	1082.21	1.56E-08
13:00	0.117	-999.99	1082.21	1.83E-08
13:00	0.134	-999.99	1082.21	2.09E-08
13:00	0.150	-999.99	1082.21	2.34E-08
13:00	0.167	-999.99	1082.21	2.61E-08
13:00	0.257	82.22	0.00	4.02E-08
13:00	0.340	82.22	0.00	5.31E-08
13:00	0.424	82.24	-0.02	6.62E-08
13:00	0.507	82.24	-0.02	7.92E-08
13:00	0.590	82.25	-0.03	9.22E-08
13:00	0.674	82.26	-0.04	1.05E-07
13:00	0.757	82.28	-0.06	1.18E-07
13:00	0.840	82.29	-0.07	1.31E-07
13:00	0.924	82.31	-0.09	1.44E-07
13:01	1.007	82.32	-0.10	1.57E-07
13:01	1.417	82.44	-0.22	2.21E-07
13:01	1.750	82.54	-0.32	2.73E-07
13:02	2.084	82.66	-0.44	3.26E-07
13:02	2.417	82.76	-0.54	3.78E-07
13:02	2.750	82.87	-0.65	4.30E-07
13:03	3.084	82.96	-0.74	4.82E-07
13:03	3.417	83.06	-0.84	5.34E-07
13:03	3.750	83.18	-0.96	5.86E-07
13:04	4.084	83.27	-1.05	6.38E-07
13:04	4.417	83.35	-1.13	6.90E-07
13:04	4.750	83.44	-1.22	7.42E-07
13:05	5.084	83.51	-1.29	7.94E-07
13:05	5.417	83.59	-1.37	8.46E-07
13:05	5.750	83.66	-1.44	8.98E-07
13:06	6.084	83.73	-1.51	9.51E-07
13:06	6.417	83.79	-1.57	1.00E-06
13:06	6.750	83.85	-1.63	1.05E-06
13:07	7.084	83.91	-1.69	1.11E-06
13:07	7.417	83.96	-1.74	1.16E-06

13:07	7.750	84.02	-1.80	1.21E-06
13:08	8.084	84.07	-1.85	1.26E-06
13:08	8.417	84.11	-1.89	1.32E-06
13:08	8.750	84.17	-1.95	1.37E-06
13:09	9.084	84.21	-1.99	1.42E-06
13:09	9.417	84.26	-2.04	1.47E-06
13:09	9.750	84.24	-2.02	1.52E-06
13:10	10.084	84.34	-2.12	1.58E-06
13:12	12.101	84.52	-2.30	1.89E-06
13:14	14.188	84.71	-2.49	2.22E-06
13:16	16.139	84.82	-2.60	2.52E-06
13:18	18.237	84.95	-2.73	2.85E-06
13:20	20.233	85.07	-2.85	3.16E-06
13:22	22.233	85.16	-2.94	3.47E-06
13:24	24.233	85.26	-3.04	3.79E-06
13:26	26.233	85.34	-3.12	4.10E-06
13:28	28.233	85.42	-3.20	4.41E-06
13:30	30.233	85.49	-3.27	4.72E-06
13:32	32.152	85.56	-3.34	5.02E-06
13:34	34.620	85.65	-3.43	5.41E-06
13:36	36.095	85.69	-3.47	5.64E-06
13:38	38.095	85.75	-3.53	5.95E-06
13:40	40.095	85.81	-3.59	6.26E-06
13:42	42.195	85.85	-3.63	6.59E-06
13:44	44.232	85.91	-3.69	6.91E-06
13:46	46.232	85.97	-3.75	7.22E-06
13:48	48.252	86.03	-3.81	7.54E-06
13:50	50.122	86.06	-3.84	7.83E-06
13:52	52.122	86.12	-3.90	8.14E-06
13:54	54.122	86.16	-3.94	8.46E-06
13:56	56.122	86.20	-3.98	8.77E-06
13:58	58.122	86.25	-4.03	9.08E-06
14:00	60.122	86.28	-4.06	9.39E-06
14:02	62.122	86.33	-4.11	9.71E-06
14:04	64.122	86.39	-4.17	1.00E-05
14:06	66.442	86.45	-4.23	1.04E-05
14:08	68.122	86.51	-4.29	1.06E-05
14:10	70.335	86.57	-4.35	1.10E-05
14:12	72.160	86.59	-4.37	1.13E-05
14:14	74.160	86.64	-4.42	1.16E-05
14:16	76.167	86.71	-4.49	1.19E-05
14:18	78.230	86.75	-4.53	1.22E-05
14:20	80.217	86.81	-4.59	1.25E-05
14:22	82.213	86.86	-4.64	1.28E-05
14:24	84.213	86.91	-4.69	1.32E-05
14:26	86.213	86.96	-4.74	1.35E-05
14:28	88.213	87.00	-4.78	1.38E-05
14:30	90.213	87.02	-4.80	1.41E-05
14:32	92.213	87.05	-4.83	1.44E-05
14:34	94.213	87.06	-4.84	1.47E-05
14:36	96.213	87.07	-4.85	1.50E-05
14:38	98.238	87.09	-4.87	1.53E-05
15:00	120.220	87.23	-5.01	1.88E-05
15:20	140.130	87.35	-5.13	2.19E-05
15:40	160.130	87.54	-5.32	2.50E-05
16:00	180.370	87.68	-5.46	2.82E-05

16:20	200.200	87.77	-5.55	3.13E-05
16:40	220.200	87.90	-5.68	3.44E-05
17:00	240.080	88.02	-5.80	3.75E-05
17:20	260.220	88.16	-5.94	4.07E-05
17:40	280.150	88.29	-6.07	4.38E-05
18:00	300.150	88.41	-6.19	4.69E-05
18:20	320.130	88.54	-6.32	5.00E-05
18:40	340.220	88.67	-6.45	5.32E-05
19:00	360.180	88.79	-6.57	5.63E-05
19:20	380.220	88.89	-6.67	5.94E-05
19:40	400.220	89.01	-6.79	6.25E-05
20:00	420.220	89.11	-6.89	6.57E-05
20:20	440.220	89.21	-6.99	6.88E-05
20:40	460.220	89.33	-7.11	7.19E-05
21:00	480.120	89.43	-7.21	7.50E-05
21:20	500.220	89.54	-7.32	7.82E-05
21:40	520.320	89.66	-7.44	8.13E-05
22:00	540.200	89.78	-7.56	8.44E-05
22:20	560.100	89.91	-7.69	8.75E-05
22:40	580.100	90.05	-7.83	9.06E-05
23:00	600.150	90.21	-7.99	9.38E-05
23:20	620.150	90.34	-8.12	9.69E-05
23:40	640.180	90.47	-8.25	1.00E-04
00:00	660.180	90.62	-8.40	1.03E-04
00:20	680.180	90.77	-8.55	1.06E-04
00:40	700.180	90.87	-8.65	1.09E-04
01:00	720.180	91.00	-8.78	1.13E-04
01:20	740.180	91.19	-8.97	1.16E-04
01:40	760.180	91.32	-9.10	1.19E-04
02:00	780.180	91.38	-9.16	1.22E-04
02:20	800.180	91.46	-9.24	1.25E-04
02:40	820.180	91.56	-9.34	1.28E-04
03:00	840.180	91.65	-9.43	1.31E-04
03:20	860.180	91.75	-9.53	1.34E-04
03:40	880.180	91.78	-9.56	1.38E-04
04:00	900.180	91.83	-9.61	1.41E-04
04:20	920.180	91.90	-9.68	1.44E-04
04:40	940.180	91.96	-9.74	1.47E-04
05:00	960.180	92.03	-9.81	1.50E-04
05:20	980.180	92.10	-9.88	1.53E-04
05:40	1000.200	92.18	-9.96	1.56E-04
06:40	1060.400	92.35	-10.13	1.66E-04
07:40	1120.500	92.54	-10.32	1.75E-04
08:40	1180.300	92.71	-10.49	1.84E-04
09:40	1240.300	92.87	-10.65	1.94E-04
10:40	1300.200	93.03	-10.81	2.03E-04
11:40	1360.300	92.09	-9.87	2.13E-04
12:40	1420.300	91.59	-9.37	2.22E-04
13:40	1480.200	91.54	-9.32	2.31E-04
14:40	1540.300	91.48	-9.26	2.41E-04
15:40	1600.300	91.51	-9.29	2.50E-04
16:30	1650.600	91.52	-9.30	2.58E-04

TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: GW-25 INPUT 2  
 RADIUS: 66.670 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 82.22 FEET  
 WATER STOP LEVEL: 91.52 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)	t/r2	t/t'
16:30	0.017	-999.99	1091.51	1082.21	2.66E-09	9.71E+04
16:30	0.034	-999.99	1091.51	1082.21	5.31E-09	4.85E+04
16:30	0.050	-999.99	1091.51	1082.21	7.81E-09	3.30E+04
16:30	0.067	-999.99	1091.51	1082.21	1.05E-08	2.46E+04
16:30	0.084	-999.99	1091.51	1082.21	1.31E-08	1.97E+04
16:30	0.100	-999.99	1091.51	1082.21	1.56E-08	1.65E+04
16:30	0.117	-999.99	1091.51	1082.21	1.83E-08	1.41E+04
16:30	0.134	-999.99	1091.51	1082.21	2.09E-08	1.23E+04
16:30	0.150	-999.99	1091.51	1082.21	2.34E-08	1.10E+04
16:30	0.167	-999.99	1091.51	1082.21	2.61E-08	9.88E+03
16:30	0.257	91.49	0.03	9.27	4.02E-08	6.42E+03
16:30	0.340	91.49	0.03	9.27	5.31E-08	4.86E+03
16:30	0.424	91.49	0.03	9.27	6.62E-08	3.89E+03
16:30	0.507	91.48	0.04	9.26	7.92E-08	3.26E+03
16:30	0.591	91.46	0.06	9.24	9.23E-08	2.79E+03
16:30	0.674	91.46	0.06	9.24	1.05E-07	2.45E+03
16:30	0.757	91.45	0.07	9.23	1.18E-07	2.18E+03
16:30	0.840	91.43	0.09	9.21	1.31E-07	1.97E+03
16:30	0.924	91.42	0.10	9.20	1.44E-07	1.79E+03
16:31	1.007	91.42	0.10	9.20	1.57E-07	1.64E+03
16:31	1.417	91.35	0.17	9.13	2.21E-07	1.17E+03
16:31	1.751	91.27	0.25	9.05	2.74E-07	9.44E+02
16:32	2.084	91.20	0.32	8.98	3.26E-07	7.93E+02
16:32	2.417	91.14	0.38	8.92	3.78E-07	6.84E+02
16:32	2.751	91.07	0.45	8.85	4.30E-07	6.01E+02
16:33	3.084	91.00	0.52	8.78	4.82E-07	5.36E+02
16:33	3.417	90.94	0.58	8.72	5.34E-07	4.84E+02
16:33	3.751	90.87	0.65	8.65	5.86E-07	4.41E+02
16:34	4.084	90.81	0.71	8.59	6.38E-07	4.05E+02
16:34	4.417	90.75	0.77	8.53	6.90E-07	3.75E+02
16:34	4.751	90.71	0.81	8.49	7.42E-07	3.48E+02
16:35	5.084	90.65	0.87	8.43	7.94E-07	3.26E+02
16:35	5.417	90.61	0.91	8.39	8.46E-07	3.06E+02
16:35	5.751	90.56	0.96	8.34	8.99E-07	2.88E+02
16:36	6.084	90.52	1.00	8.30	9.51E-07	2.72E+02
16:36	6.417	90.49	1.03	8.27	1.00E-06	2.58E+02
16:36	6.751	90.45	1.07	8.23	1.05E-06	2.45E+02
16:37	7.084	90.42	1.10	8.20	1.11E-06	2.34E+02
16:37	7.417	90.37	1.15	8.15	1.16E-06	2.24E+02
16:37	7.751	90.34	1.18	8.12	1.21E-06	2.14E+02
16:38	8.084	90.30	1.22	8.08	1.26E-06	2.05E+02
16:38	8.417	90.27	1.25	8.05	1.32E-06	1.97E+02

16:38	8.751	90.24	1.28	8.02	1.37E-06	1.90E+02
16:39	9.084	90.21	1.31	7.99	1.42E-06	1.83E+02
16:39	9.417	90.20	1.32	7.98	1.47E-06	1.76E+02
16:39	9.751	90.17	1.35	7.95	1.52E-06	1.70E+02
16:40	10.084	90.14	1.38	7.92	1.58E-06	1.65E+02
16:42	12.120	90.01	1.51	7.79	1.89E-06	1.37E+02
16:44	14.120	89.89	1.63	7.67	2.21E-06	1.18E+02
16:46	16.120	89.79	1.73	7.57	2.52E-06	1.03E+02
16:48	18.120	89.72	1.80	7.50	2.83E-06	9.21E+01
16:50	20.142	89.65	1.87	7.43	3.15E-06	8.29E+01
16:52	22.225	89.57	1.95	7.35	3.47E-06	7.53E+01
16:54	24.225	89.52	2.00	7.30	3.78E-06	6.91E+01
16:56	26.225	89.46	2.06	7.24	4.10E-06	6.39E+01
16:58	28.225	89.40	2.12	7.18	4.41E-06	5.95E+01
17:00	30.225	89.36	2.16	7.14	4.72E-06	5.56E+01
17:02	32.225	89.31	2.21	7.09	5.03E-06	5.22E+01
17:04	34.225	89.27	2.25	7.05	5.35E-06	4.92E+01
17:06	36.225	89.23	2.29	7.01	5.66E-06	4.66E+01
17:08	38.225	89.18	2.34	6.96	5.97E-06	4.42E+01
17:10	40.225	89.14	2.38	6.92	6.28E-06	4.20E+01
17:12	42.225	89.11	2.41	6.89	6.60E-06	4.01E+01
17:14	44.225	89.08	2.44	6.86	6.91E-06	3.83E+01
17:16	46.225	89.04	2.48	6.82	7.22E-06	3.67E+01
17:18	48.225	89.01	2.51	6.79	7.53E-06	3.52E+01
17:20	50.342	88.98	2.54	6.76	7.87E-06	3.38E+01
17:22	52.220	88.95	2.57	6.73	8.16E-06	3.26E+01
17:24	54.222	88.92	2.60	6.70	8.47E-06	3.14E+01
17:26	56.222	88.89	2.63	6.67	8.78E-06	3.04E+01
17:28	58.220	88.86	2.66	6.64	9.10E-06	2.94E+01
17:30	60.120	88.83	2.69	6.61	9.39E-06	2.85E+01
17:32	62.220	88.80	2.72	6.58	9.72E-06	2.75E+01
17:34	64.222	88.77	2.75	6.55	1.00E-05	2.67E+01
17:36	66.220	88.76	2.76	6.54	1.03E-05	2.59E+01
17:38	68.220	88.73	2.79	6.51	1.07E-05	2.52E+01
17:40	70.220	88.70	2.82	6.48	1.10E-05	2.45E+01
17:42	72.220	88.69	2.83	6.47	1.13E-05	2.39E+01
17:44	74.222	88.66	2.86	6.44	1.16E-05	2.32E+01
17:46	76.095	88.64	2.88	6.42	1.19E-05	2.27E+01
17:48	78.180	88.61	2.91	6.39	1.22E-05	2.21E+01
17:50	80.575	88.59	2.93	6.37	1.26E-05	2.15E+01
17:52	82.215	88.57	2.95	6.35	1.28E-05	2.11E+01
17:54	84.215	88.56	2.96	6.34	1.32E-05	2.06E+01
17:56	86.215	88.53	2.99	6.31	1.35E-05	2.01E+01
17:58	88.215	88.51	3.01	6.29	1.38E-05	1.97E+01
18:00	90.493	88.48	3.04	6.26	1.41E-05	1.92E+01
18:02	92.210	88.47	3.05	6.25	1.44E-05	1.89E+01
18:04	94.248	88.45	3.07	6.23	1.47E-05	1.85E+01
18:06	96.248	88.43	3.09	6.21	1.50E-05	1.81E+01
18:08	98.248	88.41	3.11	6.19	1.53E-05	1.78E+01
18:30	120.250	88.21	3.31	5.99	1.88E-05	1.47E+01
18:50	140.250	88.05	3.47	5.83	2.19E-05	1.28E+01
19:10	160.180	87.90	3.62	5.68	2.50E-05	1.13E+01
19:30	180.170	87.77	3.75	5.55	2.81E-05	1.02E+01
19:50	200.220	87.64	3.88	5.42	3.13E-05	9.24E+00
20:10	220.150	87.52	4.00	5.30	3.44E-05	8.50E+00
20:30	240.150	87.42	4.10	5.20	3.75E-05	7.87E+00

20:50	260.150	87.32	4.20	5.10	4.06E-05	7.34E+00
21:10	280.250	87.22	4.30	5.00	4.38E-05	6.89E+00
21:30	300.250	87.13	4.39	4.91	4.69E-05	6.50E+00
21:50	320.250	87.05	4.47	4.83	5.00E-05	6.15E+00
22:10	340.250	86.97	4.55	4.75	5.32E-05	5.85E+00
22:30	360.220	86.90	4.62	4.68	5.63E-05	5.58E+00
22:50	380.080	86.83	4.69	4.61	5.94E-05	5.34E+00
23:10	400.080	86.75	4.77	4.53	6.25E-05	5.13E+00
23:30	420.150	86.68	4.84	4.46	6.56E-05	4.93E+00
23:50	440.080	86.62	4.90	4.40	6.88E-05	4.75E+00
00:10	460.220	86.57	4.95	4.35	7.19E-05	4.59E+00
00:30	480.220	86.49	5.03	4.27	7.50E-05	4.44E+00
00:50	500.220	86.43	5.09	4.21	7.82E-05	4.30E+00
01:10	520.220	86.38	5.14	4.16	8.13E-05	4.17E+00
01:30	540.220	86.33	5.19	4.11	8.44E-05	4.06E+00
01:50	560.220	86.28	5.24	4.06	8.75E-05	3.95E+00
02:10	580.220	86.23	5.29	4.01	9.07E-05	3.84E+00
02:30	600.220	86.19	5.33	3.97	9.38E-05	3.75E+00
02:50	620.220	86.13	5.39	3.91	9.69E-05	3.66E+00
03:10	640.220	86.09	5.43	3.87	1.00E-04	3.58E+00
03:30	660.220	86.04	5.48	3.82	1.03E-04	3.50E+00
03:50	680.220	86.00	5.52	3.78	1.06E-04	3.43E+00
04:10	700.220	85.96	5.56	3.74	1.09E-04	3.36E+00
04:30	720.220	85.91	5.61	3.69	1.13E-04	3.29E+00
04:50	740.220	85.87	5.65	3.65	1.16E-04	3.23E+00
05:10	760.220	85.84	5.68	3.62	1.19E-04	3.17E+00
05:30	780.220	85.80	5.72	3.58	1.22E-04	3.12E+00
05:50	800.220	85.75	5.77	3.53	1.25E-04	3.06E+00
06:10	820.220	85.72	5.80	3.50	1.28E-04	3.01E+00
06:30	840.220	85.69	5.83	3.47	1.31E-04	2.96E+00
06:50	860.220	85.65	5.87	3.43	1.34E-04	2.92E+00
07:10	880.180	85.62	5.90	3.40	1.38E-04	2.88E+00
07:30	900.180	85.58	5.94	3.36	1.41E-04	2.83E+00
07:50	920.180	85.55	5.97	3.33	1.44E-04	2.79E+00
08:10	940.180	85.52	6.00	3.30	1.47E-04	2.76E+00
08:30	960.180	85.49	6.03	3.27	1.50E-04	2.72E+00
08:50	980.170	85.46	6.06	3.24	1.53E-04	2.68E+00
09:10	1000.200	85.43	6.09	3.21	1.56E-04	2.65E+00
10:10	1060.400	85.36	6.16	3.14	1.66E-04	2.56E+00
11:10	1120.700	85.29	6.23	3.07	1.75E-04	2.47E+00
12:10	1180.300	85.20	6.32	2.98	1.84E-04	2.40E+00
13:10	1240.300	85.13	6.39	2.91	1.94E-04	2.33E+00
14:10	1300.400	85.07	6.45	2.85	2.03E-04	2.27E+00
15:10	1360.300	85.01	6.51	2.79	2.13E-04	2.21E+00
16:10	1420.200	84.95	6.57	2.73	2.22E-04	2.16E+00
17:10	1480.300	84.89	6.63	2.67	2.31E-04	2.12E+00
18:10	1540.300	84.82	6.70	2.60	2.41E-04	2.07E+00
19:10	1600.300	84.76	6.76	2.54	2.50E-04	2.03E+00
20:10	1660.300	84.71	6.81	2.49	2.59E-04	1.99E+00
21:10	1720.300	84.65	6.87	2.43	2.69E-04	1.96E+00
22:10	1780.300	84.59	6.93	2.37	2.78E-04	1.93E+00
23:10	1840.300	84.55	6.97	2.33	2.88E-04	1.90E+00
00:10	1900.300	84.49	7.03	2.27	2.97E-04	1.87E+00
01:10	1960.300	84.46	7.06	2.24	3.06E-04	1.84E+00
02:10	2020.300	84.40	7.12	2.18	3.16E-04	1.82E+00
03:10	2080.300	84.36	7.16	2.14	3.25E-04	1.79E+00



04:10	2140.300	84.31	7.21	2.09	3.34E-04	1.77E+00
05:10	2200.300	84.27	7.25	2.05	3.44E-04	1.75E+00
06:10	2260.300	84.23	7.29	2.01	3.53E-04	1.73E+00
07:10	2320.300	84.18	7.34	1.96	3.63E-04	1.71E+00
08:10	2380.300	84.15	7.37	1.93	3.72E-04	1.69E+00
09:10	2440.300	84.11	7.41	1.89	3.81E-04	1.68E+00
10:10	2500.300	84.08	7.44	1.86	3.91E-04	1.66E+00
11:10	2560.300	84.07	7.45	1.85	4.00E-04	1.64E+00
12:10	2620.400	84.04	7.48	1.82	4.09E-04	1.63E+00
13:10	2680.400	84.01	7.51	1.79	4.19E-04	1.62E+00
14:10	2740.400	83.96	7.56	1.74	4.28E-04	1.60E+00
15:10	2800.400	83.95	7.57	1.73	4.38E-04	1.59E+00
16:10	2860.400	83.91	7.61	1.69	4.47E-04	1.58E+00
17:10	2920.400	83.89	7.63	1.67	4.56E-04	1.57E+00
18:10	2980.400	83.86	7.66	1.64	4.66E-04	1.55E+00
19:10	3040.200	83.83	7.69	1.61	4.75E-04	1.54E+00
20:10	3100.200	83.79	7.73	1.57	4.84E-04	1.53E+00
21:10	3160.200	83.78	7.74	1.56	4.94E-04	1.52E+00
22:10	3220.200	83.73	7.79	1.51	5.03E-04	1.51E+00
23:10	3280.200	83.72	7.80	1.50	5.12E-04	1.50E+00
00:10	3340.200	83.69	7.83	1.47	5.22E-04	1.49E+00
01:10	3400.200	83.67	7.85	1.45	5.31E-04	1.49E+00
02:10	3460.200	83.66	7.86	1.44	5.41E-04	1.48E+00
03:10	3520.200	83.63	7.89	1.41	5.50E-04	1.47E+00
04:10	3580.300	83.62	7.90	1.40	5.59E-04	1.46E+00
05:10	3640.300	83.57	7.95	1.35	5.69E-04	1.45E+00
06:10	3700.300	83.57	7.95	1.35	5.78E-04	1.45E+00
07:10	3760.300	83.53	7.99	1.31	5.87E-04	1.44E+00
07:36	3786.600	83.51	8.01	1.29	5.92E-04	1.44E+00

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: REI 11 INPUT 12  
 RADIUS: 427.782 FEET  
 START DATE: 15-Sep-86  
 START TIME: 13:00  
 WATER START LEVEL: 78.78 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
13:00	0.000	78.78	0.00	0.00E+00
13:00	0.017	-999.99	1078.77	6.45E-11
13:00	0.034	-999.99	1078.77	1.29E-10
13:00	0.050	-999.99	1078.77	1.90E-10
13:00	0.067	-999.99	1078.77	2.54E-10
13:00	0.084	-999.99	1078.77	3.19E-10
13:00	0.100	-999.99	1078.77	3.79E-10
13:00	0.117	-999.99	1078.77	4.44E-10
13:00	0.134	-999.99	1078.77	5.09E-10
13:00	0.150	-999.99	1078.77	5.69E-10
13:00	0.167	-999.99	1078.77	6.34E-10
13:00	0.257	78.78	0.00	9.75E-10
13:00	0.340	78.78	0.00	1.29E-09
13:00	0.424	78.78	0.00	1.61E-09
13:00	0.507	78.78	0.00	1.92E-09
13:00	0.590	78.78	0.00	2.24E-09
13:00	0.674	78.78	0.00	2.56E-09
13:00	0.757	78.78	0.00	2.87E-09
13:00	0.840	78.78	0.00	3.19E-09
13:00	0.924	78.78	0.00	3.51E-09
13:01	1.007	78.78	0.00	3.82E-09
13:01	1.417	78.78	0.00	5.38E-09
13:01	1.750	78.78	0.00	6.64E-09
13:02	2.084	78.79	-0.01	7.91E-09
13:02	2.417	78.79	-0.01	9.17E-09
13:02	2.750	78.79	-0.01	1.04E-08
13:03	3.084	78.79	-0.01	1.17E-08
13:03	3.417	78.78	0.00	1.30E-08
13:03	3.750	78.78	0.00	1.42E-08
13:04	4.084	78.78	0.00	1.55E-08
13:04	4.417	78.78	0.00	1.68E-08
13:04	4.750	78.78	0.00	1.80E-08
13:05	5.084	78.78	0.00	1.93E-08
13:05	5.417	78.78	0.00	2.06E-08
13:05	5.750	78.78	0.00	2.18E-08
13:06	6.084	78.78	0.00	2.31E-08
13:06	6.417	78.78	0.00	2.44E-08
13:06	6.750	78.78	0.00	2.56E-08
13:07	7.084	78.78	0.00	2.69E-08
13:07	7.417	78.78	0.00	2.81E-08

13:07	7.750	78.78	0.00	2.94E-08
13:08	8.084	78.78	0.00	3.07E-08
13:08	8.417	78.78	0.00	3.19E-08
13:08	8.750	78.78	0.00	3.32E-08
13:09	9.084	78.78	0.00	3.45E-08
13:09	9.417	78.78	0.00	3.57E-08
13:09	9.750	78.78	0.00	3.70E-08
13:10	10.084	78.79	-0.01	3.83E-08
13:12	12.101	78.80	-0.02	4.59E-08
13:14	14.188	78.82	-0.04	5.38E-08
13:16	16.139	78.83	-0.05	6.12E-08
13:18	18.237	78.84	-0.06	6.92E-08
13:20	20.233	78.86	-0.08	7.68E-08
13:22	22.233	78.88	-0.10	8.44E-08
13:24	24.233	78.91	-0.13	9.20E-08
13:26	26.233	78.93	-0.15	9.95E-08
13:28	28.233	78.96	-0.18	1.07E-07
13:30	30.233	78.98	-0.20	1.15E-07
13:32	32.152	79.00	-0.22	1.22E-07
13:34	34.620	79.04	-0.26	1.31E-07
13:36	36.095	79.05	-0.27	1.37E-07
13:38	38.095	79.08	-0.30	1.45E-07
13:40	40.095	79.11	-0.33	1.52E-07
13:42	42.195	79.13	-0.35	1.60E-07
13:44	44.232	79.15	-0.37	1.68E-07
13:46	46.232	79.18	-0.40	1.75E-07
13:48	48.252	79.21	-0.43	1.83E-07
13:50	50.122	79.23	-0.45	1.90E-07
13:52	52.122	79.25	-0.47	1.98E-07
13:54	54.122	79.30	-0.52	2.05E-07
13:56	56.122	79.32	-0.54	2.13E-07
13:58	58.122	79.35	-0.57	2.21E-07
14:00	60.122	79.37	-0.59	2.28E-07
14:02	62.122	79.39	-0.61	2.36E-07
14:04	64.122	79.41	-0.63	2.43E-07
14:06	66.442	79.44	-0.66	2.52E-07
14:08	68.122	79.47	-0.69	2.59E-07
14:10	70.335	79.50	-0.72	2.67E-07
14:12	72.160	79.52	-0.74	2.74E-07
14:14	74.160	79.54	-0.76	2.81E-07
14:16	76.167	79.57	-0.79	2.89E-07
14:18	78.230	79.60	-0.82	2.97E-07
14:20	80.217	79.62	-0.84	3.04E-07
14:22	82.213	79.64	-0.86	3.12E-07
14:24	84.213	79.67	-0.89	3.20E-07
14:26	86.213	79.69	-0.91	3.27E-07
14:28	88.213	79.72	-0.94	3.35E-07
14:30	90.213	79.74	-0.96	3.42E-07
14:32	92.213	79.77	-0.99	3.50E-07
14:34	94.213	79.79	-1.01	3.58E-07
14:36	96.213	79.81	-1.03	3.65E-07
14:38	98.238	79.84	-1.06	3.73E-07
15:00	120.220	80.09	-1.31	4.56E-07
15:20	140.130	80.29	-1.51	5.32E-07
15:40	160.130	80.47	-1.69	6.08E-07
16:00	180.370	80.63	-1.85	6.84E-07

16:20	200.200	80.78	-2.00	7.60E-07
16:40	220.200	80.93	-2.15	8.36E-07
17:00	240.080	81.06	-2.28	9.11E-07
17:20	260.220	81.19	-2.41	9.87E-07
17:40	280.150	81.31	-2.53	1.06E-06
18:00	300.150	81.43	-2.65	1.14E-06
18:20	320.130	81.54	-2.76	1.21E-06
18:40	340.220	81.66	-2.88	1.29E-06
19:00	360.180	81.76	-2.98	1.37E-06
19:20	380.220	81.87	-3.09	1.44E-06
19:40	400.220	81.98	-3.20	1.52E-06
20:00	420.220	82.08	-3.30	1.59E-06
20:20	440.220	82.18	-3.40	1.67E-06
20:40	460.220	82.27	-3.49	1.75E-06
21:00	480.120	82.37	-3.59	1.82E-06
21:20	500.220	82.46	-3.68	1.90E-06
21:40	520.320	82.55	-3.77	1.97E-06
22:00	540.200	82.65	-3.87	2.05E-06
22:20	560.100	82.74	-3.96	2.13E-06
22:40	580.100	82.83	-4.05	2.20E-06
23:00	600.150	82.92	-4.14	2.28E-06
23:20	620.150	83.03	-4.25	2.35E-06
23:40	640.180	83.11	-4.33	2.43E-06
00:00	660.180	83.21	-4.43	2.51E-06
00:20	680.180	83.30	-4.52	2.58E-06
00:40	700.180	83.39	-4.61	2.66E-06
01:00	720.180	83.48	-4.70	2.73E-06
01:20	740.180	83.57	-4.79	2.81E-06
01:40	760.180	83.67	-4.89	2.88E-06
02:00	780.180	83.76	-4.98	2.96E-06
02:20	800.180	83.85	-5.07	3.04E-06
02:40	820.180	83.93	-5.15	3.11E-06
03:00	840.180	84.02	-5.24	3.19E-06
03:20	860.180	84.10	-5.32	3.26E-06
03:40	880.180	84.18	-5.40	3.34E-06
04:00	900.180	84.25	-5.47	3.42E-06
04:20	920.180	84.32	-5.54	3.49E-06
04:40	940.180	84.38	-5.60	3.57E-06
05:00	960.180	84.45	-5.67	3.64E-06
05:20	980.180	84.51	-5.73	3.72E-06
05:40	1000.200	84.58	-5.80	3.80E-06
06:40	1060.400	84.76	-5.98	4.02E-06
07:40	1120.500	84.94	-6.16	4.25E-06
08:40	1180.300	85.11	-6.33	4.48E-06
09:40	1240.300	85.28	-6.50	4.71E-06
10:40	1300.200	85.45	-6.67	4.93E-06
11:40	1360.300	85.46	-6.68	5.16E-06
12:40	1420.300	85.33	-6.55	5.39E-06
13:40	1480.200	85.22	-6.44	5.62E-06
14:40	1540.300	85.15	-6.37	5.85E-06
15:40	1600.300	85.11	-6.33	6.07E-06
16:30	1650.600	85.11	-6.33	6.26E-06

TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 11 INPUT 12  
 RADIUS: 427.782 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 78.78 FEET  
 WATER STOP LEVEL: 85.11 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (RED)	Delta H (RES)	t/r2	t/t'
16:30	0.017	-999.99	1085.10	1078.77	6.45E-11	9.71E+04
16:30	0.034	-999.99	1085.10	1078.77	1.29E-10	4.85E+04
16:30	0.050	-999.99	1085.10	1078.77	1.90E-10	3.30E+04
16:30	0.067	-999.99	1085.10	1078.77	2.54E-10	2.46E+04
16:30	0.084	-999.99	1085.10	1078.77	3.19E-10	1.97E+04
16:30	0.100	-999.99	1085.10	1078.77	3.79E-10	1.65E+04
16:30	0.117	-999.99	1085.10	1078.77	4.44E-10	1.41E+04
16:30	0.134	-999.99	1085.10	1078.77	5.09E-10	1.23E+04
16:30	0.150	-999.99	1085.10	1078.77	5.69E-10	1.10E+04
16:30	0.167	-999.99	1085.10	1078.77	6.34E-10	9.88E+03
16:30	0.257	85.11	0.00	6.33	9.75E-10	6.42E+03
16:30	0.340	85.11	0.00	6.33	1.29E-09	4.86E+03
16:30	0.424	85.11	0.00	6.33	1.61E-09	3.89E+03
16:30	0.507	85.11	0.00	6.33	1.92E-09	3.26E+03
16:30	0.591	85.11	0.00	6.33	2.24E-09	2.79E+03
16:30	0.674	85.11	0.00	6.33	2.56E-09	2.45E+03
16:30	0.757	85.11	0.00	6.33	2.87E-09	2.18E+03
16:30	0.840	85.11	0.00	6.33	3.19E-09	1.97E+03
16:30	0.924	85.11	0.00	6.33	3.51E-09	1.79E+03
16:31	1.007	85.11	0.00	6.33	3.82E-09	1.64E+03
16:31	1.417	85.11	0.00	6.33	5.38E-09	1.17E+03
16:31	1.751	85.11	0.00	6.33	6.64E-09	9.44E+02
16:32	2.084	85.11	0.00	6.33	7.91E-09	7.93E+02
16:32	2.417	85.11	0.00	6.33	9.17E-09	6.84E+02
16:32	2.751	85.11	0.00	6.33	1.04E-08	6.01E+02
16:33	3.084	85.11	0.00	6.33	1.17E-08	5.36E+02
16:33	3.417	85.11	0.00	6.33	1.30E-08	4.84E+02
16:33	3.751	85.11	0.00	6.33	1.42E-08	4.41E+02
16:34	4.084	85.11	0.00	6.33	1.55E-08	4.05E+02
16:34	4.417	85.11	0.00	6.33	1.68E-08	3.75E+02
16:34	4.751	85.11	0.00	6.33	1.80E-08	3.48E+02
16:35	5.084	85.11	0.00	6.33	1.93E-08	3.26E+02
16:35	5.417	85.11	0.00	6.33	2.06E-08	3.06E+02
16:35	5.751	85.11	0.00	6.33	2.18E-08	2.88E+02
16:36	6.084	85.11	0.00	6.33	2.31E-08	2.72E+02
16:36	6.417	85.11	0.00	6.33	2.44E-08	2.58E+02
16:36	6.751	85.11	0.00	6.33	2.56E-08	2.45E+02
16:37	7.084	85.11	0.00	6.33	2.69E-08	2.34E+02
16:37	7.417	85.11	0.00	6.33	2.81E-08	2.24E+02
16:37	7.751	85.11	0.00	6.33	2.94E-08	2.14E+02
16:38	8.084	85.11	0.00	6.33	3.07E-08	2.05E+02
16:38	8.417	85.11	0.00	6.33	3.19E-08	1.97E+02

16:38	8.751	85.11	0.00	6.33	3.32E-08	1.90E+02
16:39	9.084	85.11	0.00	6.33	3.45E-08	1.83E+02
16:39	9.417	85.11	0.00	6.33	3.57E-08	1.76E+02
16:39	9.751	85.11	0.00	6.33	3.70E-08	1.70E+02
16:40	10.084	85.11	0.00	6.33	3.83E-08	1.65E+02
16:42	12.120	85.10	0.01	6.32	4.60E-08	1.37E+02
16:44	14.120	85.09	0.02	6.31	5.36E-08	1.18E+02
16:46	16.120	85.08	0.03	6.30	6.12E-08	1.03E+02
16:48	18.120	85.06	0.05	6.28	6.88E-08	9.21E+01
16:50	20.142	85.05	0.06	6.27	7.64E-08	8.29E+01
16:52	22.225	85.03	0.08	6.25	8.43E-08	7.53E+01
16:54	24.225	85.02	0.09	6.24	9.19E-08	6.91E+01
16:56	26.225	85.00	0.11	6.22	9.95E-08	6.39E+01
16:58	28.225	84.98	0.13	6.20	1.07E-07	5.95E+01
17:00	30.225	84.97	0.14	6.19	1.15E-07	5.56E+01
17:02	32.225	84.95	0.16	6.17	1.22E-07	5.22E+01
17:04	34.225	84.93	0.18	6.15	1.30E-07	4.92E+01
17:06	36.225	84.91	0.20	6.13	1.37E-07	4.66E+01
17:08	38.225	84.90	0.21	6.12	1.45E-07	4.42E+01
17:10	40.225	84.88	0.23	6.10	1.53E-07	4.20E+01
17:12	42.225	84.86	0.25	6.08	1.60E-07	4.01E+01
17:14	44.225	84.84	0.27	6.06	1.68E-07	3.83E+01
17:16	46.225	84.83	0.28	6.05	1.75E-07	3.67E+01
17:18	48.225	84.81	0.30	6.03	1.83E-07	3.52E+01
17:20	50.342	84.79	0.32	6.01	1.91E-07	3.38E+01
17:22	52.220	84.77	0.34	5.99	1.98E-07	3.26E+01
17:24	54.222	84.76	0.35	5.98	2.06E-07	3.14E+01
17:26	56.222	84.74	0.37	5.96	2.13E-07	3.04E+01
17:28	58.220	84.72	0.39	5.94	2.21E-07	2.94E+01
17:30	60.120	84.70	0.41	5.92	2.28E-07	2.85E+01
17:32	62.220	84.69	0.42	5.91	2.36E-07	2.75E+01
17:34	64.222	84.67	0.44	5.89	2.44E-07	2.67E+01
17:36	66.220	84.66	0.45	5.88	2.51E-07	2.59E+01
17:38	68.220	84.64	0.47	5.86	2.59E-07	2.52E+01
17:40	70.220	84.62	0.49	5.84	2.66E-07	2.45E+01
17:42	72.220	84.61	0.50	5.83	2.74E-07	2.39E+01
17:44	74.222	84.59	0.52	5.81	2.82E-07	2.32E+01
17:46	76.095	84.58	0.53	5.80	2.89E-07	2.27E+01
17:48	78.180	84.56	0.55	5.78	2.97E-07	2.21E+01
17:50	80.575	84.54	0.57	5.76	3.06E-07	2.15E+01
17:52	82.215	84.53	0.58	5.75	3.12E-07	2.11E+01
17:54	84.215	84.51	0.60	5.73	3.20E-07	2.06E+01
17:56	86.215	84.50	0.61	5.72	3.27E-07	2.01E+01
17:58	88.215	84.48	0.63	5.70	3.35E-07	1.97E+01
18:00	90.493	84.47	0.64	5.69	3.43E-07	1.92E+01
18:02	92.210	84.45	0.66	5.67	3.50E-07	1.89E+01
18:04	94.248	84.44	0.67	5.66	3.58E-07	1.85E+01
18:06	96.248	84.42	0.69	5.64	3.65E-07	1.81E+01
18:08	98.248	84.41	0.70	5.63	3.73E-07	1.78E+01
18:30	120.250	84.26	0.85	5.48	4.56E-07	1.47E+01
18:50	140.250	84.13	0.98	5.35	5.32E-07	1.28E+01
19:10	160.180	84.00	1.11	5.22	6.08E-07	1.13E+01
19:30	180.170	83.89	1.22	5.11	6.84E-07	1.02E+01
19:50	200.220	83.78	1.33	5.00	7.60E-07	9.24E+00
20:10	220.150	83.67	1.44	4.89	8.35E-07	8.50E+00
20:30	240.150	83.58	1.53	4.80	9.11E-07	7.87E+00

20:50	260.150	83.48	1.63	4.70	9.87E-07	7.34E+00
21:10	280.250	83.40	1.71	4.62	1.06E-06	6.89E+00
21:30	300.250	83.31	1.80	4.53	1.14E-06	6.50E+00
21:50	320.250	83.23	1.88	4.45	1.22E-06	6.15E+00
22:10	340.250	83.15	1.96	4.37	1.29E-06	5.85E+00
22:30	360.220	83.08	2.03	4.30	1.37E-06	5.58E+00
22:50	380.080	83.01	2.10	4.23	1.44E-06	5.34E+00
23:10	400.080	82.94	2.17	4.16	1.52E-06	5.13E+00
23:30	420.150	82.88	2.23	4.10	1.59E-06	4.93E+00
23:50	440.080	82.81	2.30	4.03	1.67E-06	4.75E+00
00:10	460.220	82.75	2.36	3.97	1.75E-06	4.59E+00
00:30	480.220	82.69	2.42	3.91	1.82E-06	4.44E+00
00:50	500.220	82.64	2.47	3.86	1.90E-06	4.30E+00
01:10	520.220	82.58	2.53	3.80	1.97E-06	4.17E+00
01:30	540.220	82.53	2.58	3.75	2.05E-06	4.06E+00
01:50	560.220	82.48	2.63	3.70	2.13E-06	3.95E+00
02:10	580.220	82.43	2.68	3.65	2.20E-06	3.84E+00
02:30	600.220	82.38	2.73	3.60	2.28E-06	3.75E+00
02:50	620.220	82.34	2.77	3.56	2.35E-06	3.66E+00
03:10	640.220	82.29	2.82	3.51	2.43E-06	3.58E+00
03:30	660.220	82.25	2.86	3.47	2.51E-06	3.50E+00
03:50	680.220	82.20	2.91	3.42	2.58E-06	3.43E+00
04:10	700.220	82.16	2.95	3.38	2.66E-06	3.36E+00
04:30	720.220	82.12	2.99	3.34	2.73E-06	3.29E+00
04:50	740.220	82.08	3.03	3.30	2.81E-06	3.23E+00
05:10	760.220	82.04	3.07	3.26	2.88E-06	3.17E+00
05:30	780.220	82.00	3.11	3.22	2.96E-06	3.12E+00
05:50	800.220	81.97	3.14	3.19	3.04E-06	3.06E+00
06:10	820.220	81.93	3.18	3.15	3.11E-06	3.01E+00
06:30	840.220	81.90	3.21	3.12	3.19E-06	2.96E+00
06:50	860.220	81.87	3.24	3.09	3.26E-06	2.92E+00
07:10	880.180	81.84	3.27	3.06	3.34E-06	2.88E+00
07:30	900.180	81.81	3.30	3.03	3.42E-06	2.83E+00
07:50	920.180	81.78	3.33	3.00	3.49E-06	2.79E+00
08:10	940.180	81.75	3.36	2.97	3.57E-06	2.76E+00
08:30	960.180	81.73	3.38	2.95	3.64E-06	2.72E+00
08:50	980.170	81.70	3.41	2.92	3.72E-06	2.68E+00
09:10	1000.200	81.68	3.43	2.90	3.80E-06	2.65E+00
10:10	1060.400	81.61	3.50	2.83	4.02E-06	2.56E+00
11:10	1120.700	81.53	3.58	2.75	4.25E-06	2.47E+00
12:10	1180.300	81.46	3.65	2.68	4.48E-06	2.40E+00
13:10	1240.300	81.39	3.72	2.61	4.71E-06	2.33E+00
14:10	1300.400	81.33	3.78	2.55	4.93E-06	2.27E+00
15:10	1360.300	81.25	3.86	2.47	5.16E-06	2.21E+00
16:10	1420.200	81.19	3.92	2.41	5.39E-06	2.16E+00
17:10	1480.300	81.14	3.97	2.36	5.62E-06	2.12E+00
18:10	1540.300	81.08	4.03	2.30	5.85E-06	2.07E+00
19:10	1600.300	81.03	4.08	2.25	6.07E-06	2.03E+00
20:10	1660.300	80.98	4.13	2.20	6.30E-06	1.99E+00
21:10	1720.300	80.94	4.17	2.16	6.53E-06	1.96E+00
22:10	1780.300	80.90	4.21	2.12	6.76E-06	1.93E+00
23:10	1840.300	80.86	4.25	2.08	6.98E-06	1.90E+00
00:10	1900.300	80.82	4.29	2.04	7.21E-06	1.87E+00
01:10	1960.300	80.78	4.33	2.00	7.44E-06	1.84E+00
02:10	2020.300	80.74	4.37	1.96	7.67E-06	1.82E+00
03:10	2080.300	80.70	4.41	1.92	7.89E-06	1.79E+00

04:10	2140.300	80.67	4.44	1.89	8.12E-06	1.77E+00
05:10	2200.300	80.63	4.48	1.85	8.35E-06	1.75E+00
06:10	2260.300	80.59	4.52	1.81	8.58E-06	1.73E+00
07:10	2320.300	80.55	4.56	1.77	8.81E-06	1.71E+00
08:10	2380.300	80.53	4.58	1.75	9.03E-06	1.69E+00
09:10	2440.300	80.51	4.60	1.73	9.26E-06	1.68E+00
10:10	2500.300	80.49	4.62	1.71	9.49E-06	1.66E+00
11:10	2560.300	80.44	4.67	1.66	9.72E-06	1.64E+00
12:10	2620.400	80.43	4.68	1.65	9.94E-06	1.63E+00
13:10	2680.400	80.38	4.73	1.60	1.02E-05	1.62E+00
14:10	2740.400	80.37	4.74	1.59	1.04E-05	1.60E+00
15:10	2800.400	80.33	4.78	1.55	1.06E-05	1.59E+00
16:10	2860.400	80.29	4.82	1.51	1.09E-05	1.58E+00
17:10	2920.400	80.27	4.84	1.49	1.11E-05	1.57E+00
18:10	2980.400	80.24	4.87	1.46	1.13E-05	1.55E+00
19:10	3040.200	80.20	4.91	1.42	1.15E-05	1.54E+00
20:10	3100.200	80.18	4.93	1.40	1.18E-05	1.53E+00
21:10	3160.200	80.16	4.95	1.38	1.20E-05	1.52E+00
22:10	3220.200	80.15	4.96	1.37	1.22E-05	1.51E+00
23:10	3280.200	80.13	4.98	1.35	1.24E-05	1.50E+00
00:10	3340.200	80.11	5.00	1.33	1.27E-05	1.49E+00
01:10	3400.200	80.08	5.03	1.30	1.29E-05	1.49E+00
02:10	3460.200	80.06	5.05	1.28	1.31E-05	1.48E+00
03:10	3520.200	80.04	5.07	1.26	1.34E-05	1.47E+00
04:10	3580.300	80.02	5.09	1.24	1.36E-05	1.46E+00
05:10	3640.300	80.00	5.11	1.22	1.38E-05	1.45E+00
06:10	3700.300	79.98	5.13	1.20	1.40E-05	1.45E+00
07:10	3760.300	79.94	5.17	1.16	1.43E-05	1.44E+00
07:36	3786.600	79.93	5.18	1.15	1.44E-05	1.44E+00



PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: REI 7 INPUT 5  
 RADIUS: 1012.704 FEET  
 START DATE: 15-Sep-86  
 START TIME: 13:00  
 WATER START LEVEL: 80.77 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
13:00	0.000	80.77	0.00	0.00E+00
13:00	0.017	-999.99	1080.76	1.15E-11
13:00	0.034	-999.99	1080.76	2.30E-11
13:00	0.050	-999.99	1080.76	3.39E-11
13:00	0.067	-999.99	1080.76	4.54E-11
13:00	0.084	-999.99	1080.76	5.69E-11
13:00	0.100	-999.99	1080.76	6.77E-11
13:00	0.117	-999.99	1080.76	7.92E-11
13:00	0.134	-999.99	1080.76	9.07E-11
13:00	0.150	-999.99	1080.76	1.02E-10
13:00	0.167	-999.99	1080.76	1.13E-10
13:00	0.257	80.77	0.00	1.74E-10
13:00	0.340	80.77	0.00	2.30E-10
13:00	0.424	80.77	0.00	2.87E-10
13:00	0.507	80.77	0.00	3.43E-10
13:00	0.590	80.77	0.00	4.00E-10
13:00	0.674	80.77	0.00	4.56E-10
13:00	0.757	80.77	0.00	5.13E-10
13:00	0.840	80.77	0.00	5.69E-10
13:00	0.924	80.77	0.00	6.26E-10
13:01	1.007	80.77	0.00	6.82E-10
13:01	1.417	80.78	-0.01	9.59E-10
13:01	1.750	80.77	0.00	1.18E-09
13:02	2.084	80.77	0.00	1.41E-09
13:02	2.417	80.77	0.00	1.64E-09
13:02	2.750	80.78	-0.01	1.86E-09
13:03	3.084	80.77	0.00	2.09E-09
13:03	3.417	80.77	0.00	2.31E-09
13:03	3.750	80.77	0.00	2.54E-09
13:04	4.084	80.77	0.00	2.77E-09
13:04	4.417	80.77	0.00	2.99E-09
13:04	4.750	80.77	0.00	3.22E-09
13:05	5.084	80.77	0.00	3.44E-09
13:05	5.417	80.77	0.00	3.67E-09
13:05	5.750	80.76	0.01	3.89E-09
13:06	6.084	80.76	0.01	4.12E-09
13:06	6.417	80.76	0.01	4.35E-09
13:06	6.750	80.76	0.01	4.57E-09
13:07	7.084	80.76	0.01	4.80E-09
13:07	7.417	80.76	0.01	5.02E-09

13:07	7.750	80.76	0.01	5.25E-09
13:08	8.084	80.76	0.01	5.47E-09
13:08	8.417	80.76	0.01	5.70E-09
13:08	8.750	80.76	0.01	5.92E-09
13:09	9.084	80.76	0.01	6.15E-09
13:09	9.417	80.76	0.01	6.38E-09
13:09	9.750	80.76	0.01	6.60E-09
13:10	10.084	80.76	0.01	6.83E-09
13:12	12.101	80.76	0.01	8.19E-09
13:14	14.188	80.76	0.01	9.61E-09
13:16	16.139	80.76	0.01	1.09E-08
13:18	18.237	80.76	0.01	1.23E-08
13:20	20.233	80.75	0.02	1.37E-08
13:22	22.233	80.75	0.02	1.51E-08
13:24	24.233	80.75	0.02	1.64E-08
13:26	26.233	80.75	0.02	1.78E-08
13:28	28.233	80.75	0.02	1.91E-08
13:30	30.233	80.76	0.01	2.05E-08
13:32	32.152	80.75	0.02	2.18E-08
13:34	34.620	80.75	0.02	2.34E-08
13:36	36.095	80.75	0.02	2.44E-08
13:38	38.095	80.75	0.02	2.58E-08
13:40	40.095	80.75	0.02	2.71E-08
13:42	42.195	80.75	0.02	2.86E-08
13:44	44.232	80.75	0.02	3.00E-08
13:46	46.232	80.74	0.03	3.13E-08
13:48	48.252	80.75	0.02	3.27E-08
13:50	50.122	80.74	0.03	3.39E-08
13:52	52.122	80.75	0.02	3.53E-08
13:54	54.122	80.75	0.02	3.66E-08
13:56	56.122	80.75	0.02	3.80E-08
13:58	58.122	80.76	0.01	3.94E-08
14:00	60.122	80.75	0.02	4.07E-08
14:02	62.122	80.75	0.02	4.21E-08
14:04	64.122	80.75	0.02	4.34E-08
14:06	66.442	80.75	0.02	4.50E-08
14:08	68.122	80.75	0.02	4.61E-08
14:10	70.335	80.75	0.02	4.76E-08
14:12	72.160	80.76	0.01	4.89E-08
14:14	74.160	80.76	0.01	5.02E-08
14:16	76.167	80.76	0.01	5.16E-08
14:18	78.230	80.76	0.01	5.30E-08
14:20	80.217	80.75	0.02	5.43E-08
14:22	82.213	80.75	0.02	5.57E-08
14:24	84.213	80.75	0.02	5.70E-08
14:26	86.213	80.75	0.02	5.84E-08
14:28	88.213	80.76	0.01	5.97E-08
14:30	90.213	80.75	0.02	6.11E-08
14:32	92.213	80.75	0.02	6.24E-08
14:34	94.213	80.75	0.02	6.38E-08
14:36	96.213	80.75	0.02	6.51E-08
14:38	98.238	80.75	0.02	6.65E-08
15:00	120.220	80.75	0.02	8.14E-08
15:20	140.130	80.74	0.03	9.49E-08
15:40	160.130	80.75	0.02	1.08E-07
16:00	180.370	80.75	0.02	1.22E-07

16:20	200.200	80.75	0.02	1.36E-07
16:40	220.200	80.75	0.02	1.49E-07
17:00	240.080	80.75	0.02	1.63E-07
17:20	260.220	80.75	0.02	1.76E-07
17:40	280.150	80.75	0.02	1.90E-07
18:00	300.150	80.75	0.02	2.03E-07
18:20	320.130	80.75	0.02	2.17E-07
18:40	340.220	80.76	0.01	2.30E-07
19:00	360.180	80.76	0.01	2.44E-07
19:20	380.220	80.76	0.01	2.57E-07
19:40	400.220	80.77	0.00	2.71E-07
20:00	420.220	80.77	0.00	2.85E-07
20:20	440.220	80.78	-0.01	2.98E-07
20:40	460.220	80.79	-0.02	3.12E-07
21:00	480.120	80.80	-0.03	3.25E-07
21:20	500.220	80.80	-0.03	3.39E-07
21:40	520.320	80.81	-0.04	3.52E-07
22:00	540.200	80.82	-0.05	3.66E-07
22:20	560.100	80.82	-0.05	3.79E-07
22:40	580.100	80.83	-0.06	3.93E-07
23:00	600.150	80.84	-0.07	4.06E-07
23:20	620.150	80.85	-0.08	4.20E-07
23:40	640.180	80.86	-0.09	4.33E-07
00:00	660.180	80.87	-0.10	4.47E-07
00:20	680.180	80.87	-0.10	4.61E-07
00:40	700.180	80.88	-0.11	4.74E-07
01:00	720.180	80.89	-0.12	4.88E-07
01:20	740.180	80.90	-0.13	5.01E-07
01:40	760.180	80.91	-0.14	5.15E-07
02:00	780.180	80.92	-0.15	5.28E-07
02:20	800.180	80.93	-0.16	5.42E-07
02:40	820.180	80.93	-0.16	5.55E-07
03:00	840.180	80.94	-0.17	5.69E-07
03:20	860.180	80.95	-0.18	5.82E-07
03:40	880.180	80.96	-0.19	5.96E-07
04:00	900.180	80.97	-0.20	6.10E-07
04:20	920.180	80.98	-0.21	6.23E-07
04:40	940.180	80.99	-0.22	6.37E-07
05:00	960.180	81.00	-0.23	6.50E-07
05:20	980.180	81.01	-0.24	6.64E-07
05:40	1000.200	81.02	-0.25	6.77E-07
06:40	1060.400	81.05	-0.28	7.18E-07
07:40	1120.500	81.08	-0.31	7.59E-07
08:40	1180.300	81.12	-0.35	7.99E-07
09:40	1240.300	81.15	-0.38	8.40E-07
10:40	1300.200	81.20	-0.43	8.80E-07
11:40	1360.300	81.24	-0.47	9.21E-07
12:40	1420.300	81.25	-0.48	9.62E-07
13:40	1480.200	81.30	-0.53	1.00E-06
14:40	1540.300	81.30	-0.53	1.04E-06
15:40	1600.300	81.32	-0.55	1.08E-06
16:30	1650.600	81.34	-0.57	1.12E-06

TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 7 INPUT 5  
 RADIUS: 1012.704 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 80.77 FEET  
 WATER STOP LEVEL: 81.34 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)	t/r2	t/t'
16:30	0.017	-999.99	1081.33	1080.76	1.15E-11	9.71E+04
16:30	0.034	-999.99	1081.33	1080.76	2.30E-11	4.85E+04
16:30	0.050	-999.99	1081.33	1080.76	3.39E-11	3.30E+04
16:30	0.067	-999.99	1081.33	1080.76	4.54E-11	2.46E+04
16:30	0.084	-999.99	1081.33	1080.76	5.69E-11	1.97E+04
16:30	0.100	-999.99	1081.33	1080.76	6.77E-11	1.65E+04
16:30	0.117	-999.99	1081.33	1080.76	7.92E-11	1.41E+04
16:30	0.134	-999.99	1081.33	1080.76	9.07E-11	1.23E+04
16:30	0.150	-999.99	1081.33	1080.76	1.02E-10	1.10E+04
16:30	0.167	-999.99	1081.33	1080.76	1.13E-10	9.88E+03
16:30	0.257	81.34	0.00	0.57	1.74E-10	6.42E+03
16:30	0.340	81.34	0.00	0.57	2.30E-10	4.86E+03
16:30	0.424	81.35	-0.01	0.58	2.87E-10	3.89E+03
16:30	0.507	81.35	-0.01	0.58	3.43E-10	3.26E+03
16:30	0.591	81.34	0.00	0.57	4.00E-10	2.79E+03
16:30	0.674	81.34	0.00	0.57	4.56E-10	2.45E+03
16:30	0.757	81.34	0.00	0.57	5.13E-10	2.18E+03
16:30	0.840	81.34	0.00	0.57	5.69E-10	1.97E+03
16:30	0.924	81.34	0.00	0.57	6.26E-10	1.79E+03
16:31	1.007	81.34	0.00	0.57	6.82E-10	1.64E+03
16:31	1.417	81.35	-0.01	0.58	9.59E-10	1.17E+03
16:31	1.751	81.35	-0.01	0.58	1.19E-09	9.44E+02
16:32	2.084	81.35	-0.01	0.58	1.41E-09	7.93E+02
16:32	2.417	81.35	-0.01	0.58	1.64E-09	6.84E+02
16:32	2.751	81.35	-0.01	0.58	1.86E-09	6.01E+02
16:33	3.084	81.35	-0.01	0.58	2.09E-09	5.36E+02
16:33	3.417	81.35	-0.01	0.58	2.31E-09	4.84E+02
16:33	3.751	81.35	-0.01	0.58	2.54E-09	4.41E+02
16:34	4.084	81.35	-0.01	0.58	2.77E-09	4.05E+02
16:34	4.417	81.35	-0.01	0.58	2.99E-09	3.75E+02
16:34	4.751	81.35	-0.01	0.58	3.22E-09	3.48E+02
16:35	5.084	81.35	-0.01	0.58	3.44E-09	3.26E+02
16:35	5.417	81.35	-0.01	0.58	3.67E-09	3.06E+02
16:35	5.751	81.35	-0.01	0.58	3.89E-09	2.88E+02
16:36	6.084	81.35	-0.01	0.58	4.12E-09	2.72E+02
16:36	6.417	81.35	-0.01	0.58	4.35E-09	2.58E+02
16:36	6.751	81.35	-0.01	0.58	4.57E-09	2.45E+02
16:37	7.084	81.35	-0.01	0.58	4.80E-09	2.34E+02
16:37	7.417	81.35	-0.01	0.58	5.02E-09	2.24E+02
16:37	7.751	81.35	-0.01	0.58	5.25E-09	2.14E+02
16:38	8.084	81.35	-0.01	0.58	5.47E-09	2.05E+02
16:38	8.417	81.35	-0.01	0.58	5.70E-09	1.97E+02

16:38	8.751	81.35	-0.01	0.58	5.93E-09	1.90E+02
16:39	9.084	81.35	-0.01	0.58	6.15E-09	1.83E+02
16:39	9.417	81.35	-0.01	0.58	6.38E-09	1.76E+02
16:39	9.751	81.35	-0.01	0.58	6.60E-09	1.70E+02
16:40	10.084	81.35	-0.01	0.58	6.83E-09	1.65E+02
16:42	12.120	81.35	-0.01	0.58	8.21E-09	1.37E+02
16:44	14.120	81.35	-0.01	0.58	9.56E-09	1.18E+02
16:46	16.120	81.35	-0.01	0.58	1.09E-08	1.03E+02
16:48	18.120	81.35	-0.01	0.58	1.23E-08	9.21E+01
16:50	20.142	81.35	-0.01	0.58	1.36E-08	8.29E+01
16:52	22.225	81.35	-0.01	0.58	1.50E-08	7.53E+01
16:54	24.225	81.35	-0.01	0.58	1.64E-08	6.91E+01
16:56	26.225	81.36	-0.02	0.59	1.78E-08	6.39E+01
16:58	28.225	81.36	-0.02	0.59	1.91E-08	5.95E+01
17:00	30.225	81.36	-0.02	0.59	2.05E-08	5.56E+01
17:02	32.225	81.35	-0.01	0.58	2.18E-08	5.22E+01
17:04	34.225	81.35	-0.01	0.58	2.32E-08	4.92E+01
17:06	36.225	81.35	-0.01	0.58	2.45E-08	4.66E+01
17:08	38.225	81.35	-0.01	0.58	2.59E-08	4.42E+01
17:10	40.225	81.36	-0.02	0.59	2.72E-08	4.20E+01
17:12	42.225	81.36	-0.02	0.59	2.86E-08	4.01E+01
17:14	44.225	81.36	-0.02	0.59	2.99E-08	3.83E+01
17:16	46.225	81.36	-0.02	0.59	3.13E-08	3.67E+01
17:18	48.225	81.36	-0.02	0.59	3.27E-08	3.52E+01
17:20	50.342	81.36	-0.02	0.59	3.41E-08	3.38E+01
17:22	52.220	81.36	-0.02	0.59	3.54E-08	3.26E+01
17:24	54.222	81.36	-0.02	0.59	3.67E-08	3.14E+01
17:26	56.222	81.36	-0.02	0.59	3.81E-08	3.04E+01
17:28	58.220	81.36	-0.02	0.59	3.94E-08	2.94E+01
17:30	60.120	81.36	-0.02	0.59	4.07E-08	2.85E+01
17:32	62.220	81.36	-0.02	0.59	4.21E-08	2.75E+01
17:34	64.222	81.36	-0.02	0.59	4.35E-08	2.67E+01
17:36	66.220	81.36	-0.02	0.59	4.48E-08	2.59E+01
17:38	68.220	81.36	-0.02	0.59	4.62E-08	2.52E+01
17:40	70.220	81.36	-0.02	0.59	4.75E-08	2.45E+01
17:42	72.220	81.37	-0.03	0.60	4.89E-08	2.39E+01
17:44	74.222	81.36	-0.02	0.59	5.03E-08	2.32E+01
17:46	76.095	81.37	-0.03	0.60	5.15E-08	2.27E+01
17:48	78.180	81.37	-0.03	0.60	5.29E-08	2.21E+01
17:50	80.575	81.37	-0.03	0.60	5.46E-08	2.15E+01
17:52	82.215	81.37	-0.03	0.60	5.57E-08	2.11E+01
17:54	84.215	81.37	-0.03	0.60	5.70E-08	2.06E+01
17:56	86.215	81.37	-0.03	0.60	5.84E-08	2.01E+01
17:58	88.215	81.37	-0.03	0.60	5.97E-08	1.97E+01
18:00	90.493	81.37	-0.03	0.60	6.13E-08	1.92E+01
18:02	92.210	81.37	-0.03	0.60	6.24E-08	1.89E+01
18:04	94.248	81.37	-0.03	0.60	6.38E-08	1.85E+01
18:06	96.248	81.37	-0.03	0.60	6.52E-08	1.81E+01
18:08	98.248	81.37	-0.03	0.60	6.65E-08	1.78E+01
18:30	120.250	81.38	-0.04	0.61	8.14E-08	1.47E+01
18:50	140.250	81.39	-0.05	0.62	9.50E-08	1.28E+01
19:10	160.180	81.39	-0.05	0.62	1.08E-07	1.13E+01
19:30	180.170	81.40	-0.06	0.63	1.22E-07	1.02E+01
19:50	200.220	81.40	-0.06	0.63	1.36E-07	9.24E+00
20:10	220.150	81.41	-0.07	0.64	1.49E-07	8.50E+00
20:30	240.150	81.42	-0.08	0.65	1.63E-07	7.87E+00

20:50	260.150	81.42	-0.08	0.65	1.76E-07	7.34E+00
21:10	280.250	81.43	-0.09	0.66	1.90E-07	6.89E+00
21:30	300.250	81.43	-0.09	0.66	2.03E-07	6.50E+00
21:50	320.250	81.44	-0.10	0.67	2.17E-07	6.15E+00
22:10	340.250	81.44	-0.10	0.67	2.30E-07	5.85E+00
22:30	360.220	81.44	-0.10	0.67	2.44E-07	5.58E+00
22:50	380.080	81.45	-0.11	0.68	2.57E-07	5.34E+00
23:10	400.080	81.45	-0.11	0.68	2.71E-07	5.13E+00
23:30	420.150	81.45	-0.11	0.68	2.84E-07	4.93E+00
23:50	440.080	81.46	-0.12	0.69	2.98E-07	4.75E+00
00:10	460.220	81.45	-0.11	0.68	3.12E-07	4.59E+00
00:30	480.220	81.46	-0.12	0.69	3.25E-07	4.44E+00
00:50	500.220	81.46	-0.12	0.69	3.39E-07	4.30E+00
01:10	520.220	81.46	-0.12	0.69	3.52E-07	4.17E+00
01:30	540.220	81.45	-0.11	0.68	3.66E-07	4.06E+00
01:50	560.220	81.45	-0.11	0.68	3.79E-07	3.95E+00
02:10	580.220	81.45	-0.11	0.68	3.93E-07	3.84E+00
02:30	600.220	81.45	-0.11	0.68	4.06E-07	3.75E+00
02:50	620.220	81.45	-0.11	0.68	4.20E-07	3.66E+00
03:10	640.220	81.45	-0.11	0.68	4.34E-07	3.58E+00
03:30	660.220	81.45	-0.11	0.68	4.47E-07	3.50E+00
03:50	680.220	81.44	-0.10	0.67	4.61E-07	3.43E+00
04:10	700.220	81.44	-0.10	0.67	4.74E-07	3.36E+00
04:30	720.220	81.44	-0.10	0.67	4.88E-07	3.29E+00
04:50	740.220	81.44	-0.10	0.67	5.01E-07	3.23E+00
05:10	760.220	81.43	-0.09	0.66	5.15E-07	3.17E+00
05:30	780.220	81.43	-0.09	0.66	5.28E-07	3.12E+00
05:50	800.220	81.43	-0.09	0.66	5.42E-07	3.06E+00
06:10	820.220	81.43	-0.09	0.66	5.55E-07	3.01E+00
06:30	840.220	81.42	-0.08	0.65	5.69E-07	2.96E+00
06:50	860.220	81.42	-0.08	0.65	5.82E-07	2.92E+00
07:10	880.180	81.42	-0.08	0.65	5.96E-07	2.88E+00
07:30	900.180	81.42	-0.08	0.65	6.10E-07	2.83E+00
07:50	920.180	81.42	-0.08	0.65	6.23E-07	2.79E+00
08:10	940.180	81.41	-0.07	0.64	6.37E-07	2.76E+00
08:30	960.180	81.41	-0.07	0.64	6.50E-07	2.72E+00
08:50	980.170	81.40	-0.06	0.63	6.64E-07	2.68E+00
09:10	1000.200	81.40	-0.06	0.63	6.77E-07	2.65E+00
10:10	1060.400	81.40	-0.06	0.63	7.18E-07	2.56E+00
11:10	1120.700	81.41	-0.07	0.64	7.59E-07	2.47E+00
12:10	1180.300	81.41	-0.07	0.64	7.99E-07	2.40E+00
13:10	1240.300	81.39	-0.05	0.62	8.40E-07	2.33E+00
14:10	1300.400	81.39	-0.05	0.62	8.81E-07	2.27E+00
15:10	1360.300	81.37	-0.03	0.60	9.21E-07	2.21E+00
16:10	1420.200	81.35	-0.01	0.58	9.62E-07	2.16E+00
17:10	1480.300	81.35	-0.01	0.58	1.00E-06	2.12E+00
18:10	1540.300	81.33	0.01	0.56	1.04E-06	2.07E+00
19:10	1600.300	81.33	0.01	0.56	1.08E-06	2.03E+00
20:10	1660.300	81.32	0.02	0.55	1.12E-06	1.99E+00
21:10	1720.300	81.32	0.02	0.55	1.16E-06	1.96E+00
22:10	1780.300	81.31	0.03	0.54	1.21E-06	1.93E+00
23:10	1840.300	81.30	0.04	0.53	1.25E-06	1.90E+00
00:10	1900.300	81.30	0.04	0.53	1.29E-06	1.87E+00
01:10	1960.300	81.29	0.05	0.52	1.33E-06	1.84E+00
02:10	2020.300	81.28	0.06	0.51	1.37E-06	1.82E+00
03:10	2080.300	81.27	0.07	0.50	1.41E-06	1.79E+00

04:10	2140.300	81.26	0.08	0.49	1.45E-06	1.77E+00
05:10	2200.300	81.25	0.09	0.48	1.49E-06	1.75E+00
06:10	2260.300	81.24	0.10	0.47	1.53E-06	1.73E+00
07:10	2320.300	81.24	0.10	0.47	1.57E-06	1.71E+00
08:10	2380.300	81.23	0.11	0.46	1.61E-06	1.69E+00
09:10	2440.300	81.23	0.11	0.46	1.65E-06	1.68E+00
10:10	2500.300	81.23	0.11	0.46	1.69E-06	1.66E+00
11:10	2560.300	81.22	0.12	0.45	1.73E-06	1.64E+00
12:10	2620.400	81.24	0.10	0.47	1.77E-06	1.63E+00
13:10	2680.400	81.21	0.13	0.44	1.81E-06	1.62E+00
14:10	2740.400	81.23	0.11	0.46	1.86E-06	1.60E+00
15:10	2800.400	81.22	0.12	0.45	1.90E-06	1.59E+00
16:10	2860.400	81.19	0.15	0.42	1.94E-06	1.58E+00
17:10	2920.400	81.18	0.16	0.41	1.98E-06	1.57E+00
18:10	2980.400	81.17	0.17	0.40	2.02E-06	1.55E+00
19:10	3040.200	81.16	0.18	0.39	2.06E-06	1.54E+00
20:10	3100.200	81.16	0.18	0.39	2.10E-06	1.53E+00
21:10	3160.200	81.15	0.19	0.38	2.14E-06	1.52E+00
22:10	3220.200	81.15	0.19	0.38	2.18E-06	1.51E+00
23:10	3280.200	81.14	0.20	0.37	2.22E-06	1.50E+00
00:10	3340.200	81.14	0.20	0.37	2.26E-06	1.49E+00
01:10	3400.200	81.13	0.21	0.36	2.30E-06	1.49E+00
02:10	3460.200	81.13	0.21	0.36	2.34E-06	1.48E+00
03:10	3520.200	81.12	0.22	0.35	2.38E-06	1.47E+00
04:10	3580.300	81.11	0.23	0.34	2.42E-06	1.46E+00
05:10	3640.300	81.11	0.23	0.34	2.46E-06	1.45E+00
06:10	3700.300	81.10	0.24	0.33	2.51E-06	1.45E+00
07:10	3760.300	81.08	0.26	0.31	2.55E-06	1.44E+00
07:36	3786.600	81.08	0.26	0.31	2.56E-06	1.44E+00

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: REI 3-4 INPUT 4  
 RADIUS: 784.360 FEET  
 START DATE: 15-Sep-86  
 START TIME: 13:00  
 WATER START LEVEL: 81.18 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
13:00	0.000	81.18	0.00	0.00E+00
13:00	0.017	-999.99	1081.17	1.92E-11
13:00	0.034	-999.99	1081.17	3.84E-11
13:00	0.050	-999.99	1081.17	5.64E-11
13:00	0.067	-999.99	1081.17	7.56E-11
13:00	0.084	-999.99	1081.17	9.48E-11
13:00	0.100	-999.99	1081.17	1.13E-10
13:00	0.117	-999.99	1081.17	1.32E-10
13:00	0.134	-999.99	1081.17	1.51E-10
13:00	0.150	-999.99	1081.17	1.69E-10
13:00	0.167	-999.99	1081.17	1.89E-10
13:00	0.257	81.18	0.00	2.90E-10
13:00	0.340	81.18	0.00	3.84E-10
13:00	0.424	81.18	0.00	4.79E-10
13:00	0.507	81.18	0.00	5.72E-10
13:00	0.590	81.18	0.00	6.66E-10
13:00	0.674	81.18	0.00	7.61E-10
13:00	0.757	81.18	0.00	8.54E-10
13:00	0.840	81.18	0.00	9.48E-10
13:00	0.924	81.19	-0.01	1.04E-09
13:01	1.007	81.19	-0.01	1.14E-09
13:01	1.417	81.19	-0.01	1.60E-09
13:01	1.750	81.19	-0.01	1.98E-09
13:02	2.084	81.19	-0.01	2.35E-09
13:02	2.417	81.19	-0.01	2.73E-09
13:02	2.750	81.19	-0.01	3.10E-09
13:03	3.084	81.19	-0.01	3.48E-09
13:03	3.417	81.19	-0.01	3.86E-09
13:03	3.750	81.18	0.00	4.23E-09
13:04	4.084	81.18	0.00	4.61E-09
13:04	4.417	81.18	0.00	4.99E-09
13:04	4.750	81.18	0.00	5.36E-09
13:05	5.084	81.18	0.00	5.74E-09
13:05	5.417	81.18	0.00	6.11E-09
13:05	5.750	81.18	0.00	6.49E-09
13:06	6.084	81.18	0.00	6.87E-09
13:06	6.417	81.17	0.01	7.24E-09
13:06	6.750	81.17	0.01	7.62E-09
13:07	7.084	81.17	0.01	8.00E-09
13:07	7.417	81.17	0.01	8.37E-09



13:07	7.750	81.17	0.01	8.75E-09
13:08	8.084	81.17	0.01	9.13E-09
13:08	8.417	81.17	0.01	9.50E-09
13:08	8.750	81.17	0.01	9.88E-09
13:09	9.084	81.17	0.01	1.03E-08
13:09	9.417	81.17	0.01	1.06E-08
13:09	9.750	81.17	0.01	1.10E-08
13:10	10.084	81.17	0.01	1.14E-08
13:12	12.101	81.17	0.01	1.37E-08
13:14	14.188	81.18	0.00	1.60E-08
13:16	16.139	81.18	0.00	1.82E-08
13:18	18.237	81.17	0.01	2.06E-08
13:20	20.233	81.18	0.00	2.28E-08
13:22	22.233	81.17	0.01	2.51E-08
13:24	24.233	81.17	0.01	2.74E-08
13:26	26.233	81.18	0.00	2.96E-08
13:28	28.233	81.18	0.00	3.19E-08
13:30	30.233	81.18	0.00	3.41E-08
13:32	32.152	81.19	-0.01	3.63E-08
13:34	34.620	81.19	-0.01	3.91E-08
13:36	36.095	81.20	-0.02	4.07E-08
13:38	38.095	81.20	-0.02	4.30E-08
13:40	40.095	81.21	-0.03	4.53E-08
13:42	42.195	81.22	-0.04	4.76E-08
13:44	44.232	81.22	-0.04	4.99E-08
13:46	46.232	81.23	-0.05	5.22E-08
13:48	48.252	81.24	-0.06	5.45E-08
13:50	50.122	81.25	-0.07	5.66E-08
13:52	52.122	81.26	-0.08	5.88E-08
13:54	54.122	81.27	-0.09	6.11E-08
13:56	56.122	81.29	-0.11	6.33E-08
13:58	58.122	81.31	-0.13	6.56E-08
14:00	60.122	81.31	-0.13	6.79E-08
14:02	62.122	81.32	-0.14	7.01E-08
14:04	64.122	81.33	-0.15	7.24E-08
14:06	66.442	81.35	-0.17	7.50E-08
14:08	68.122	81.36	-0.18	7.69E-08
14:10	70.335	81.38	-0.20	7.94E-08
14:12	72.160	81.39	-0.21	8.15E-08
14:14	74.160	81.40	-0.22	8.37E-08
14:16	76.167	81.42	-0.24	8.60E-08
14:18	78.230	81.43	-0.25	8.83E-08
14:20	80.217	81.45	-0.27	9.05E-08
14:22	82.213	81.46	-0.28	9.28E-08
14:24	84.213	81.48	-0.30	9.51E-08
14:26	86.213	81.49	-0.31	9.73E-08
14:28	88.213	81.50	-0.32	9.96E-08
14:30	90.213	81.52	-0.34	1.02E-07
14:32	92.213	81.54	-0.36	1.04E-07
14:34	94.213	81.55	-0.37	1.06E-07
14:36	96.213	81.56	-0.38	1.09E-07
14:38	98.238	81.58	-0.40	1.11E-07
15:00	120.220	81.75	-0.57	1.36E-07
15:20	140.130	81.90	-0.72	1.58E-07
15:40	160.130	82.06	-0.88	1.81E-07
16:00	180.370	82.22	-1.04	2.04E-07

16:20	200.200	82.36	-1.18	2.26E-07
16:40	220.200	82.50	-1.32	2.49E-07
17:00	240.080	82.63	-1.45	2.71E-07
17:20	260.220	82.76	-1.58	2.94E-07
17:40	280.150	82.88	-1.70	3.16E-07
18:00	300.150	82.99	-1.81	3.39E-07
18:20	320.130	83.10	-1.92	3.61E-07
18:40	340.220	83.20	-2.02	3.84E-07
19:00	360.180	83.30	-2.12	4.07E-07
19:20	380.220	83.41	-2.23	4.29E-07
19:40	400.220	83.50	-2.32	4.52E-07
20:00	420.220	83.60	-2.42	4.74E-07
20:20	440.220	83.69	-2.51	4.97E-07
20:40	460.220	83.79	-2.61	5.19E-07
21:00	480.120	83.88	-2.70	5.42E-07
21:20	500.220	83.97	-2.79	5.65E-07
21:40	520.320	84.05	-2.87	5.87E-07
22:00	540.200	84.14	-2.96	6.10E-07
22:20	560.100	84.22	-3.04	6.32E-07
22:40	580.100	84.30	-3.12	6.55E-07
23:00	600.150	84.38	-3.20	6.77E-07
23:20	620.150	84.46	-3.28	7.00E-07
23:40	640.180	84.55	-3.37	7.23E-07
00:00	660.180	84.63	-3.45	7.45E-07
00:20	680.180	84.71	-3.53	7.68E-07
00:40	700.180	84.79	-3.61	7.90E-07
01:00	720.180	84.88	-3.70	8.13E-07
01:20	740.180	84.96	-3.78	8.35E-07
01:40	760.180	85.04	-3.86	8.58E-07
02:00	780.180	85.12	-3.94	8.81E-07
02:20	800.180	85.20	-4.02	9.03E-07
02:40	820.180	85.28	-4.10	9.26E-07
03:00	840.180	85.36	-4.18	9.48E-07
03:20	860.180	85.43	-4.25	9.71E-07
03:40	880.180	85.51	-4.33	9.94E-07
04:00	900.180	85.58	-4.40	1.02E-06
04:20	920.180	85.65	-4.47	1.04E-06
04:40	940.180	85.72	-4.54	1.06E-06
05:00	960.180	85.78	-4.60	1.08E-06
05:20	980.180	85.84	-4.66	1.11E-06
05:40	1000.200	85.91	-4.73	1.13E-06
06:40	1060.400	86.09	-4.91	1.20E-06
07:40	1120.500	86.25	-5.07	1.26E-06
08:40	1180.300	86.41	-5.23	1.33E-06
09:40	1240.300	86.57	-5.39	1.40E-06
10:40	1300.200	86.71	-5.53	1.47E-06
11:40	1360.300	86.83	-5.65	1.54E-06
12:40	1420.300	86.83	-5.65	1.60E-06
13:40	1480.200	86.79	-5.61	1.67E-06
14:40	1540.300	86.72	-5.54	1.74E-06
15:40	1600.300	86.68	-5.50	1.81E-06
16:30	1650.600	86.68	-5.50	1.86E-06

TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 3-4 INPUT 4  
 RADIUS: 784.360 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 81.18 FEET  
 WATER STOP LEVEL: 86.68 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)	t/r2	t/t'
16:30	0.017	-999.99	1086.67	1081.17	1.92E-11	9.71E+04
16:30	0.034	-999.99	1086.67	1081.17	3.84E-11	4.85E+04
16:30	0.050	-999.99	1086.67	1081.17	5.64E-11	3.30E+04
16:30	0.067	-999.99	1086.67	1081.17	7.56E-11	2.46E+04
16:30	0.084	-999.99	1086.67	1081.17	9.48E-11	1.97E+04
16:30	0.100	-999.99	1086.67	1081.17	1.13E-10	1.65E+04
16:30	0.117	-999.99	1086.67	1081.17	1.32E-10	1.41E+04
16:30	0.134	-999.99	1086.67	1081.17	1.51E-10	1.23E+04
16:30	0.150	-999.99	1086.67	1081.17	1.69E-10	1.10E+04
16:30	0.167	-999.99	1086.67	1081.17	1.89E-10	9.88E+03
16:30	0.257	86.68	0.00	5.50	2.90E-10	6.42E+03
16:30	0.340	86.68	0.00	5.50	3.84E-10	4.86E+03
16:30	0.424	86.68	0.00	5.50	4.79E-10	3.89E+03
16:30	0.507	86.68	0.00	5.50	5.72E-10	3.26E+03
16:30	0.591	86.68	0.00	5.50	6.67E-10	2.79E+03
16:30	0.674	86.68	0.00	5.50	7.61E-10	2.45E+03
16:30	0.757	86.67	0.01	5.49	8.54E-10	2.18E+03
16:30	0.840	86.68	0.00	5.50	9.48E-10	1.97E+03
16:30	0.924	86.68	0.00	5.50	1.04E-09	1.79E+03
16:31	1.007	86.68	0.00	5.50	1.14E-09	1.64E+03
16:31	1.417	86.68	0.00	5.50	1.60E-09	1.17E+03
16:31	1.751	86.68	0.00	5.50	1.98E-09	9.44E+02
16:32	2.084	86.67	0.01	5.49	2.35E-09	7.93E+02
16:32	2.417	86.68	0.00	5.50	2.73E-09	6.84E+02
16:32	2.751	86.68	0.00	5.50	3.11E-09	6.01E+02
16:33	3.084	86.68	0.00	5.50	3.48E-09	5.36E+02
16:33	3.417	86.67	0.01	5.49	3.86E-09	4.84E+02
16:33	3.751	86.68	0.00	5.50	4.23E-09	4.41E+02
16:34	4.084	86.68	0.00	5.50	4.61E-09	4.05E+02
16:34	4.417	86.68	0.00	5.50	4.99E-09	3.75E+02
16:34	4.751	86.67	0.01	5.49	5.36E-09	3.48E+02
16:35	5.084	86.67	0.01	5.49	5.74E-09	3.26E+02
16:35	5.417	86.67	0.01	5.49	6.11E-09	3.06E+02
16:35	5.751	86.68	0.00	5.50	6.49E-09	2.88E+02
16:36	6.084	86.67	0.01	5.49	6.87E-09	2.72E+02
16:36	6.417	86.68	0.00	5.50	7.24E-09	2.58E+02
16:36	6.751	86.67	0.01	5.49	7.62E-09	2.45E+02
16:37	7.084	86.68	0.00	5.50	8.00E-09	2.34E+02
16:37	7.417	86.68	0.00	5.50	8.37E-09	2.24E+02
16:37	7.751	86.68	0.00	5.50	8.75E-09	2.14E+02
16:38	8.084	86.68	0.00	5.50	9.13E-09	2.05E+02
16:38	8.417	86.68	0.00	5.50	9.50E-09	1.97E+02

16:38	8.751	86.68	0.00	5.50	9.88E-09	1.90E+02
16:39	9.084	86.68	0.00	5.50	1.03E-08	1.83E+02
16:39	9.417	86.68	0.00	5.50	1.06E-08	1.76E+02
16:39	9.751	86.68	0.00	5.50	1.10E-08	1.70E+02
16:40	10.084	86.68	0.00	5.50	1.14E-08	1.65E+02
16:42	12.120	86.67	0.01	5.49	1.37E-08	1.37E+02
16:44	14.120	86.67	0.01	5.49	1.59E-08	1.18E+02
16:46	16.120	86.67	0.01	5.49	1.82E-08	1.03E+02
16:48	18.120	86.67	0.01	5.49	2.05E-08	9.21E+01
16:50	20.142	86.67	0.01	5.49	2.27E-08	8.29E+01
16:52	22.225	86.66	0.02	5.48	2.51E-08	7.53E+01
16:54	24.225	86.66	0.02	5.48	2.73E-08	6.91E+01
16:56	26.225	86.66	0.02	5.48	2.96E-08	6.39E+01
16:58	28.225	86.66	0.02	5.48	3.19E-08	5.95E+01
17:00	30.225	86.65	0.03	5.47	3.41E-08	5.56E+01
17:02	32.225	86.65	0.03	5.47	3.64E-08	5.22E+01
17:04	34.225	86.65	0.03	5.47	3.86E-08	4.92E+01
17:06	36.225	86.64	0.04	5.46	4.09E-08	4.66E+01
17:08	38.225	86.64	0.04	5.46	4.31E-08	4.42E+01
17:10	40.225	86.63	0.05	5.45	4.54E-08	4.20E+01
17:12	42.225	86.63	0.05	5.45	4.77E-08	4.01E+01
17:14	44.225	86.62	0.06	5.44	4.99E-08	3.83E+01
17:16	46.225	86.62	0.06	5.44	5.22E-08	3.67E+01
17:18	48.225	86.61	0.07	5.43	5.44E-08	3.52E+01
17:20	50.342	86.61	0.07	5.43	5.68E-08	3.38E+01
17:22	52.220	86.60	0.08	5.42	5.89E-08	3.26E+01
17:24	54.222	86.59	0.09	5.41	6.12E-08	3.14E+01
17:26	56.222	86.58	0.10	5.40	6.35E-08	3.04E+01
17:28	58.220	86.58	0.10	5.40	6.57E-08	2.94E+01
17:30	60.120	86.57	0.11	5.39	6.79E-08	2.85E+01
17:32	62.220	86.56	0.12	5.38	7.02E-08	2.75E+01
17:34	64.222	86.55	0.13	5.37	7.25E-08	2.67E+01
17:36	66.220	86.54	0.14	5.36	7.47E-08	2.59E+01
17:38	68.220	86.54	0.14	5.36	7.70E-08	2.52E+01
17:40	70.220	86.53	0.15	5.35	7.93E-08	2.45E+01
17:42	72.220	86.52	0.16	5.34	8.15E-08	2.39E+01
17:44	74.222	86.51	0.17	5.33	8.38E-08	2.32E+01
17:46	76.095	86.50	0.18	5.32	8.59E-08	2.27E+01
17:48	78.180	86.50	0.18	5.32	8.82E-08	2.21E+01
17:50	80.575	86.48	0.20	5.30	9.10E-08	2.15E+01
17:52	82.215	86.48	0.20	5.30	9.28E-08	2.11E+01
17:54	84.215	86.47	0.21	5.29	9.51E-08	2.06E+01
17:56	86.215	86.45	0.23	5.27	9.73E-08	2.01E+01
17:58	88.215	86.45	0.23	5.27	9.96E-08	1.97E+01
18:00	90.493	86.44	0.24	5.26	1.02E-07	1.92E+01
18:02	92.210	86.43	0.25	5.25	1.04E-07	1.89E+01
18:04	94.248	86.42	0.26	5.24	1.06E-07	1.85E+01
18:06	96.248	86.41	0.27	5.23	1.09E-07	1.81E+01
18:08	98.248	86.40	0.28	5.22	1.11E-07	1.78E+01
18:30	120.250	86.29	0.39	5.11	1.36E-07	1.47E+01
18:50	140.250	86.18	0.50	5.00	1.58E-07	1.28E+01
19:10	160.180	86.08	0.60	4.90	1.81E-07	1.13E+01
19:30	180.170	85.98	0.70	4.80	2.03E-07	1.02E+01
19:50	200.220	85.88	0.80	4.70	2.26E-07	9.24E+00
20:10	220.150	85.79	0.89	4.61	2.48E-07	8.50E+00
20:30	240.150	85.70	0.98	4.52	2.71E-07	7.87E+00

20:50	260.150	85.61	1.07	4.43	2.94E-07	7.34E+00
21:10	280.250	85.53	1.15	4.35	3.16E-07	6.89E+00
21:30	300.250	85.45	1.23	4.27	3.39E-07	6.50E+00
21:50	320.250	85.38	1.30	4.20	3.61E-07	6.15E+00
22:10	340.250	85.30	1.38	4.12	3.84E-07	5.85E+00
22:30	360.220	85.23	1.45	4.05	4.07E-07	5.58E+00
22:50	380.080	85.16	1.52	3.98	4.29E-07	5.34E+00
23:10	400.080	85.10	1.58	3.92	4.52E-07	5.13E+00
23:30	420.150	85.03	1.65	3.85	4.74E-07	4.93E+00
23:50	440.080	84.97	1.71	3.79	4.97E-07	4.75E+00
00:10	460.220	84.91	1.77	3.73	5.19E-07	4.59E+00
00:30	480.220	84.85	1.83	3.67	5.42E-07	4.44E+00
00:50	500.220	84.80	1.88	3.62	5.65E-07	4.30E+00
01:10	520.220	84.74	1.94	3.56	5.87E-07	4.17E+00
01:30	540.220	84.69	1.99	3.51	6.10E-07	4.06E+00
01:50	560.220	84.64	2.04	3.46	6.32E-07	3.95E+00
02:10	580.220	84.59	2.09	3.41	6.55E-07	3.84E+00
02:30	600.220	84.54	2.14	3.36	6.78E-07	3.75E+00
02:50	620.220	84.50	2.18	3.32	7.00E-07	3.66E+00
03:10	640.220	84.45	2.23	3.27	7.23E-07	3.58E+00
03:30	660.220	84.41	2.27	3.23	7.45E-07	3.50E+00
03:50	680.220	84.36	2.32	3.18	7.68E-07	3.43E+00
04:10	700.220	84.32	2.36	3.14	7.90E-07	3.36E+00
04:30	720.220	84.28	2.40	3.10	8.13E-07	3.29E+00
04:50	740.220	84.24	2.44	3.06	8.36E-07	3.23E+00
05:10	760.220	84.21	2.47	3.03	8.58E-07	3.17E+00
05:30	780.220	84.17	2.51	2.99	8.81E-07	3.12E+00
05:50	800.220	84.13	2.55	2.95	9.03E-07	3.06E+00
06:10	820.220	84.10	2.58	2.92	9.26E-07	3.01E+00
06:30	840.220	84.07	2.61	2.89	9.48E-07	2.96E+00
06:50	860.220	84.03	2.65	2.85	9.71E-07	2.92E+00
07:10	880.180	84.00	2.68	2.82	9.94E-07	2.88E+00
07:30	900.180	83.97	2.71	2.79	1.02E-06	2.83E+00
07:50	920.180	83.94	2.74	2.76	1.04E-06	2.79E+00
08:10	940.180	83.92	2.76	2.74	1.06E-06	2.76E+00
08:30	960.180	83.89	2.79	2.71	1.08E-06	2.72E+00
08:50	980.170	83.87	2.81	2.69	1.11E-06	2.68E+00
09:10	1000.200	83.84	2.84	2.66	1.13E-06	2.65E+00
10:10	1060.400	83.78	2.90	2.60	1.20E-06	2.56E+00
11:10	1120.700	83.71	2.97	2.53	1.27E-06	2.47E+00
12:10	1180.300	83.64	3.04	2.46	1.33E-06	2.40E+00
13:10	1240.300	83.56	3.12	2.38	1.40E-06	2.33E+00
14:10	1300.400	83.51	3.17	2.33	1.47E-06	2.27E+00
15:10	1360.300	83.43	3.25	2.25	1.54E-06	2.21E+00
16:10	1420.200	83.38	3.30	2.20	1.60E-06	2.16E+00
17:10	1480.300	83.34	3.34	2.16	1.67E-06	2.12E+00
18:10	1540.300	83.28	3.40	2.10	1.74E-06	2.07E+00
19:10	1600.300	83.23	3.45	2.05	1.81E-06	2.03E+00
20:10	1660.300	83.18	3.50	2.00	1.87E-06	1.99E+00
21:10	1720.300	83.14	3.54	1.96	1.94E-06	1.96E+00
22:10	1780.300	83.11	3.57	1.93	2.01E-06	1.93E+00
23:10	1840.300	83.07	3.61	1.89	2.08E-06	1.90E+00
00:10	1900.300	83.03	3.65	1.85	2.15E-06	1.87E+00
01:10	1960.300	82.99	3.69	1.81	2.21E-06	1.84E+00
02:10	2020.300	82.95	3.73	1.77	2.28E-06	1.82E+00
03:10	2080.300	82.92	3.76	1.74	2.35E-06	1.79E+00

04:10	2140.300	82.88	3.80	1.70	2.42E-06	1.77E+00
05:10	2200.300	82.84	3.84	1.66	2.48E-06	1.75E+00
06:10	2260.300	82.81	3.87	1.63	2.55E-06	1.73E+00
07:10	2320.300	82.77	3.91	1.59	2.62E-06	1.71E+00
08:10	2380.300	82.75	3.93	1.57	2.69E-06	1.69E+00
09:10	2440.300	82.73	3.95	1.55	2.75E-06	1.68E+00
10:10	2500.300	82.71	3.97	1.53	2.82E-06	1.66E+00
11:10	2560.300	82.66	4.02	1.48	2.89E-06	1.64E+00
12:10	2620.400	82.66	4.02	1.48	2.96E-06	1.63E+00
13:10	2680.400	82.61	4.07	1.43	3.03E-06	1.62E+00
14:10	2740.400	82.61	4.07	1.43	3.09E-06	1.60E+00
15:10	2800.400	82.57	4.11	1.39	3.16E-06	1.59E+00
16:10	2860.400	82.54	4.14	1.36	3.23E-06	1.58E+00
17:10	2920.400	82.53	4.15	1.35	3.30E-06	1.57E+00
18:10	2980.400	82.50	4.18	1.32	3.36E-06	1.55E+00
19:10	3040.200	82.47	4.21	1.29	3.43E-06	1.54E+00
20:10	3100.200	82.44	4.24	1.26	3.50E-06	1.53E+00
21:10	3160.200	82.43	4.25	1.25	3.57E-06	1.52E+00
22:10	3220.200	82.41	4.27	1.23	3.63E-06	1.51E+00
23:10	3280.200	82.39	4.29	1.21	3.70E-06	1.50E+00
00:10	3340.200	82.38	4.30	1.20	3.77E-06	1.49E+00
01:10	3400.200	82.35	4.33	1.17	3.84E-06	1.49E+00
02:10	3460.200	82.33	4.35	1.15	3.91E-06	1.48E+00
03:10	3520.200	82.31	4.37	1.13	3.97E-06	1.47E+00
04:10	3580.300	82.29	4.39	1.11	4.04E-06	1.46E+00
05:10	3640.300	82.27	4.41	1.09	4.11E-06	1.45E+00
06:10	3700.300	82.25	4.43	1.07	4.18E-06	1.45E+00
07:10	3760.300	82.22	4.46	1.04	4.24E-06	1.44E+00
07:36	3786.600	82.21	4.47	1.03	4.27E-06	1.44E+00

PROJECT NAME: FRENCH, LTD.  
 PROJECT NUMBER: 275-14  
 TEST NAME: REI 10-1 RUN #1  
 TEST DATE: 15-Sep-86  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: REI 12-1 INPUT 1  
 LEVEL (F) TOC (ADJ.)  
 RADIUS: 1492.112 FEET  
 STARTING WATER LEVEL: 78.050 FEET (ADJ.)

ELAPSED TIME (MIN - ADJ)	LEVEL (FEET) (ADJ.)	DELTA HEAD (FEET)	t/r <sup>2</sup>
28.000	78.06	0.01	8.73E-09
58.000	78.07	0.02	1.81E-08
88.000	78.06	0.01	2.74E-08
118.000	78.05	0.00	3.68E-08
148.000	78.04	-0.01	4.62E-08
178.000	78.01	-0.04	5.55E-08
208.000	78.02	-0.03	6.49E-08
238.000	78.06	0.01	7.42E-08
268.000	78.12	0.07	8.36E-08
298.000	78.17	0.12	9.30E-08
328.000	78.24	0.19	1.02E-07
358.000	78.31	0.26	1.12E-07
388.000	78.39	0.34	1.21E-07
418.000	78.47	0.42	1.30E-07
448.000	78.55	0.50	1.40E-07
478.000	78.64	0.59	1.49E-07
508.000	78.72	0.67	1.58E-07
538.000	78.82	0.77	1.68E-07
568.000	78.91	0.86	1.77E-07
598.000	79.00	0.95	1.87E-07
628.000	79.09	1.04	1.96E-07
658.000	79.18	1.13	2.05E-07
688.000	79.27	1.22	2.15E-07
718.000	79.36	1.31	2.24E-07
748.000	79.45	1.40	2.33E-07
778.000	79.55	1.50	2.43E-07
808.000	79.64	1.59	2.52E-07
838.000	79.73	1.68	2.61E-07
868.000	79.83	1.78	2.71E-07
898.000	79.92	1.87	2.80E-07
928.000	80.02	1.97	2.89E-07
958.000	80.12	2.07	2.99E-07
988.000	80.21	2.16	3.08E-07
1018.000	80.31	2.26	3.18E-07
1048.000	80.40	2.35	3.27E-07
1078.000	80.50	2.45	3.36E-07
1108.000	80.60	2.55	3.46E-07
1138.000	80.69	2.64	3.55E-07
1168.000	80.79	2.74	3.64E-07
1198.000	80.88	2.83	3.74E-07
1228.000	80.97	2.92	3.83E-07
1258.000	81.07	3.02	3.92E-07

1288.000	81.16	3.11	4.02E-07
1318.000	81.26	3.21	4.11E-07
1348.000	81.35	3.30	4.20E-07
1378.000	81.44	3.39	4.30E-07
1408.000	81.52	3.47	4.39E-07
1438.000	81.61	3.56	4.49E-07
1468.000	81.69	3.64	4.58E-07
1498.000	81.75	3.70	4.67E-07
1528.000	81.81	3.76	4.77E-07
1558.000	81.86	3.81	4.86E-07
1588.000	81.92	3.87	4.95E-07
1618.000	81.98	3.93	5.05E-07
1648.000	82.03	3.98	5.14E-07
1678.000	82.08	4.03	5.23E-07
1708.000	82.12	4.07	5.33E-07
1738.000	82.17	4.12	5.42E-07
1768.000	82.20	4.15	5.51E-07
1798.000	82.23	4.18	5.61E-07
1828.000	82.25	4.20	5.70E-07
1858.000	82.27	4.22	5.80E-07
1888.000	82.28	4.23	5.89E-07
1918.000	82.28	4.23	5.98E-07
1948.000	82.28	4.23	6.08E-07
1978.000	82.28	4.23	6.17E-07
2008.000	82.27	4.22	6.26E-07
2038.000	82.25	4.20	6.36E-07
2068.000	82.24	4.19	6.45E-07
2098.000	82.21	4.16	6.54E-07
2128.000	82.19	4.14	6.64E-07
2158.000	82.16	4.11	6.73E-07
2188.000	82.14	4.09	6.82E-07
2218.000	82.11	4.06	6.92E-07
2248.000	82.08	4.03	7.01E-07
2278.000	82.04	3.99	7.11E-07
2308.000	82.01	3.96	7.20E-07
2338.000	81.98	3.93	7.29E-07
2368.000	81.95	3.90	7.39E-07
2398.000	81.91	3.86	7.48E-07
2428.000	81.87	3.82	7.57E-07
2458.000	81.83	3.78	7.67E-07
2488.000	81.80	3.75	7.76E-07
2518.000	81.77	3.72	7.85E-07
2548.000	81.74	3.69	7.95E-07
2578.000	81.70	3.65	8.04E-07
2608.000	81.67	3.62	8.13E-07
2638.000	81.62	3.57	8.23E-07
2668.000	81.59	3.54	8.32E-07
2698.000	81.56	3.51	8.42E-07
2728.000	81.53	3.48	8.51E-07
2758.000	81.50	3.45	8.60E-07
2788.000	81.48	3.43	8.70E-07
2818.000	81.45	3.40	8.79E-07
2848.000	81.41	3.36	8.88E-07
2878.000	81.38	3.33	8.98E-07
2908.000	81.35	3.30	9.07E-07
2938.000	81.32	3.27	9.16E-07
2968.000	81.29	3.24	9.26E-07
2998.000	81.24	3.19	9.35E-07



3028.000	81.20	3.15	9.44E-07
3058.000	81.17	3.12	9.54E-07
3088.000	81.14	3.09	9.63E-07
3118.000	81.12	3.07	9.73E-07
3148.000	81.09	3.04	9.82E-07
3178.000	81.05	3.00	9.91E-07
3208.000	81.02	2.97	1.00E-06
3238.000	80.99	2.94	1.01E-06
3268.000	80.96	2.91	1.02E-06
3298.000	80.93	2.88	1.03E-06
3328.000	80.91	2.86	1.04E-06
3358.000	80.88	2.83	1.05E-06
3388.000	80.86	2.81	1.06E-06
3418.000	80.84	2.79	1.07E-06
3448.000	80.81	2.76	1.08E-06
3478.000	80.79	2.74	1.08E-06
3508.000	80.77	2.72	1.09E-06
3538.000	80.74	2.69	1.10E-06
3568.000	80.72	2.67	1.11E-06
3598.000	80.69	2.64	1.12E-06
3628.000	80.67	2.62	1.13E-06
3658.000	80.65	2.60	1.14E-06
3688.000	80.62	2.57	1.15E-06
3718.000	80.60	2.55	1.16E-06
3748.000	80.58	2.53	1.17E-06
3778.000	80.55	2.50	1.18E-06
3808.000	80.53	2.48	1.19E-06
3838.000	80.51	2.46	1.20E-06
3868.000	80.48	2.43	1.21E-06
3898.000	80.46	2.41	1.22E-06
3928.000	80.44	2.39	1.23E-06
3958.000	80.42	2.37	1.23E-06
3988.000	80.40	2.35	1.24E-06
4018.000	80.38	2.33	1.25E-06
4048.000	80.36	2.31	1.26E-06
4078.000	80.34	2.29	1.27E-06
4108.000	80.33	2.28	1.28E-06
4138.000	80.31	2.26	1.29E-06
4168.000	80.30	2.25	1.30E-06
4198.000	80.28	2.23	1.31E-06
4228.000	80.26	2.21	1.32E-06
4258.000	80.25	2.20	1.33E-06
4288.000	80.23	2.18	1.34E-06
4318.000	80.20	2.15	1.35E-06
4348.000	80.19	2.14	1.36E-06
4378.000	80.17	2.12	1.37E-06
4408.000	80.17	2.12	1.37E-06
4438.000	80.15	2.10	1.38E-06
4468.000	80.13	2.08	1.39E-06
4498.000	80.11	2.06	1.40E-06
4528.000	80.08	2.03	1.41E-06
4558.000	80.07	2.02	1.42E-06
4588.000	80.04	1.99	1.43E-06
4618.000	80.02	1.97	1.44E-06
4648.000	80.00	1.95	1.45E-06
4678.000	79.98	1.93	1.46E-06
4708.000	79.96	1.91	1.47E-06
4738.000	79.95	1.90	1.48E-06

4768.000	79.93	1.88	1.49E-06
4798.000	79.92	1.87	1.50E-06
4828.000	79.90	1.85	1.51E-06
4858.000	79.89	1.84	1.52E-06
4888.000	79.88	1.83	1.52E-06
4918.000	79.87	1.82	1.53E-06
4948.000	79.86	1.81	1.54E-06
4978.000	79.84	1.79	1.55E-06
5008.000	79.83	1.78	1.56E-06
5038.000	79.82	1.77	1.57E-06
5068.000	79.80	1.75	1.58E-06
5098.000	79.79	1.74	1.59E-06
5128.000	79.78	1.73	1.60E-06
5158.000	79.76	1.71	1.61E-06
5188.000	79.75	1.70	1.62E-06
5218.000	79.73	1.68	1.63E-06
5248.000	79.72	1.67	1.64E-06
5278.000	79.70	1.65	1.65E-06
5308.000	79.69	1.64	1.66E-06
5338.000	79.67	1.62	1.66E-06
5368.000	79.65	1.60	1.67E-06
5398.000	79.63	1.58	1.68E-06
5428.000	79.61	1.56	1.69E-06
5458.000	79.60	1.55	1.70E-06
5488.000	79.60	1.55	1.71E-06
5518.000	79.57	1.52	1.72E-06
5548.000	79.56	1.51	1.73E-06
5578.000	79.55	1.50	1.74E-06
5608.000	79.54	1.49	1.75E-06
5638.000	79.53	1.48	1.76E-06
5668.000	79.52	1.47	1.77E-06
5698.000	79.51	1.46	1.78E-06
5728.000	79.49	1.44	1.79E-06
5758.000	79.48	1.43	1.80E-06
5788.000	79.48	1.43	1.81E-06
5818.000	79.48	1.43	1.81E-06
5848.000	79.49	1.44	1.82E-06
5878.000	79.51	1.46	1.83E-06
5908.000	79.54	1.49	1.84E-06
5938.000	79.58	1.53	1.85E-06
5968.000	79.64	1.59	1.86E-06

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME: REI 10-1 RUN # 1  
TEST TYPE: DRAWDOWN  
WELL NUMBER: P 10-2 INPUT 6  
RADIUS: 20.845 FEET  
START DATE: 15-Sep-86  
START TIME: 13:00  
WATER START LEVEL: 46.07 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
13:00	0.000	46.07	0.00
13:00	0.017	-999.99	1046.06
13:00	0.034	-999.99	1046.06
13:00	0.050	-999.99	1046.06
13:00	0.067	-999.99	1046.06
13:00	0.084	-999.99	1046.06
13:00	0.100	-999.99	1046.06
13:00	0.117	-999.99	1046.06
13:00	0.134	-999.99	1046.06
13:00	0.150	-999.99	1046.06
13:00	0.167	-999.99	1046.06
13:00	0.257	46.06	0.01
13:00	0.340	46.06	0.01
13:00	0.424	46.06	0.01
13:00	0.507	46.05	0.02
13:00	0.590	46.05	0.02
13:00	0.674	46.05	0.02
13:00	0.757	46.05	0.02
13:00	0.840	46.06	0.01
13:00	0.924	46.05	0.02
13:01	1.007	46.05	0.02
13:01	1.417	46.06	0.01
13:01	1.750	46.06	0.01
13:02	2.084	46.06	0.01
13:02	2.417	46.05	0.02
13:02	2.750	46.06	0.01
13:03	3.084	46.05	0.02
13:03	3.417	46.05	0.02
13:03	3.750	46.04	0.03
13:04	4.084	46.04	0.03
13:04	4.417	46.04	0.03
13:04	4.750	46.03	0.04
13:05	5.084	46.02	0.05
13:05	5.417	46.02	0.05
13:05	5.750	46.01	0.06
13:06	6.084	46.00	0.07
13:06	6.417	46.00	0.07
13:06	6.750	45.99	0.08
13:07	7.084	45.99	0.08
13:07	7.417	45.98	0.09

13:07	7.750	45.98	0.09
13:08	8.084	45.98	0.09
13:08	8.417	45.98	0.09
13:08	8.750	45.98	0.09
13:09	9.084	45.98	0.09
13:09	9.417	45.98	0.09
13:09	9.750	45.98	0.09
13:10	10.084	45.98	0.09
13:12	12.101	45.99	0.08
13:14	14.188	46.00	0.07
13:16	16.139	45.99	0.08
13:18	18.237	45.98	0.09
13:20	20.233	45.97	0.10
13:22	22.233	45.96	0.11
13:24	24.233	45.96	0.11
13:26	26.233	45.96	0.11
13:28	28.233	45.97	0.10
13:30	30.233	45.96	0.11
13:32	32.152	45.97	0.10
13:34	34.620	45.97	0.10
13:36	36.095	45.97	0.10
13:38	38.095	45.98	0.09
13:40	40.095	45.97	0.10
13:42	42.195	45.98	0.09
13:44	44.232	45.97	0.10
13:46	46.232	45.96	0.11
13:48	48.252	45.96	0.11
13:50	50.122	45.97	0.10
13:52	52.122	45.99	0.08
13:54	54.122	46.00	0.07
13:56	56.122	46.00	0.07
13:58	58.122	46.01	0.06
14:00	60.122	46.02	0.05
14:02	62.122	46.00	0.07
14:04	64.122	46.00	0.07
14:06	66.442	46.00	0.07
14:08	68.122	46.01	0.06
14:10	70.335	46.02	0.05
14:12	72.160	46.03	0.04
14:14	74.160	46.03	0.04
14:16	76.167	46.03	0.04
14:18	78.230	46.02	0.05
14:20	80.217	46.03	0.04
14:22	82.213	46.03	0.04
14:24	84.213	46.02	0.05
14:26	86.213	46.02	0.05
14:28	88.213	46.01	0.06
14:30	90.213	46.00	0.07
14:32	92.213	46.01	0.06
14:34	94.213	46.00	0.07
14:36	96.213	46.00	0.07
14:38	98.238	45.99	0.08
15:00	120.220	46.01	0.06
15:20	140.130	45.99	0.08
15:40	160.130	46.00	0.07
16:00	180.370	45.99	0.08

16:20	200.200	45.99	0.08
16:40	220.200	46.00	0.07
17:00	240.080	46.00	0.07
17:20	260.220	46.00	0.07
17:40	280.150	46.01	0.06
18:00	300.150	45.97	0.10
18:20	320.130	45.98	0.09
18:40	340.220	45.99	0.08
19:00	360.180	46.00	0.07
19:20	380.220	46.00	0.07
19:40	400.220	45.98	0.09
20:00	420.220	45.96	0.11
20:20	440.220	45.96	0.11
20:40	460.220	45.97	0.10
21:00	480.120	45.97	0.10
21:20	500.220	45.97	0.10
21:40	520.320	45.97	0.10
22:00	540.200	45.98	0.09
22:20	560.100	45.98	0.09
22:40	580.100	45.98	0.09
23:00	600.150	45.98	0.09
23:20	620.150	45.98	0.09
23:40	640.180	46.00	0.07
00:00	660.180	45.98	0.09
00:20	680.180	45.98	0.09
00:40	700.180	45.96	0.11
01:00	720.180	45.96	0.11
01:20	740.180	45.97	0.10
01:40	760.180	46.01	0.06
02:00	780.180	46.01	0.06
02:20	800.180	45.99	0.08
02:40	820.180	45.98	0.09
03:00	840.180	45.98	0.09
03:20	860.180	45.97	0.10
03:40	880.180	45.97	0.10
04:00	900.180	45.96	0.11
04:20	920.180	45.96	0.11
04:40	940.180	45.96	0.11
05:00	960.180	45.96	0.11
05:20	980.180	45.95	0.12
05:40	1000.200	45.95	0.12
06:40	1060.400	45.94	0.13
07:40	1120.500	45.93	0.14
08:40	1180.300	45.94	0.13
09:40	1240.300	45.94	0.13
10:40	1300.200	45.95	0.12
11:40	1360.300	45.99	0.08
12:40	1420.300	45.99	0.08
13:40	1480.200	46.04	0.03
14:40	1540.300	45.97	0.10
15:40	1600.300	45.98	0.09
16:30	1650.600	45.98	0.09

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: P 10-2 INPUT 6  
 RADIUS: 20.845 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 46.07 FEET  
 WATER STOP LEVEL: 45.98 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
16:30	0.017	-999.99	1045.97	1046.06
16:30	0.034	-999.99	1045.97	1046.06
16:30	0.050	-999.99	1045.97	1046.06
16:30	0.067	-999.99	1045.97	1046.06
16:30	0.084	-999.99	1045.97	1046.06
16:30	0.100	-999.99	1045.97	1046.06
16:30	0.117	-999.99	1045.97	1046.06
16:30	0.134	-999.99	1045.97	1046.06
16:30	0.150	-999.99	1045.97	1046.06
16:30	0.167	-999.99	1045.97	1046.06
16:30	0.257	45.98	0.00	0.09
16:30	0.340	45.98	0.00	0.09
16:30	0.424	45.98	0.00	0.09
16:30	0.507	45.98	0.00	0.09
16:30	0.591	45.99	-0.01	0.08
16:30	0.674	45.99	-0.01	0.08
16:30	0.757	45.99	-0.01	0.08
16:30	0.840	45.99	-0.01	0.08
16:30	0.924	45.99	-0.01	0.08
16:31	1.007	45.99	-0.01	0.08
16:31	1.417	45.99	-0.01	0.08
16:31	1.751	46.00	-0.02	0.07
16:32	2.084	46.00	-0.02	0.07
16:32	2.417	46.00	-0.02	0.07
16:32	2.751	46.01	-0.03	0.06
16:33	3.084	46.01	-0.03	0.06
16:33	3.417	46.01	-0.03	0.06
16:33	3.751	46.01	-0.03	0.06
16:34	4.084	46.02	-0.04	0.05
16:34	4.417	46.02	-0.04	0.05
16:34	4.751	46.03	-0.05	0.04
16:35	5.084	46.03	-0.05	0.04
16:35	5.417	46.03	-0.05	0.04
16:35	5.751	46.03	-0.05	0.04
16:36	6.084	46.04	-0.06	0.03
16:36	6.417	46.05	-0.07	0.02
16:36	6.751	46.05	-0.07	0.02
16:37	7.084	46.06	-0.08	0.01

16:37	7.417	46.07	-0.09	0.00
16:37	7.751	46.07	-0.09	0.00
16:38	8.084	46.07	-0.09	0.00
16:38	8.417	46.08	-0.10	0.01
16:38	8.751	46.08	-0.10	0.01
16:39	9.084	46.08	-0.10	0.01
16:39	9.417	46.08	-0.10	0.01
16:39	9.751	46.09	-0.11	0.02
16:40	10.084	46.09	-0.11	0.02
16:42	12.120	46.09	-0.11	0.02
16:44	14.120	46.08	-0.10	0.01
16:46	16.120	46.05	-0.07	0.02
16:48	18.120	46.03	-0.05	0.04
16:50	20.142	46.03	-0.05	0.04
16:52	22.225	46.03	-0.05	0.04
16:54	24.225	46.03	-0.05	0.04
16:56	26.225	46.02	-0.04	0.05
16:58	28.225	46.02	-0.04	0.05
17:00	30.225	46.02	-0.04	0.05
17:02	32.225	46.02	-0.04	0.05
17:04	34.225	46.02	-0.04	0.05
17:06	36.225	46.01	-0.03	0.06
17:08	38.225	46.01	-0.03	0.06
17:10	40.225	46.01	-0.03	0.06
17:12	42.225	46.02	-0.04	0.05
17:14	44.225	46.01	-0.03	0.06
17:16	46.225	46.01	-0.03	0.06
17:18	48.225	46.01	-0.03	0.06
17:20	50.342	46.01	-0.03	0.06
17:22	52.220	46.01	-0.03	0.06
17:24	54.222	46.01	-0.03	0.06
17:26	56.222	46.01	-0.03	0.06
17:28	58.220	46.01	-0.03	0.06
17:30	60.120	46.01	-0.03	0.06
17:32	62.220	46.01	-0.03	0.06
17:34	64.222	46.01	-0.03	0.06
17:36	66.220	46.01	-0.03	0.06
17:38	68.220	46.01	-0.03	0.06
17:40	70.220	46.01	-0.03	0.06
17:42	72.220	46.01	-0.03	0.06
17:44	74.222	46.02	-0.04	0.05
17:46	76.095	46.02	-0.04	0.05
17:48	78.180	46.03	-0.05	0.04
17:50	80.575	46.03	-0.05	0.04
17:52	82.215	46.03	-0.05	0.04
17:54	84.215	46.03	-0.05	0.04
17:56	86.215	46.03	-0.05	0.04
17:58	88.215	46.02	-0.04	0.05
18:00	90.493	46.02	-0.04	0.05
18:02	92.210	46.02	-0.04	0.05
18:04	94.248	46.02	-0.04	0.05
18:06	96.248	46.02	-0.04	0.05
18:08	98.248	46.02	-0.04	0.05
18:30	120.250	46.03	-0.05	0.04
18:50	140.250	46.03	-0.05	0.04
19:10	160.180	46.02	-0.04	0.05

19:30	180.170	46.02	-0.04	0.05
19:50	200.220	46.03	-0.05	0.04
20:10	220.150	46.03	-0.05	0.04
20:30	240.150	46.02	-0.04	0.05
20:50	260.150	46.03	-0.05	0.04
21:10	280.250	46.03	-0.05	0.04
21:30	300.250	46.03	-0.05	0.04
21:50	320.250	46.03	-0.05	0.04
22:10	340.250	46.03	-0.05	0.04
22:30	360.220	46.03	-0.05	0.04
22:50	380.080	46.03	-0.05	0.04
23:10	400.080	46.03	-0.05	0.04
23:30	420.150	46.03	-0.05	0.04
23:50	440.080	46.04	-0.06	0.03
00:10	460.220	46.03	-0.05	0.04
00:30	480.220	46.04	-0.06	0.03
00:50	500.220	46.03	-0.05	0.04
01:10	520.220	46.03	-0.05	0.04
01:30	540.220	46.04	-0.06	0.03
01:50	560.220	46.05	-0.07	0.02
02:10	580.220	46.06	-0.08	0.01
02:30	600.220	46.06	-0.08	0.01
02:50	620.220	46.06	-0.08	0.01
03:10	640.220	46.06	-0.08	0.01
03:30	660.220	46.05	-0.07	0.02
03:50	680.220	46.05	-0.07	0.02
04:10	700.220	46.05	-0.07	0.02
04:30	720.220	46.04	-0.06	0.03
04:50	740.220	46.04	-0.06	0.03
05:10	760.220	46.03	-0.05	0.04
05:30	780.220	46.03	-0.05	0.04
05:50	800.220	46.03	-0.05	0.04
06:10	820.220	46.03	-0.05	0.04
06:30	840.220	46.02	-0.04	0.05
06:50	860.220	46.03	-0.05	0.04
07:10	880.180	45.98	0.00	0.09
07:30	900.180	45.97	0.01	0.10
07:50	920.180	45.99	-0.01	0.08
08:10	940.180	45.99	-0.01	0.08
08:30	960.180	46.01	-0.03	0.06
08:50	980.170	46.02	-0.04	0.05
09:10	1000.200	46.02	-0.04	0.05
10:10	1060.400	46.04	-0.06	0.03
11:10	1120.700	46.06	-0.08	0.01
12:10	1180.300	46.09	-0.11	0.02
13:10	1240.300	46.05	-0.07	0.02
14:10	1300.400	46.12	-0.14	0.05
15:10	1360.300	46.07	-0.09	0.00
16:10	1420.200	46.09	-0.11	0.02
17:10	1480.300	46.09	-0.11	0.02
18:10	1540.300	46.06	-0.08	0.01
19:10	1600.300	46.05	-0.07	0.02
20:10	1660.300	46.05	-0.07	0.02
21:10	1720.300	46.05	-0.07	0.02
22:10	1780.300	46.04	-0.06	0.03
23:10	1840.300	46.04	-0.06	0.03



00:10	1900.300	46.04	-0.06	0.03
01:10	1960.300	46.07	-0.09	0.00
02:10	2020.300	46.07	-0.09	0.00
03:10	2080.300	46.05	-0.07	0.02
04:10	2140.300	46.05	-0.07	0.02
05:10	2200.300	46.04	-0.06	0.03
06:10	2260.300	46.04	-0.06	0.03
07:10	2320.300	46.01	-0.03	0.06
08:10	2380.300	46.01	-0.03	0.06
09:10	2440.300	46.03	-0.05	0.04
10:10	2500.300	46.05	-0.07	0.02
11:10	2560.300	46.05	-0.07	0.02
12:10	2620.400	46.11	-0.13	0.04
13:10	2680.400	46.07	-0.09	0.00
14:10	2740.400	46.14	-0.16	0.07
15:10	2800.400	46.12	-0.14	0.05
16:10	2860.400	46.08	-0.10	0.01
17:10	2920.400	46.14	-0.16	0.07
18:10	2980.400	46.10	-0.12	0.03
19:10	3040.200	46.08	-0.10	0.01
20:10	3100.200	46.09	-0.11	0.02
21:10	3160.200	46.11	-0.13	0.04
22:10	3220.200	46.05	-0.07	0.02
23:10	3280.200	46.05	-0.07	0.02
00:10	3340.200	46.09	-0.11	0.02
01:10	3400.200	46.07	-0.09	0.00
02:10	3460.200	46.11	-0.13	0.04
03:10	3520.200	46.12	-0.14	0.05
04:10	3580.300	46.12	-0.14	0.05
05:10	3640.300	46.13	-0.15	0.06
06:10	3700.300	46.11	-0.13	0.04
07:10	3760.300	46.10	-0.12	0.03
07:36	3786.600	46.09	-0.11	0.02

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: P 10-3 INPUT 7  
 RADIUS: 20.220 FEET  
 START DATE: 15-Sep-86  
 START TIME: 13:00  
 WATER START LEVEL: 40.09 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
13:00	0.000	40.09	0.00
13:00	0.017	-999.99	1040.08
13:00	0.034	-999.99	1040.08
13:00	0.050	-999.99	1040.08
13:00	0.067	-999.99	1040.08
13:00	0.084	-999.99	1040.08
13:00	0.100	-999.99	1040.08
13:00	0.117	-999.99	1040.08
13:00	0.134	-999.99	1040.08
13:00	0.150	-999.99	1040.08
13:00	0.167	-999.99	1040.08
13:00	0.257	40.09	0.00
13:00	0.340	40.09	0.00
13:00	0.424	40.09	0.00
13:00	0.507	40.09	0.00
13:00	0.590	40.10	-0.01
13:00	0.674	40.10	-0.01
13:00	0.757	40.10	-0.01
13:00	0.840	40.10	-0.01
13:00	0.924	40.10	-0.01
13:01	1.007	40.10	-0.01
13:01	1.417	40.10	-0.01
13:01	1.750	40.10	-0.01
13:02	2.084	40.10	-0.01
13:02	2.417	40.10	-0.01
13:02	2.750	40.10	-0.01
13:03	3.084	40.10	-0.01
13:03	3.417	40.10	-0.01
13:03	3.750	40.10	-0.01
13:04	4.084	40.10	-0.01
13:04	4.417	40.10	-0.01
13:04	4.750	40.09	0.00
13:05	5.084	40.09	0.00
13:05	5.417	40.09	0.00
13:05	5.750	40.09	0.00
13:06	6.084	40.09	0.00
13:06	6.417	40.09	0.00
13:06	6.750	40.09	0.00
13:07	7.084	40.09	0.00
13:07	7.417	40.09	0.00

13:07	7.750	40.09	0.00
13:08	8.084	40.09	0.00
13:08	8.417	40.09	0.00
13:08	8.750	40.09	0.00
13:09	9.084	40.09	0.00
13:09	9.417	40.09	0.00
13:09	9.750	40.09	0.00
13:10	10.084	40.09	0.00
13:12	12.101	40.09	0.00
13:14	14.188	40.10	-0.01
13:16	16.139	40.09	0.00
13:18	18.237	40.09	0.00
13:20	20.233	40.09	0.00
13:22	22.233	40.09	0.00
13:24	24.233	40.09	0.00
13:26	26.233	40.09	0.00
13:28	28.233	40.09	0.00
13:30	30.233	40.09	0.00
13:32	32.152	40.09	0.00
13:34	34.620	40.09	0.00
13:36	36.095	40.09	0.00
13:38	38.095	40.09	0.00
13:40	40.095	40.09	0.00
13:42	42.195	40.09	0.00
13:44	44.232	40.09	0.00
13:46	46.232	40.09	0.00
13:48	48.252	40.09	0.00
13:50	50.122	40.09	0.00
13:52	52.122	40.09	0.00
13:54	54.122	40.09	0.00
13:56	56.122	40.09	0.00
13:58	58.122	40.09	0.00
14:00	60.122	40.09	0.00
14:02	62.122	40.09	0.00
14:04	64.122	40.09	0.00
14:06	66.442	40.09	0.00
14:08	68.122	40.10	-0.01
14:10	70.335	40.09	0.00
14:12	72.160	40.09	0.00
14:14	74.160	40.09	0.00
14:16	76.167	40.09	0.00
14:18	78.230	40.09	0.00
14:20	80.217	40.09	0.00
14:22	82.213	40.09	0.00
14:24	84.213	40.09	0.00
14:26	86.213	40.09	0.00
14:28	88.213	40.09	0.00
14:30	90.213	40.09	0.00
14:32	92.213	40.09	0.00
14:34	94.213	40.09	0.00
14:36	96.213	40.09	0.00
14:38	98.238	40.09	0.00
15:00	120.220	40.09	0.00
15:20	140.130	40.09	0.00
15:40	160.130	40.09	0.00
16:00	180.370	40.09	0.00

16:20	200.200	40.09	0.00
16:40	220.200	40.09	0.00
17:00	240.080	40.09	0.00
17:20	260.220	40.09	0.00
17:40	280.150	40.09	0.00
18:00	300.150	40.08	0.01
18:20	320.130	40.08	0.01
18:40	340.220	40.08	0.01
19:00	360.180	40.08	0.01
19:20	380.220	40.08	0.01
19:40	400.220	40.08	0.01
20:00	420.220	40.08	0.01
20:20	440.220	40.08	0.01
20:40	460.220	40.08	0.01
21:00	480.120	40.08	0.01
21:20	500.220	40.08	0.01
21:40	520.320	40.08	0.01
22:00	540.200	40.08	0.01
22:20	560.100	40.08	0.01
22:40	580.100	40.08	0.01
23:00	600.150	40.08	0.01
23:20	620.150	40.07	0.02
23:40	640.180	40.08	0.01
00:00	660.180	40.08	0.01
00:20	680.180	40.07	0.02
00:40	700.180	40.07	0.02
01:00	720.180	40.07	0.02
01:20	740.180	40.07	0.02
01:40	760.180	40.08	0.01
02:00	780.180	40.07	0.02
02:20	800.180	40.07	0.02
02:40	820.180	40.07	0.02
03:00	840.180	40.07	0.02
03:20	860.180	40.07	0.02
03:40	880.180	40.07	0.02
04:00	900.180	40.07	0.02
04:20	920.180	40.07	0.02
04:40	940.180	40.07	0.02
05:00	960.180	40.07	0.02
05:20	980.180	40.07	0.02
05:40	1000.200	40.07	0.02
06:40	1060.400	40.07	0.02
07:40	1120.500	40.07	0.02
08:40	1180.300	40.07	0.02
09:40	1240.300	40.07	0.02
10:40	1300.200	40.07	0.02
11:40	1360.300	40.07	0.02
12:40	1420.300	40.07	0.02
13:40	1480.200	40.08	0.01
14:40	1540.300	40.08	0.01
15:40	1600.300	40.08	0.01
16:30	1650.600	40.08	0.01

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: P 10-3 INPUT 7  
 RADIUS: 20.220 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 40.09 FEET  
 WATER STOP LEVEL: 40.08 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
16:30	0.017	-999.99	1040.07	1040.08
16:30	0.034	-999.99	1040.07	1040.08
16:30	0.050	-999.99	1040.07	1040.08
16:30	0.067	-999.99	1040.07	1040.08
16:30	0.084	-999.99	1040.07	1040.08
16:30	0.100	-999.99	1040.07	1040.08
16:30	0.117	-999.99	1040.07	1040.08
16:30	0.134	-999.99	1040.07	1040.08
16:30	0.150	-999.99	1040.07	1040.08
16:30	0.167	-999.99	1040.07	1040.08
16:30	0.257	40.08	0.00	0.01
16:30	0.340	40.08	0.00	0.01
16:30	0.424	40.08	0.00	0.01
16:30	0.507	40.08	0.00	0.01
16:30	0.591	40.08	0.00	0.01
16:30	0.674	40.08	0.00	0.01
16:30	0.757	40.08	0.00	0.01
16:30	0.840	40.08	0.00	0.01
16:30	0.924	40.08	0.00	0.01
16:31	1.007	40.08	0.00	0.01
16:31	1.417	40.08	0.00	0.01
16:31	1.751	40.08	0.00	0.01
16:32	2.084	40.08	0.00	0.01
16:32	2.417	40.08	0.00	0.01
16:32	2.751	40.08	0.00	0.01
16:33	3.084	40.08	0.00	0.01
16:33	3.417	40.08	0.00	0.01
16:33	3.751	40.08	0.00	0.01
16:34	4.084	40.08	0.00	0.01
16:34	4.417	40.08	0.00	0.01
16:34	4.751	40.08	0.00	0.01
16:35	5.084	40.08	0.00	0.01
16:35	5.417	40.08	0.00	0.01
16:35	5.751	40.08	0.00	0.01
16:36	6.084	40.08	0.00	0.01
16:36	6.417	40.08	0.00	0.01
16:36	6.751	40.08	0.00	0.01
16:37	7.084	40.08	0.00	0.01

16:37	7.417	40.08	0.00	0.01
16:37	7.751	40.08	0.00	0.01
16:38	8.084	40.08	0.00	0.01
16:38	8.417	40.08	0.00	0.01
16:38	8.751	40.08	0.00	0.01
16:39	9.084	40.08	0.00	0.01
16:39	9.417	40.08	0.00	0.01
16:39	9.751	40.08	0.00	0.01
16:40	10.084	40.08	0.00	0.01
16:42	12.120	40.08	0.00	0.01
16:44	14.120	40.08	0.00	0.01
16:46	16.120	40.08	0.00	0.01
16:48	18.120	40.08	0.00	0.01
16:50	20.142	40.08	0.00	0.01
16:52	22.225	40.08	0.00	0.01
16:54	24.225	40.08	0.00	0.01
16:56	26.225	40.08	0.00	0.01
16:58	28.225	40.08	0.00	0.01
17:00	30.225	40.08	0.00	0.01
17:02	32.225	40.08	0.00	0.01
17:04	34.225	40.08	0.00	0.01
17:06	36.225	40.08	0.00	0.01
17:08	38.225	40.08	0.00	0.01
17:10	40.225	40.08	0.00	0.01
17:12	42.225	40.08	0.00	0.01
17:14	44.225	40.08	0.00	0.01
17:16	46.225	40.08	0.00	0.01
17:18	48.225	40.08	0.00	0.01
17:20	50.342	40.08	0.00	0.01
17:22	52.220	40.08	0.00	0.01
17:24	54.222	40.08	0.00	0.01
17:26	56.222	40.08	0.00	0.01
17:28	58.220	40.08	0.00	0.01
17:30	60.120	40.08	0.00	0.01
17:32	62.220	40.08	0.00	0.01
17:34	64.222	40.08	0.00	0.01
17:36	66.220	40.08	0.00	0.01
17:38	68.220	40.08	0.00	0.01
17:40	70.220	40.08	0.00	0.01
17:42	72.220	40.08	0.00	0.01
17:44	74.222	40.08	0.00	0.01
17:46	76.095	40.08	0.00	0.01
17:48	78.180	40.08	0.00	0.01
17:50	80.575	40.08	0.00	0.01
17:52	82.215	40.08	0.00	0.01
17:54	84.215	40.08	0.00	0.01
17:56	86.215	40.08	0.00	0.01
17:58	88.215	40.08	0.00	0.01
18:00	90.493	40.08	0.00	0.01
18:02	92.210	40.08	0.00	0.01
18:04	94.248	40.08	0.00	0.01
18:06	96.248	40.08	0.00	0.01
18:08	98.248	40.08	0.00	0.01
18:30	120.250	40.08	0.00	0.01
18:50	140.250	40.08	0.00	0.01
19:10	160.180	40.08	0.00	0.01

19:30	180.170	40.08	0.00	0.01
19:50	200.220	40.08	0.00	0.01
20:10	220.150	40.08	0.00	0.01
20:30	240.150	40.08	0.00	0.01
20:50	260.150	40.08	0.00	0.01
21:10	280.250	40.08	0.00	0.01
21:30	300.250	40.08	0.00	0.01
21:50	320.250	40.08	0.00	0.01
22:10	340.250	40.08	0.00	0.01
22:30	360.220	40.08	0.00	0.01
22:50	380.080	40.08	0.00	0.01
23:10	400.080	40.09	-0.01	0.00
23:30	420.150	40.09	-0.01	0.00
23:50	440.080	40.09	-0.01	0.00
00:10	460.220	40.09	-0.01	0.00
00:30	480.220	40.09	-0.01	0.00
00:50	500.220	40.09	-0.01	0.00
01:10	520.220	40.09	-0.01	0.00
01:30	540.220	40.09	-0.01	0.00
01:50	560.220	40.09	-0.01	0.00
02:10	580.220	40.09	-0.01	0.00
02:30	600.220	40.09	-0.01	0.00
02:50	620.220	40.09	-0.01	0.00
03:10	640.220	40.09	-0.01	0.00
03:30	660.220	40.09	-0.01	0.00
03:50	680.220	40.09	-0.01	0.00
04:10	700.220	40.09	-0.01	0.00
04:30	720.220	40.09	-0.01	0.00
04:50	740.220	40.09	-0.01	0.00
05:10	760.220	40.09	-0.01	0.00
05:30	780.220	40.09	-0.01	0.00
05:50	800.220	40.09	-0.01	0.00
06:10	820.220	40.09	-0.01	0.00
06:30	840.220	40.09	-0.01	0.00
06:50	860.220	40.09	-0.01	0.00
07:10	880.180	40.09	-0.01	0.00
07:30	900.180	40.09	-0.01	0.00
07:50	920.180	40.09	-0.01	0.00
08:10	940.180	40.09	-0.01	0.00
08:30	960.180	40.09	-0.01	0.00
08:50	980.170	40.09	-0.01	0.00
09:10	1000.200	40.09	-0.01	0.00
10:10	1060.400	40.09	-0.01	0.00
11:10	1120.700	40.10	-0.02	0.01
12:10	1180.300	40.10	-0.02	0.01
13:10	1240.300	40.09	-0.01	0.00
14:10	1300.400	40.10	-0.02	0.01
15:10	1360.300	40.10	-0.02	0.01
16:10	1420.200	40.10	-0.02	0.01
17:10	1480.300	40.10	-0.02	0.01
18:10	1540.300	40.10	-0.02	0.01
19:10	1600.300	40.10	-0.02	0.01
20:10	1660.300	40.10	-0.02	0.01
21:10	1720.300	40.10	-0.02	0.01
22:10	1780.300	40.10	-0.02	0.01
23:10	1840.300	40.10	-0.02	0.01

00:10	1900.300	40.10	-0.02	0.01
01:10	1960.300	40.10	-0.02	0.01
02:10	2020.300	40.10	-0.02	0.01
03:10	2080.300	40.10	-0.02	0.01
04:10	2140.300	40.10	-0.02	0.01
05:10	2200.300	40.10	-0.02	0.01
06:10	2260.300	40.10	-0.02	0.01
07:10	2320.300	40.10	-0.02	0.01
08:10	2380.300	40.10	-0.02	0.01
09:10	2440.300	40.10	-0.02	0.01
10:10	2500.300	40.10	-0.02	0.01
11:10	2560.300	40.10	-0.02	0.01
12:10	2620.400	40.10	-0.02	0.01
13:10	2680.400	40.10	-0.02	0.01
14:10	2740.400	40.09	-0.01	0.00
15:10	2800.400	40.10	-0.02	0.01
16:10	2860.400	40.10	-0.02	0.01
17:10	2920.400	40.10	-0.02	0.01
18:10	2980.400	40.10	-0.02	0.01
19:10	3040.200	40.10	-0.02	0.01
20:10	3100.200	40.10	-0.02	0.01
21:10	3160.200	40.10	-0.02	0.01
22:10	3220.200	40.10	-0.02	0.01
23:10	3280.200	40.10	-0.02	0.01
00:10	3340.200	40.10	-0.02	0.01
01:10	3400.200	40.10	-0.02	0.01
02:10	3460.200	40.10	-0.02	0.01
03:10	3520.200	40.10	-0.02	0.01
04:10	3580.300	40.10	-0.02	0.01
05:10	3640.300	40.10	-0.02	0.01
06:10	3700.300	40.10	-0.02	0.01
07:10	3760.300	40.10	-0.02	0.01
07:36	3786.600	40.10	-0.02	0.01



PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: P 10-4 INPUT 8  
 RADIUS: 20.053 FEET  
 START DATE: 15-Sep-86  
 START TIME: 13:00  
 WATER START LEVEL: 38.82 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
13:00	0.000	38.82	0.00
13:00	0.017	-999.99	1038.81
13:00	0.034	-999.99	1038.81
13:00	0.050	-999.99	1038.81
13:00	0.067	-999.99	1038.81
13:00	0.084	-999.99	1038.81
13:00	0.100	-999.99	1038.81
13:00	0.117	-999.99	1038.81
13:00	0.134	-999.99	1038.81
13:00	0.150	-999.99	1038.81
13:00	0.167	-999.99	1038.81
13:00	0.257	38.82	0.00
13:00	0.340	38.83	-0.01
13:00	0.424	38.83	-0.01
13:00	0.507	38.83	-0.01
13:00	0.590	38.83	-0.01
13:00	0.674	38.83	-0.01
13:00	0.757	38.83	-0.01
13:00	0.840	38.83	-0.01
13:00	0.924	38.83	-0.01
13:01	1.007	38.83	-0.01
13:01	1.417	38.83	-0.01
13:01	1.750	38.83	-0.01
13:02	2.084	38.83	-0.01
13:02	2.417	38.83	-0.01
13:02	2.750	38.83	-0.01
13:03	3.084	38.82	0.00
13:03	3.417	38.83	-0.01
13:03	3.750	38.83	-0.01
13:04	4.084	38.83	-0.01
13:04	4.417	38.83	-0.01
13:04	4.750	38.82	0.00
13:05	5.084	38.82	0.00
13:05	5.417	38.82	0.00
13:05	5.750	38.82	0.00
13:06	6.084	38.82	0.00
13:06	6.417	38.82	0.00
13:06	6.750	38.82	0.00
13:07	7.084	38.82	0.00
13:07	7.417	38.82	0.00

13:07	7.750	38.83	-0.01
13:08	8.084	38.83	-0.01
13:08	8.417	38.83	-0.01
13:08	8.750	38.83	-0.01
13:09	9.084	38.83	-0.01
13:09	9.417	38.83	-0.01
13:09	9.750	38.83	-0.01
13:10	10.084	38.83	-0.01
13:12	12.101	38.83	-0.01
13:14	14.188	38.83	-0.01
13:16	16.139	38.82	0.00
13:18	18.237	38.82	0.00
13:20	20.233	38.82	0.00
13:22	22.233	38.83	-0.01
13:24	24.233	38.83	-0.01
13:26	26.233	38.82	0.00
13:28	28.233	38.82	0.00
13:30	30.233	38.82	0.00
13:32	32.152	38.82	0.00
13:34	34.620	38.83	-0.01
13:36	36.095	38.82	0.00
13:38	38.095	38.82	0.00
13:40	40.095	38.82	0.00
13:42	42.195	38.82	0.00
13:44	44.232	38.82	0.00
13:46	46.232	38.82	0.00
13:48	48.252	38.82	0.00
13:50	50.122	38.82	0.00
13:52	52.122	38.83	-0.01
13:54	54.122	38.83	-0.01
13:56	56.122	38.83	-0.01
13:58	58.122	38.83	-0.01
14:00	60.122	38.82	0.00
14:02	62.122	38.82	0.00
14:04	64.122	38.82	0.00
14:06	66.442	38.82	0.00
14:08	68.122	38.82	0.00
14:10	70.335	38.82	0.00
14:12	72.160	38.82	0.00
14:14	74.160	38.82	0.00
14:16	76.167	38.82	0.00
14:18	78.230	38.82	0.00
14:20	80.217	38.82	0.00
14:22	82.213	38.82	0.00
14:24	84.213	38.82	0.00
14:26	86.213	38.82	0.00
14:28	88.213	38.82	0.00
14:30	90.213	38.82	0.00
14:32	92.213	38.82	0.00
14:34	94.213	38.82	0.00
14:36	96.213	38.82	0.00
14:38	98.238	38.82	0.00
15:00	120.220	38.82	0.00
15:20	140.130	38.82	0.00
15:40	160.130	38.82	0.00
16:00	180.370	38.82	0.00

16:20	200.200	38.82	0.00
16:40	220.200	38.81	0.01
17:00	240.080	38.81	0.01
17:20	260.220	38.81	0.01
17:40	280.150	38.81	0.01
18:00	300.150	38.81	0.01
18:20	320.130	38.81	0.01
18:40	340.220	38.81	0.01
19:00	360.180	38.81	0.01
19:20	380.220	38.81	0.01
19:40	400.220	38.81	0.01
20:00	420.220	38.81	0.01
20:20	440.220	38.80	0.02
20:40	460.220	38.81	0.01
21:00	480.120	38.80	0.02
21:20	500.220	38.80	0.02
21:40	520.320	38.80	0.02
22:00	540.200	38.80	0.02
22:20	560.100	38.80	0.02
22:40	580.100	38.80	0.02
23:00	600.150	38.80	0.02
23:20	620.150	38.81	0.01
23:40	640.180	38.80	0.02
00:00	660.180	38.80	0.02
00:20	680.180	38.80	0.02
00:40	700.180	38.80	0.02
01:00	720.180	38.80	0.02
01:20	740.180	38.80	0.02
01:40	760.180	38.80	0.02
02:00	780.180	38.80	0.02
02:20	800.180	38.80	0.02
02:40	820.180	38.80	0.02
03:00	840.180	38.80	0.02
03:20	860.180	38.80	0.02
03:40	880.180	38.80	0.02
04:00	900.180	38.80	0.02
04:20	920.180	38.80	0.02
04:40	940.180	38.80	0.02
05:00	960.180	38.80	0.02
05:20	980.180	38.80	0.02
05:40	1000.200	38.80	0.02
06:40	1060.400	38.80	0.02
07:40	1120.500	38.80	0.02
08:40	1180.300	38.80	0.02
09:40	1240.300	38.80	0.02
10:40	1300.200	38.81	0.01
11:40	1360.300	38.81	0.01
12:40	1420.300	38.81	0.01
13:40	1480.200	38.81	0.01
14:40	1540.300	38.81	0.01
15:40	1600.300	38.81	0.01
16:30	1650.600	38.81	0.01

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: P 10-4 INPUT 8  
 RADIUS: 20.053 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 38.82 FEET  
 WATER STOP LEVEL: 38.81 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
16:30	0.017	-999.99	1038.80	1038.81
16:30	0.034	-999.99	1038.80	1038.81
16:30	0.050	-999.99	1038.80	1038.81
16:30	0.067	-999.99	1038.80	1038.81
16:30	0.084	-999.99	1038.80	1038.81
16:30	0.100	-999.99	1038.80	1038.81
16:30	0.117	-999.99	1038.80	1038.81
16:30	0.134	-999.99	1038.80	1038.81
16:30	0.150	-999.99	1038.80	1038.81
16:30	0.167	-999.99	1038.80	1038.81
16:30	0.257	38.81	0.00	0.01
16:30	0.340	38.81	0.00	0.01
16:30	0.424	38.81	0.00	0.01
16:30	0.507	38.81	0.00	0.01
16:30	0.591	38.81	0.00	0.01
16:30	0.674	38.81	0.00	0.01
16:30	0.757	38.81	0.00	0.01
16:30	0.840	38.81	0.00	0.01
16:30	0.924	38.81	0.00	0.01
16:31	1.007	38.81	0.00	0.01
16:31	1.417	38.81	0.00	0.01
16:31	1.751	38.81	0.00	0.01
16:32	2.084	38.81	0.00	0.01
16:32	2.417	38.81	0.00	0.01
16:32	2.751	38.81	0.00	0.01
16:33	3.084	38.81	0.00	0.01
16:33	3.417	38.81	0.00	0.01
16:33	3.751	38.81	0.00	0.01
16:34	4.084	38.81	0.00	0.01
16:34	4.417	38.81	0.00	0.01
16:34	4.751	38.81	0.00	0.01
16:35	5.084	38.81	0.00	0.01
16:35	5.417	38.81	0.00	0.01
16:35	5.751	38.81	0.00	0.01
16:36	6.084	38.81	0.00	0.01
16:36	6.417	38.81	0.00	0.01
16:36	6.751	38.81	0.00	0.01
16:37	7.084	38.81	0.00	0.01

16:37	7.417	38.81	0.00	0.01
16:37	7.751	38.81	0.00	0.01
16:38	8.084	38.81	0.00	0.01
16:38	8.417	38.81	0.00	0.01
16:38	8.751	38.81	0.00	0.01
16:39	9.084	38.81	0.00	0.01
16:39	9.417	38.81	0.00	0.01
16:39	9.751	38.81	0.00	0.01
16:40	10.084	38.81	0.00	0.01
16:42	12.120	38.81	0.00	0.01
16:44	14.120	38.80	0.01	0.02
16:46	16.120	38.80	0.01	0.02
16:48	18.120	38.81	0.00	0.01
16:50	20.142	38.81	0.00	0.01
16:52	22.225	38.81	0.00	0.01
16:54	24.225	38.81	0.00	0.01
16:56	26.225	38.81	0.00	0.01
16:58	28.225	38.81	0.00	0.01
17:00	30.225	38.81	0.00	0.01
17:02	32.225	38.81	0.00	0.01
17:04	34.225	38.81	0.00	0.01
17:06	36.225	38.81	0.00	0.01
17:08	38.225	38.81	0.00	0.01
17:10	40.225	38.81	0.00	0.01
17:12	42.225	38.81	0.00	0.01
17:14	44.225	38.81	0.00	0.01
17:16	46.225	38.81	0.00	0.01
17:18	48.225	38.81	0.00	0.01
17:20	50.342	38.81	0.00	0.01
17:22	52.220	38.81	0.00	0.01
17:24	54.222	38.81	0.00	0.01
17:26	56.222	38.81	0.00	0.01
17:28	58.220	38.81	0.00	0.01
17:30	60.120	38.81	0.00	0.01
17:32	62.220	38.81	0.00	0.01
17:34	64.222	38.81	0.00	0.01
17:36	66.220	38.81	0.00	0.01
17:38	68.220	38.81	0.00	0.01
17:40	70.220	38.81	0.00	0.01
17:42	72.220	38.81	0.00	0.01
17:44	74.222	38.81	0.00	0.01
17:46	76.095	38.81	0.00	0.01
17:48	78.180	38.81	0.00	0.01
17:50	80.575	38.81	0.00	0.01
17:52	82.215	38.81	0.00	0.01
17:54	84.215	38.81	0.00	0.01
17:56	86.215	38.81	0.00	0.01
17:58	88.215	38.81	0.00	0.01
18:00	90.493	38.81	0.00	0.01
18:02	92.210	38.81	0.00	0.01
18:04	94.248	38.81	0.00	0.01
18:06	96.248	38.81	0.00	0.01
18:08	98.248	38.81	0.00	0.01
18:30	120.250	38.81	0.00	0.01
18:50	140.250	38.81	0.00	0.01
19:10	160.180	38.81	0.00	0.01

19:30	180.170	38.81	0.00	0.01
19:50	200.220	38.81	0.00	0.01
20:10	220.150	38.81	0.00	0.01
20:30	240.150	38.81	0.00	0.01
20:50	260.150	38.81	0.00	0.01
21:10	280.250	38.81	0.00	0.01
21:30	300.250	38.81	0.00	0.01
21:50	320.250	38.81	0.00	0.01
22:10	340.250	38.81	0.00	0.01
22:30	360.220	38.81	0.00	0.01
22:50	380.080	38.81	0.00	0.01
23:10	400.080	38.81	0.00	0.01
23:30	420.150	38.81	0.00	0.01
23:50	440.080	38.81	0.00	0.01
00:10	460.220	38.81	0.00	0.01
00:30	480.220	38.81	0.00	0.01
00:50	500.220	38.81	0.00	0.01
01:10	520.220	38.81	0.00	0.01
01:30	540.220	38.81	0.00	0.01
01:50	560.220	38.81	0.00	0.01
02:10	580.220	38.82	-0.01	0.00
02:30	600.220	38.81	0.00	0.01
02:50	620.220	38.81	0.00	0.01
03:10	640.220	38.82	-0.01	0.00
03:30	660.220	38.82	-0.01	0.00
03:50	680.220	38.82	-0.01	0.00
04:10	700.220	38.82	-0.01	0.00
04:30	720.220	38.82	-0.01	0.00
04:50	740.220	38.82	-0.01	0.00
05:10	760.220	38.82	-0.01	0.00
05:30	780.220	38.82	-0.01	0.00
05:50	800.220	38.82	-0.01	0.00
06:10	820.220	38.82	-0.01	0.00
06:30	840.220	38.82	-0.01	0.00
06:50	860.220	38.82	-0.01	0.00
07:10	880.180	38.82	-0.01	0.00
07:30	900.180	38.82	-0.01	0.00
07:50	920.180	38.82	-0.01	0.00
08:10	940.180	38.82	-0.01	0.00
08:30	960.180	38.82	-0.01	0.00
08:50	980.170	38.82	-0.01	0.00
09:10	1000.200	38.82	-0.01	0.00
10:10	1060.400	38.82	-0.01	0.00
11:10	1120.700	38.82	-0.01	0.00
12:10	1180.300	38.82	-0.01	0.00
13:10	1240.300	38.82	-0.01	0.00
14:10	1300.400	38.82	-0.01	0.00
15:10	1360.300	38.82	-0.01	0.00
16:10	1420.200	38.82	-0.01	0.00
17:10	1480.300	38.83	-0.02	0.01
18:10	1540.300	38.82	-0.01	0.00
19:10	1600.300	38.83	-0.02	0.01
20:10	1660.300	38.82	-0.01	0.00
21:10	1720.300	38.83	-0.02	0.01
22:10	1780.300	38.83	-0.02	0.01
23:10	1840.300	38.83	-0.02	0.01

00:10	1900.300	38.83	-0.02	0.01
01:10	1960.300	38.83	-0.02	0.01
02:10	2020.300	38.83	-0.02	0.01
03:10	2080.300	38.83	-0.02	0.01
04:10	2140.300	38.83	-0.02	0.01
05:10	2200.300	38.83	-0.02	0.01
06:10	2260.300	38.83	-0.02	0.01
07:10	2320.300	38.83	-0.02	0.01
08:10	2380.300	38.83	-0.02	0.01
09:10	2440.300	38.84	-0.03	0.02
10:10	2500.300	38.84	-0.03	0.02
11:10	2560.300	38.84	-0.03	0.02
12:10	2620.400	38.84	-0.03	0.02
13:10	2680.400	38.84	-0.03	0.02
14:10	2740.400	38.85	-0.04	0.03
15:10	2800.400	38.84	-0.03	0.02
16:10	2860.400	38.84	-0.03	0.02
17:10	2920.400	38.84	-0.03	0.02
18:10	2980.400	38.84	-0.03	0.02
19:10	3040.200	38.84	-0.03	0.02
20:10	3100.200	38.84	-0.03	0.02
21:10	3160.200	38.84	-0.03	0.02
22:10	3220.200	38.84	-0.03	0.02
23:10	3280.200	38.85	-0.04	0.03
00:10	3340.200	38.85	-0.04	0.03
01:10	3400.200	38.85	-0.04	0.03
02:10	3460.200	38.85	-0.04	0.03
03:10	3520.200	38.85	-0.04	0.03
04:10	3580.300	38.85	-0.04	0.03
05:10	3640.300	38.85	-0.04	0.03
06:10	3700.300	38.85	-0.04	0.03
07:10	3760.300	38.85	-0.04	0.03
07:36	3786.600	38.85	-0.04	0.03

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: REI 10-2 INPUT 9  
 RADIUS: 25.391 FEET  
 START DATE: 15-Sep-86  
 START TIME: 13:00  
 WATER START LEVEL: 5.66 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
13:00	0.000	5.66	0.00
13:00	0.017	-999.99	1005.65
13:00	0.034	-999.99	1005.65
13:00	0.050	-999.99	1005.65
13:00	0.067	-999.99	1005.65
13:00	0.084	-999.99	1005.65
13:00	0.100	-999.99	1005.65
13:00	0.117	-999.99	1005.65
13:00	0.134	-999.99	1005.65
13:00	0.150	-999.99	1005.65
13:00	0.167	-999.99	1005.65
13:00	0.257	5.67	-0.01
13:00	0.340	5.67	-0.01
13:00	0.424	5.67	-0.01
13:00	0.507	5.67	-0.01
13:00	0.590	5.67	-0.01
13:00	0.674	5.67	-0.01
13:00	0.757	5.67	-0.01
13:00	0.840	5.67	-0.01
13:00	0.924	5.68	-0.02
13:01	1.007	5.68	-0.02
13:01	1.417	5.69	-0.03
13:01	1.750	5.70	-0.04
13:02	2.084	5.71	-0.05
13:02	2.417	5.71	-0.05
13:02	2.750	5.72	-0.06
13:03	3.084	5.71	-0.05
13:03	3.417	5.70	-0.04
13:03	3.750	5.70	-0.04
13:04	4.084	5.70	-0.04
13:04	4.417	5.69	-0.03
13:04	4.750	5.69	-0.03
13:05	5.084	5.68	-0.02
13:05	5.417	5.67	-0.01
13:05	5.750	5.67	-0.01
13:06	6.084	5.66	0.00
13:06	6.417	5.66	0.00
13:06	6.750	5.65	0.01
13:07	7.084	5.65	0.01
13:07	7.417	5.65	0.01



13:07	7.750	5.65	0.01
13:08	8.084	5.65	0.01
13:08	8.417	5.65	0.01
13:08	8.750	5.66	0.00
13:09	9.084	5.66	0.00
13:09	9.417	5.66	0.00
13:09	9.750	5.66	0.00
13:10	10.084	5.66	0.00
13:12	12.101	5.66	0.00
13:14	14.188	5.67	-0.01
13:16	16.139	5.67	-0.01
13:18	18.237	5.65	0.01
13:20	20.233	5.64	0.02
13:22	22.233	5.64	0.02
13:24	24.233	5.64	0.02
13:26	26.233	5.65	0.01
13:28	28.233	5.64	0.02
13:30	30.233	5.64	0.02
13:32	32.152	5.64	0.02
13:34	34.620	5.64	0.02
13:36	36.095	5.64	0.02
13:38	38.095	5.64	0.02
13:40	40.095	5.64	0.02
13:42	42.195	5.63	0.03
13:44	44.232	5.62	0.04
13:46	46.232	5.61	0.05
13:48	48.252	5.63	0.03
13:50	50.122	5.63	0.03
13:52	52.122	5.64	0.02
13:54	54.122	5.64	0.02
13:56	56.122	5.63	0.03
13:58	58.122	5.65	0.01
14:00	60.122	5.64	0.02
14:02	62.122	5.62	0.04
14:04	64.122	5.63	0.03
14:06	66.442	5.63	0.03
14:08	68.122	5.64	0.02
14:10	70.335	5.64	0.02
14:12	72.160	5.65	0.01
14:14	74.160	5.64	0.02
14:16	76.167	5.63	0.03
14:18	78.230	5.63	0.03
14:20	80.217	5.63	0.03
14:22	82.213	5.63	0.03
14:24	84.213	5.62	0.04
14:26	86.213	5.62	0.04
14:28	88.213	5.62	0.04
14:30	90.213	5.62	0.04
14:32	92.213	5.62	0.04
14:34	94.213	5.61	0.05
14:36	96.213	5.61	0.05
14:38	98.238	5.61	0.05
15:00	120.220	5.61	0.05
15:20	140.130	5.59	0.07
15:40	160.130	5.58	0.08
16:00	180.370	5.58	0.08

16:20	200.200	5.58	0.08
16:40	220.200	5.57	0.09
17:00	240.080	5.56	0.10
17:20	260.220	5.56	0.10
17:40	280.150	5.56	0.10
18:00	300.150	5.55	0.11
18:20	320.130	5.55	0.11
18:40	340.220	5.55	0.11
19:00	360.180	5.55	0.11
19:20	380.220	5.54	0.12
19:40	400.220	5.55	0.11
20:00	420.220	5.54	0.12
20:20	440.220	5.54	0.12
20:40	460.220	5.54	0.12
21:00	480.120	5.54	0.12
21:20	500.220	5.54	0.12
21:40	520.320	5.54	0.12
22:00	540.200	5.55	0.11
22:20	560.100	5.54	0.12
22:40	580.100	5.54	0.12
23:00	600.150	5.54	0.12
23:20	620.150	5.53	0.13
23:40	640.180	5.53	0.13
00:00	660.180	5.53	0.13
00:20	680.180	5.53	0.13
00:40	700.180	5.53	0.13
01:00	720.180	5.53	0.13
01:20	740.180	5.53	0.13
01:40	760.180	5.53	0.13
02:00	780.180	5.53	0.13
02:20	800.180	5.52	0.14
02:40	820.180	5.52	0.14
03:00	840.180	5.52	0.14
03:20	860.180	5.51	0.15
03:40	880.180	5.50	0.16
04:00	900.180	5.50	0.16
04:20	920.180	5.50	0.16
04:40	940.180	5.50	0.16
05:00	960.180	5.49	0.17
05:20	980.180	5.49	0.17
05:40	1000.200	5.49	0.17
06:40	1060.400	5.49	0.17
07:40	1120.500	5.49	0.17
08:40	1180.300	5.50	0.16
09:40	1240.300	5.49	0.17
10:40	1300.200	5.50	0.16
11:40	1360.300	5.51	0.15
12:40	1420.300	5.49	0.17
13:40	1480.200	5.48	0.18
14:40	1540.300	5.44	0.22
15:40	1600.300	5.42	0.24
16:30	1650.600	5.41	0.25

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 10-2 INPUT 9  
 RADIUS: 25.391 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 5.66 FEET  
 WATER STOP LEVEL: 5.41 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
16:30	0.017	-999.99	1005.40	1005.65
16:30	0.034	-999.99	1005.40	1005.65
16:30	0.050	-999.99	1005.40	1005.65
16:30	0.067	-999.99	1005.40	1005.65
16:30	0.084	-999.99	1005.40	1005.65
16:30	0.100	-999.99	1005.40	1005.65
16:30	0.117	-999.99	1005.40	1005.65
16:30	0.134	-999.99	1005.40	1005.65
16:30	0.150	-999.99	1005.40	1005.65
16:30	0.167	-999.99	1005.40	1005.65
16:30	0.257	5.41	0.00	0.25
16:30	0.340	5.41	0.00	0.25
16:30	0.424	5.41	0.00	0.25
16:30	0.507	5.41	0.00	0.25
16:30	0.591	5.41	0.00	0.25
16:30	0.674	5.41	0.00	0.25
16:30	0.757	5.41	0.00	0.25
16:30	0.840	5.41	0.00	0.25
16:30	0.924	5.41	0.00	0.25
16:31	1.007	5.40	0.01	0.26
16:31	1.417	5.40	0.01	0.26
16:31	1.751	5.40	0.01	0.26
16:32	2.084	5.40	0.01	0.26
16:32	2.417	5.40	0.01	0.26
16:32	2.751	5.40	0.01	0.26
16:33	3.084	5.40	0.01	0.26
16:33	3.417	5.40	0.01	0.26
16:33	3.751	5.40	0.01	0.26
16:34	4.084	5.41	0.00	0.25
16:34	4.417	5.41	0.00	0.25
16:34	4.751	5.41	0.00	0.25
16:35	5.084	5.41	0.00	0.25
16:35	5.417	5.41	0.00	0.25
16:35	5.751	5.41	0.00	0.25
16:36	6.084	5.41	0.00	0.25
16:36	6.417	5.41	0.00	0.25
16:36	6.751	5.42	-0.01	0.24
16:37	7.084	5.42	-0.01	0.24

16:37	7.417	5.42	-0.01	0.24
16:37	7.751	5.42	-0.01	0.24
16:38	8.084	5.42	-0.01	0.24
16:38	8.417	5.42	-0.01	0.24
16:38	8.751	5.42	-0.01	0.24
16:39	9.084	5.42	-0.01	0.24
16:39	9.417	5.42	-0.01	0.24
16:39	9.751	5.42	-0.01	0.24
16:40	10.084	5.42	-0.01	0.24
16:42	12.120	5.41	0.00	0.25
16:44	14.120	5.40	0.01	0.26
16:46	16.120	5.39	0.02	0.27
16:48	18.120	5.39	0.02	0.27
16:50	20.142	5.39	0.02	0.27
16:52	22.225	5.40	0.01	0.26
16:54	24.225	5.40	0.01	0.26
16:56	26.225	5.40	0.01	0.26
16:58	28.225	5.40	0.01	0.26
17:00	30.225	5.40	0.01	0.26
17:02	32.225	5.40	0.01	0.26
17:04	34.225	5.40	0.01	0.26
17:06	36.225	5.40	0.01	0.26
17:08	38.225	5.40	0.01	0.26
17:10	40.225	5.40	0.01	0.26
17:12	42.225	5.40	0.01	0.26
17:14	44.225	5.40	0.01	0.26
17:16	46.225	5.40	0.01	0.26
17:18	48.225	5.39	0.02	0.27
17:20	50.342	5.40	0.01	0.26
17:22	52.220	5.40	0.01	0.26
17:24	54.222	5.39	0.02	0.27
17:26	56.222	5.39	0.02	0.27
17:28	58.220	5.39	0.02	0.27
17:30	60.120	5.39	0.02	0.27
17:32	62.220	5.39	0.02	0.27
17:34	64.222	5.39	0.02	0.27
17:36	66.220	5.39	0.02	0.27
17:38	68.220	5.40	0.01	0.26
17:40	70.220	5.39	0.02	0.27
17:42	72.220	5.40	0.01	0.26
17:44	74.222	5.40	0.01	0.26
17:46	76.095	5.40	0.01	0.26
17:48	78.180	5.40	0.01	0.26
17:50	80.575	5.40	0.01	0.26
17:52	82.215	5.39	0.02	0.27
17:54	84.215	5.39	0.02	0.27
17:56	86.215	5.39	0.02	0.27
17:58	88.215	5.39	0.02	0.27
18:00	90.493	5.39	0.02	0.27
18:02	92.210	5.39	0.02	0.27
18:04	94.248	5.39	0.02	0.27
18:06	96.248	5.39	0.02	0.27
18:08	98.248	5.39	0.02	0.27
18:30	120.250	5.39	0.02	0.27
18:50	140.250	5.39	0.02	0.27
19:10	160.180	5.38	0.03	0.28

19:30	180.170	5.39	0.02	0.27
19:50	200.220	5.39	0.02	0.27
20:10	220.150	5.39	0.02	0.27
20:30	240.150	5.40	0.01	0.26
20:50	260.150	5.41	0.00	0.25
21:10	280.250	5.42	-0.01	0.24
21:30	300.250	5.42	-0.01	0.24
21:50	320.250	5.42	-0.01	0.24
22:10	340.250	5.42	-0.01	0.24
22:30	360.220	5.43	-0.02	0.23
22:50	380.080	5.43	-0.02	0.23
23:10	400.080	5.42	-0.01	0.24
23:30	420.150	5.42	-0.01	0.24
23:50	440.080	5.42	-0.01	0.24
00:10	460.220	5.41	0.00	0.25
00:30	480.220	5.41	0.00	0.25
00:50	500.220	5.41	0.00	0.25
01:10	520.220	5.41	0.00	0.25
01:30	540.220	5.40	0.01	0.26
01:50	560.220	5.40	0.01	0.26
02:10	580.220	5.40	0.01	0.26
02:30	600.220	5.40	0.01	0.26
02:50	620.220	5.39	0.02	0.27
03:10	640.220	5.39	0.02	0.27
03:30	660.220	5.39	0.02	0.27
03:50	680.220	5.38	0.03	0.28
04:10	700.220	5.38	0.03	0.28
04:30	720.220	5.38	0.03	0.28
04:50	740.220	5.37	0.04	0.29
05:10	760.220	5.37	0.04	0.29
05:30	780.220	5.37	0.04	0.29
05:50	800.220	5.37	0.04	0.29
06:10	820.220	5.37	0.04	0.29
06:30	840.220	5.37	0.04	0.29
06:50	860.220	5.37	0.04	0.29
07:10	880.180	5.37	0.04	0.29
07:30	900.180	5.37	0.04	0.29
07:50	920.180	5.38	0.03	0.28
08:10	940.180	5.38	0.03	0.28
08:30	960.180	5.39	0.02	0.27
08:50	980.170	5.39	0.02	0.27
09:10	1000.200	5.39	0.02	0.27
10:10	1060.400	5.39	0.02	0.27
11:10	1120.700	5.40	0.01	0.26
12:10	1180.300	5.39	0.02	0.27
13:10	1240.300	5.34	0.07	0.32
14:10	1300.400	5.36	0.05	0.30
15:10	1360.300	5.32	0.09	0.34
16:10	1420.200	5.31	0.10	0.35
17:10	1480.300	5.29	0.12	0.37
18:10	1540.300	5.29	0.12	0.37
19:10	1600.300	5.29	0.12	0.37
20:10	1660.300	5.30	0.11	0.36
21:10	1720.300	5.31	0.10	0.35
22:10	1780.300	5.32	0.09	0.34
23:10	1840.300	5.33	0.08	0.33

00:10	1900.300	5.34	0.07	0.32
01:10	1960.300	5.34	0.07	0.32
02:10	2020.300	5.34	0.07	0.32
03:10	2080.300	5.33	0.08	0.33
04:10	2140.300	5.33	0.08	0.33
05:10	2200.300	5.32	0.09	0.34
06:10	2260.300	5.32	0.09	0.34
07:10	2320.300	5.32	0.09	0.34
08:10	2380.300	5.33	0.08	0.33
09:10	2440.300	5.33	0.08	0.33
10:10	2500.300	5.34	0.07	0.32
11:10	2560.300	5.33	0.08	0.33
12:10	2620.400	5.33	0.08	0.33
13:10	2680.400	5.31	0.10	0.35
14:10	2740.400	5.32	0.09	0.34
15:10	2800.400	5.27	0.14	0.39
16:10	2860.400	5.25	0.16	0.41
17:10	2920.400	5.26	0.15	0.40
18:10	2980.400	5.25	0.16	0.41
19:10	3040.200	5.25	0.16	0.41
20:10	3100.200	5.26	0.15	0.40
21:10	3160.200	5.27	0.14	0.39
22:10	3220.200	5.27	0.14	0.39
23:10	3280.200	5.29	0.12	0.37
00:10	3340.200	5.31	0.10	0.35
01:10	3400.200	5.32	0.09	0.34
02:10	3460.200	5.32	0.09	0.34
03:10	3520.200	5.31	0.10	0.35
04:10	3580.300	5.30	0.11	0.36
05:10	3640.300	5.29	0.12	0.37
06:10	3700.300	5.29	0.12	0.37
07:10	3760.300	5.28	0.13	0.38
07:36	3786.600	5.28	0.13	0.38

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: REI 10-3 INPUT 10  
 RADIUS: 63.843 FEET  
 START DATE: 15-Sep-86  
 START TIME: 13:00  
 WATER START LEVEL: 7.03 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
13:00	0.000	7.03	0.00
13:00	0.017	-999.99	1007.02
13:00	0.034	-999.99	1007.02
13:00	0.050	-999.99	1007.02
13:00	0.067	-999.99	1007.02
13:00	0.084	-999.99	1007.02
13:00	0.100	-999.99	1007.02
13:00	0.117	-999.99	1007.02
13:00	0.134	-999.99	1007.02
13:00	0.150	-999.99	1007.02
13:00	0.167	-999.99	1007.02
13:00	0.257	7.06	-0.03
13:00	0.340	7.06	-0.03
13:00	0.424	7.07	-0.04
13:00	0.507	7.07	-0.04
13:00	0.590	7.08	-0.05
13:00	0.674	7.09	-0.06
13:00	0.757	7.09	-0.06
13:00	0.840	7.10	-0.07
13:00	0.924	7.11	-0.08
13:01	1.007	7.11	-0.08
13:01	1.417	7.13	-0.10
13:01	1.750	7.14	-0.11
13:02	2.084	7.15	-0.12
13:02	2.417	7.15	-0.12
13:02	2.750	7.15	-0.12
13:03	3.084	7.12	-0.09
13:03	3.417	7.10	-0.07
13:03	3.750	7.11	-0.08
13:04	4.084	7.11	-0.08
13:04	4.417	7.09	-0.06
13:04	4.750	7.07	-0.04
13:05	5.084	7.06	-0.03
13:05	5.417	7.05	-0.02
13:05	5.750	7.04	-0.01
13:06	6.084	7.04	-0.01
13:06	6.417	7.04	-0.01
13:06	6.750	7.04	-0.01
13:07	7.084	7.04	-0.01
13:07	7.417	7.04	-0.01

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: DRAWDOWN  
 WELL NUMBER: REI 10-3 INPUT 10  
 RADIUS: 63.843 FEET  
 START DATE: 15-Sep-86  
 START TIME: 13:00  
 WATER START LEVEL: 7.03 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
13:00	0.000	7.03	0.00
13:00	0.017	-999.99	1007.02
13:00	0.034	-999.99	1007.02
13:00	0.050	-999.99	1007.02
13:00	0.067	-999.99	1007.02
13:00	0.084	-999.99	1007.02
13:00	0.100	-999.99	1007.02
13:00	0.117	-999.99	1007.02
13:00	0.134	-999.99	1007.02
13:00	0.150	-999.99	1007.02
13:00	0.167	-999.99	1007.02
13:00	0.257	7.06	-0.03
13:00	0.340	7.06	-0.03
13:00	0.424	7.07	-0.04
13:00	0.507	7.07	-0.04
13:00	0.590	7.08	-0.05
13:00	0.674	7.09	-0.06
13:00	0.757	7.09	-0.06
13:00	0.840	7.10	-0.07
13:00	0.924	7.11	-0.08
13:01	1.007	7.11	-0.08
13:01	1.417	7.13	-0.10
13:01	1.750	7.14	-0.11
13:02	2.084	7.15	-0.12
13:02	2.417	7.15	-0.12
13:02	2.750	7.15	-0.12
13:03	3.084	7.12	-0.09
13:03	3.417	7.10	-0.07
13:03	3.750	7.11	-0.08
13:04	4.084	7.11	-0.08
13:04	4.417	7.09	-0.06
13:04	4.750	7.07	-0.04
13:05	5.084	7.06	-0.03
13:05	5.417	7.05	-0.02
13:05	5.750	7.04	-0.01
13:06	6.084	7.04	-0.01
13:06	6.417	7.04	-0.01
13:06	6.750	7.04	-0.01
13:07	7.084	7.04	-0.01
13:07	7.417	7.04	-0.01



13:07	7.750	7.04	-0.01
13:08	8.084	7.05	-0.02
13:08	8.417	7.05	-0.02
13:08	8.750	7.05	-0.02
13:09	9.084	7.05	-0.02
13:09	9.417	7.06	-0.03
13:09	9.750	7.06	-0.03
13:10	10.084	7.06	-0.03
13:12	12.101	7.06	-0.03
13:14	14.188	7.11	-0.08
13:16	16.139	7.06	-0.03
13:18	18.237	7.04	-0.01
13:20	20.233	7.04	-0.01
13:22	22.233	7.05	-0.02
13:24	24.233	7.06	-0.03
13:26	26.233	7.06	-0.03
13:28	28.233	7.06	-0.03
13:30	30.233	7.06	-0.03
13:32	32.152	7.06	-0.03
13:34	34.620	7.07	-0.04
13:36	36.095	7.06	-0.03
13:38	38.095	7.07	-0.04
13:40	40.095	7.07	-0.04
13:42	42.195	7.04	-0.01
13:44	44.232	7.04	-0.01
13:46	46.232	7.05	-0.02
13:48	48.252	7.06	-0.03
13:50	50.122	7.07	-0.04
13:52	52.122	7.11	-0.08
13:54	54.122	7.09	-0.06
13:56	56.122	7.08	-0.05
13:58	58.122	7.09	-0.06
14:00	60.122	7.06	-0.03
14:02	62.122	7.04	-0.01
14:04	64.122	7.05	-0.02
14:06	66.442	7.06	-0.03
14:08	68.122	7.09	-0.06
14:10	70.335	7.10	-0.07
14:12	72.160	7.09	-0.06
14:14	74.160	7.08	-0.05
14:16	76.167	7.07	-0.04
14:18	78.230	7.07	-0.04
14:20	80.217	7.06	-0.03
14:22	82.213	7.06	-0.03
14:24	84.213	7.06	-0.03
14:26	86.213	7.06	-0.03
14:28	88.213	7.06	-0.03
14:30	90.213	7.06	-0.03
14:32	92.213	7.06	-0.03
14:34	94.213	7.05	-0.02
14:36	96.213	7.05	-0.02
14:38	98.238	7.04	-0.01
15:00	120.220	7.05	-0.02
15:20	140.130	7.05	-0.02
15:40	160.130	7.04	-0.01
16:00	180.370	7.04	-0.01

16:20	200.200	7.03	0.00
16:40	220.200	7.04	-0.01
17:00	240.080	7.03	0.00
17:20	260.220	7.03	0.00
17:40	280.150	7.03	0.00
18:00	300.150	7.04	-0.01
18:20	320.130	7.04	-0.01
18:40	340.220	7.04	-0.01
19:00	360.180	7.04	-0.01
19:20	380.220	7.04	-0.01
19:40	400.220	7.05	-0.02
20:00	420.220	7.05	-0.02
20:20	440.220	7.05	-0.02
20:40	460.220	7.06	-0.03
21:00	480.120	7.07	-0.04
21:20	500.220	7.08	-0.05
21:40	520.320	7.08	-0.05
22:00	540.200	7.08	-0.05
22:20	560.100	7.09	-0.06
22:40	580.100	7.08	-0.05
23:00	600.150	7.09	-0.06
23:20	620.150	7.10	-0.07
23:40	640.180	7.09	-0.06
00:00	660.180	7.09	-0.06
00:20	680.180	7.09	-0.06
00:40	700.180	7.09	-0.06
01:00	720.180	7.09	-0.06
01:20	740.180	7.09	-0.06
01:40	760.180	7.09	-0.06
02:00	780.180	7.10	-0.07
02:20	800.180	7.09	-0.06
02:40	820.180	7.08	-0.05
03:00	840.180	7.08	-0.05
03:20	860.180	7.08	-0.05
03:40	880.180	7.08	-0.05
04:00	900.180	7.08	-0.05
04:20	920.180	7.08	-0.05
04:40	940.180	7.08	-0.05
05:00	960.180	7.08	-0.05
05:20	980.180	7.08	-0.05
05:40	1000.200	7.08	-0.05
06:40	1060.400	7.08	-0.05
07:40	1120.500	7.10	-0.07
08:40	1180.300	7.11	-0.08
09:40	1240.300	7.10	-0.07
10:40	1300.200	7.13	-0.10
11:40	1360.300	7.15	-0.12
12:40	1420.300	7.12	-0.09
13:40	1480.200	7.13	-0.10
14:40	1540.300	7.08	-0.05
15:40	1600.300	7.06	-0.03
16:30	1650.600	7.06	-0.03

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 10-3 INPUT 10  
 RADIUS: 63.843 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 7.03 FEET  
 WATER STOP LEVEL: 7.06 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
16:30	0.017	-999.99	1007.05	1007.02
16:30	0.034	-999.99	1007.05	1007.02
16:30	0.050	-999.99	1007.05	1007.02
16:30	0.067	-999.99	1007.05	1007.02
16:30	0.084	-999.99	1007.05	1007.02
16:30	0.100	-999.99	1007.05	1007.02
16:30	0.117	-999.99	1007.05	1007.02
16:30	0.134	-999.99	1007.05	1007.02
16:30	0.150	-999.99	1007.05	1007.02
16:30	0.167	-999.99	1007.05	1007.02
16:30	0.257	7.06	0.00	0.03
16:30	0.340	7.06	0.00	0.03
16:30	0.424	7.06	0.00	0.03
16:30	0.507	7.06	0.00	0.03
16:30	0.591	7.06	0.00	0.03
16:30	0.674	7.06	0.00	0.03
16:30	0.757	7.06	0.00	0.03
16:30	0.840	7.06	0.00	0.03
16:30	0.924	7.06	0.00	0.03
16:31	1.007	7.06	0.00	0.03
16:31	1.417	7.06	0.00	0.03
16:31	1.751	7.06	0.00	0.03
16:32	2.084	7.06	0.00	0.03
16:32	2.417	7.06	0.00	0.03
16:32	2.751	7.06	0.00	0.03
16:33	3.084	7.06	0.00	0.03
16:33	3.417	7.06	0.00	0.03
16:33	3.751	7.06	0.00	0.03
16:34	4.084	7.07	-0.01	0.04
16:34	4.417	7.07	-0.01	0.04
16:34	4.751	7.06	0.00	0.03
16:35	5.084	7.07	-0.01	0.04
16:35	5.417	7.07	-0.01	0.04
16:35	5.751	7.08	-0.02	0.05
16:36	6.084	7.09	-0.03	0.06
16:36	6.417	7.09	-0.03	0.06
16:36	6.751	7.10	-0.04	0.07
16:37	7.084	7.10	-0.04	0.07

16:37	7.417	7.10	-0.04	0.07
16:37	7.751	7.10	-0.04	0.07
16:38	8.084	7.10	-0.04	0.07
16:38	8.417	7.09	-0.03	0.06
16:38	8.751	7.09	-0.03	0.06
16:39	9.084	7.09	-0.03	0.06
16:39	9.417	7.09	-0.03	0.06
16:39	9.751	7.10	-0.04	0.07
16:40	10.084	7.09	-0.03	0.06
16:42	12.120	7.08	-0.02	0.05
16:44	14.120	7.05	0.01	0.02
16:46	16.120	7.04	0.02	0.01
16:48	18.120	7.04	0.02	0.01
16:50	20.142	7.05	0.01	0.02
16:52	22.225	7.05	0.01	0.02
16:54	24.225	7.05	0.01	0.02
16:56	26.225	7.05	0.01	0.02
16:58	28.225	7.05	0.01	0.02
17:00	30.225	7.05	0.01	0.02
17:02	32.225	7.05	0.01	0.02
17:04	34.225	7.05	0.01	0.02
17:06	36.225	7.05	0.01	0.02
17:08	38.225	7.05	0.01	0.02
17:10	40.225	7.05	0.01	0.02
17:12	42.225	7.05	0.01	0.02
17:14	44.225	7.05	0.01	0.02
17:16	46.225	7.05	0.01	0.02
17:18	48.225	7.05	0.01	0.02
17:20	50.342	7.05	0.01	0.02
17:22	52.220	7.05	0.01	0.02
17:24	54.222	7.05	0.01	0.02
17:26	56.222	7.05	0.01	0.02
17:28	58.220	7.05	0.01	0.02
17:30	60.120	7.05	0.01	0.02
17:32	62.220	7.05	0.01	0.02
17:34	64.222	7.05	0.01	0.02
17:36	66.220	7.05	0.01	0.02
17:38	68.220	7.06	0.00	0.03
17:40	70.220	7.06	0.00	0.03
17:42	72.220	7.06	0.00	0.03
17:44	74.222	7.06	0.00	0.03
17:46	76.095	7.06	0.00	0.03
17:48	78.180	7.06	0.00	0.03
17:50	80.575	7.06	0.00	0.03
17:52	82.215	7.06	0.00	0.03
17:54	84.215	7.06	0.00	0.03
17:56	86.215	7.06	0.00	0.03
17:58	88.215	7.06	0.00	0.03
18:00	90.493	7.06	0.00	0.03
18:02	92.210	7.06	0.00	0.03
18:04	94.248	7.06	0.00	0.03
18:06	96.248	7.06	0.00	0.03
18:08	98.248	7.06	0.00	0.03
18:30	120.250	7.06	0.00	0.03
18:50	140.250	7.06	0.00	0.03
19:10	160.180	7.06	0.00	0.03

19:30	180.170	7.06	0.00	0.03
19:50	200.220	7.07	-0.01	0.04
20:10	220.150	7.08	-0.02	0.05
20:30	240.150	7.08	-0.02	0.05
20:50	260.150	7.09	-0.03	0.06
21:10	280.250	7.11	-0.05	0.08
21:30	300.250	7.11	-0.05	0.08
21:50	320.250	7.11	-0.05	0.08
22:10	340.250	7.11	-0.05	0.08
22:30	360.220	7.12	-0.06	0.09
22:50	380.080	7.12	-0.06	0.09
23:10	400.080	7.12	-0.06	0.09
23:30	420.150	7.12	-0.06	0.09
23:50	440.080	7.11	-0.05	0.08
00:10	460.220	7.11	-0.05	0.08
00:30	480.220	7.11	-0.05	0.08
00:50	500.220	7.11	-0.05	0.08
01:10	520.220	7.11	-0.05	0.08
01:30	540.220	7.10	-0.04	0.07
01:50	560.220	7.11	-0.05	0.08
02:10	580.220	7.10	-0.04	0.07
02:30	600.220	7.10	-0.04	0.07
02:50	620.220	7.10	-0.04	0.07
03:10	640.220	7.10	-0.04	0.07
03:30	660.220	7.09	-0.03	0.06
03:50	680.220	7.09	-0.03	0.06
04:10	700.220	7.09	-0.03	0.06
04:30	720.220	7.09	-0.03	0.06
04:50	740.220	7.08	-0.02	0.05
05:10	760.220	7.08	-0.02	0.05
05:30	780.220	7.08	-0.02	0.05
05:50	800.220	7.08	-0.02	0.05
06:10	820.220	7.08	-0.02	0.05
06:30	840.220	7.08	-0.02	0.05
06:50	860.220	7.09	-0.03	0.06
07:10	880.180	7.08	-0.02	0.05
07:30	900.180	7.09	-0.03	0.06
07:50	920.180	7.10	-0.04	0.07
08:10	940.180	7.10	-0.04	0.07
08:30	960.180	7.10	-0.04	0.07
08:50	980.170	7.10	-0.04	0.07
09:10	1000.200	7.12	-0.06	0.09
10:10	1060.400	7.11	-0.05	0.08
11:10	1120.700	7.14	-0.08	0.11
12:10	1180.300	7.13	-0.07	0.10
13:10	1240.300	7.05	0.01	0.02
14:10	1300.400	-999.99	1007.05	1007.02
15:10	1360.300	-999.99	1007.05	1007.02
16:10	1420.200	7.05	0.01	0.02
17:10	1480.300	7.05	0.01	0.02
18:10	1540.300	7.05	0.01	0.02
19:10	1600.300	7.05	0.01	0.02
20:10	1660.300	7.06	0.00	0.03
21:10	1720.300	7.09	-0.03	0.06
22:10	1780.300	7.09	-0.03	0.06
23:10	1840.300	7.10	-0.04	0.07

00:10	1900.300	7.11	-0.05	0.08
01:10	1960.300	7.11	-0.05	0.08
02:10	2020.300	7.11	-0.05	0.08
03:10	2080.300	7.11	-0.05	0.08
04:10	2140.300	7.11	-0.05	0.08
05:10	2200.300	7.11	-0.05	0.08
06:10	2260.300	7.11	-0.05	0.08
07:10	2320.300	7.12	-0.06	0.09
08:10	2380.300	7.13	-0.07	0.10
09:10	2440.300	7.14	-0.08	0.11
10:10	2500.300	7.15	-0.09	0.12
11:10	2560.300	7.14	-0.08	0.11
12:10	2620.400	7.16	-0.10	0.13
13:10	2680.400	7.13	-0.07	0.10
14:10	2740.400	7.18	-0.12	0.15
15:10	2800.400	7.11	-0.05	0.08
16:10	2860.400	7.08	-0.02	0.05
17:10	2920.400	7.11	-0.05	0.08
18:10	2980.400	7.10	-0.04	0.07
19:10	3040.200	7.10	-0.04	0.07
20:10	3100.200	7.12	-0.06	0.09
21:10	3160.200	7.13	-0.07	0.10
22:10	3220.200	7.14	-0.08	0.11
23:10	3280.200	7.16	-0.10	0.13
00:10	3340.200	7.17	-0.11	0.14
01:10	3400.200	7.17	-0.11	0.14
02:10	3460.200	7.17	-0.11	0.14
03:10	3520.200	7.16	-0.10	0.13
04:10	3580.300	7.15	-0.09	0.12
05:10	3640.300	7.15	-0.09	0.12
06:10	3700.300	7.16	-0.10	0.13
07:10	3760.300	7.15	-0.09	0.12
07:36	3786.600	7.15	-0.09	0.12

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 10-1 RUN # 1  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 10-4 INPUT 11  
 RADIUS : 34.651 FEET  
 START DATE : 15-Sep-86  
 START TIME : 13:00  
 WATER START LEVEL : 7.52 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
13:00	0.000	7.52	0.00
13:00	0.017	-999.99	1007.51
13:00	0.034	-999.99	1007.51
13:00	0.050	-999.99	1007.51
13:00	0.067	-999.99	1007.51
13:00	0.084	-999.99	1007.51
13:00	0.100	-999.99	1007.51
13:00	0.117	-999.99	1007.51
13:00	0.134	-999.99	1007.51
13:00	0.150	-999.99	1007.51
13:00	0.167	-999.99	1007.51
13:00	0.257	7.53	-0.01
13:00	0.340	7.53	-0.01
13:00	0.424	7.53	-0.01
13:00	0.507	7.53	-0.01
13:00	0.590	7.53	-0.01
13:00	0.674	7.53	-0.01
13:00	0.757	7.54	-0.02
13:00	0.840	7.54	-0.02
13:00	0.924	7.55	-0.03
13:01	1.007	7.55	-0.03
13:01	1.417	7.56	-0.04
13:01	1.750	7.56	-0.04
13:02	2.084	7.56	-0.04
13:02	2.417	7.55	-0.03
13:02	2.750	7.55	-0.03
13:03	3.084	7.54	-0.02
13:03	3.417	7.53	-0.01
13:03	3.750	7.54	-0.02
13:04	4.084	7.54	-0.02
13:04	4.417	7.53	-0.01
13:04	4.750	7.53	-0.01
13:05	5.084	7.52	0.00
13:05	5.417	7.51	0.01
13:05	5.750	7.51	0.01
13:06	6.084	7.51	0.01
13:06	6.417	7.51	0.01
13:06	6.750	7.51	0.01
13:07	7.084	7.51	0.01
13:07	7.417	7.51	0.01

13:07	7.750	7.51	0.01
13:08	8.084	7.51	0.01
13:08	8.417	7.51	0.01
13:08	8.750	7.51	0.01
13:09	9.084	7.51	0.01
13:09	9.417	7.51	0.01
13:09	9.750	7.51	0.01
13:10	10.084	7.51	0.01
13:12	12.101	7.51	0.01
13:14	14.188	7.52	0.00
13:16	16.139	7.50	0.02
13:18	18.237	7.49	0.03
13:20	20.233	7.50	0.02
13:22	22.233	7.49	0.03
13:24	24.233	7.50	0.02
13:26	26.233	7.49	0.03
13:28	28.233	7.49	0.03
13:30	30.233	7.49	0.03
13:32	32.152	7.48	0.04
13:34	34.620	7.49	0.03
13:36	36.095	7.49	0.03
13:38	38.095	7.49	0.03
13:40	40.095	7.48	0.04
13:42	42.195	7.48	0.04
13:44	44.232	7.48	0.04
13:46	46.232	7.48	0.04
13:48	48.252	7.48	0.04
13:50	50.122	7.48	0.04
13:52	52.122	7.49	0.03
13:54	54.122	7.48	0.04
13:56	56.122	7.47	0.05
13:58	58.122	7.49	0.03
14:00	60.122	7.47	0.05
14:02	62.122	7.46	0.06
14:04	64.122	7.46	0.06
14:06	66.442	7.47	0.05
14:08	68.122	7.48	0.04
14:10	70.335	7.48	0.04
14:12	72.160	7.47	0.05
14:14	74.160	7.46	0.06
14:16	76.167	7.46	0.06
14:18	78.230	7.45	0.07
14:20	80.217	7.46	0.06
14:22	82.213	7.45	0.07
14:24	84.213	7.45	0.07
14:26	86.213	7.45	0.07
14:28	88.213	7.45	0.07
14:30	90.213	7.44	0.08
14:32	92.213	7.44	0.08
14:34	94.213	7.43	0.09
14:36	96.213	7.43	0.09
14:38	98.238	7.43	0.09
15:00	120.220	7.42	0.10
15:20	140.130	7.39	0.13
15:40	160.130	7.37	0.15
16:00	180.370	7.37	0.15



16:20	200.200	7.36	0.16
16:40	220.200	7.35	0.17
17:00	240.080	7.34	0.18
17:20	260.220	7.33	0.19
17:40	280.150	7.32	0.20
18:00	300.150	7.32	0.20
18:20	320.130	7.30	0.22
18:40	340.220	7.29	0.23
19:00	360.180	7.29	0.23
19:20	380.220	7.28	0.24
19:40	400.220	7.27	0.25
20:00	420.220	7.27	0.25
20:20	440.220	7.27	0.25
20:40	460.220	7.27	0.25
21:00	480.120	7.27	0.25
21:20	500.220	7.27	0.25
21:40	520.320	7.27	0.25
22:00	540.200	7.27	0.25
22:20	560.100	7.26	0.26
22:40	580.100	7.25	0.27
23:00	600.150	7.25	0.27
23:20	620.150	7.24	0.28
23:40	640.180	7.24	0.28
00:00	660.180	7.23	0.29
00:20	680.180	7.23	0.29
00:40	700.180	7.23	0.29
01:00	720.180	7.23	0.29
01:20	740.180	7.22	0.30
01:40	760.180	7.22	0.30
02:00	780.180	7.22	0.30
02:20	800.180	7.21	0.31
02:40	820.180	7.20	0.32
03:00	840.180	7.20	0.32
03:20	860.180	7.19	0.33
03:40	880.180	7.19	0.33
04:00	900.180	7.18	0.34
04:20	920.180	7.19	0.33
04:40	940.180	7.19	0.33
05:00	960.180	7.18	0.34
05:20	980.180	7.18	0.34
05:40	1000.200	7.17	0.35
06:40	1060.400	7.17	0.35
07:40	1120.500	7.18	0.34
08:40	1180.300	7.18	0.34
09:40	1240.300	7.18	0.34
10:40	1300.200	7.19	0.33
11:40	1360.300	7.18	0.34
12:40	1420.300	7.16	0.36
13:40	1480.200	7.15	0.37
14:40	1540.300	7.11	0.41
15:40	1600.300	7.09	0.43
16:30	1650.600	7.07	0.45

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 1  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 10-4 INPUT 11  
 RADIUS: 34.651 FEET  
 START DATE: 15-Sep-86  
 START TIME: 16:30  
 WATER START LEVEL: 7.52 FEET  
 WATER STOP LEVEL: 7.07 FEET  
 TOTAL PUMPING TIME: 1650.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
16:30	0.017	-999.99	1007.06	1007.51
16:30	0.034	-999.99	1007.06	1007.51
16:30	0.050	-999.99	1007.06	1007.51
16:30	0.067	-999.99	1007.06	1007.51
16:30	0.084	-999.99	1007.06	1007.51
16:30	0.100	-999.99	1007.06	1007.51
16:30	0.117	-999.99	1007.06	1007.51
16:30	0.134	-999.99	1007.06	1007.51
16:30	0.150	-999.99	1007.06	1007.51
16:30	0.167	-999.99	1007.06	1007.51
16:30	0.257	7.07	0.00	0.45
16:30	0.340	7.07	0.00	0.45
16:30	0.424	7.07	0.00	0.45
16:30	0.507	7.07	0.00	0.45
16:30	0.591	7.07	0.00	0.45
16:30	0.674	7.07	0.00	0.45
16:30	0.757	7.07	0.00	0.45
16:30	0.840	7.07	0.00	0.45
16:30	0.924	7.07	0.00	0.45
16:31	1.007	7.07	0.00	0.45
16:31	1.417	7.07	0.00	0.45
16:31	1.751	7.07	0.00	0.45
16:32	2.084	7.07	0.00	0.45
16:32	2.417	7.07	0.00	0.45
16:32	2.751	7.07	0.00	0.45
16:33	3.084	7.07	0.00	0.45
16:33	3.417	7.07	0.00	0.45
16:33	3.751	7.07	0.00	0.45
16:34	4.084	7.07	0.00	0.45
16:34	4.417	7.07	0.00	0.45
16:34	4.751	7.07	0.00	0.45
16:35	5.084	7.07	0.00	0.45
16:35	5.417	7.07	0.00	0.45
16:35	5.751	7.08	-0.01	0.44
16:36	6.084	7.08	-0.01	0.44
16:36	6.417	7.08	-0.01	0.44
16:36	6.751	7.08	-0.01	0.44
16:37	7.084	7.09	-0.02	0.43

16:37	7.417	7.08	-0.01	0.44
16:37	7.751	7.09	-0.02	0.43
16:38	8.084	7.08	-0.01	0.44
16:38	8.417	7.08	-0.01	0.44
16:38	8.751	7.08	-0.01	0.44
16:39	9.084	7.08	-0.01	0.44
16:39	9.417	7.08	-0.01	0.44
16:39	9.751	7.08	-0.01	0.44
16:40	10.084	7.08	-0.01	0.44
16:42	12.120	7.07	0.00	0.45
16:44	14.120	7.07	0.00	0.45
16:46	16.120	7.06	0.01	0.46
16:48	18.120	7.07	0.00	0.45
16:50	20.142	7.07	0.00	0.45
16:52	22.225	7.06	0.01	0.46
16:54	24.225	7.07	0.00	0.45
16:56	26.225	7.06	0.01	0.46
16:58	28.225	7.06	0.01	0.46
17:00	30.225	7.06	0.01	0.46
17:02	32.225	7.06	0.01	0.46
17:04	34.225	7.06	0.01	0.46
17:06	36.225	7.06	0.01	0.46
17:08	38.225	7.06	0.01	0.46
17:10	40.225	7.06	0.01	0.46
17:12	42.225	7.06	0.01	0.46
17:14	44.225	7.06	0.01	0.46
17:16	46.225	7.06	0.01	0.46
17:18	48.225	7.06	0.01	0.46
17:20	50.342	7.06	0.01	0.46
17:22	52.220	7.06	0.01	0.46
17:24	54.222	7.06	0.01	0.46
17:26	56.222	7.06	0.01	0.46
17:28	58.220	7.06	0.01	0.46
17:30	60.120	7.06	0.01	0.46
17:32	62.220	7.06	0.01	0.46
17:34	64.222	7.06	0.01	0.46
17:36	66.220	7.06	0.01	0.46
17:38	68.220	7.06	0.01	0.46
17:40	70.220	7.06	0.01	0.46
17:42	72.220	7.06	0.01	0.46
17:44	74.222	7.06	0.01	0.46
17:46	76.095	7.06	0.01	0.46
17:48	78.180	7.06	0.01	0.46
17:50	80.575	7.06	0.01	0.46
17:52	82.215	7.06	0.01	0.46
17:54	84.215	7.06	0.01	0.46
17:56	86.215	7.06	0.01	0.46
17:58	88.215	7.06	0.01	0.46
18:00	90.493	7.06	0.01	0.46
18:02	92.210	7.05	0.02	0.47
18:04	94.248	7.06	0.01	0.46
18:06	96.248	7.06	0.01	0.46
18:08	98.248	7.06	0.01	0.46
18:30	120.250	7.05	0.02	0.47
18:50	140.250	7.05	0.02	0.47
19:10	160.180	7.05	0.02	0.47

19:30	180.170	7.05	0.02	0.47
19:50	200.220	7.05	0.02	0.47
20:10	220.150	7.06	0.01	0.46
20:30	240.150	7.06	0.01	0.46
20:50	260.150	7.07	0.00	0.45
21:10	280.250	7.08	-0.01	0.44
21:30	300.250	7.08	-0.01	0.44
21:50	320.250	7.08	-0.01	0.44
22:10	340.250	7.08	-0.01	0.44
22:30	360.220	7.08	-0.01	0.44
22:50	380.080	7.08	-0.01	0.44
23:10	400.080	7.07	0.00	0.45
23:30	420.150	7.07	0.00	0.45
23:50	440.080	7.06	0.01	0.46
00:10	460.220	7.07	0.00	0.45
00:30	480.220	7.06	0.01	0.46
00:50	500.220	7.06	0.01	0.46
01:10	520.220	7.05	0.02	0.47
01:30	540.220	7.05	0.02	0.47
01:50	560.220	7.04	0.03	0.48
02:10	580.220	7.04	0.03	0.48
02:30	600.220	7.03	0.04	0.49
02:50	620.220	7.02	0.05	0.50
03:10	640.220	7.02	0.05	0.50
03:30	660.220	7.01	0.06	0.51
03:50	680.220	7.00	0.07	0.52
04:10	700.220	7.00	0.07	0.52
04:30	720.220	6.99	0.08	0.53
04:50	740.220	6.98	0.09	0.54
05:10	760.220	6.98	0.09	0.54
05:30	780.220	6.98	0.09	0.54
05:50	800.220	6.98	0.09	0.54
06:10	820.220	6.98	0.09	0.54
06:30	840.220	6.98	0.09	0.54
06:50	860.220	6.99	0.08	0.53
07:10	880.180	6.98	0.09	0.54
07:30	900.180	7.08	-0.01	0.44
07:50	920.180	7.07	0.00	0.45
08:10	940.180	7.05	0.02	0.47
08:30	960.180	7.04	0.03	0.48
08:50	980.170	7.03	0.04	0.49
09:10	1000.200	7.11	-0.04	0.41
10:10	1060.400	7.08	-0.01	0.44
11:10	1120.700	7.12	-0.05	0.40
12:10	1180.300	7.08	-0.01	0.44
13:10	1240.300	7.01	0.06	0.51
14:10	1300.400	7.04	0.03	0.48
15:10	1360.300	6.98	0.09	0.54
16:10	1420.200	7.01	0.06	0.51
17:10	1480.300	6.97	0.10	0.55
18:10	1540.300	7.03	0.04	0.49
19:10	1600.300	7.00	0.07	0.52
20:10	1660.300	6.98	0.09	0.54
21:10	1720.300	7.09	-0.02	0.43
22:10	1780.300	7.08	-0.01	0.44
23:10	1840.300	7.07	0.00	0.45

00:10	1900.300	7.05	0.02	0.47
01:10	1960.300	7.03	0.04	0.49
02:10	2020.300	7.01	0.06	0.51
03:10	2080.300	7.09	-0.02	0.43
04:10	2140.300	7.06	0.01	0.46
05:10	2200.300	7.04	0.03	0.48
06:10	2260.300	7.02	0.05	0.50
07:10	2320.300	7.01	0.06	0.51
08:10	2380.300	7.02	0.05	0.50
09:10	2440.300	7.13	-0.06	0.39
10:10	2500.300	7.13	-0.06	0.39
11:10	2560.300	7.11	-0.04	0.41
12:10	2620.400	7.10	-0.03	0.42
13:10	2680.400	7.06	0.01	0.46
14:10	2740.400	7.04	0.03	0.48
15:10	2800.400	7.01	0.06	0.51
16:10	2860.400	6.99	0.08	0.53
17:10	2920.400	6.98	0.09	0.54
18:10	2980.400	6.98	0.09	0.54
19:10	3040.200	6.97	0.10	0.55
20:10	3100.200	6.97	0.10	0.55
21:10	3160.200	7.07	0.00	0.45
22:10	3220.200	7.08	-0.01	0.44
23:10	3280.200	7.09	-0.02	0.43
00:10	3340.200	7.09	-0.02	0.43
01:10	3400.200	7.08	-0.01	0.44
02:10	3460.200	7.07	0.00	0.45
03:10	3520.200	7.05	0.02	0.47
04:10	3580.300	7.03	0.04	0.49
05:10	3640.300	7.03	0.04	0.49
06:10	3700.300	7.03	0.04	0.49
07:10	3760.300	7.01	0.06	0.51
07:36	3786.600	7.02	0.05	0.50

SHEET 1 OF 1

WELL NUMBER: Staff gauge in pond  
r IN FEET: \_\_\_\_\_  
STARTING WATER LEVEL: \_\_\_\_\_

9/17/86

**SHEET 2**

WELL NUMBER: GW-25  
 r IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

9/17/86

# REN

SHEET 1 OF

WELL NUMBER: REI-11  
 r IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

9/17/86



## THE END OF

WELL NUMBER: REI-3-4  
 IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

9/17/86

**REN**

Appendix 19

REI 10-1 Run #2 Pumping Test Data Sheets

FRENCH Ltd. REI 10-1 Pump Test  
Run  
10/07/86

SE200B DATA  
constant rate test

TRANSDUCER TABLE

Input 1: REI 10-1  
Transducer s/n: 139  
Scale factor: 49.59  
Initial level: 81.34 feet

FAST DATA

Input 2: REI-11  
Transducer s/n: 1076/849  
Scale factor: 10.07  
Initial level: 78.42 feet

Input 3: none  
Transducer s/n: none  
Scale factor: 1

Input 4: REI 3-4  
Transducer s/n: 1059/854  
Scale factor: 10.09  
Initial level: 80.79 feet

Input 5: REI-7  
Transducer s/n: 1366/851  
Scale factor: 10.09  
Initial level: 80.33 feet

Input 6: P-10-2  
Transducer s/n: 1634/857  
Scale factor: 10.08  
Initial level: 46.06 feet

Input 7: P-10-3  
Transducer s/n: 1518/854  
Scale factor: 10.08  
Initial level: 39.72 feet

Input 8: P-10-4  
Transducer s/n: 2344/85n  
Scale factor: 10.13  
Initial level: 38.82 feet

Input 9: REI 10-2  
Transducer s/n: 516/830  
Scale factor: 10.04  
Initial level: 5.78 feet

Input 10: REI 10-7  
Transducer s/n: 596/841  
Scale factor: 10.03  
Initial level: 7.14 feet

Input 11: REI 10-4  
Transducer s/n: 1631/857  
Scale factor: 10.09  
Initial level: 7.66 feet

# CALCULATIONS AND COMPUTATIONS

SHEET 1 OF     

PROJECT: French Ltd Ret/O-1 Run #2  
10-7-86

JOB NO.:     

SUBJECT: FLOW RATE MONITORING SHEET  
10-7-86

COMPUTED BY:      DATE:     

CHECKED BY:      DATE:     

FLOW RATE	TIME (2400)	MONITORS INITIALS		FLOW RATE	TIME (2400)	MONITORS INITIALS
0	0:900:00	Qcm	Test start	12.1 → 12.0	10:20	J.A.
12.0	0901:18	Qcm		12.1 → 12.0	10:25	J.A.
12.0	0902	Qcm		12.0	10:31	J.A.
12.0	0904	Qcm		11.9 → 12.0	10:35	J.A.
12.0	0906	Qcm		12.1 → 12.0	10:40	J.A.
11.9 <del>12.0</del>	0908	<del>Qcm</del> DWD		12.1 → 12.0	10:45	J.A.
11.9	0910	DWD		12.0 → 12.0	10:50	DWD
11.8 → 12.0	0912	DWD		12.1	10:55	DWD
12.0	0914	DWD		12.1	10:59	DWD
12.0	0916	DWD		12.1	11:07	DWD
12.0	0918	DWD		12.0	11:10	DWD
12.0	0920	DWD		12.0	11:15	DWD
12.0	0922	DWD		12.0	11:20	D.W.D
12.0 → 11.9	0924	DWP		12.0	11:25	D.W.D
12.0 → 11.9	0926	DWD		12.0	11:30	D.W.D
12.0	0928	DWD		12.0	11:36	J.A.
12.0	0930	DWD		12.0	11:40	J.A.
11.9	0935	DWD		12.0	11:45	J.A.
11.9	0939	Qcm		12.0	11:50	J.A.
12.0	0940	Qcm		12.0	11:55	J.A.
12.0	0945	Qcm		12.0	12:00	D.W.D
12.0	0950	Qcm		12.1	12:17	D.W.D
12.0	0954	Qcm		12.0	12:30	D.W.D
12.1 → 12.0	10:00	J.A.		12.0	12:43	D.W.D
12.0	10:05	J.A.		12.0 → 12.2	1:00	D.W.D
12.0	10:10	J.A.		11.9	13:15	DWD
12.0	10:15	J.A.		12.1	13:30	D.W.D

Within .5  
of 12.0  
after 30 seconds  
in do  
+ test 1

2

Flow drift + ↓ ↓

Readings  
on 2min intervals

5

Readings  
on 5min  
intervals

5min  
interval

15min  
interval

bucket method

17.8 gpm →  
D.W.D

**1000**

# CALCULATIONS AND COMPUTATIONS

SHEET 2 OF

PROJECT: French Ltd. REI 10-J Run #2

JOB NO.:

10-7-86-10-81

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY: DATE:

CHECKED BY: DATE:

m

FLOW RATE	TIME (2400)	MONITORS INITIALS		FLOW RATE	TIME (2400)	MONITORS INITIALS
12.1	13:45	A	5 gal/17 sec	12.3	1901	MC
12.1	14:00	A				
12.0-12.1	14:15	D.W.D				
12.4	14:30	D.W.D	5 gal/17 sec	10/10	2258	TR
12.0	14:45	A	5 gal/17 sec			
12.0-12.1	15:00	A.B	5 gal/16.5 sec		00:30	
12.0	15:10	A.B	5 gal/17 sec	10/8/86	1:30	
12-1	15:25	D.W.D	5 gal/17 sec		5:00	
11.8-11.9	15:35	AB	5 gal/17 sec		4:30	A.T.
12.0	15:40	AB	5 gal/17 sec		6:00	A.T.
12.1	15:50	AB	5 gal/17 sec		7:10	D.W.D
12.1	16:00	AB	5 gal/17-18 sec		7:44	D.W.D
12.1	16:10	AB	5 gal/17-18 sec		8:00	D.W.D
12.0	16:20	AB	5 gal/17-18 sec	10.2 (meter)	8:15	D.W.D
12.1	16:30	AB	5 gal/17-18 sec	10.2 (meter)	8:30	D.W.D
12.1	16:42	AB	5 gal/17-18 sec	10.2 (meter)	8:45	D.W.D
12.0	16:50	AB	5 gal/17-18 sec	10.2 (meter)	9:00	D.W.D
11.9	16:59	D.W.D	5 gal/17-18 sec	10.2 (meter)	9:15	D.W.D
12.1	17:17	D.W.D	5 gal/17 sec	10.1 (meter)	9:30	D.W.D
12.1	17:45	AB	5 gal/17-18 sec	9.9 (meter)	9:45	D.W.D
36.7	18:08	D.W.D	← valve opened with 13 sec/5 gal	5 gal/17-18 sec 9.5 (meter)	10:03	D.W.D
17:0	18:10	D.W.D		5 gal/17-18 sec 9.5 (meter)	10:16	D.W.D
12.0	18:11	D.W.D	17 sec/5 gal	5 gal/17-18 sec 9.9 (meter)	10:30	D.W.D
12.5	18:27	D.W.D	17-18 sec/5 gal	5 gal/17-18 sec 9.8 (meter)	10:45	D.W.D
12.4	18:28	D.W.D	17-18 sec/5 gal	5 gal/17-18 sec (12 meter)	11:01	D.W.D
12.4	18:43	MC	17 sec/5 gal	5 gal/17-18 sec	11:16	D.W.D
12.3	19:00	MC	17 sec/5 gal	5 gal/17-18 sec	11:45	D.W.D

IBIP

Bucket method = 17.5 gpm

Bucket method = 17.5 gpm

Bucket method = 17.5 gpm

BUCKET 5 gal/17 sec

# CALCULATIONS AND COMPUTATIONS

SHEET 3 OF 3

PROJECT: French Lk. REI 10-1

JOB NO.: \_\_\_\_\_

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

FLOW RATE	TIME (2400)	MONITORS INITIALS	FLOW RATE	TIME (2400)	MONITORS INITIALS
Sgal/17-18 sec.	12:08	DRG	Sgal/17	5:31 sec	A.T
Sgal/17.18s.	12:30	DWD	Sgal/17	6:15 sec	A.T
Sgal/17.88s	12:47	DWD/DRG	Sgal/17.8	7:00 sec.	A.T
Sgal/17.88sec.	13:00	DWD	Sgal/17.9sec.	7:30	D.W.D.
Sgal/18sec.	13:45	DWD	Sgal/17.41sec.	8:39	D.W.D.
Sgal/17-18sec.	14:00	DWD	Sgal/17.42s	9:36	DRG
Sgal/17.88s.	14:35	DWD	Sgal/17.61sec.	10:02	DWD
Sgal/17.84s	14:46	DWD	Sgal/17.64s	10:31	DWD
Sgal/17.90s	15:02	DWD	Sgal/17.12s	11:01	DWD
Sgal/17.65sec.	16:05	M.C.	Sgal/17.53s	11:35	DRG
Sgal/17.5sec.	17:10	M.C.	Sgal/17.79s	12:04	DRG
Sgal/17.63sec.	17:33	M.C.	Sgal/17.87s	12:30	DRG
Sgal/17.5sec.	18:10	M.C.	Sgal/17.50s	13:02	DWD
Sgal/17.5sec.	19:46	M.C.	Sgal/17.73s	13:30	DRG
Sgal/17.5sec.	20:45	M.C.	Sgal/17.93s	14:01	DWD
Sgal/17.5sec.	21:30	M.C.	Sgal/17.66s	14:31	DWD
Sgal/17.5sec.	22:15	M.C.	Sgal/17.70s	15:02	DWD
Sgal/17.5sec.	23:30	A.T	SGAL/17.5s	16:00	M.C.
Sgal/17.5sec.	0:00	A.T	SGAL/17.5s	16:30	M.C.
Sgal/17.5sec.	0:32	A.T	SGAL/17.2	16:59	M.C.
Sgal/17.5sec.	1:08	A.T	SGAL/17.5s	17:30	M.C.
Sgal/17.5sec.	1:31	A.T	SGAL/17.5s	18:00	M.C.
Sgal/17.8sec.	2:10	A.T	Sgal/17.67sec.	19:15	A.B
Sgal/17.5sec.	2:57	A.T	Sgal/17.64	20:21	A.B
Sgal/17.5sec.	3:38	A.T	Sgal/17.56	21:00	M.C.
Sgal/17.8sec.	4:00	A.T	SGAL/17.25	22:00	AB
Sgal/17.5sec.	9:50	A.T	Sgal/17.5	23:00	A.T

10/8/86

15

30 60  
10

10/9/86

watch  
is not  
digital

10/21

# CALCULATIONS AND COMPUTATIONS

SHEET 4 OF 4

PROJECT: FRANK LTD REI 10-1

JOB NO.: \_\_\_\_\_

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

FLOW RATE	TIME (2400)	MONITOR'S INITIALS		FLOW RATE	TIME (2400)	MONITOR'S INITIALS
<del>5 Gal/17.5</del>	00:02	A.T.		5 gal/17.9s	14:05	DWD
5 Gal/17.5	01:05	A.T.		5 gal/17.6s	14:31	DWD
5 Gal/17	02:03	A.T.		5 gal/17.5s	15:06	DWD
5 Gal/17	03:04	A.T.		5 gal/17.5s	15:31	DWD
5 Gal/17	03:50	A.T.		5 gal/17.31	16:04	A.B.
5 Gal/17	05:06	A.T.		5 gal/17.25	16:38	A.B.
5 Gal/17	06:01	A.T.		5 gal/18.70	17:40	A.B.
5 Gal/17	06:57	A.T.		5 gal/18.66	18:04	A.B.
5 gal/17.43	07:13	DWD		5 gal/17.61sec	18:05	A.B.
5 gal/17.52	7:30	DWD		5 gal/17.60	18:30	JG
5 gal/17.52	7:45	DWD		5 gal/17.57	19:05	A.B.
5 gal/17.52	8:00	DWD		5 gal/17.25	19:32	A.B.
5 gal/17.84s	8:21	DWD		5 gal/17.19	20:15	JG
5 gal/17.52	8:50	DWD		5 gal/17.30	20:34	JG
5 gal/17.6s	8:47	DWD		5 gal/17.60	21:00	JG
5 gal/17.42	9:00	DWD		5 gal/17.51	21:35	JG
5 gal/17.56	9:30	DWD		5 gal/17.53	22:10	JG
5 gal/17.37	10:00	DWD		5 gal/17.66	22:50	A.B.
5 gal/17.56	10:30	DWD		5 gal/17	23:54	A.T.
5 gal/17.5s	11:00	DRG		5 Gal/17.5	01:14	A.T.
5 gal/17.52	11:30	DWD		5 Gal/17.5	02:08	A.T.
5 gal/17.5s	12:00	DWD		5 Gal/17.5	03:11	A.T.
5 gal/17.13s	12:10	DWD		5 Gal/17.5	04:02	A.T.
5 gal/17.43	12:23	DWD		5 Gal/17.5	05:03	A.T.
5 gal/17.8s	12:45	DWD		5 Gal/17.5	06:01	A.T.
5 gal/17.5s	13:14	DWD		5 Gal/17.5	06:55	A.T.
5 gal/17.13s	13:51	DWD		5 gal/17.7	08:02	A.B.

Switched generators A.B.

adjusted flow rate A.B.

10/11/86

10-10-86

1208  
Pump turned  
off for  
2 seconds

10/11/86

# CALCULATIONS AND COMPUTATIONS

SHEET 5 OF     

PROJECT: French Ltd REI 10-1

JOB NO.:     

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY:      DATE:     

CHECKED BY:      DATE:     

FLOW RATE	TIME (2400)	MONITORS INITIALS	FLOW RATE	TIME (2400)	MONITORS INITIALS
Sgal/17.6s	08:30	AB	Sgal/17.5s	800	DWN
Sgal/17.4s	09:02	DRG	Sgal/17.5s	830	DWD
Sgal/17.6s	09:33	DRG	Sgal/17.5s	170	DWN
Sgal/17.9s	10:02	DRG	Sgal/17.5s	200	DWN
Sgal/17.8s	10:34	DRG	Sgal/17.5s	1034	DWN
Sgal/17.7s	10:56	DRG	Sgal/17.5s	11:15	DWD
Sgal/17.67	11:58	AB	Sgal/17.5s	11:30	DWD
Sgal/17.5s	12:57	DRG	Sgal/17.5s	12:04	DWD
Sgal/17.82	13:53	AB	Sgal/17.5s	12:30	DWN
Sgal/17.7	14:57	DRG	Sgal/17.5s	13:10	DWD
Sgal/17.8s	15:25	DD	Sgal/17.5s	14:00	DWN
Sgal/17.75s	16:00	DD	Sgal/17.5s	14:30	DWN
Sgal/17.7	16:50	MC	Sgal/17.5s	15:20	DWD
Sgal/17.6	17:30	MC	Sgal/17.5	17:20	MC
Sgal/17.9	18:00	DD	Sgal/17.4	18:40	MC
Sgal/17.95	18:56	DD	Sgal/17.5	20:19	MC
Sgal/17.66	20:00	DD	Sgal/17.81	21:12	AB
Sgal/17.6	21:04	MC	Sgal/17.35	22:34	MC
Sgal/17.7	22:02	MC	Sgal/17.55	23:19	MC
Sgal/17.7	23:06	DD	Sgal/17.5	01:20	S.B.
Sgal/17.5	00:08	A.T.	Sgal/18 sec	03:12	S.B.
Sgal/17.5	01:21	A.T.	Sgal/17.5	05:32	J.E.
Sgal/17.5	02:04	A.T.	Sgal/17.8	07:13	DRG
Sgal/17.5	03:12	A.T.	Sgal/17.83	07:32	DRG
Sgal/17.5	04:02	A.T.	Sgal/17.95	08:06	PCM
Sgal/17.5	05:08	A.T.	Sgal/17.87	08:55	DRG
Sgal/17.5	06:58	A.T.	Sgal/18.08	09:12	PCM
Sgal/17.5	2:30	DWD			

10/11/86

10-1386

10-12-86

**REI**



# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_ OF \_\_\_

PROJECT: \_\_\_\_\_

JOB NO.: \_\_\_\_\_

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

FLOW RATE	TIME (2400)	MONITOR'S INITIALS		FLOW RATE	TIME (2400)	MONITOR'S INITIALS
5 gal/17.70	10:32	PCM		5 gal/17.9 sec	10:15	DWD
5 gal/17.64	11:32	DRG	17.01	5 gal/17.5 sec	10:57	DWD
5 gal/17.44	11:50	PCM	17.20	5 gal/17.7 sec	11:09	DWD
5 gal/17.27	12:30	PCM	17.37	Pump turn off	11:10	DWD
5 gal/17.06	13:10	PCM	17.58			
5 gal/17.98	13:13	PCM	16.67			
5 gal/17.92	13:18	PCM	16.84			
5 gal/17.63	13:38	DRG	17.02			
5 gal/18.21	13:58	PCM	16.82			
5 gal/17.74	14:14	DRG	16.86			
5 gal/17.83	14:29	PCM	16.83			
5 gal/18.17	14:41	PCM	16.51			
5 gal/17.59	14:44	PCM	17.06			
5 gal/17.69	14:45	PCM	16.96			
5 gal/17.64	14:46	PCM	16.96			
5 gal/17.71	14:50	PCM	16.94			
5 gal/17.82	15:09	PCM	16.79			
5 gal/17.60	15:30	PCM				
5 gal/17	00:02	A-T				
5 gal/17	04:05	A-T				
5 gal/17	02:02	A-T				
5 gal/17	03:45	A-T				
5 gal/17	05:01	A-T				
5 gal/17	06:07	A-T				
5 gal/17.6 sec	7:07	DWD				
5 gal/17.5 sec	8:00	DWD				
5 gal/17.9 sec	9:00	DWD				

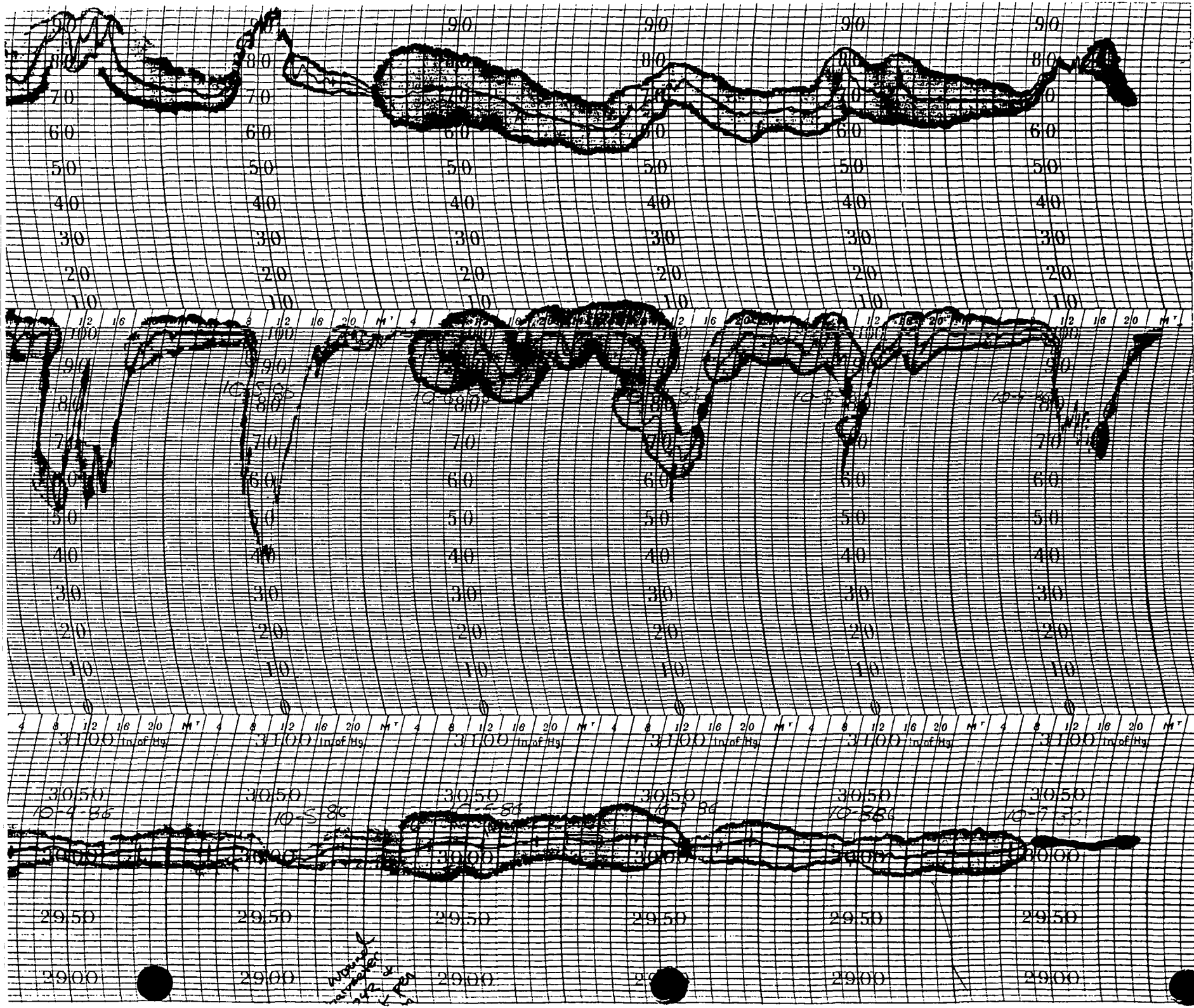
10-13-86

adj. rate  
sl. gate  
at 13:12

adj. rate  
at 14:42

10-14-86

IRPA



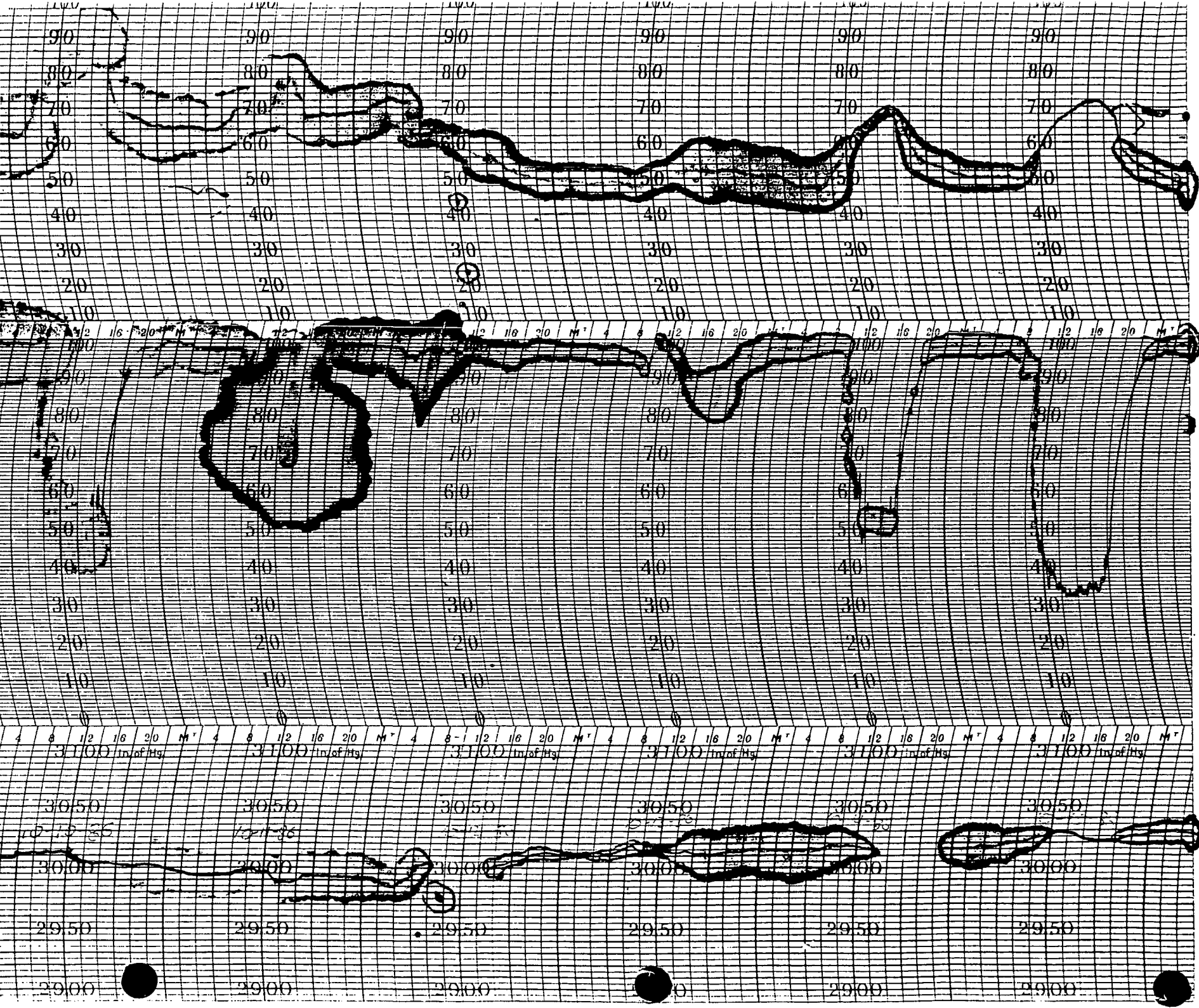
Pump Tact 10-2 Run#2

METEORO GRAPH  
DATE ON 10-3-86  
DATE OFF 2100

WEATHER MEASURE CORPORATION  
STATION FRENCH LTD

10-9-86

C701-W  
P/N 69



PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 10-1 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 10-1 INPUT 1  
 RADIUS: 0.166 FEET  
 START DATE : 07-Oct-86  
 START TIME : 09:00  
 WATER START LEVEL: 81.34 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
09:00	0.000	81.34	0.00	0.00E+00
09:00	0.017	81.73	-0.39	4.28E-04
09:00	0.034	85.94	-4.60	8.57E-04
09:00	0.050	88.12	-6.78	1.26E-03
09:00	0.067	90.19	-8.85	1.69E-03
09:00	0.084	90.69	-9.35	2.12E-03
09:00	0.100	90.69	-9.35	2.52E-03
09:00	0.117	91.89	-10.55	2.95E-03
09:00	0.134	92.38	-11.04	3.38E-03
09:00	0.150	92.11	-10.77	3.78E-03
09:00	0.167	91.99	-10.65	4.21E-03
09:00	0.257	93.98	-12.64	6.48E-03
09:00	0.340	94.35	-13.01	8.57E-03
09:00	0.424	95.47	-14.13	1.07E-02
09:00	0.507	96.37	-15.03	1.28E-02
09:00	0.590	97.33	-15.99	1.49E-02
09:00	0.674	97.97	-16.63	1.70E-02
09:00	0.757	98.77	-17.43	1.91E-02
09:00	0.840	99.24	-17.90	2.12E-02
09:00	0.924	99.48	-18.14	2.33E-02
09:01	1.007	100.16	-18.82	2.54E-02
09:01	1.414	102.16	-20.82	3.56E-02
09:01	1.748	103.14	-21.80	4.41E-02
09:02	2.081	103.76	-22.42	5.24E-02
09:02	2.414	104.27	-22.93	6.08E-02
09:02	2.748	104.83	-23.49	6.93E-02
09:03	3.081	105.07	-23.73	7.76E-02
09:03	3.415	105.47	-24.13	8.61E-02
09:03	3.748	105.65	-24.31	9.45E-02
09:04	4.081	105.97	-24.63	1.03E-01
09:04	4.414	106.12	-24.78	1.11E-01
09:04	4.748	106.19	-24.85	1.20E-01
09:05	5.081	106.32	-24.98	1.28E-01
09:05	5.414	106.38	-25.04	1.36E-01
09:05	5.748	106.46	-25.12	1.45E-01
09:06	6.081	106.47	-25.13	1.53E-01
09:06	6.415	106.47	-25.13	1.62E-01
09:06	6.748	106.66	-25.32	1.70E-01
09:07	7.081	106.66	-25.32	1.78E-01
09:07	7.415	106.79	-25.45	1.87E-01
09:07	7.748	106.88	-25.54	1.95E-01

09:09	8.081	106.89	-25.55	2.04E-01
09:08	8.415	106.90	-25.56	2.12E-01
09:08	8.748	107.03	-25.69	2.20E-01
09:09	9.081	107.09	-25.75	2.29E-01
09:09	9.414	107.23	-25.89	2.37E-01
09:09	9.748	107.10	-25.76	2.46E-01
09:10	10.081	107.25	-25.91	2.54E-01
09:12	12.108	107.38	-26.04	3.05E-01
09:14	14.152	108.13	-26.79	3.57E-01
09:16	16.152	108.23	-26.89	4.07E-01
09:18	18.152	108.46	-27.12	4.57E-01
09:20	20.152	108.58	-27.24	5.08E-01
09:22	22.152	108.66	-27.32	5.58E-01
09:24	24.152	108.86	-27.52	6.09E-01
09:26	26.152	108.94	-27.60	6.59E-01
09:28	28.215	109.09	-27.75	7.11E-01
09:30	30.197	109.37	-28.03	7.61E-01
09:32	32.197	109.45	-28.11	8.11E-01
09:34	34.197	109.71	-28.37	8.62E-01
09:36	36.197	109.67	-28.33	9.12E-01
09:38	38.197	109.95	-28.61	9.63E-01
09:40	40.197	110.14	-28.80	1.01E+00
09:42	42.197	110.14	-28.80	1.06E+00
09:44	44.197	110.28	-28.94	1.11E+00
09:46	46.197	110.48	-29.14	1.16E+00
09:48	48.197	110.55	-29.21	1.21E+00
09:50	50.197	110.68	-29.34	1.27E+00
09:52	52.197	110.79	-29.45	1.32E+00
09:54	54.197	111.15	-29.81	1.37E+00
09:56	56.217	111.25	-29.91	1.42E+00
09:58	58.100	111.38	-30.04	1.46E+00
10:00	60.245	111.57	-30.23	1.52E+00
10:02	62.245	111.64	-30.30	1.57E+00
10:04	64.245	111.60	-30.26	1.62E+00
10:06	66.245	111.48	-30.14	1.67E+00
10:08	68.245	111.62	-30.28	1.72E+00
10:10	70.245	111.74	-30.40	1.77E+00
10:12	72.245	111.77	-30.43	1.82E+00
10:14	74.245	111.71	-30.37	1.87E+00
10:16	76.245	111.87	-30.53	1.92E+00
10:18	78.245	111.87	-30.53	1.97E+00
10:20	80.245	111.81	-30.47	2.02E+00
10:22	82.245	111.78	-30.44	2.07E+00
10:24	84.245	111.82	-30.48	2.12E+00
10:26	86.245	111.88	-30.54	2.17E+00
10:28	88.245	111.82	-30.48	2.22E+00
10:30	90.245	111.84	-30.50	2.27E+00
10:32	92.245	111.84	-30.50	2.32E+00
10:34	94.245	111.92	-30.58	2.38E+00
10:36	96.245	111.98	-30.64	2.43E+00
10:38	98.245	112.05	-30.71	2.48E+00
11:00	120.210	112.14	-30.80	3.03E+00
11:20	140.210	111.99	-30.65	3.53E+00
11:40	160.210	112.18	-30.84	4.04E+00
12:00	180.220	112.45	-31.11	4.54E+00
12:20	200.220	112.64	-31.30	5.05E+00

12:40	220.220	111.57	-30.23	5.55E+00
13:00	240.220	111.64	-30.30	6.05E+00
13:20	260.220	111.02	-29.68	6.56E+00
13:40	280.230	110.68	-29.34	7.06E+00
14:00	300.230	111.42	-30.08	7.57E+00
14:20	320.230	109.88	-28.54	8.07E+00
14:40	340.180	109.24	-27.90	8.57E+00
15:00	360.100	109.74	-28.40	9.07E+00
15:20	380.100	109.58	-28.24	9.58E+00
15:40	400.100	109.41	-28.07	1.01E+01
16:00	420.170	109.37	-28.03	1.06E+01
16:20	440.250	109.19	-27.85	1.11E+01
16:40	460.200	109.15	-27.81	1.16E+01
17:00	480.170	108.99	-27.65	1.21E+01
17:20	500.170	109.64	-28.30	1.26E+01
17:40	520.130	109.59	-28.25	1.31E+01
18:00	540.120	110.47	-29.13	1.36E+01
18:20	560.220	114.26	-32.92	1.41E+01
18:40	580.080	115.83	-34.49	1.46E+01
19:00	600.220	115.83	-34.49	1.51E+01
19:20	620.230	116.13	-34.79	1.56E+01
19:40	640.220	116.20	-34.86	1.61E+01
20:00	660.220	116.17	-34.83	1.66E+01
20:20	680.130	116.29	-34.95	1.71E+01
20:40	700.120	116.23	-34.89	1.76E+01
21:00	720.230	116.37	-35.03	1.82E+01
21:20	740.300	116.73	-35.39	1.87E+01
21:40	760.230	116.67	-35.33	1.92E+01
22:00	780.230	116.71	-35.37	1.97E+01
22:20	800.230	116.91	-35.57	2.02E+01
22:40	820.180	116.96	-35.62	2.07E+01
23:00	840.570	117.03	-35.69	2.12E+01
23:20	860.180	117.13	-35.79	2.17E+01
23:40	880.080	117.17	-35.83	2.22E+01
00:00	900.170	117.20	-35.86	2.27E+01
00:20	920.170	117.34	-36.00	2.32E+01
00:40	940.170	117.40	-36.06	2.37E+01
01:00	960.170	117.47	-36.13	2.42E+01
01:20	980.170	117.43	-36.09	2.47E+01
01:40	1000.200	117.57	-36.23	2.52E+01
02:40	1060.300	117.72	-36.38	2.67E+01
03:40	1120.300	117.99	-36.65	2.82E+01
04:40	1180.300	118.20	-36.86	2.97E+01
05:40	1240.300	118.39	-37.05	3.13E+01
06:40	1300.300	118.19	-36.85	3.28E+01
07:40	1360.200	118.37	-37.03	3.43E+01
08:40	1420.200	118.14	-36.80	3.58E+01
09:40	1480.200	118.54	-37.20	3.73E+01
10:40	1540.200	118.46	-37.12	3.88E+01
11:40	1600.300	118.60	-37.26	4.03E+01
12:40	1660.300	118.80	-37.46	4.18E+01
13:40	1720.200	119.07	-37.73	4.34E+01
14:40	1780.300	119.33	-37.99	4.49E+01
15:40	1840.300	119.27	-37.93	4.64E+01
16:40	1900.300	119.29	-37.95	4.79E+01
17:40	1960.200	119.40	-38.06	4.94E+01

18:40	2020.200	119.60	-38.26	5.09E+01
19:40	2080.200	119.70	-38.36	5.24E+01
20:40	2140.200	119.80	-38.46	5.39E+01
21:40	2200.300	119.87	-38.53	5.55E+01
22:40	2260.300	120.07	-38.73	5.70E+01
23:40	2320.200	120.09	-38.75	5.85E+01
00:40	2380.200	120.30	-38.96	6.00E+01
01:40	2440.200	120.17	-38.83	6.15E+01
02:40	2500.200	120.52	-39.18	6.30E+01
03:40	2560.200	120.59	-39.25	6.45E+01
04:40	2620.200	120.56	-39.22	6.60E+01
05:40	2680.200	120.69	-39.35	6.75E+01
06:40	2740.200	120.83	-39.49	6.91E+01
07:40	2800.200	120.85	-39.51	7.06E+01
08:40	2860.300	121.82	-40.48	7.21E+01
09:40	2920.300	121.76	-40.42	7.36E+01
10:40	2980.300	121.85	-40.51	7.51E+01
11:40	3040.200	121.89	-40.55	7.66E+01
12:40	3100.200	121.90	-40.56	7.81E+01
13:40	3160.300	121.95	-40.61	7.96E+01
14:40	3220.300	122.02	-40.68	8.12E+01
15:40	3280.200	122.05	-40.71	8.27E+01
16:40	3340.200	122.25	-40.91	8.42E+01
17:40	3400.300	122.16	-40.82	8.57E+01
18:40	3460.300	122.43	-41.09	8.72E+01
19:40	3520.300	122.39	-41.05	8.87E+01
20:40	3580.200	122.42	-41.08	9.02E+01
21:40	3640.200	122.55	-41.21	9.17E+01
22:40	3700.200	122.52	-41.18	9.32E+01
23:40	3760.200	122.68	-41.34	9.48E+01
00:40	3820.200	122.73	-41.39	9.63E+01
01:40	3880.200	122.88	-41.54	9.78E+01
02:40	3940.200	122.96	-41.62	9.93E+01
03:40	4000.200	122.93	-41.59	1.01E+02
04:40	4060.200	123.05	-41.71	1.02E+02
05:40	4120.200	124.06	-42.72	1.04E+02
06:40	4180.200	123.35	-42.01	1.05E+02
07:40	4240.300	123.35	-42.01	1.07E+02
08:40	4300.300	123.25	-41.91	1.08E+02
09:40	4360.700	123.33	-41.99	1.10E+02
10:40	4420.300	123.19	-41.85	1.11E+02
11:40	4480.300	123.21	-41.87	1.13E+02
12:40	4540.300	123.86	-42.52	1.14E+02
13:40	4600.300	123.93	-42.59	1.16E+02
14:40	4660.300	123.85	-42.51	1.17E+02
15:40	4720.300	123.91	-42.57	1.19E+02
16:40	4780.300	123.93	-42.59	1.20E+02
17:40	4840.300	121.68	-40.34	1.22E+02
18:40	4900.300	123.21	-41.87	1.23E+02
19:40	4960.300	123.29	-41.95	1.25E+02
20:40	5020.300	123.43	-42.09	1.27E+02
21:40	5080.300	123.35	-42.01	1.28E+02
22:40	5140.300	123.42	-42.08	1.30E+02
23:40	5200.300	123.46	-42.12	1.31E+02
00:40	5260.300	123.55	-42.21	1.33E+02
01:40	5320.300	123.59	-42.25	1.34E+02

02:40	5380.300	123.59	-42.25	1.36E+02
03:40	5440.300	123.66	-42.32	1.37E+02
04:40	5500.300	123.72	-42.38	1.39E+02
05:40	5560.300	123.76	-42.42	1.40E+02
06:40	5620.300	123.78	-42.44	1.42E+02
07:40	5680.300	123.79	-42.45	1.43E+02
08:40	5740.300	123.92	-42.58	1.45E+02
09:40	5800.300	123.86	-42.52	1.46E+02
10:40	5860.300	123.92	-42.58	1.48E+02
11:40	5920.300	123.92	-42.58	1.49E+02
12:40	5980.300	123.89	-42.55	1.51E+02
13:40	6040.300	123.88	-42.54	1.52E+02
14:40	6100.300	123.99	-42.65	1.54E+02
15:40	6160.500	123.89	-42.55	1.55E+02
16:40	6220.300	124.02	-42.68	1.57E+02
17:40	6280.300	124.05	-42.71	1.58E+02
18:40	6340.300	124.12	-42.78	1.60E+02
19:40	6400.400	124.18	-42.84	1.61E+02
20:40	6460.200	124.21	-42.87	1.63E+02
21:40	6520.200	124.16	-42.82	1.64E+02
22:40	6580.300	124.31	-42.97	1.66E+02
23:40	6640.300	124.34	-43.00	1.67E+02
00:40	6700.300	124.29	-42.95	1.69E+02
01:40	6760.300	124.36	-43.02	1.70E+02
02:40	6820.300	124.36	-43.02	1.72E+02
03:40	6880.300	124.39	-43.05	1.73E+02
04:40	6940.300	124.39	-43.05	1.75E+02
05:40	7000.300	124.49	-43.15	1.76E+02
06:40	7060.300	124.58	-43.24	1.78E+02
07:40	7120.300	124.71	-43.37	1.79E+02
08:40	7180.300	124.18	-42.84	1.81E+02
09:40	7240.300	124.21	-42.87	1.82E+02
10:40	7300.300	124.65	-43.31	1.84E+02
11:40	7360.300	124.64	-43.30	1.85E+02
12:40	7420.300	124.58	-43.24	1.87E+02
13:40	7480.300	124.55	-43.21	1.89E+02
14:40	7540.300	124.58	-43.24	1.90E+02
15:40	7600.300	124.51	-43.17	1.92E+02
16:40	7660.300	124.53	-43.19	1.93E+02
17:40	7720.300	124.52	-43.18	1.95E+02
18:40	7780.200	124.56	-43.22	1.96E+02
19:40	7840.200	124.62	-43.28	1.98E+02
20:40	7900.300	124.73	-43.39	1.99E+02
21:40	7960.300	124.78	-43.44	2.01E+02
22:40	8020.300	124.68	-43.34	2.02E+02
23:40	8080.300	124.84	-43.50	2.04E+02
00:40	8140.300	124.96	-43.62	2.05E+02
01:40	8200.300	125.06	-43.72	2.07E+02
02:40	8260.300	125.12	-43.78	2.08E+02
03:40	8320.300	125.03	-43.69	2.10E+02
04:40	8380.300	124.94	-43.60	2.11E+02
05:40	8440.300	125.12	-43.78	2.13E+02
06:40	8500.300	125.18	-43.84	2.14E+02
07:40	8560.200	124.98	-43.64	2.16E+02
08:40	8620.300	125.02	-43.68	2.17E+02
09:00	8640.600	125.08	-43.74	2.18E+02



PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : REI 10-1 INPUT 1  
RADIUS: 0.166 FEET  
START DATE : 13-Oct-86  
START TIME : 10:25  
WATER START LEVEL: 81.34 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
10:25	8725.000	124.97	-43.63	2.20E+02
10:35	8735.071	124.81	-43.47	2.20E+02
10:45	8745.070	124.96	-43.62	2.20E+02
10:55	8755.072	125.08	-43.74	2.21E+02
11:05	8765.072	125.11	-43.77	2.21E+02
11:15	8775.072	125.00	-43.66	2.21E+02
11:25	8785.072	124.90	-43.56	2.21E+02
11:35	8795.072	124.88	-43.54	2.22E+02
11:45	8805.072	125.07	-43.73	2.22E+02
11:55	8815.102	125.08	-43.74	2.22E+02
12:05	8825.090	124.87	-43.53	2.22E+02
12:15	8835.090	124.98	-43.64	2.23E+02
12:25	8845.090	122.30	-40.96	2.23E+02
12:35	8855.090	125.46	-44.12	2.23E+02
12:45	8865.090	125.54	-44.20	2.23E+02
12:55	8875.120	125.64	-44.30	2.24E+02
13:04	8884.970	125.57	-44.23	2.24E+02
13:14	8894.970	124.76	-43.42	2.24E+02
13:25	8904.970	124.51	-43.17	2.24E+02
13:34	8914.970	124.57	-43.23	2.25E+02
13:45	8924.970	124.48	-43.14	2.25E+02
13:54	8934.970	124.40	-43.06	2.25E+02
14:05	8944.970	124.41	-43.07	2.25E+02
14:14	8955.020	124.44	-43.10	2.26E+02
14:25	8965.080	124.53	-43.19	2.26E+02
14:35	8975.080	124.53	-43.19	2.26E+02
14:45	8985.080	125.63	-44.29	2.26E+02
14:55	8995.080	125.69	-44.35	2.27E+02
15:05	9005.080	125.79	-44.45	2.27E+02
15:15	9015.080	125.38	-44.04	2.27E+02
15:25	9025.080	125.40	-44.06	2.27E+02
15:35	9035.080	125.43	-44.09	2.28E+02
15:45	9045.080	125.41	-44.07	2.28E+02
15:55	9055.080	125.31	-43.97	2.28E+02
16:04	9065.020	125.41	-44.07	2.28E+02
16:15	9075.020	125.47	-44.13	2.29E+02
16:25	9084.970	125.77	-44.43	2.29E+02
16:35	9095.080	125.83	-44.49	2.29E+02
16:45	9105.080	125.73	-44.39	2.29E+02
16:55	9115.080	125.79	-44.45	2.30E+02

## ADJUSTED DATA

17:05	9125.080	125.69	-44.35	2.30E+02
17:15	9135.080	125.86	-44.52	2.30E+02
17:25	9145.080	125.74	-44.40	2.30E+02
17:35	9155.080	125.73	-44.39	2.31E+02
17:45	9165.080	125.80	-44.46	2.31E+02
17:55	9175.080	125.87	-44.53	2.31E+02
18:05	9185.080	125.74	-44.40	2.31E+02
18:15	9195.080	125.69	-44.35	2.32E+02
18:25	9205.080	123.61	-42.27	2.32E+02
18:35	9215.080	125.67	-44.33	2.32E+02
18:45	9225.080	125.51	-44.17	2.32E+02
18:55	9235.080	125.44	-44.10	2.33E+02
19:05	9245.080	125.64	-44.30	2.33E+02
19:15	9255.080	125.43	-44.09	2.33E+02
19:25	9265.080	125.58	-44.24	2.33E+02
19:35	9275.070	125.57	-44.23	2.34E+02
19:45	9285.080	125.47	-44.13	2.34E+02
19:55	9295.080	125.63	-44.29	2.34E+02
20:05	9305.080	125.48	-44.14	2.34E+02
20:15	9315.080	125.57	-44.23	2.35E+02
20:25	9325.080	125.66	-44.32	2.35E+02
20:35	9335.080	125.70	-44.36	2.35E+02
20:45	9345.080	125.61	-44.27	2.36E+02
20:55	9355.080	125.58	-44.24	2.36E+02
21:05	9365.080	125.48	-44.14	2.36E+02
21:15	9375.080	125.50	-44.16	2.36E+02
21:25	9385.080	125.46	-44.12	2.37E+02
21:35	9395.080	125.69	-44.35	2.37E+02
21:45	9405.080	125.70	-44.36	2.37E+02
21:55	9415.080	125.67	-44.33	2.37E+02
22:05	9425.080	125.74	-44.40	2.38E+02
22:15	9435.080	125.71	-44.37	2.38E+02
22:25	9445.080	125.76	-44.42	2.38E+02
22:35	9455.080	125.73	-44.39	2.38E+02
22:45	9465.080	125.80	-44.46	2.39E+02
22:54	9475.020	125.76	-44.42	2.39E+02
23:05	9485.020	125.69	-44.35	2.39E+02
23:14	9495.020	125.83	-44.49	2.39E+02
23:25	9505.020	125.93	-44.59	2.40E+02
23:34	9515.020	125.83	-44.49	2.40E+02
23:45	9525.020	125.84	-44.50	2.40E+02
23:55	9535.020	125.81	-44.47	2.40E+02
00:05	9545.020	125.84	-44.50	2.41E+02
00:15	9555.020	125.86	-44.52	2.41E+02
00:25	9565.030	125.89	-44.55	2.41E+02
00:35	9575.030	125.86	-44.52	2.41E+02
00:44	9585.030	125.90	-44.56	2.42E+02
00:55	9595.030	125.87	-44.53	2.42E+02
01:04	9605.030	125.87	-44.53	2.42E+02
01:15	9615.030	125.93	-44.59	2.42E+02
01:25	9625.030	125.93	-44.59	2.43E+02
01:35	9635.030	125.96	-44.62	2.43E+02
01:45	9645.030	125.93	-44.59	2.43E+02
01:55	9655.030	125.93	-44.59	2.43E+02
02:05	9665.030	126.01	-44.67	2.44E+02
02:14	9675.030	125.94	-44.60	2.44E+02

## ADJUSTED DATA

02:25	9685.030	125.94	-44.60	2.44E+02
02:34	9695.030	125.91	-44.57	2.44E+02
02:45	9705.030	125.89	-44.55	2.45E+02
02:55	9715.030	125.91	-44.57	2.45E+02
03:04	9725.000	125.91	-44.57	2.45E+02
03:15	9735.000	125.96	-44.62	2.45E+02
03:24	9745.000	125.99	-44.65	2.46E+02
03:35	9755.100	125.93	-44.59	2.46E+02
03:44	9765.000	125.97	-44.63	2.46E+02
03:55	9775.000	125.97	-44.63	2.46E+02
04:04	9785.000	126.01	-44.67	2.47E+02
04:15	9795.000	125.67	-44.33	2.47E+02
04:25	9805.000	125.79	-44.45	2.47E+02
04:34	9815.000	125.74	-44.40	2.47E+02
04:45	9825.000	125.51	-44.17	2.48E+02
04:54	9835.000	125.54	-44.20	2.48E+02
05:05	9845.000	125.71	-44.37	2.48E+02
05:14	9855.000	125.66	-44.32	2.48E+02
05:25	9865.000	126.07	-44.73	2.49E+02
05:34	9875.000	126.07	-44.73	2.49E+02
05:45	9885.000	126.07	-44.73	2.49E+02
05:55	9895.000	126.10	-44.76	2.49E+02
06:04	9905.000	126.09	-44.75	2.50E+02
06:15	9915.000	125.71	-44.37	2.50E+02
06:24	9925.000	125.73	-44.39	2.50E+02
06:35	9935.000	125.84	-44.50	2.50E+02
06:44	9945.000	126.06	-44.72	2.51E+02
06:55	9955.000	126.04	-44.70	2.51E+02
07:05	9965.100	126.07	-44.73	2.51E+02
07:15	9975.100	126.00	-44.66	2.51E+02
07:25	9985.100	126.01	-44.67	2.52E+02
07:35	9995.100	126.00	-44.66	2.52E+02
07:45	10005.100	126.01	-44.67	2.52E+02
07:55	10015.100	126.04	-44.70	2.52E+02
08:05	10025.100	126.14	-44.80	2.53E+02
08:15	10035.100	126.10	-44.76	2.53E+02
08:25	10045.100	126.16	-44.82	2.53E+02
08:35	10055.100	126.16	-44.82	2.53E+02
08:45	10065.100	126.10	-44.76	2.54E+02
08:55	10075.000	126.07	-44.73	2.54E+02
09:04	10085.000	126.11	-44.77	2.54E+02
09:15	10095.000	126.16	-44.82	2.54E+02
09:24	10105.000	126.17	-44.83	2.55E+02
09:28	10108.200	126.17	-44.83	2.55E+02

TEST NAME: REI 10-1 RUN # 2  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 10-1 INPUT 1  
 RADIUS: 0.166 FEET  
 START DATE: 07-Oct-86  
 START TIME: 11:10  
 WATER START LEVEL: 81.34 FEET  
 WATER STOP LEVEL: 127.32 FEET  
 TOTAL PUMPING TIME: 10210.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)	t/r2	t/t
11:10	0.017	124.36	2.96	43.02	4.28E-04	6.01E+05
11:10	0.034	123.90	3.42	42.56	8.57E-04	3.00E+05
11:10	0.050	123.43	3.89	42.09	1.26E-03	2.04E+05
11:10	0.067	122.99	4.33	41.65	1.69E-03	1.52E+05
11:10	0.084	122.53	4.79	41.19	2.12E-03	1.22E+05
11:10	0.100	122.10	5.22	40.76	2.52E-03	1.02E+05
11:10	0.117	121.66	5.66	40.32	2.95E-03	8.73E+04
11:10	0.134	121.23	6.09	39.89	3.38E-03	7.62E+04
11:10	0.150	120.81	6.51	39.47	3.78E-03	6.81E+04
11:10	0.167	120.41	6.91	39.07	4.21E-03	6.11E+04
11:10	0.257	118.31	9.01	36.97	6.48E-03	3.97E+04
11:10	0.341	116.53	10.79	35.19	8.59E-03	2.99E+04
11:10	0.424	114.88	12.44	33.54	1.07E-02	2.41E+04
11:10	0.507	113.35	13.97	32.01	1.28E-02	2.01E+04
11:10	0.591	111.94	15.38	30.60	1.49E-02	1.73E+04
11:10	0.674	110.65	16.67	29.31	1.70E-02	1.52E+04
11:10	0.757	109.46	17.86	28.12	1.91E-02	1.35E+04
11:10	0.841	108.37	18.95	27.03	2.12E-02	1.21E+04
11:10	0.924	107.39	19.93	26.05	2.33E-02	1.11E+04
11:11	1.007	106.47	20.85	25.13	2.54E-02	1.01E+04
11:11	1.413	103.07	24.25	21.73	3.56E-02	7.23E+03
11:11	1.747	101.21	26.11	19.87	4.40E-02	5.85E+03
11:12	2.080	99.97	27.35	18.63	5.24E-02	4.91E+03
11:12	2.413	99.11	28.21	17.77	6.08E-02	4.23E+03
11:12	2.747	98.52	28.80	17.18	6.92E-02	3.72E+03
11:13	3.080	98.10	29.22	16.76	7.76E-02	3.32E+03
11:13	3.413	97.80	29.52	16.46	8.60E-02	2.99E+03
11:13	3.747	97.56	29.76	16.22	9.44E-02	2.73E+03
11:14	4.080	97.39	29.93	16.05	1.03E-01	2.50E+03
11:14	4.413	97.25	30.07	15.91	1.11E-01	2.31E+03
11:14	4.747	97.14	30.18	15.80	1.20E-01	2.15E+03
11:15	5.080	97.04	30.28	15.70	1.28E-01	2.01E+03
11:15	5.413	96.96	30.36	15.62	1.36E-01	1.89E+03
11:15	5.747	96.88	30.44	15.54	1.45E-01	1.78E+03
11:16	6.080	96.82	30.50	15.48	1.53E-01	1.68E+03
11:16	6.413	96.75	30.57	15.41	1.62E-01	1.59E+03
11:16	6.747	96.71	30.61	15.37	1.70E-01	1.51E+03
11:17	7.080	96.65	30.67	15.31	1.78E-01	1.44E+03
11:17	7.413	96.61	30.71	15.27	1.87E-01	1.38E+03
11:17	7.747	96.56	30.76	15.22	1.95E-01	1.32E+03
11:18	8.080	96.52	30.80	15.18	2.04E-01	1.26E+03
11:18	8.413	96.48	30.84	15.14	2.12E-01	1.21E+03

11:18	8.747	96.44	30.88	15.10	2.20E-01	1.17E+03
11:19	9.080	96.41	30.91	15.07	2.29E-01	1.13E+03
11:19	9.413	96.38	30.94	15.04	2.37E-01	1.09E+03
11:19	9.747	96.34	30.98	15.00	2.46E-01	1.05E+03
11:20	10.080	96.31	31.01	14.97	2.54E-01	1.01E+03
11:22	12.115	96.14	31.18	14.80	3.05E-01	8.44E+02
11:24	14.115	95.99	31.33	14.65	3.56E-01	7.24E+02
11:26	16.115	95.88	31.44	14.54	4.06E-01	6.35E+02
11:28	18.115	95.76	31.56	14.42	4.57E-01	5.65E+02
11:30	20.115	95.68	31.64	14.34	5.07E-01	5.09E+02
11:32	22.115	95.59	31.73	14.25	5.57E-01	4.63E+02
11:34	24.115	95.52	31.80	14.18	6.08E-01	4.24E+02
11:36	26.115	95.45	31.87	14.11	6.58E-01	3.92E+02
11:38	28.115	95.38	31.94	14.04	7.09E-01	3.64E+02
11:40	30.115	95.32	32.00	13.98	7.59E-01	3.40E+02
11:42	32.115	95.26	32.06	13.92	8.09E-01	3.19E+02
11:44	34.115	95.21	32.11	13.87	8.60E-01	3.00E+02
11:46	36.115	95.15	32.17	13.81	9.10E-01	2.84E+02
11:48	38.115	95.11	32.21	13.77	9.61E-01	2.69E+02
11:50	40.115	95.06	32.26	13.72	1.01E+00	2.56E+02
11:52	42.115	95.01	32.31	13.67	1.06E+00	2.43E+02
11:54	44.115	94.96	32.36	13.62	1.11E+00	2.32E+02
11:56	46.115	94.94	32.38	13.60	1.16E+00	2.22E+02
11:58	48.115	94.88	32.44	13.54	1.21E+00	2.13E+02
12:00	50.115	94.83	32.49	13.49	1.26E+00	2.05E+02
12:02	52.115	94.81	32.51	13.47	1.31E+00	1.97E+02
12:04	54.115	94.76	32.56	13.42	1.36E+00	1.90E+02
12:06	56.115	94.73	32.59	13.39	1.41E+00	1.83E+02
12:08	58.115	94.71	32.61	13.37	1.46E+00	1.77E+02
12:10	60.115	94.66	32.66	13.32	1.51E+00	1.71E+02
12:12	62.102	94.64	32.68	13.30	1.57E+00	1.65E+02
12:14	64.492	94.59	32.73	13.25	1.63E+00	1.59E+02
12:16	66.188	94.56	32.76	13.22	1.67E+00	1.55E+02
12:18	68.188	94.53	32.79	13.19	1.72E+00	1.51E+02
12:20	70.188	94.51	32.81	13.17	1.77E+00	1.46E+02
12:22	72.188	94.48	32.84	13.14	1.82E+00	1.42E+02
12:24	74.188	94.45	32.87	13.11	1.87E+00	1.39E+02
12:26	76.188	94.42	32.90	13.08	1.92E+00	1.35E+02
12:28	78.188	94.39	32.93	13.05	1.97E+00	1.32E+02
12:30	80.188	94.36	32.96	13.02	2.02E+00	1.28E+02
12:32	82.188	94.33	32.99	12.99	2.07E+00	1.25E+02
12:34	84.188	94.31	33.01	12.97	2.12E+00	1.22E+02
12:36	86.188	94.28	33.04	12.94	2.17E+00	1.19E+02
12:38	88.188	94.26	33.06	12.92	2.22E+00	1.17E+02
12:40	90.188	94.22	33.10	12.88	2.27E+00	1.14E+02
12:42	92.188	94.21	33.11	12.87	2.32E+00	1.12E+02
12:44	94.188	94.18	33.14	12.84	2.37E+00	1.09E+02
12:46	96.188	94.15	33.17	12.81	2.42E+00	1.07E+02
12:48	98.188	94.12	33.20	12.78	2.47E+00	1.05E+02
13:10	120.110	93.88	33.44	12.54	3.03E+00	8.60E+01
13:30	140.110	93.66	33.66	12.32	3.53E+00	7.39E+01
13:50	160.120	93.49	33.83	12.15	4.04E+00	6.48E+01
14:10	180.120	93.32	34.00	11.98	4.54E+00	5.77E+01
14:30	200.120	93.15	34.17	11.81	5.04E+00	5.20E+01
14:50	220.120	92.99	34.33	11.65	5.55E+00	4.74E+01
15:10	240.120	92.85	34.47	11.51	6.05E+00	4.35E+01

15:30	260.120	92.73	34.59	11.39	6.56E+00	4.03E+01
15:50	280.120	92.59	34.73	11.25	7.06E+00	3.75E+01
16:10	300.120	92.48	34.84	11.14	7.56E+00	3.50E+01
16:30	320.050	92.36	34.96	11.02	8.07E+00	3.29E+01
16:49	340.050	92.25	35.07	10.91	8.57E+00	3.10E+01
17:10	360.050	92.15	35.17	10.81	9.07E+00	2.94E+01
17:30	380.050	92.05	35.27	10.71	9.58E+00	2.79E+01
17:50	400.050	91.95	35.37	10.61	1.01E+01	2.65E+01
18:10	420.050	91.85	35.47	10.51	1.06E+01	2.53E+01
18:30	440.050	91.76	35.56	10.42	1.11E+01	2.42E+01
18:50	460.050	91.68	35.64	10.34	1.16E+01	2.32E+01
19:10	480.050	91.59	35.73	10.25	1.21E+01	2.23E+01
19:30	500.050	91.52	35.80	10.18	1.26E+01	2.14E+01
19:49	520.050	91.43	35.89	10.09	1.31E+01	2.06E+01
20:10	540.050	91.36	35.96	10.02	1.36E+01	1.99E+01
20:30	560.050	91.29	36.03	9.95	1.41E+01	1.92E+01
20:50	580.050	91.22	36.10	9.88	1.46E+01	1.86E+01
21:10	600.050	91.15	36.17	9.81	1.51E+01	1.80E+01
21:30	620.050	91.07	36.25	9.73	1.56E+01	1.75E+01
21:50	640.050	91.00	36.32	9.66	1.61E+01	1.70E+01
22:10	660.050	90.93	36.39	9.59	1.66E+01	1.65E+01
22:30	680.050	90.87	36.45	9.53	1.71E+01	1.60E+01
22:49	700.050	90.82	36.50	9.48	1.76E+01	1.56E+01
23:10	720.050	90.76	36.56	9.42	1.81E+01	1.52E+01
23:30	740.050	90.70	36.62	9.36	1.87E+01	1.48E+01
23:50	760.100	90.63	36.69	9.29	1.92E+01	1.44E+01
00:10	780.100	90.59	36.73	9.25	1.97E+01	1.41E+01
00:30	800.100	90.53	36.79	9.19	2.02E+01	1.38E+01
00:50	820.100	90.46	36.86	9.12	2.07E+01	1.35E+01
01:10	840.100	90.40	36.92	9.06	2.12E+01	1.32E+01
01:30	860.100	90.36	36.96	9.02	2.17E+01	1.29E+01
01:50	880.100	90.30	37.02	8.96	2.22E+01	1.26E+01
02:10	900.100	90.25	37.07	8.91	2.27E+01	1.23E+01
02:30	920.100	90.20	37.12	8.86	2.32E+01	1.21E+01
02:50	940.100	90.14	37.18	8.80	2.37E+01	1.19E+01
03:10	960.100	90.10	37.22	8.76	2.42E+01	1.16E+01
03:30	980.100	90.04	37.28	8.70	2.47E+01	1.14E+01
03:50	1000.100	90.00	37.32	8.66	2.52E+01	1.12E+01
04:50	1060.300	89.86	37.46	8.52	2.67E+01	1.06E+01
05:50	1120.300	89.71	37.61	8.37	2.82E+01	1.01E+01
06:50	1180.300	89.59	37.73	8.25	2.97E+01	9.65E+00
07:50	1240.300	89.46	37.86	8.12	3.13E+01	9.23E+00
08:50	1300.300	89.34	37.98	8.00	3.28E+01	8.85E+00
09:50	1360.300	89.24	38.08	7.90	3.43E+01	8.51E+00
10:50	1420.300	89.13	38.19	7.79	3.58E+01	8.19E+00
11:50	1480.300	89.03	38.29	7.69	3.73E+01	7.90E+00
12:50	1540.300	88.91	38.41	7.57	3.88E+01	7.63E+00
13:50	1600.300	88.82	38.50	7.48	4.03E+01	7.38E+00
14:50	1660.300	88.71	38.61	7.37	4.18E+01	7.15E+00
15:50	1720.100	88.61	38.71	7.27	4.33E+01	6.94E+00
16:50	1780.100	88.53	38.79	7.19	4.49E+01	6.74E+00
17:50	1840.100	88.43	38.89	7.09	4.64E+01	6.55E+00
18:50	1900.100	88.34	38.98	7.00	4.79E+01	6.37E+00
19:50	1960.100	88.24	39.08	6.90	4.94E+01	6.21E+00
20:50	2020.100	88.17	39.15	6.83	5.09E+01	6.05E+00
21:50	2080.100	88.09	39.23	6.75	5.24E+01	5.91E+00

22:50	2140.100	88.01	39.31	6.67	5.39E+01	5.77E+00
23:50	2200.100	87.93	39.39	6.59	5.54E+01	5.64E+00
00:50	2260.100	87.86	39.46	6.52	5.70E+01	5.52E+00
01:50	2320.100	87.78	39.54	6.44	5.85E+01	5.40E+00
02:50	2380.100	87.71	39.61	6.37	6.00E+01	5.29E+00
03:50	2440.100	87.63	39.69	6.29	6.15E+01	5.18E+00
04:50	2500.100	87.56	39.76	6.22	6.30E+01	5.08E+00
05:50	2560.100	87.50	39.82	6.16	6.45E+01	4.99E+00
06:50	2620.100	87.43	39.89	6.09	6.60E+01	4.90E+00
07:50	2680.100	87.37	39.95	6.03	6.75E+01	4.81E+00
08:50	2740.200	87.30	40.02	5.96	6.91E+01	4.73E+00
09:50	2800.200	87.24	40.08	5.90	7.06E+01	4.65E+00
10:50	2860.200	87.18	40.14	5.84	7.21E+01	4.57E+00
11:50	2920.100	87.13	40.19	5.79	7.36E+01	4.50E+00
12:50	2980.200	87.07	40.25	5.73	7.51E+01	4.43E+00
13:50	3040.200	87.00	40.32	5.66	7.66E+01	4.36E+00
14:50	3100.200	86.94	40.38	5.60	7.81E+01	4.29E+00
15:50	3160.200	86.88	40.44	5.54	7.96E+01	4.23E+00
16:50	3220.200	86.83	40.49	5.49	8.12E+01	4.17E+00
17:50	3280.200	86.77	40.55	5.43	8.27E+01	4.11E+00
18:50	3340.200	86.71	40.61	5.37	8.42E+01	4.06E+00
19:50	3400.200	86.67	40.65	5.33	8.57E+01	4.00E+00
20:50	3460.200	86.61	40.71	5.27	8.72E+01	3.95E+00
21:50	3520.200	86.57	40.75	5.23	8.87E+01	3.90E+00
22:50	3580.200	86.53	40.79	5.19	9.02E+01	3.85E+00
23:50	3640.200	86.47	40.85	5.13	9.17E+01	3.80E+00
00:50	3700.200	86.43	40.89	5.09	9.32E+01	3.76E+00
01:50	3760.200	86.38	40.94	5.04	9.48E+01	3.72E+00
02:50	3820.200	86.33	40.99	4.99	9.63E+01	3.67E+00
03:50	3880.200	86.28	41.04	4.94	9.78E+01	3.63E+00
04:50	3940.200	86.23	41.09	4.89	9.93E+01	3.59E+00
05:50	4000.200	86.18	41.14	4.84	1.01E+02	3.55E+00
06:50	4060.200	86.14	41.18	4.80	1.02E+02	3.51E+00
07:50	4120.200	86.10	41.22	4.76	1.04E+02	3.48E+00
08:50	4180.200	86.05	41.27	4.71	1.05E+02	3.44E+00
09:50	4240.200	86.03	41.29	4.69	1.07E+02	3.41E+00
10:50	4300.200	85.98	41.34	4.64	1.08E+02	3.37E+00
11:04	4314.800	85.97	41.35	4.63	1.09E+02	3.37E+00

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 10-1 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 11 INPUT 2  
 RADIUS: 427.782 FEET  
 START DATE : 07-Oct-86  
 START TIME : 09:00  
 WATER START LEVEL: 78.42 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
09:00	0.000	78.42	0.00	0.00E+00
09:00	0.017	-99.99	178.41	6.45E-11
09:00	0.034	-99.99	178.41	1.29E-10
09:00	0.050	-99.99	178.41	1.90E-10
09:00	0.067	-99.99	178.41	2.54E-10
09:00	0.084	-99.99	178.41	3.19E-10
09:00	0.100	-99.99	178.41	3.79E-10
09:00	0.117	-99.99	178.41	4.44E-10
09:00	0.134	-99.99	178.41	5.09E-10
09:00	0.150	-99.99	178.41	5.69E-10
09:00	0.167	-99.99	178.41	6.34E-10
09:00	0.257	78.42	0.00	9.75E-10
09:00	0.340	78.42	0.00	1.29E-09
09:00	0.424	78.42	0.00	1.61E-09
09:00	0.507	78.42	0.00	1.92E-09
09:00	0.590	78.42	0.00	2.24E-09
09:00	0.674	78.42	0.00	2.56E-09
09:00	0.757	78.42	0.00	2.87E-09
09:00	0.840	78.42	0.00	3.19E-09
09:00	0.924	78.42	0.00	3.51E-09
09:01	1.007	78.42	0.00	3.82E-09
09:01	1.414	78.42	0.00	5.37E-09
09:01	1.748	78.42	0.00	6.63E-09
09:02	2.081	78.42	0.00	7.90E-09
09:02	2.414	78.42	0.00	9.16E-09
09:02	2.748	78.42	0.00	1.04E-08
09:03	3.081	78.42	0.00	1.17E-08
09:03	3.415	78.42	0.00	1.30E-08
09:03	3.748	78.42	0.00	1.42E-08
09:04	4.081	78.42	0.00	1.55E-08
09:04	4.414	78.42	0.00	1.68E-08
09:04	4.748	78.42	0.00	1.80E-08
09:05	5.081	78.42	0.00	1.93E-08
09:05	5.414	78.42	0.00	2.05E-08
09:05	5.748	78.42	0.00	2.18E-08
09:06	6.081	78.42	0.00	2.31E-08
09:06	6.415	78.42	0.00	2.43E-08
09:06	6.748	78.43	-0.01	2.56E-08
09:07	7.081	78.43	-0.01	2.69E-08
09:07	7.415	78.43	-0.01	2.81E-08
09:07	7.748	78.43	-0.01	2.94E-08



09:08	8.081	78.43	-0.01	3.07E-08
09:09	8.415	78.43	-0.01	3.19E-08
09:08	8.748	78.43	-0.01	3.32E-08
09:09	9.081	78.43	-0.01	3.45E-08
09:09	9.414	78.43	-0.01	3.57E-08
09:09	9.748	78.43	-0.01	3.70E-08
09:10	10.081	78.43	-0.01	3.83E-08
09:12	12.108	78.44	-0.02	4.59E-08
09:14	14.152	78.44	-0.02	5.37E-08
09:16	16.152	78.46	-0.04	6.13E-08
09:18	18.152	78.47	-0.05	6.89E-08
09:20	20.152	78.49	-0.07	7.65E-08
09:22	22.152	78.50	-0.08	8.41E-08
09:24	24.152	78.52	-0.10	9.17E-08
09:26	26.152	78.54	-0.12	9.92E-08
09:28	28.215	78.57	-0.15	1.07E-07
09:30	30.197	78.59	-0.17	1.15E-07
09:32	32.197	78.61	-0.19	1.22E-07
09:34	34.197	78.64	-0.22	1.30E-07
09:36	36.197	78.66	-0.24	1.37E-07
09:38	38.197	78.69	-0.27	1.45E-07
09:40	40.197	78.71	-0.29	1.53E-07
09:42	42.197	78.73	-0.31	1.60E-07
09:44	44.197	78.76	-0.34	1.68E-07
09:46	46.197	78.78	-0.36	1.75E-07
09:48	48.197	78.81	-0.39	1.83E-07
09:50	50.197	78.83	-0.41	1.90E-07
09:52	52.197	78.86	-0.44	1.98E-07
09:54	54.197	78.88	-0.46	2.06E-07
09:56	56.217	78.91	-0.49	2.13E-07
09:58	58.100	78.93	-0.51	2.20E-07
10:00	60.245	78.95	-0.53	2.29E-07
10:02	62.245	78.98	-0.56	2.36E-07
10:04	64.245	79.00	-0.58	2.44E-07
10:06	66.245	79.03	-0.61	2.51E-07
10:08	68.245	79.05	-0.63	2.59E-07
10:10	70.245	79.07	-0.65	2.67E-07
10:12	72.245	79.10	-0.68	2.74E-07
10:14	74.245	79.12	-0.70	2.82E-07
10:16	76.245	79.14	-0.72	2.89E-07
10:18	78.245	79.16	-0.74	2.97E-07
10:20	80.245	79.19	-0.77	3.05E-07
10:22	82.245	79.21	-0.79	3.12E-07
10:24	84.245	79.23	-0.81	3.20E-07
10:26	86.245	79.25	-0.83	3.27E-07
10:28	88.245	79.28	-0.86	3.35E-07
10:30	90.245	79.30	-0.88	3.42E-07
10:32	92.245	79.32	-0.90	3.50E-07
10:34	94.245	79.34	-0.92	3.58E-07
10:36	96.245	79.37	-0.95	3.65E-07
10:38	98.245	79.39	-0.97	3.73E-07
11:00	120.210	79.61	-1.19	4.56E-07
11:20	140.210	79.82	-1.40	5.32E-07
11:40	160.210	79.99	-1.57	6.08E-07
12:00	180.220	80.16	-1.74	6.84E-07
12:20	200.220	80.32	-1.90	7.60E-07

12:40	220.220	80.47	-2.05	8.36E-07
13:00	240.220	80.61	-2.19	9.12E-07
13:20	260.220	80.74	-2.32	9.87E-07
13:40	280.230	80.85	-2.43	1.06E-06
14:00	300.230	80.97	-2.55	1.14E-06
14:20	320.230	81.07	-2.65	1.22E-06
14:40	340.180	81.16	-2.74	1.29E-06
15:00	360.100	81.25	-2.83	1.37E-06
15:20	380.100	81.33	-2.91	1.44E-06
15:40	400.100	81.40	-2.98	1.52E-06
16:00	420.170	81.47	-3.05	1.59E-06
16:20	440.250	81.54	-3.12	1.67E-06
16:40	460.200	81.61	-3.19	1.75E-06
17:00	480.170	81.67	-3.25	1.82E-06
17:20	500.170	81.73	-3.31	1.90E-06
17:40	520.130	81.80	-3.38	1.97E-06
18:00	540.120	81.86	-3.44	2.05E-06
18:20	560.220	81.93	-3.51	2.13E-06
18:40	580.080	82.03	-3.61	2.20E-06
19:00	600.220	82.11	-3.69	2.28E-06
19:20	620.230	82.19	-3.77	2.35E-06
19:40	640.220	82.27	-3.85	2.43E-06
20:00	660.220	82.34	-3.92	2.51E-06
20:20	680.130	82.41	-3.99	2.58E-06
20:40	700.120	82.48	-4.06	2.66E-06
21:00	720.230	82.54	-4.12	2.73E-06
21:20	740.300	82.61	-4.19	2.81E-06
21:40	760.230	82.67	-4.25	2.88E-06
22:00	780.230	82.74	-4.32	2.96E-06
22:20	800.230	82.80	-4.38	3.04E-06
22:40	820.180	82.86	-4.44	3.11E-06
23:00	840.570	82.92	-4.50	3.19E-06
23:20	860.180	82.97	-4.55	3.26E-06
23:40	880.080	83.03	-4.61	3.34E-06
00:00	900.170	83.09	-4.67	3.42E-06
00:20	920.170	83.14	-4.72	3.49E-06
00:40	940.170	83.19	-4.77	3.57E-06
01:00	960.170	83.25	-4.83	3.64E-06
01:20	980.170	83.30	-4.88	3.72E-06
01:40	1000.200	83.35	-4.93	3.80E-06
02:40	1060.300	83.49	-5.07	4.02E-06
03:40	1120.300	83.63	-5.21	4.25E-06
04:40	1180.300	83.76	-5.34	4.48E-06
05:40	1240.300	83.89	-5.47	4.71E-06
06:40	1300.300	84.01	-5.59	4.93E-06
07:40	1360.200	84.12	-5.70	5.16E-06
08:40	1420.200	84.22	-5.80	5.39E-06
09:40	1480.200	84.33	-5.91	5.62E-06
10:40	1540.200	84.43	-6.01	5.84E-06
11:40	1600.300	84.52	-6.10	6.07E-06
12:40	1660.300	84.59	-6.17	6.30E-06
13:40	1720.200	84.53	-6.11	6.53E-06
14:40	1780.300	84.70	-6.28	6.76E-06
15:40	1840.300	84.78	-6.36	6.98E-06
16:40	1900.300	84.84	-6.42	7.21E-06
17:40	1960.200	84.92	-6.50	7.44E-06

18:40	2020.200	84.98	-6.56	7.67E-06
19:40	2080.200	85.07	-6.65	7.89E-06
20:40	2140.200	85.17	-6.75	8.12E-06
21:40	2200.300	85.25	-6.83	8.35E-06
22:40	2260.300	85.33	-6.91	8.58E-06
23:40	2320.200	85.39	-6.97	8.80E-06
00:40	2380.200	85.47	-7.05	9.03E-06
01:40	2440.200	85.54	-7.12	9.26E-06
02:40	2500.200	85.62	-7.20	9.49E-06
03:40	2560.200	85.70	-7.28	9.72E-06
04:40	2620.200	85.77	-7.35	9.94E-06
05:40	2680.200	85.83	-7.41	1.02E-05
06:40	2740.200	85.89	-7.47	1.04E-05
07:40	2800.200	85.95	-7.53	1.06E-05
08:40	2860.300	86.01	-7.59	1.09E-05
09:40	2920.300	86.10	-7.68	1.11E-05
10:40	2980.300	86.16	-7.74	1.13E-05
11:40	3040.200	86.24	-7.82	1.15E-05
12:40	3100.200	86.31	-7.89	1.18E-05
13:40	3160.300	86.37	-7.95	1.20E-05
14:40	3220.300	86.44	-8.02	1.22E-05
15:40	3280.200	86.51	-8.09	1.24E-05
16:40	3340.200	86.58	-8.16	1.27E-05
17:40	3400.300	86.60	-8.18	1.29E-05
18:40	3460.300	86.67	-8.25	1.31E-05
19:40	3520.300	86.72	-8.30	1.34E-05
20:40	3580.200	86.78	-8.36	1.36E-05
21:40	3640.200	86.84	-8.42	1.38E-05
22:40	3700.200	86.91	-8.49	1.40E-05
23:40	3760.200	86.97	-8.55	1.43E-05
00:40	3820.200	87.02	-8.60	1.45E-05
01:40	3880.200	87.06	-8.64	1.47E-05
02:40	3940.200	87.10	-8.68	1.50E-05
03:40	4000.200	87.15	-8.73	1.52E-05
04:40	4060.200	87.20	-8.78	1.54E-05
05:40	4120.200	87.26	-8.84	1.56E-05
06:40	4180.200	87.31	-8.89	1.59E-05
07:40	4240.300	87.35	-8.93	1.61E-05
08:40	4300.300	87.40	-8.98	1.63E-05
09:40	4360.700	87.46	-9.04	1.65E-05
10:40	4420.300	87.50	-9.08	1.68E-05
11:40	4480.300	87.54	-9.12	1.70E-05
12:40	4540.300	87.58	-9.16	1.72E-05
13:40	4600.300	87.62	-9.20	1.75E-05
14:40	4660.300	87.67	-9.25	1.77E-05
15:40	4720.300	87.69	-9.27	1.79E-05
16:40	4780.300	87.74	-9.32	1.81E-05
17:40	4840.300	87.78	-9.36	1.84E-05
18:40	4900.300	87.78	-9.36	1.86E-05
19:40	4960.300	87.81	-9.39	1.88E-05
20:40	5020.300	87.85	-9.43	1.91E-05
21:40	5080.300	87.88	-9.46	1.93E-05
22:40	5140.300	87.91	-9.49	1.95E-05
23:40	5200.300	87.94	-9.52	1.97E-05
00:40	5260.300	87.97	-9.55	2.00E-05
01:40	5320.300	88.00	-9.58	2.02E-05

02:40	5380.300	88.03	-9.61	2.04E-05
03:40	5440.300	88.06	-9.64	2.06E-05
04:40	5500.300	88.09	-9.67	2.09E-05
05:40	5560.300	88.12	-9.70	2.11E-05
06:40	5620.300	88.15	-9.73	2.13E-05
07:40	5680.300	88.19	-9.77	2.16E-05
08:40	5740.300	88.22	-9.80	2.18E-05
09:40	5800.300	88.25	-9.83	2.20E-05
10:40	5860.300	88.28	-9.86	2.22E-05
11:40	5920.300	88.31	-9.89	2.25E-05
12:40	5980.300	88.32	-9.90	2.27E-05
13:40	6040.300	88.34	-9.92	2.29E-05
14:40	6100.300	88.36	-9.94	2.31E-05
15:40	6160.500	88.38	-9.96	2.34E-05
16:40	6220.300	88.41	-9.99	2.36E-05
17:40	6280.300	88.43	-10.01	2.38E-05
18:40	6340.300	88.46	-10.04	2.41E-05
19:40	6400.400	88.48	-10.06	2.43E-05
20:40	6460.200	88.51	-10.09	2.45E-05
21:40	6520.200	88.54	-10.12	2.47E-05
22:40	6580.300	88.57	-10.15	2.50E-05
23:40	6640.300	88.60	-10.18	2.52E-05
00:40	6700.300	88.62	-10.20	2.54E-05
01:40	6760.300	88.64	-10.22	2.57E-05
02:40	6820.300	88.67	-10.25	2.59E-05
03:40	6880.300	88.69	-10.27	2.61E-05
04:40	6940.300	88.71	-10.29	2.63E-05
05:40	7000.300	88.73	-10.31	2.66E-05
06:40	7060.300	88.75	-10.33	2.68E-05
07:40	7120.300	88.75	-10.33	2.70E-05
08:40	7180.300	88.72	-10.30	2.72E-05
09:40	7240.300	88.65	-10.23	2.75E-05
10:40	7300.300	88.59	-10.17	2.77E-05
11:40	7360.300	88.54	-10.12	2.79E-05
12:40	7420.300	88.51	-10.09	2.82E-05
13:40	7480.300	88.49	-10.07	2.84E-05
14:40	7540.300	88.50	-10.08	2.86E-05
15:40	7600.300	88.52	-10.10	2.88E-05
16:40	7660.300	88.56	-10.14	2.91E-05
17:40	7720.300	88.60	-10.18	2.93E-05
18:40	7780.200	88.64	-10.22	2.95E-05
19:40	7840.200	88.69	-10.27	2.98E-05
20:40	7900.300	88.75	-10.33	3.00E-05
21:40	7960.300	88.80	-10.38	3.02E-05
22:40	8020.300	88.80	-10.38	3.04E-05
23:40	8080.300	88.81	-10.39	3.07E-05
00:40	8140.300	88.81	-10.39	3.09E-05
01:40	8200.300	88.81	-10.39	3.11E-05
02:40	8260.300	88.82	-10.40	3.13E-05
03:40	8320.300	88.81	-10.39	3.16E-05
04:40	8380.300	88.82	-10.40	3.18E-05
05:40	8440.300	88.82	-10.40	3.20E-05
06:40	8500.300	88.82	-10.40	3.23E-05
07:40	8560.200	88.82	-10.40	3.25E-05
08:40	8620.300	88.82	-10.40	3.27E-05
09:00	8640.600	88.82	-10.40	3.28E-05

## ADJUSTED DATA

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 10-1 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI-11 INPUT 2  
 RADIUS: 427.782 FEET  
 START DATE : 13-Oct-86  
 START TIME : 10:25  
 WATER START LEVEL: 78.42 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
10:25	8725.000	88.82	-10.40	3.31E-05
10:35	8735.071	88.82	-10.40	3.31E-05
10:45	8745.070	88.82	-10.40	3.32E-05
10:55	8755.072	88.81	-10.39	3.32E-05
11:05	8765.072	88.81	-10.39	3.33E-05
11:15	8775.072	88.81	-10.39	3.33E-05
11:25	8785.072	88.82	-10.40	3.33E-05
11:35	8795.072	88.81	-10.39	3.34E-05
11:45	8805.072	88.82	-10.40	3.34E-05
11:55	8815.102	88.82	-10.40	3.35E-05
12:05	8825.090	88.82	-10.40	3.35E-05
12:15	8835.090	88.82	-10.40	3.35E-05
12:25	8845.090	88.82	-10.40	3.36E-05
12:35	8855.090	88.82	-10.40	3.36E-05
12:45	8865.090	88.82	-10.40	3.36E-05
12:55	8875.120	88.81	-10.39	3.37E-05
13:04	8884.970	88.81	-10.39	3.37E-05
13:14	8894.970	88.81	-10.39	3.38E-05
13:25	8904.970	88.81	-10.39	3.38E-05
13:34	8914.970	88.82	-10.40	3.38E-05
13:45	8924.970	88.82	-10.40	3.39E-05
13:54	8934.970	88.81	-10.39	3.39E-05
14:05	8944.970	88.82	-10.40	3.39E-05
14:14	8955.020	88.81	-10.39	3.40E-05
14:25	8965.080	88.82	-10.40	3.40E-05
14:35	8975.080	88.81	-10.39	3.41E-05
14:45	8985.080	88.81	-10.39	3.41E-05
14:55	8995.080	88.81	-10.39	3.41E-05
15:05	9005.080	88.81	-10.39	3.42E-05
15:15	9015.080	88.81	-10.39	3.42E-05
15:25	9025.080	88.81	-10.39	3.42E-05
15:35	9035.080	88.81	-10.39	3.43E-05
15:45	9045.080	88.81	-10.39	3.43E-05
15:55	9055.080	88.81	-10.39	3.44E-05
16:04	9065.020	88.81	-10.39	3.44E-05
16:15	9075.020	88.81	-10.39	3.44E-05
16:25	9084.970	88.81	-10.39	3.45E-05
16:35	9095.080	88.81	-10.39	3.45E-05
16:45	9105.080	88.81	-10.39	3.46E-05
16:55	9115.080	88.81	-10.39	3.46E-05

## ADJUSTED DATA

17:05	9125.080	88.81	-10.39	3.46E-05
17:15	9135.080	88.81	-10.39	3.47E-05
17:25	9145.080	88.81	-10.39	3.47E-05
17:35	9155.080	88.81	-10.39	3.47E-05
17:45	9165.080	88.81	-10.39	3.48E-05
17:55	9175.080	88.81	-10.39	3.48E-05
18:05	9185.080	88.81	-10.39	3.49E-05
18:15	9195.080	88.81	-10.39	3.49E-05
18:25	9205.080	88.81	-10.39	3.49E-05
18:35	9215.080	88.81	-10.39	3.50E-05
18:45	9225.080	88.81	-10.39	3.50E-05
18:55	9235.080	88.81	-10.39	3.50E-05
19:05	9245.080	88.81	-10.39	3.51E-05
19:15	9255.080	88.81	-10.39	3.51E-05
19:25	9265.080	88.81	-10.39	3.52E-05
19:35	9275.070	88.81	-10.39	3.52E-05
19:45	9285.080	88.85	-10.43	3.52E-05
19:55	9295.080	88.86	-10.44	3.53E-05
20:05	9305.080	88.86	-10.44	3.53E-05
20:15	9315.080	88.85	-10.43	3.53E-05
20:25	9325.080	88.85	-10.43	3.54E-05
20:35	9335.080	88.85	-10.43	3.54E-05
20:45	9345.080	88.85	-10.43	3.55E-05
20:55	9355.080	88.85	-10.43	3.55E-05
21:05	9365.080	88.85	-10.43	3.55E-05
21:15	9375.080	88.85	-10.43	3.56E-05
21:25	9385.080	88.85	-10.43	3.56E-05
21:35	9395.080	88.85	-10.43	3.57E-05
21:45	9405.080	88.83	-10.41	3.57E-05
21:55	9415.080	88.83	-10.41	3.57E-05
22:05	9425.080	88.83	-10.41	3.58E-05
22:15	9435.080	88.83	-10.41	3.58E-05
22:25	9445.080	88.83	-10.41	3.58E-05
22:35	9455.080	88.83	-10.41	3.59E-05
22:45	9465.080	88.83	-10.41	3.59E-05
22:54	9475.020	88.82	-10.40	3.60E-05
23:05	9485.020	88.82	-10.40	3.60E-05
23:14	9495.020	88.83	-10.41	3.60E-05
23:25	9505.020	88.82	-10.40	3.61E-05
23:34	9515.020	88.83	-10.41	3.61E-05
23:45	9525.020	88.83	-10.41	3.61E-05
23:55	9535.020	88.84	-10.42	3.62E-05
00:05	9545.020	88.84	-10.42	3.62E-05
00:15	9555.020	88.84	-10.42	3.63E-05
00:25	9565.030	88.85	-10.43	3.63E-05
00:35	9575.030	88.85	-10.43	3.63E-05
00:44	9585.030	88.84	-10.42	3.64E-05
00:55	9595.030	88.84	-10.42	3.64E-05
01:04	9605.030	88.84	-10.42	3.64E-05
01:15	9615.030	88.84	-10.42	3.65E-05
01:25	9625.030	88.84	-10.42	3.65E-05
01:35	9635.030	88.84	-10.42	3.66E-05
01:45	9645.030	88.84	-10.42	3.66E-05
01:55	9655.030	88.84	-10.42	3.66E-05
02:05	9665.030	88.84	-10.42	3.67E-05
02:14	9675.030	88.85	-10.43	3.67E-05

## ADJUSTED DATA

02:25	9685.030	88.85	-10.43	3.68E-05
02:34	9695.030	88.85	-10.43	3.68E-05
02:45	9705.030	88.85	-10.43	3.68E-05
02:55	9715.030	88.85	-10.43	3.69E-05
03:04	9725.000	88.85	-10.43	3.69E-05
03:15	9735.000	88.85	-10.43	3.69E-05
03:24	9745.000	88.85	-10.43	3.70E-05
03:35	9755.100	88.85	-10.43	3.70E-05
03:44	9765.000	88.85	-10.43	3.71E-05
03:55	9775.000	88.85	-10.43	3.71E-05
04:04	9785.000	88.85	-10.43	3.71E-05
04:15	9795.000	88.85	-10.43	3.72E-05
04:25	9805.000	88.85	-10.43	3.72E-05
04:34	9815.000	88.85	-10.43	3.72E-05
04:45	9825.000	88.84	-10.42	3.73E-05
04:54	9835.000	88.84	-10.42	3.73E-05
05:05	9845.000	88.84	-10.42	3.74E-05
05:14	9855.000	88.85	-10.43	3.74E-05
05:25	9865.000	88.85	-10.43	3.74E-05
05:34	9875.000	88.85	-10.43	3.75E-05
05:45	9885.000	88.85	-10.43	3.75E-05
05:55	9895.000	88.85	-10.43	3.75E-05
06:04	9905.000	88.85	-10.43	3.76E-05
06:15	9915.000	88.84	-10.42	3.76E-05
06:24	9925.000	88.85	-10.43	3.77E-05
06:35	9935.000	88.85	-10.43	3.77E-05
06:44	9945.000	88.85	-10.43	3.77E-05
06:55	9955.000	88.85	-10.43	3.78E-05
07:05	9965.100	88.85	-10.43	3.78E-05
07:15	9975.100	88.85	-10.43	3.79E-05
07:25	9985.100	88.85	-10.43	3.79E-05
07:35	9995.100	88.85	-10.43	3.79E-05
07:45	10005.100	88.85	-10.43	3.80E-05
07:55	10015.100	88.85	-10.43	3.80E-05
08:05	10025.100	88.85	-10.43	3.80E-05
08:15	10035.100	88.85	-10.43	3.81E-05
08:25	10045.100	88.85	-10.43	3.81E-05
08:35	10055.100	88.85	-10.43	3.82E-05
08:45	10065.100	88.85	-10.43	3.82E-05
08:55	10075.000	88.85	-10.43	3.82E-05
09:04	10085.000	88.85	-10.43	3.83E-05
09:15	10095.000	88.85	-10.43	3.83E-05
09:24	10105.000	88.85	-10.43	3.83E-05
09:28	10108.200	88.85	-10.43	3.84E-05

TEST NAME: REI 10-1 RUN # 2  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI-11 INPUT 2  
 RADIUS: 427.782 FEET  
 START DATE: 07-Oct-86  
 START TIME: 11:10  
 WATER START LEVEL: 78.42 FEET  
 WATER STOP LEVEL: 90.06 FEET  
 TOTAL PUMPING TIME: 10210.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)	t/r2	t/t'
11:10	0.017	-999.99	1090.05	1078.41	6.45E-11	6.01E+05
11:10	0.034	-999.99	1090.05	1078.41	1.29E-10	3.00E+05
11:10	0.050	-999.99	1090.05	1078.41	1.90E-10	2.04E+05
11:10	0.067	-999.99	1090.05	1078.41	2.54E-10	1.52E+05
11:10	0.084	-999.99	1090.05	1078.41	3.19E-10	1.22E+05
11:10	0.100	-999.99	1090.05	1078.41	3.79E-10	1.02E+05
11:10	0.117	-999.99	1090.05	1078.41	4.44E-10	8.73E+04
11:10	0.134	-999.99	1090.05	1078.41	5.09E-10	7.62E+04
11:10	0.150	-999.99	1090.05	1078.41	5.69E-10	6.81E+04
11:10	0.167	-999.99	1090.05	1078.41	6.34E-10	6.11E+04
11:10	0.257	90.05	0.01	11.63	9.75E-10	3.97E+04
11:10	0.341	90.05	0.01	11.63	1.29E-09	2.99E+04
11:10	0.424	90.05	0.01	11.63	1.61E-09	2.41E+04
11:10	0.507	90.05	0.01	11.63	1.92E-09	2.01E+04
11:10	0.591	90.05	0.01	11.63	2.24E-09	1.73E+04
11:10	0.674	90.05	0.01	11.63	2.56E-09	1.52E+04
11:10	0.757	90.05	0.01	11.63	2.87E-09	1.35E+04
11:10	0.841	90.05	0.01	11.63	3.19E-09	1.21E+04
11:10	0.924	90.05	0.01	11.63	3.51E-09	1.11E+04
11:11	1.007	90.06	0.00	11.64	3.82E-09	1.01E+04
11:11	1.413	90.06	0.00	11.64	5.36E-09	7.23E+03
11:11	1.747	90.06	0.00	11.64	6.63E-09	5.85E+03
11:12	2.080	90.06	0.00	11.64	7.89E-09	4.91E+03
11:12	2.413	90.06	0.00	11.64	9.16E-09	4.23E+03
11:12	2.747	90.06	0.00	11.64	1.04E-08	3.72E+03
11:13	3.080	90.06	0.00	11.64	1.17E-08	3.32E+03
11:13	3.413	90.06	0.00	11.64	1.30E-08	2.99E+03
11:13	3.747	90.06	0.00	11.64	1.42E-08	2.73E+03
11:14	4.080	90.06	0.00	11.64	1.55E-08	2.50E+03
11:14	4.413	90.06	0.00	11.64	1.67E-08	2.31E+03
11:14	4.747	90.06	0.00	11.64	1.80E-08	2.15E+03
11:15	5.080	90.06	0.00	11.64	1.93E-08	2.01E+03
11:15	5.413	90.06	0.00	11.64	2.05E-08	1.89E+03
11:15	5.747	90.06	0.00	11.64	2.18E-08	1.78E+03
11:16	6.080	90.06	0.00	11.64	2.31E-08	1.68E+03
11:16	6.413	90.06	0.00	11.64	2.43E-08	1.59E+03
11:16	6.747	90.06	0.00	11.64	2.56E-08	1.51E+03
11:17	7.080	90.06	0.00	11.64	2.69E-08	1.44E+03
11:17	7.413	90.05	0.01	11.63	2.81E-08	1.38E+03
11:17	7.747	90.06	0.00	11.64	2.94E-08	1.32E+03
11:18	8.080	90.05	0.01	11.63	3.07E-08	1.26E+03
11:18	8.413	90.05	0.01	11.63	3.19E-08	1.21E+03



11:18	8.747	90.05	0.01	11.63	3.32E-08	1.17E+03
11:19	9.080	90.05	0.01	11.63	3.45E-08	1.13E+03
11:19	9.413	90.05	0.01	11.63	3.57E-08	1.09E+03
11:19	9.747	90.05	0.01	11.63	3.70E-08	1.05E+03
11:20	10.080	90.05	0.01	11.63	3.83E-08	1.01E+03
11:22	12.115	90.04	0.02	11.62	4.60E-08	8.44E+02
11:24	14.115	90.03	0.03	11.61	5.36E-08	7.24E+02
11:26	16.115	90.03	0.03	11.61	6.12E-08	6.35E+02
11:28	18.115	90.01	0.05	11.59	6.87E-08	5.65E+02
11:30	20.115	90.00	0.06	11.58	7.63E-08	5.09E+02
11:32	22.115	89.98	0.08	11.56	8.39E-08	4.63E+02
11:34	24.115	89.96	0.10	11.54	9.15E-08	4.24E+02
11:36	26.115	89.94	0.12	11.52	9.91E-08	3.92E+02
11:38	28.115	89.92	0.14	11.50	1.07E-07	3.64E+02
11:40	30.115	89.90	0.16	11.48	1.14E-07	3.40E+02
11:42	32.115	89.88	0.18	11.46	1.22E-07	3.19E+02
11:44	34.115	89.85	0.21	11.43	1.29E-07	3.00E+02
11:46	36.115	89.83	0.23	11.41	1.37E-07	2.84E+02
11:48	38.115	89.81	0.25	11.39	1.45E-07	2.69E+02
11:50	40.115	89.79	0.27	11.37	1.52E-07	2.56E+02
11:52	42.115	89.77	0.29	11.35	1.60E-07	2.43E+02
11:54	44.115	89.75	0.31	11.33	1.67E-07	2.32E+02
11:56	46.115	89.72	0.34	11.30	1.75E-07	2.22E+02
11:58	48.115	89.70	0.36	11.28	1.83E-07	2.13E+02
12:00	50.115	89.68	0.38	11.26	1.90E-07	2.05E+02
12:02	52.115	89.66	0.40	11.24	1.98E-07	1.97E+02
12:04	54.115	89.64	0.42	11.22	2.05E-07	1.90E+02
12:06	56.115	89.62	0.44	11.20	2.13E-07	1.83E+02
12:08	58.115	89.60	0.46	11.18	2.21E-07	1.77E+02
12:10	60.115	89.58	0.48	11.16	2.28E-07	1.71E+02
12:12	62.102	89.56	0.50	11.14	2.36E-07	1.65E+02
12:14	64.492	89.53	0.53	11.11	2.45E-07	1.59E+02
12:16	66.188	89.51	0.55	11.09	2.51E-07	1.55E+02
12:18	68.188	89.49	0.57	11.07	2.59E-07	1.51E+02
12:20	70.188	89.47	0.59	11.05	2.66E-07	1.46E+02
12:22	72.188	89.45	0.61	11.03	2.74E-07	1.42E+02
12:24	74.188	89.43	0.63	11.01	2.82E-07	1.39E+02
12:26	76.188	89.41	0.65	10.99	2.89E-07	1.35E+02
12:28	78.188	89.39	0.67	10.97	2.97E-07	1.32E+02
12:30	80.188	89.37	0.69	10.95	3.04E-07	1.28E+02
12:32	82.188	89.35	0.71	10.93	3.12E-07	1.25E+02
12:34	84.188	89.33	0.73	10.91	3.19E-07	1.22E+02
12:36	86.188	89.31	0.75	10.89	3.27E-07	1.19E+02
12:38	88.188	89.29	0.77	10.87	3.35E-07	1.17E+02
12:40	90.188	89.27	0.79	10.85	3.42E-07	1.14E+02
12:42	92.188	89.24	0.82	10.82	3.50E-07	1.12E+02
12:44	94.188	89.23	0.83	10.81	3.57E-07	1.09E+02
12:46	96.188	89.22	0.84	10.80	3.65E-07	1.07E+02
12:48	98.188	89.20	0.86	10.78	3.73E-07	1.05E+02
13:10	120.110	88.85	1.21	10.43	4.56E-07	8.60E+01
13:30	140.110	88.64	1.42	10.22	5.32E-07	7.39E+01
13:50	160.120	88.50	1.56	10.08	6.08E-07	6.48E+01
14:10	180.120	88.38	1.68	9.96	6.84E-07	5.77E+01
14:30	200.120	88.26	1.80	9.84	7.59E-07	5.20E+01
14:50	220.120	88.12	1.94	9.70	8.35E-07	4.74E+01
15:10	240.120	88.04	2.02	9.62	9.11E-07	4.35E+01

15:30	260.120	87.92	2.14	9.50	9.87E-07	4.03E+01
15:50	280.120	87.81	2.25	9.39	1.06E-06	3.75E+01
16:10	300.120	87.70	2.36	9.28	1.14E-06	3.50E+01
16:30	320.050	87.57	2.49	9.15	1.21E-06	3.29E+01
16:49	340.050	87.40	2.66	8.98	1.29E-06	3.10E+01
17:10	360.050	87.33	2.73	8.91	1.37E-06	2.94E+01
17:30	380.050	87.24	2.82	8.82	1.44E-06	2.79E+01
17:50	400.050	87.10	2.96	8.68	1.52E-06	2.65E+01
18:10	420.050	87.02	3.04	8.60	1.59E-06	2.53E+01
18:30	440.050	86.96	3.10	8.54	1.67E-06	2.42E+01
18:50	460.050	86.88	3.18	8.46	1.75E-06	2.32E+01
19:10	480.050	86.78	3.28	8.36	1.82E-06	2.23E+01
19:30	500.050	86.74	3.32	8.32	1.90E-06	2.14E+01
19:49	520.050	86.66	3.40	8.24	1.97E-06	2.06E+01
20:10	540.050	86.50	3.56	8.08	2.05E-06	1.99E+01
20:30	560.050	86.42	3.64	8.00	2.13E-06	1.92E+01
20:50	580.050	86.40	3.66	7.98	2.20E-06	1.86E+01
21:10	600.050	86.37	3.69	7.95	2.28E-06	1.80E+01
21:30	620.050	86.33	3.73	7.91	2.35E-06	1.75E+01
21:50	640.050	86.28	3.78	7.86	2.43E-06	1.70E+01
22:10	660.050	86.22	3.84	7.80	2.50E-06	1.65E+01
22:30	680.050	86.18	3.88	7.76	2.58E-06	1.60E+01
22:49	700.050	86.12	3.94	7.70	2.66E-06	1.56E+01
23:10	720.050	86.07	3.99	7.65	2.73E-06	1.52E+01
23:30	740.050	86.01	4.05	7.59	2.81E-06	1.48E+01
23:50	760.100	85.96	4.10	7.54	2.88E-06	1.44E+01
00:10	780.100	85.91	4.15	7.49	2.96E-06	1.41E+01
00:30	800.100	85.86	4.20	7.44	3.04E-06	1.38E+01
00:50	820.100	85.81	4.25	7.39	3.11E-06	1.35E+01
01:10	840.100	85.76	4.30	7.34	3.19E-06	1.32E+01
01:30	860.100	85.71	4.35	7.29	3.26E-06	1.29E+01
01:50	880.100	85.66	4.40	7.24	3.34E-06	1.26E+01
02:10	900.100	85.60	4.46	7.18	3.42E-06	1.23E+01
02:30	920.100	85.56	4.50	7.14	3.49E-06	1.21E+01
02:50	940.100	85.53	4.53	7.11	3.57E-06	1.19E+01
03:10	960.100	85.48	4.58	7.06	3.64E-06	1.16E+01
03:30	980.100	85.44	4.62	7.02	3.72E-06	1.14E+01
03:50	1000.100	85.40	4.66	6.98	3.80E-06	1.12E+01
04:50	1060.300	85.27	4.79	6.85	4.02E-06	1.06E+01
05:50	1120.300	85.16	4.90	6.74	4.25E-06	1.01E+01
06:50	1180.300	85.03	5.03	6.61	4.48E-06	9.65E+00
07:50	1240.300	84.94	5.12	6.52	4.71E-06	9.23E+00
08:50	1300.300	84.83	5.23	6.41	4.93E-06	8.85E+00
09:50	1360.300	84.73	5.33	6.31	5.16E-06	8.51E+00
10:50	1420.300	84.55	5.51	6.13	5.39E-06	8.19E+00
11:50	1480.300	84.51	5.55	6.09	5.62E-06	7.90E+00
12:50	1540.300	84.46	5.60	6.04	5.85E-06	7.63E+00
13:50	1600.300	84.35	5.71	5.93	6.07E-06	7.38E+00
14:50	1660.300	84.24	5.82	5.82	6.30E-06	7.15E+00
15:50	1720.100	84.14	5.92	5.72	6.53E-06	6.94E+00
16:50	1780.100	84.07	5.99	5.65	6.76E-06	6.74E+00
17:50	1840.100	83.99	6.07	5.57	6.98E-06	6.55E+00
18:50	1900.100	83.89	6.17	5.47	7.21E-06	6.37E+00
19:50	1960.100	83.84	6.22	5.42	7.44E-06	6.21E+00
20:50	2020.100	83.80	6.26	5.38	7.67E-06	6.05E+00
21:50	2080.100	83.71	6.35	5.29	7.89E-06	5.91E+00

22:50	2140.100	83.66	6.40	5.24	8.12E-06	5.77E+00
23:50	2200.100	83.62	6.44	5.20	8.35E-06	5.64E+00
00:50	2260.100	83.56	6.50	5.14	8.58E-06	5.52E+00
01:50	2320.100	83.50	6.56	5.08	8.80E-06	5.40E+00
02:50	2380.100	83.44	6.62	5.02	9.03E-06	5.29E+00
03:50	2440.100	83.38	6.68	4.96	9.26E-06	5.18E+00
04:50	2500.100	83.32	6.74	4.90	9.49E-06	5.08E+00
05:50	2560.100	83.28	6.78	4.86	9.72E-06	4.99E+00
06:50	2620.100	83.23	6.83	4.81	9.94E-06	4.90E+00
07:50	2680.100	83.17	6.89	4.75	1.02E-05	4.81E+00
08:50	2740.200	83.12	6.94	4.70	1.04E-05	4.73E+00
09:50	2800.200	83.08	6.98	4.66	1.06E-05	4.65E+00
10:50	2860.200	83.03	7.03	4.61	1.09E-05	4.57E+00
11:50	2920.100	82.98	7.08	4.56	1.11E-05	4.50E+00
12:50	2980.200	82.92	7.14	4.50	1.13E-05	4.43E+00
13:50	3040.200	82.86	7.20	4.44	1.15E-05	4.36E+00
14:50	3100.200	82.80	7.26	4.38	1.18E-05	4.29E+00
15:50	3160.200	82.74	7.32	4.32	1.20E-05	4.23E+00
16:50	3220.200	82.69	7.37	4.27	1.22E-05	4.17E+00
17:50	3280.200	82.65	7.41	4.23	1.24E-05	4.11E+00
18:50	3340.200	82.59	7.47	4.17	1.27E-05	4.06E+00
19:50	3400.200	82.56	7.50	4.14	1.29E-05	4.00E+00
20:50	3460.200	82.52	7.54	4.10	1.31E-05	3.95E+00
21:50	3520.200	82.48	7.58	4.06	1.34E-05	3.90E+00
22:50	3580.200	82.44	7.62	4.02	1.36E-05	3.85E+00
23:50	3640.200	82.40	7.66	3.98	1.38E-05	3.80E+00
00:50	3700.200	82.36	7.70	3.94	1.40E-05	3.76E+00
01:50	3760.200	82.32	7.74	3.90	1.43E-05	3.72E+00
02:50	3820.200	82.28	7.78	3.86	1.45E-05	3.67E+00
03:50	3880.200	82.24	7.82	3.82	1.47E-05	3.63E+00
04:50	3940.200	82.20	7.86	3.78	1.50E-05	3.59E+00
05:50	4000.200	82.16	7.90	3.74	1.52E-05	3.55E+00
06:50	4060.200	82.12	7.94	3.70	1.54E-05	3.51E+00
07:50	4120.200	82.08	7.98	3.66	1.56E-05	3.48E+00
08:50	4180.200	82.06	8.00	3.64	1.59E-05	3.44E+00
09:50	4240.200	82.03	8.03	3.61	1.61E-05	3.41E+00
10:50	4300.200	82.00	8.06	3.58	1.63E-05	3.37E+00
11:04	4314.800	81.99	8.07	3.57	1.64E-05	3.37E+00

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 10-1 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 3-4 INPUT 4  
 RADIUS: 784.360 FEET  
 START DATE : 07-Oct-86  
 START TIME : 09:00  
 WATER START LEVEL: 80.79 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
09:00	0.000	80.79	0.00	0.00E+00
09:00	0.017	-99.99	180.78	1.92E-11
09:00	0.034	-99.99	180.78	3.84E-11
09:00	0.050	-99.99	180.78	5.64E-11
09:00	0.067	-99.99	180.78	7.56E-11
09:00	0.084	-99.99	180.78	9.48E-11
09:00	0.100	-99.99	180.78	1.13E-10
09:00	0.117	-99.99	180.78	1.32E-10
09:00	0.134	-99.99	180.78	1.51E-10
09:00	0.150	-99.99	180.78	1.69E-10
09:00	0.167	-99.99	180.78	1.89E-10
09:00	0.257	80.79	0.00	2.90E-10
09:00	0.340	80.79	0.00	3.84E-10
09:00	0.424	80.79	0.00	4.79E-10
09:00	0.507	80.79	0.00	5.72E-10
09:00	0.590	80.79	0.00	6.66E-10
09:00	0.674	80.79	0.00	7.61E-10
09:00	0.757	80.79	0.00	8.54E-10
09:00	0.840	80.79	0.00	9.48E-10
09:00	0.924	80.79	0.00	1.04E-09
09:01	1.007	80.79	0.00	1.14E-09
09:01	1.414	80.79	0.00	1.60E-09
09:01	1.748	80.79	0.00	1.97E-09
09:02	2.081	80.79	0.00	2.35E-09
09:02	2.414	80.79	0.00	2.72E-09
09:02	2.748	80.79	0.00	3.10E-09
09:03	3.081	80.79	0.00	3.48E-09
09:03	3.415	80.79	0.00	3.85E-09
09:03	3.748	80.79	0.00	4.23E-09
09:04	4.081	80.79	0.00	4.61E-09
09:04	4.414	80.79	0.00	4.98E-09
09:04	4.748	80.79	0.00	5.36E-09
09:05	5.081	80.79	0.00	5.74E-09
09:05	5.414	80.79	0.00	6.11E-09
09:05	5.748	80.79	0.00	6.49E-09
09:06	6.081	80.79	0.00	6.86E-09
09:06	6.415	80.79	0.00	7.24E-09
09:06	6.748	80.79	0.00	7.62E-09
09:07	7.081	80.79	0.00	7.99E-09
09:07	7.415	80.79	0.00	8.37E-09
09:07	7.748	80.79	0.00	8.75E-09

09:05	8.081	80.79	0.00	9.12E-09
09:08	8.415	80.79	0.00	9.50E-09
09:08	8.748	80.79	0.00	9.87E-09
09:09	9.081	80.79	0.00	1.03E-08
09:09	9.414	80.79	0.00	1.06E-08
09:09	9.748	80.79	0.00	1.10E-08
09:10	10.081	80.79	0.00	1.14E-08
09:12	12.108	80.79	0.00	1.37E-08
09:14	14.152	80.80	-0.01	1.60E-08
09:16	16.152	80.80	-0.01	1.82E-08
09:18	18.152	80.80	-0.01	2.05E-08
09:20	20.152	80.80	-0.01	2.27E-08
09:22	22.152	80.80	-0.01	2.50E-08
09:24	24.152	80.80	-0.01	2.73E-08
09:26	26.152	80.80	-0.01	2.95E-08
09:28	28.215	80.81	-0.02	3.18E-08
09:30	30.197	80.81	-0.02	3.41E-08
09:32	32.197	80.82	-0.03	3.63E-08
09:34	34.197	80.82	-0.03	3.86E-08
09:36	36.197	80.83	-0.04	4.09E-08
09:38	38.197	80.83	-0.04	4.31E-08
09:40	40.197	80.84	-0.05	4.54E-08
09:42	42.197	80.85	-0.06	4.76E-08
09:44	44.197	80.85	-0.06	4.99E-08
09:46	46.197	80.86	-0.07	5.21E-08
09:48	48.197	80.87	-0.08	5.44E-08
09:50	50.197	80.88	-0.09	5.67E-08
09:52	52.197	80.89	-0.10	5.89E-08
09:54	54.197	80.90	-0.11	6.12E-08
09:56	56.217	80.91	-0.12	6.35E-08
09:58	58.100	80.92	-0.13	6.56E-08
10:00	60.245	80.93	-0.14	6.80E-08
10:02	62.245	80.94	-0.15	7.03E-08
10:04	64.245	80.95	-0.16	7.25E-08
10:06	66.245	80.96	-0.17	7.48E-08
10:08	68.245	80.97	-0.18	7.70E-08
10:10	70.245	80.98	-0.19	7.93E-08
10:12	72.245	80.99	-0.20	8.15E-08
10:14	74.245	81.01	-0.22	8.38E-08
10:16	76.245	81.02	-0.23	8.61E-08
10:18	78.245	81.03	-0.24	8.83E-08
10:20	80.245	81.04	-0.25	9.06E-08
10:22	82.245	81.06	-0.27	9.28E-08
10:24	84.245	81.07	-0.28	9.51E-08
10:26	86.245	81.08	-0.29	9.74E-08
10:28	88.245	81.10	-0.31	9.96E-08
10:30	90.245	81.11	-0.32	1.02E-07
10:32	92.245	81.12	-0.33	1.04E-07
10:34	94.245	81.14	-0.35	1.06E-07
10:36	96.245	81.15	-0.36	1.09E-07
10:38	98.245	81.17	-0.38	1.11E-07
11:00	120.210	81.33	-0.54	1.36E-07
11:20	140.210	81.48	-0.69	1.58E-07
11:40	160.210	81.63	-0.84	1.81E-07
12:00	180.220	81.77	-0.98	2.03E-07
12:20	200.220	81.91	-1.12	2.26E-07

12:40	220.220	82.05	-1.26	2.49E-07
13:00	240.220	82.18	-1.39	2.71E-07
13:20	260.220	82.30	-1.51	2.94E-07
13:40	280.230	82.42	-1.63	3.16E-07
14:00	300.230	82.53	-1.74	3.39E-07
14:20	320.230	82.63	-1.84	3.61E-07
14:40	340.180	82.74	-1.95	3.84E-07
15:00	360.100	82.83	-2.04	4.06E-07
15:20	380.100	82.91	-2.12	4.29E-07
15:40	400.100	83.00	-2.21	4.52E-07
16:00	420.170	83.07	-2.28	4.74E-07
16:20	440.250	83.14	-2.35	4.97E-07
16:40	460.200	83.22	-2.43	5.19E-07
17:00	480.170	83.28	-2.49	5.42E-07
17:20	500.170	83.35	-2.56	5.65E-07
17:40	520.130	83.41	-2.62	5.87E-07
18:00	540.120	83.47	-2.68	6.10E-07
18:20	560.220	83.53	-2.74	6.32E-07
18:40	580.080	83.60	-2.81	6.55E-07
19:00	600.220	83.67	-2.88	6.78E-07
19:20	620.230	83.74	-2.95	7.00E-07
19:40	640.220	83.81	-3.02	7.23E-07
20:00	660.220	83.87	-3.08	7.45E-07
20:20	680.130	83.94	-3.15	7.68E-07
20:40	700.120	84.01	-3.22	7.90E-07
21:00	720.230	84.07	-3.28	8.13E-07
21:20	740.300	84.13	-3.34	8.36E-07
21:40	760.230	84.19	-3.40	8.58E-07
22:00	780.230	84.25	-3.46	8.81E-07
22:20	800.230	84.31	-3.52	9.03E-07
22:40	820.180	84.37	-3.58	9.26E-07
23:00	840.570	84.43	-3.64	9.49E-07
23:20	860.180	84.48	-3.69	9.71E-07
23:40	880.080	84.54	-3.75	9.93E-07
00:00	900.170	84.59	-3.80	1.02E-06
00:20	920.170	84.64	-3.85	1.04E-06
00:40	940.170	84.69	-3.90	1.06E-06
01:00	960.170	84.74	-3.95	1.08E-06
01:20	980.170	84.79	-4.00	1.11E-06
01:40	1000.200	84.84	-4.05	1.13E-06
02:40	1060.300	84.98	-4.19	1.20E-06
03:40	1120.300	85.11	-4.32	1.26E-06
04:40	1180.300	85.23	-4.44	1.33E-06
05:40	1240.300	85.36	-4.57	1.40E-06
06:40	1300.300	85.47	-4.68	1.47E-06
07:40	1360.200	85.58	-4.79	1.54E-06
08:40	1420.200	85.68	-4.89	1.60E-06
09:40	1480.200	85.79	-5.00	1.67E-06
10:40	1540.200	85.88	-5.09	1.74E-06
11:40	1600.300	85.96	-5.17	1.81E-06
12:40	1660.300	86.03	-5.24	1.87E-06
13:40	1720.200	86.09	-5.30	1.94E-06
14:40	1780.300	86.17	-5.38	2.01E-06
15:40	1840.300	86.25	-5.46	2.08E-06
16:40	1900.300	86.29	-5.50	2.15E-06
17:40	1960.200	86.36	-5.57	2.21E-06

18:40	2020.200	86.44	-5.65	2.28E-06
19:40	2080.200	86.52	-5.73	2.35E-06
20:40	2140.200	86.60	-5.81	2.42E-06
21:40	2200.300	86.68	-5.89	2.48E-06
22:40	2260.300	86.76	-5.97	2.55E-06
23:40	2320.200	86.83	-6.04	2.62E-06
00:40	2380.200	86.90	-6.11	2.69E-06
01:40	2440.200	86.97	-6.18	2.75E-06
02:40	2500.200	87.04	-6.25	2.82E-06
03:40	2560.200	87.11	-6.32	2.89E-06
04:40	2620.200	87.17	-6.38	2.96E-06
05:40	2680.200	87.23	-6.44	3.03E-06
06:40	2740.200	87.30	-6.51	3.09E-06
07:40	2800.200	87.36	-6.57	3.16E-06
08:40	2860.300	87.42	-6.63	3.23E-06
09:40	2920.300	87.48	-6.69	3.30E-06
10:40	2980.300	87.55	-6.76	3.36E-06
11:40	3040.200	87.62	-6.83	3.43E-06
12:40	3100.200	87.68	-6.89	3.50E-06
13:40	3160.300	87.73	-6.94	3.57E-06
14:40	3220.300	87.79	-7.00	3.63E-06
15:40	3280.200	87.85	-7.06	3.70E-06
16:40	3340.200	87.91	-7.12	3.77E-06
17:40	3400.300	87.96	-7.17	3.84E-06
18:40	3460.300	88.01	-7.22	3.91E-06
19:40	3520.300	88.07	-7.28	3.97E-06
20:40	3580.200	88.12	-7.33	4.04E-06
21:40	3640.200	88.17	-7.38	4.11E-06
22:40	3700.200	88.22	-7.43	4.18E-06
23:40	3760.200	88.27	-7.48	4.24E-06
00:40	3820.200	88.32	-7.53	4.31E-06
01:40	3880.200	88.36	-7.57	4.38E-06
02:40	3940.200	88.41	-7.62	4.45E-06
03:40	4000.200	88.45	-7.66	4.52E-06
04:40	4060.200	88.50	-7.71	4.58E-06
05:40	4120.200	88.54	-7.75	4.65E-06
06:40	4180.200	88.60	-7.81	4.72E-06
07:40	4240.300	88.64	-7.85	4.79E-06
08:40	4300.300	88.69	-7.90	4.85E-06
09:40	4360.700	88.74	-7.95	4.92E-06
10:40	4420.300	88.78	-7.99	4.99E-06
11:40	4480.300	88.81	-8.02	5.06E-06
12:40	4540.300	88.85	-8.06	5.12E-06
13:40	4600.300	88.88	-8.09	5.19E-06
14:40	4660.300	88.94	-8.15	5.26E-06
15:40	4720.300	88.95	-8.16	5.33E-06
16:40	4780.300	88.99	-8.20	5.40E-06
17:40	4840.300	89.04	-8.25	5.46E-06
18:40	4900.300	89.06	-8.27	5.53E-06
19:40	4960.300	89.08	-8.29	5.60E-06
20:40	5020.300	89.11	-8.32	5.67E-06
21:40	5080.300	89.14	-8.35	5.73E-06
22:40	5140.300	89.17	-8.38	5.80E-06
23:40	5200.300	89.20	-8.41	5.87E-06
00:40	5260.300	89.22	-8.43	5.94E-06
01:40	5320.300	89.25	-8.46	6.01E-06

02:40	5380.300	89.28	-8.49	6.07E-06
03:40	5440.300	89.31	-8.52	6.14E-06
04:40	5500.300	89.33	-8.54	6.21E-06
05:40	5560.300	89.36	-8.57	6.28E-06
06:40	5620.300	89.40	-8.61	6.34E-06
07:40	5680.300	89.43	-8.64	6.41E-06
08:40	5740.300	89.45	-8.66	6.48E-06
09:40	5800.300	89.49	-8.70	6.55E-06
10:40	5860.300	89.52	-8.73	6.61E-06
11:40	5920.300	89.54	-8.75	6.68E-06
12:40	5980.300	89.56	-8.77	6.75E-06
13:40	6040.300	89.57	-8.78	6.82E-06
14:40	6100.300	89.59	-8.80	6.89E-06
15:40	6160.500	89.62	-8.83	6.95E-06
16:40	6220.300	89.64	-8.85	7.02E-06
17:40	6280.300	89.66	-8.87	7.09E-06
18:40	6340.300	89.69	-8.90	7.16E-06
19:40	6400.400	89.71	-8.92	7.22E-06
20:40	6460.200	89.73	-8.94	7.29E-06
21:40	6520.200	89.76	-8.97	7.36E-06
22:40	6580.300	89.78	-8.99	7.43E-06
23:40	6640.300	89.81	-9.02	7.50E-06
00:40	6700.300	89.83	-9.04	7.56E-06
01:40	6760.300	89.86	-9.07	7.63E-06
02:40	6820.300	89.87	-9.08	7.70E-06
03:40	6880.300	89.89	-9.10	7.77E-06
04:40	6940.300	89.91	-9.12	7.83E-06
05:40	7000.300	89.93	-9.14	7.90E-06
06:40	7060.300	89.95	-9.16	7.97E-06
07:40	7120.300	89.94	-9.15	8.04E-06
08:40	7180.300	89.88	-9.09	8.10E-06
09:40	7240.300	89.83	-9.04	8.17E-06
10:40	7300.300	89.77	-8.98	8.24E-06
11:40	7360.300	89.72	-8.93	8.31E-06
12:40	7420.300	89.70	-8.91	8.38E-06
13:40	7480.300	89.68	-8.89	8.44E-06
14:40	7540.300	89.69	-8.90	8.51E-06
15:40	7600.300	89.72	-8.93	8.58E-06
16:40	7660.300	89.76	-8.97	8.65E-06
17:40	7720.300	89.79	-9.00	8.71E-06
18:40	7780.200	89.84	-9.05	8.78E-06
19:40	7840.200	89.89	-9.10	8.85E-06
20:40	7900.300	89.94	-9.15	8.92E-06
21:40	7960.300	90.00	-9.21	8.99E-06
22:40	8020.300	90.04	-9.25	9.05E-06
23:40	8080.300	90.09	-9.30	9.12E-06
00:40	8140.300	90.13	-9.34	9.19E-06
01:40	8200.300	90.16	-9.37	9.26E-06
02:40	8260.300	90.19	-9.40	9.32E-06
03:40	8320.300	90.22	-9.43	9.39E-06
04:40	8380.300	90.24	-9.45	9.46E-06
05:40	8440.300	90.26	-9.47	9.53E-06
06:40	8500.300	90.29	-9.50	9.59E-06
07:40	8560.200	90.31	-9.52	9.66E-06
08:40	8620.300	90.34	-9.55	9.73E-06
09:00	8640.600	90.34	-9.55	9.75E-06



## ADJUSTED DATA

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 10-1 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 3-4 INPUT 4  
 RADIUS: 784.360 FEET  
 START DATE : 13-Oct-86  
 START TIME : 10:25  
 WATER START LEVEL: 80.79 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
10:25	8725.000	90.32	-9.53	9.85E-06
10:35	8735.071	90.32	-9.53	9.86E-06
10:45	8745.070	90.31	-9.52	9.87E-06
10:55	8755.072	90.31	-9.52	9.88E-06
11:05	8765.072	90.30	-9.51	9.89E-06
11:15	8775.072	90.30	-9.51	9.91E-06
11:25	8785.072	90.30	-9.51	9.92E-06
11:35	8795.072	90.29	-9.50	9.93E-06
11:45	8805.072	90.29	-9.50	9.94E-06
11:55	8815.102	90.29	-9.50	9.95E-06
12:05	8825.090	90.29	-9.50	9.96E-06
12:15	8835.090	90.29	-9.50	9.97E-06
12:25	8845.090	90.29	-9.50	9.98E-06
12:35	8855.090	90.30	-9.51	1.00E-05
12:45	8865.090	90.29	-9.50	1.00E-05
12:55	8875.120	90.29	-9.50	1.00E-05
13:04	8884.970	90.30	-9.51	1.00E-05
13:14	8894.970	90.30	-9.51	1.00E-05
13:25	8904.970	90.30	-9.51	1.01E-05
13:34	8914.970	90.30	-9.51	1.01E-05
13:45	8924.970	90.31	-9.52	1.01E-05
13:54	8934.970	90.30	-9.51	1.01E-05
14:05	8944.970	90.31	-9.52	1.01E-05
14:14	8955.020	90.31	-9.52	1.01E-05
14:25	8965.080	90.32	-9.53	1.01E-05
14:35	8975.080	90.32	-9.53	1.01E-05
14:45	8985.080	90.32	-9.53	1.01E-05
14:55	8995.080	90.32	-9.53	1.02E-05
15:05	9005.080	90.32	-9.53	1.02E-05
15:15	9015.080	90.33	-9.54	1.02E-05
15:25	9025.080	90.33	-9.54	1.02E-05
15:35	9035.080	90.33	-9.54	1.02E-05
15:45	9045.080	90.34	-9.55	1.02E-05
15:55	9055.080	90.34	-9.55	1.02E-05
16:04	9065.020	90.35	-9.56	1.02E-05
16:15	9075.020	90.35	-9.56	1.02E-05
16:25	9084.970	90.35	-9.56	1.03E-05
16:35	9095.080	90.36	-9.57	1.03E-05
16:45	9105.080	90.37	-9.58	1.03E-05
16:55	9115.080	90.37	-9.58	1.03E-05

## ADJUSTED DATA

17:05	9125.080	90.38	-9.59	1.03E-05
17:15	9135.080	90.38	-9.59	1.03E-05
17:25	9145.080	90.39	-9.60	1.03E-05
17:35	9155.080	90.39	-9.60	1.03E-05
17:45	9165.080	90.40	-9.61	1.03E-05
17:55	9175.080	90.41	-9.62	1.04E-05
18:05	9185.080	90.41	-9.62	1.04E-05
18:15	9195.080	90.42	-9.63	1.04E-05
18:25	9205.080	90.43	-9.64	1.04E-05
18:35	9215.080	90.43	-9.64	1.04E-05
18:45	9225.080	90.44	-9.65	1.04E-05
18:55	9235.080	90.44	-9.65	1.04E-05
19:05	9245.080	90.45	-9.66	1.04E-05
19:15	9255.080	90.46	-9.67	1.04E-05
19:25	9265.080	90.46	-9.67	1.05E-05
19:35	9275.070	90.46	-9.67	1.05E-05
19:45	9285.080	90.47	-9.68	1.05E-05
19:55	9295.080	90.48	-9.69	1.05E-05
20:05	9305.080	90.48	-9.69	1.05E-05
20:15	9315.080	90.49	-9.70	1.05E-05
20:25	9325.080	90.49	-9.70	1.05E-05
20:35	9335.080	90.50	-9.71	1.05E-05
20:45	9345.080	90.50	-9.71	1.05E-05
20:55	9355.080	90.51	-9.72	1.06E-05
21:05	9365.080	90.52	-9.73	1.06E-05
21:15	9375.080	90.53	-9.74	1.06E-05
21:25	9385.080	90.53	-9.74	1.06E-05
21:35	9395.080	90.54	-9.75	1.06E-05
21:45	9405.080	90.54	-9.75	1.06E-05
21:55	9415.080	90.55	-9.76	1.06E-05
22:05	9425.080	90.55	-9.76	1.06E-05
22:15	9435.080	90.56	-9.77	1.07E-05
22:25	9445.080	90.56	-9.77	1.07E-05
22:35	9455.080	90.57	-9.78	1.07E-05
22:45	9465.080	90.57	-9.78	1.07E-05
22:54	9475.020	90.58	-9.79	1.07E-05
23:05	9485.020	90.58	-9.79	1.07E-05
23:14	9495.020	90.59	-9.80	1.07E-05
23:25	9505.020	90.59	-9.80	1.07E-05
23:34	9515.020	90.60	-9.81	1.07E-05
23:45	9525.020	90.60	-9.81	1.08E-05
23:55	9535.020	90.61	-9.82	1.08E-05
00:05	9545.020	90.61	-9.82	1.08E-05
00:15	9555.020	90.62	-9.83	1.08E-05
00:25	9565.030	90.62	-9.83	1.08E-05
00:35	9575.030	90.62	-9.83	1.08E-05
00:44	9585.030	90.63	-9.84	1.08E-05
00:55	9595.030	90.63	-9.84	1.08E-05
01:04	9605.030	90.64	-9.85	1.08E-05
01:15	9615.030	90.64	-9.85	1.09E-05
01:25	9625.030	90.65	-9.86	1.09E-05
01:35	9635.030	90.65	-9.86	1.09E-05
01:45	9645.030	90.66	-9.87	1.09E-05
01:55	9655.030	90.66	-9.87	1.09E-05
02:05	9665.030	90.67	-9.88	1.09E-05
02:14	9675.030	90.67	-9.88	1.09E-05

## ADJUSTED DATA

02:25	9685.030	90.67	-9.88	1.09E-05
02:34	9695.030	90.68	-9.89	1.09E-05
02:45	9705.030	90.69	-9.90	1.10E-05
02:55	9715.030	90.69	-9.90	1.10E-05
03:04	9725.000	90.69	-9.90	1.10E-05
03:15	9735.000	90.70	-9.91	1.10E-05
03:24	9745.000	90.70	-9.91	1.10E-05
03:35	9755.100	90.70	-9.91	1.10E-05
03:44	9765.000	90.71	-9.92	1.10E-05
03:55	9775.000	90.71	-9.92	1.10E-05
04:04	9785.000	90.71	-9.92	1.10E-05
04:15	9795.000	90.72	-9.93	1.11E-05
04:25	9805.000	90.72	-9.93	1.11E-05
04:34	9815.000	90.73	-9.94	1.11E-05
04:45	9825.000	90.73	-9.94	1.11E-05
04:54	9835.000	90.73	-9.94	1.11E-05
05:05	9845.000	90.74	-9.95	1.11E-05
05:14	9855.000	90.74	-9.95	1.11E-05
05:25	9865.000	90.74	-9.95	1.11E-05
05:34	9875.000	90.75	-9.96	1.11E-05
05:45	9885.000	90.75	-9.96	1.12E-05
05:55	9895.000	90.76	-9.97	1.12E-05
06:04	9905.000	90.76	-9.97	1.12E-05
06:15	9915.000	90.76	-9.97	1.12E-05
06:24	9925.000	90.77	-9.98	1.12E-05
06:35	9935.000	90.77	-9.98	1.12E-05
06:44	9945.000	90.78	-9.99	1.12E-05
06:55	9955.000	90.78	-9.99	1.12E-05
07:05	9965.100	90.78	-9.99	1.12E-05
07:15	9975.100	90.79	-10.00	1.13E-05
07:25	9985.100	90.80	-10.01	1.13E-05
07:35	9995.100	90.80	-10.01	1.13E-05
07:45	10005.100	90.80	-10.01	1.13E-05
07:55	10015.100	90.81	-10.02	1.13E-05
08:05	10025.100	90.81	-10.02	1.13E-05
08:15	10035.100	90.82	-10.03	1.13E-05
08:25	10045.100	90.82	-10.03	1.13E-05
08:35	10055.100	90.83	-10.04	1.13E-05
08:45	10065.100	90.84	-10.05	1.14E-05
08:55	10075.000	90.84	-10.05	1.14E-05
09:04	10085.000	90.85	-10.06	1.14E-05
09:15	10095.000	90.85	-10.06	1.14E-05
09:24	10105.000	90.85	-10.06	1.14E-05
09:28	10108.200	90.85	-10.06	1.14E-05

TEST NAME: REI 10-1 RUN # 2  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 3-4 INPUT 4  
 RADIUS: 784.360 FEET  
 START DATE: 07-Oct-86  
 START TIME: 11:10  
 WATER START LEVEL: 80.79 FEET  
 WATER STOP LEVEL: 91.11 FEET  
 TOTAL PUMPING TIME: 10210.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)	t/r2	t/t'
11:10	0.017	-999.99	1091.10	1080.78	1.92E-11	6.01E+05
11:10	0.034	-999.99	1091.10	1080.78	3.84E-11	3.00E+05
11:10	0.050	-999.99	1091.10	1080.78	5.64E-11	2.04E+05
11:10	0.067	-999.99	1091.10	1080.78	7.56E-11	1.52E+05
11:10	0.084	-999.99	1091.10	1080.78	9.48E-11	1.22E+05
11:10	0.100	-999.99	1091.10	1080.78	1.13E-10	1.02E+05
11:10	0.117	-999.99	1091.10	1080.78	1.32E-10	8.73E+04
11:10	0.134	-999.99	1091.10	1080.78	1.51E-10	7.62E+04
11:10	0.150	-999.99	1091.10	1080.78	1.69E-10	6.81E+04
11:10	0.167	-999.99	1091.10	1080.78	1.89E-10	6.11E+04
11:10	0.257	91.11	0.00	10.32	2.90E-10	3.97E+04
11:10	0.341	91.11	0.00	10.32	3.85E-10	2.99E+04
11:10	0.424	91.11	0.00	10.32	4.79E-10	2.41E+04
11:10	0.507	91.11	0.00	10.32	5.72E-10	2.01E+04
11:10	0.591	91.11	0.00	10.32	6.67E-10	1.73E+04
11:10	0.674	91.11	0.00	10.32	7.61E-10	1.52E+04
11:10	0.757	91.11	0.00	10.32	8.54E-10	1.35E+04
11:10	0.841	91.11	0.00	10.32	9.49E-10	1.21E+04
11:10	0.924	91.11	0.00	10.32	1.04E-09	1.11E+04
11:11	1.007	91.11	0.00	10.32	1.14E-09	1.01E+04
11:11	1.413	91.11	0.00	10.32	1.59E-09	7.23E+03
11:11	1.747	91.11	0.00	10.32	1.97E-09	5.85E+03
11:12	2.080	91.11	0.00	10.32	2.35E-09	4.91E+03
11:12	2.413	91.11	0.00	10.32	2.72E-09	4.23E+03
11:12	2.747	91.11	0.00	10.32	3.10E-09	3.72E+03
11:13	3.080	91.11	0.00	10.32	3.48E-09	3.32E+03
11:13	3.413	91.11	0.00	10.32	3.85E-09	2.99E+03
11:13	3.747	91.11	0.00	10.32	4.23E-09	2.73E+03
11:14	4.080	91.11	0.00	10.32	4.61E-09	2.50E+03
11:14	4.413	91.11	0.00	10.32	4.98E-09	2.31E+03
11:14	4.747	91.11	0.00	10.32	5.36E-09	2.15E+03
11:15	5.080	91.11	0.00	10.32	5.73E-09	2.01E+03
11:15	5.413	91.11	0.00	10.32	6.11E-09	1.89E+03
11:15	5.747	91.11	0.00	10.32	6.49E-09	1.78E+03
11:16	6.080	91.11	0.00	10.32	6.86E-09	1.68E+03
11:16	6.413	91.11	0.00	10.32	7.24E-09	1.59E+03
11:16	6.747	91.11	0.00	10.32	7.62E-09	1.51E+03
11:17	7.080	91.11	0.00	10.32	7.99E-09	1.44E+03
11:17	7.413	91.11	0.00	10.32	8.37E-09	1.38E+03
11:17	7.747	91.11	0.00	10.32	8.74E-09	1.32E+03
11:18	8.080	91.11	0.00	10.32	9.12E-09	1.26E+03
11:18	8.413	91.11	0.00	10.32	9.50E-09	1.21E+03

11:18	8.747	91.11	0.00	10.32	9.87E-09	1.17E+03
11:19	9.080	91.11	0.00	10.32	1.02E-08	1.13E+03
11:19	9.413	91.11	0.00	10.32	1.06E-08	1.09E+03
11:19	9.747	91.11	0.00	10.32	1.10E-08	1.05E+03
11:20	10.080	91.11	0.00	10.32	1.14E-08	1.01E+03
11:22	12.115	91.11	0.00	10.32	1.37E-08	8.44E+02
11:24	14.115	91.11	0.00	10.32	1.59E-08	7.24E+02
11:26	16.115	91.11	0.00	10.32	1.82E-08	6.35E+02
11:28	18.115	91.11	0.00	10.32	2.04E-08	5.65E+02
11:30	20.115	91.11	0.00	10.32	2.27E-08	5.09E+02
11:32	22.115	91.11	0.00	10.32	2.50E-08	4.63E+02
11:34	24.115	91.11	0.00	10.32	2.72E-08	4.24E+02
11:36	26.115	91.11	0.00	10.32	2.95E-08	3.92E+02
11:38	28.115	91.11	0.00	10.32	3.17E-08	3.64E+02
11:40	30.115	91.10	0.01	10.31	3.40E-08	3.40E+02
11:42	32.115	91.09	0.02	10.30	3.63E-08	3.19E+02
11:44	34.115	91.09	0.02	10.30	3.85E-08	3.00E+02
11:46	36.115	91.09	0.02	10.30	4.08E-08	2.84E+02
11:48	38.115	91.09	0.02	10.30	4.30E-08	2.69E+02
11:50	40.115	91.08	0.03	10.29	4.53E-08	2.56E+02
11:52	42.115	91.08	0.03	10.29	4.75E-08	2.43E+02
11:54	44.115	91.07	0.04	10.28	4.98E-08	2.32E+02
11:56	46.115	91.07	0.04	10.28	5.21E-08	2.22E+02
11:58	48.115	91.06	0.05	10.27	5.43E-08	2.13E+02
12:00	50.115	91.05	0.06	10.26	5.66E-08	2.05E+02
12:02	52.115	91.04	0.07	10.25	5.88E-08	1.97E+02
12:04	54.115	91.03	0.08	10.24	6.11E-08	1.90E+02
12:06	56.115	91.02	0.09	10.23	6.33E-08	1.83E+02
12:08	58.115	91.01	0.10	10.22	6.56E-08	1.77E+02
12:10	60.115	91.00	0.11	10.21	6.79E-08	1.71E+02
12:12	62.102	91.00	0.11	10.21	7.01E-08	1.65E+02
12:14	64.492	90.98	0.13	10.19	7.28E-08	1.59E+02
12:16	66.188	90.98	0.13	10.19	7.47E-08	1.55E+02
12:18	68.188	90.97	0.14	10.18	7.70E-08	1.51E+02
12:20	70.188	90.96	0.15	10.17	7.92E-08	1.46E+02
12:22	72.188	90.95	0.16	10.16	8.15E-08	1.42E+02
12:24	74.188	90.94	0.17	10.15	8.37E-08	1.39E+02
12:26	76.188	90.93	0.18	10.14	8.60E-08	1.35E+02
12:28	78.188	90.92	0.19	10.13	8.83E-08	1.32E+02
12:30	80.188	90.91	0.20	10.12	9.05E-08	1.28E+02
12:32	82.188	90.89	0.22	10.10	9.28E-08	1.25E+02
12:34	84.188	90.88	0.23	10.09	9.50E-08	1.22E+02
12:36	86.188	90.87	0.24	10.08	9.73E-08	1.19E+02
12:38	88.188	90.86	0.25	10.07	9.95E-08	1.17E+02
12:40	90.188	90.85	0.26	10.06	1.02E-07	1.14E+02
12:42	92.188	90.84	0.27	10.05	1.04E-07	1.12E+02
12:44	94.188	90.83	0.28	10.04	1.06E-07	1.09E+02
12:46	96.188	90.81	0.30	10.02	1.09E-07	1.07E+02
12:48	98.188	90.80	0.31	10.01	1.11E-07	1.05E+02
13:10	120.110	90.66	0.45	9.87	1.36E-07	8.60E+01
13:30	140.110	90.54	0.57	9.75	1.58E-07	7.39E+01
13:50	160.120	90.41	0.70	9.62	1.81E-07	6.48E+01
14:10	180.120	90.29	0.82	9.50	2.03E-07	5.77E+01
14:30	200.120	90.17	0.94	9.38	2.26E-07	5.20E+01
14:50	220.120	90.06	1.05	9.27	2.48E-07	4.74E+01
15:10	240.120	89.94	1.17	9.15	2.71E-07	4.35E+01

15:30	260.120	89.82	1.29	9.03	2.94E-07	4.03E+01
15:50	280.120	89.71	1.40	8.92	3.16E-07	3.75E+01
16:10	300.120	89.60	1.51	8.81	3.39E-07	3.50E+01
16:30	320.050	89.51	1.60	8.72	3.61E-07	3.29E+01
16:49	340.050	89.41	1.70	8.62	3.84E-07	3.10E+01
17:10	360.050	89.32	1.79	8.53	4.06E-07	2.94E+01
17:30	380.050	89.23	1.88	8.44	4.29E-07	2.79E+01
17:50	400.050	89.14	1.97	8.35	4.52E-07	2.65E+01
18:10	420.050	89.05	2.06	8.26	4.74E-07	2.53E+01
18:30	440.050	88.97	2.14	8.18	4.97E-07	2.42E+01
18:50	460.050	88.89	2.22	8.10	5.19E-07	2.32E+01
19:10	480.050	88.81	2.30	8.02	5.42E-07	2.23E+01
19:30	500.050	88.74	2.37	7.95	5.64E-07	2.14E+01
19:49	520.050	88.67	2.44	7.88	5.87E-07	2.06E+01
20:10	540.050	88.60	2.51	7.81	6.10E-07	1.99E+01
20:30	560.050	88.54	2.57	7.75	6.32E-07	1.92E+01
20:50	580.050	88.47	2.64	7.68	6.55E-07	1.86E+01
21:10	600.050	88.41	2.70	7.62	6.77E-07	1.80E+01
21:30	620.050	88.35	2.76	7.56	7.00E-07	1.75E+01
21:50	640.050	88.29	2.82	7.50	7.22E-07	1.70E+01
22:10	660.050	88.23	2.88	7.44	7.45E-07	1.65E+01
22:30	680.050	88.17	2.94	7.38	7.68E-07	1.60E+01
22:49	700.050	88.12	2.99	7.33	7.90E-07	1.56E+01
23:10	720.050	88.06	3.05	7.27	8.13E-07	1.52E+01
23:30	740.050	88.00	3.11	7.21	8.35E-07	1.48E+01
23:50	760.100	87.95	3.16	7.16	8.58E-07	1.44E+01
00:10	780.100	87.90	3.21	7.11	8.81E-07	1.41E+01
00:30	800.100	87.85	3.26	7.06	9.03E-07	1.38E+01
00:50	820.100	87.80	3.31	7.01	9.26E-07	1.35E+01
01:10	840.100	87.75	3.36	6.96	9.48E-07	1.32E+01
01:30	860.100	87.70	3.41	6.91	9.71E-07	1.29E+01
01:50	880.100	87.66	3.45	6.87	9.93E-07	1.26E+01
02:10	900.100	87.61	3.50	6.82	1.02E-06	1.23E+01
02:30	920.100	87.57	3.54	6.78	1.04E-06	1.21E+01
02:50	940.100	87.52	3.59	6.73	1.06E-06	1.19E+01
03:10	960.100	87.48	3.63	6.69	1.08E-06	1.16E+01
03:30	980.100	87.43	3.68	6.64	1.11E-06	1.14E+01
03:50	1000.100	87.39	3.72	6.60	1.13E-06	1.12E+01
04:50	1060.300	87.27	3.84	6.48	1.20E-06	1.06E+01
05:50	1120.300	87.15	3.96	6.36	1.26E-06	1.01E+01
06:50	1180.300	87.04	4.07	6.25	1.33E-06	9.65E+00
07:50	1240.300	86.94	4.17	6.15	1.40E-06	9.23E+00
08:50	1300.300	86.86	4.25	6.07	1.47E-06	8.85E+00
09:50	1360.300	86.77	4.34	5.98	1.54E-06	8.51E+00
10:50	1420.300	86.68	4.43	5.89	1.60E-06	8.19E+00
11:50	1480.300	86.59	4.52	5.80	1.67E-06	7.90E+00
12:50	1540.300	86.50	4.61	5.71	1.74E-06	7.63E+00
13:50	1600.300	86.40	4.71	5.61	1.81E-06	7.38E+00
14:50	1660.300	86.34	4.77	5.55	1.87E-06	7.15E+00
15:50	1720.100	86.24	4.87	5.45	1.94E-06	6.94E+00
16:50	1780.100	86.16	4.95	5.37	2.01E-06	6.74E+00
17:50	1840.100	86.08	5.03	5.29	2.08E-06	6.55E+00
18:50	1900.100	86.01	5.10	5.22	2.14E-06	6.37E+00
19:50	1960.100	85.94	5.17	5.15	2.21E-06	6.21E+00
20:50	2020.100	85.88	5.23	5.09	2.28E-06	6.05E+00
21:50	2080.100	85.82	5.29	5.03	2.35E-06	5.91E+00

22:50	2140.100	85.76	5.35	4.97	2.42E-06	5.77E+00
23:50	2200.100	85.70	5.41	4.91	2.48E-06	5.64E+00
00:50	2260.100	85.63	5.48	4.84	2.55E-06	5.52E+00
01:50	2320.100	85.58	5.53	4.79	2.62E-06	5.40E+00
02:50	2380.100	85.51	5.60	4.72	2.69E-06	5.29E+00
03:50	2440.100	85.46	5.65	4.67	2.75E-06	5.18E+00
04:50	2500.100	85.40	5.71	4.61	2.82E-06	5.08E+00
05:50	2560.100	85.35	5.76	4.56	2.89E-06	4.99E+00
06:50	2620.100	85.29	5.82	4.50	2.96E-06	4.90E+00
07:50	2680.100	85.24	5.87	4.45	3.03E-06	4.81E+00
08:50	2740.200	85.20	5.91	4.41	3.09E-06	4.73E+00
09:50	2800.200	85.16	5.95	4.37	3.16E-06	4.65E+00
10:50	2860.200	85.11	6.00	4.32	3.23E-06	4.57E+00
11:50	2920.100	85.06	6.05	4.27	3.30E-06	4.50E+00
12:50	2980.200	85.01	6.10	4.22	3.36E-06	4.43E+00
13:50	3040.200	84.94	6.17	4.15	3.43E-06	4.36E+00
14:50	3100.200	84.91	6.20	4.12	3.50E-06	4.29E+00
15:50	3160.200	84.84	6.27	4.05	3.57E-06	4.23E+00
16:50	3220.200	84.80	6.31	4.01	3.63E-06	4.17E+00
17:50	3280.200	84.75	6.36	3.96	3.70E-06	4.11E+00
18:50	3340.200	84.71	6.40	3.92	3.77E-06	4.06E+00
19:50	3400.200	84.67	6.44	3.88	3.84E-06	4.00E+00
20:50	3460.200	84.63	6.48	3.84	3.91E-06	3.95E+00
21:50	3520.200	84.60	6.51	3.81	3.97E-06	3.90E+00
22:50	3580.200	84.56	6.55	3.77	4.04E-06	3.85E+00
23:50	3640.200	84.53	6.58	3.74	4.11E-06	3.80E+00
00:50	3700.200	84.49	6.62	3.70	4.18E-06	3.76E+00
01:50	3760.200	84.45	6.66	3.66	4.24E-06	3.72E+00
02:50	3820.200	84.41	6.70	3.62	4.31E-06	3.67E+00
03:50	3880.200	84.37	6.74	3.58	4.38E-06	3.63E+00
04:50	3940.200	84.33	6.78	3.54	4.45E-06	3.59E+00
05:50	4000.200	84.29	6.82	3.50	4.52E-06	3.55E+00
06:50	4060.200	84.26	6.85	3.47	4.58E-06	3.51E+00
07:50	4120.200	84.22	6.89	3.43	4.65E-06	3.48E+00
08:50	4180.200	84.20	6.91	3.41	4.72E-06	3.44E+00
09:50	4240.200	84.18	6.93	3.39	4.79E-06	3.41E+00
10:50	4300.200	-999.99	1091.10	1080.78	4.85E-06	3.37E+00
11:04	4314.800	-999.99	1091.10	1080.78	4.87E-06	3.37E+00

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 10-1 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 7 INPUT 5  
 RADIUS: 1012.704 FEET  
 START DATE : 07-Oct-86  
 START TIME : 09:00  
 WATER START LEVEL: 80.33 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r2
09:00	0.000	80.33	0.00	0.00E+00
09:00	0.017	-99.99	180.32	1.15E-11
09:00	0.034	-99.99	180.32	2.30E-11
09:00	0.050	-99.99	180.32	3.39E-11
09:00	0.067	-99.99	180.32	4.54E-11
09:00	0.084	-99.99	180.32	5.69E-11
09:00	0.100	-99.99	180.32	6.77E-11
09:00	0.117	-99.99	180.32	7.92E-11
09:00	0.134	-99.99	180.32	9.07E-11
09:00	0.150	-99.99	180.32	1.02E-10
09:00	0.167	-99.99	180.32	1.13E-10
09:00	0.257	80.33	0.00	1.74E-10
09:00	0.340	80.33	0.00	2.30E-10
09:00	0.424	80.33	0.00	2.87E-10
09:00	0.507	80.33	0.00	3.43E-10
09:00	0.590	80.33	0.00	4.00E-10
09:00	0.674	80.33	0.00	4.56E-10
09:00	0.757	80.33	0.00	5.13E-10
09:00	0.840	80.33	0.00	5.69E-10
09:00	0.924	80.33	0.00	6.26E-10
09:01	1.007	80.33	0.00	6.82E-10
09:01	1.414	80.33	0.00	9.57E-10
09:01	1.748	80.33	0.00	1.18E-09
09:02	2.081	80.33	0.00	1.41E-09
09:02	2.414	80.33	0.00	1.63E-09
09:02	2.748	80.33	0.00	1.86E-09
09:03	3.081	80.33	0.00	2.09E-09
09:03	3.415	80.33	0.00	2.31E-09
09:03	3.748	80.33	0.00	2.54E-09
09:04	4.081	80.33	0.00	2.76E-09
09:04	4.414	80.33	0.00	2.99E-09
09:04	4.748	80.33	0.00	3.22E-09
09:05	5.081	80.33	0.00	3.44E-09
09:05	5.414	80.33	0.00	3.67E-09
09:05	5.748	80.33	0.00	3.89E-09
09:06	6.081	80.33	0.00	4.12E-09
09:06	6.415	80.33	0.00	4.34E-09
09:06	6.748	80.33	0.00	4.57E-09
09:07	7.081	80.33	0.00	4.79E-09
09:07	7.415	80.33	0.00	5.02E-09
09:07	7.748	80.33	0.00	5.25E-09



09:08	8.081	80.33	0.00	5.47E-09
09:08	8.415	80.33	0.00	5.70E-09
09:08	8.748	80.33	0.00	5.92E-09
09:09	9.081	80.33	0.00	6.15E-09
09:09	9.414	80.33	0.00	6.37E-09
09:09	9.748	80.33	0.00	6.60E-09
09:10	10.081	80.33	0.00	6.83E-09
09:12	12.108	80.33	0.00	8.20E-09
09:14	14.152	80.33	0.00	9.58E-09
09:16	16.152	80.33	0.00	1.09E-08
09:18	18.152	80.33	0.00	1.23E-08
09:20	20.152	80.33	0.00	1.36E-08
09:22	22.152	80.33	0.00	1.50E-08
09:24	24.152	80.33	0.00	1.64E-08
09:26	26.152	80.33	0.00	1.77E-08
09:28	28.215	80.33	0.00	1.91E-08
09:30	30.197	80.33	0.00	2.04E-08
09:32	32.197	80.33	0.00	2.18E-08
09:34	34.197	80.34	-0.01	2.32E-08
09:36	36.197	80.34	-0.01	2.45E-08
09:38	38.197	80.34	-0.01	2.59E-08
09:40	40.197	80.33	0.00	2.72E-08
09:42	42.197	80.34	-0.01	2.86E-08
09:44	44.197	80.34	-0.01	2.99E-08
09:46	46.197	80.34	-0.01	3.13E-08
09:48	48.197	80.34	-0.01	3.26E-08
09:50	50.197	80.34	-0.01	3.40E-08
09:52	52.197	80.34	-0.01	3.53E-08
09:54	54.197	80.34	-0.01	3.67E-08
09:56	56.217	80.34	-0.01	3.81E-08
09:58	58.100	80.34	-0.01	3.93E-08
10:00	60.245	80.34	-0.01	4.08E-08
10:02	62.245	80.34	-0.01	4.21E-08
10:04	64.245	80.34	-0.01	4.35E-08
10:06	66.245	80.34	-0.01	4.49E-08
10:08	68.245	80.34	-0.01	4.62E-08
10:10	70.245	80.34	-0.01	4.76E-08
10:12	72.245	80.34	-0.01	4.89E-08
10:14	74.245	80.34	-0.01	5.03E-08
10:16	76.245	80.34	-0.01	5.16E-08
10:18	78.245	80.34	-0.01	5.30E-08
10:20	80.245	80.34	-0.01	5.43E-08
10:22	82.245	80.34	-0.01	5.57E-08
10:24	84.245	80.34	-0.01	5.70E-08
10:26	86.245	80.34	-0.01	5.84E-08
10:28	88.245	80.34	-0.01	5.98E-08
10:30	90.245	80.34	-0.01	6.11E-08
10:32	92.245	80.34	-0.01	6.25E-08
10:34	94.245	80.34	-0.01	6.38E-08
10:36	96.245	80.34	-0.01	6.52E-08
10:38	98.245	80.34	-0.01	6.65E-08
11:00	120.210	80.34	-0.01	8.14E-08
11:20	140.210	80.35	-0.02	9.49E-08
11:40	160.210	80.35	-0.02	1.08E-07
12:00	180.220	80.35	-0.02	1.22E-07
12:20	200.220	80.35	-0.02	1.36E-07

12:40	220.220	80.35	-0.02	1.49E-07
13:00	240.220	80.36	-0.03	1.63E-07
13:20	260.220	80.36	-0.03	1.76E-07
13:40	280.230	80.37	-0.04	1.90E-07
14:00	300.230	80.37	-0.04	2.03E-07
14:20	320.230	80.37	-0.04	2.17E-07
14:40	340.180	80.38	-0.05	2.30E-07
15:00	360.100	80.38	-0.05	2.44E-07
15:20	380.100	80.39	-0.06	2.57E-07
15:40	400.100	80.39	-0.06	2.71E-07
16:00	420.170	80.39	-0.06	2.85E-07
16:20	440.250	80.40	-0.07	2.98E-07
16:40	460.200	80.40	-0.07	3.12E-07
17:00	480.170	80.41	-0.08	3.25E-07
17:20	500.170	80.41	-0.08	3.39E-07
17:40	520.130	80.42	-0.09	3.52E-07
18:00	540.120	80.43	-0.10	3.66E-07
18:20	560.220	80.43	-0.10	3.79E-07
18:40	580.080	80.44	-0.11	3.93E-07
19:00	600.220	80.45	-0.12	4.06E-07
19:20	620.230	80.45	-0.12	4.20E-07
19:40	640.220	80.47	-0.14	4.34E-07
20:00	660.220	80.47	-0.14	4.47E-07
20:20	680.130	80.48	-0.15	4.61E-07
20:40	700.120	80.49	-0.16	4.74E-07
21:00	720.230	80.49	-0.16	4.88E-07
21:20	740.300	80.51	-0.18	5.01E-07
21:40	760.230	80.51	-0.18	5.15E-07
22:00	780.230	80.52	-0.19	5.28E-07
22:20	800.230	80.53	-0.20	5.42E-07
22:40	820.180	80.54	-0.21	5.55E-07
23:00	840.570	80.55	-0.22	5.69E-07
23:20	860.180	80.56	-0.23	5.82E-07
23:40	880.080	80.57	-0.24	5.96E-07
00:00	900.170	80.58	-0.25	6.10E-07
00:20	920.170	80.59	-0.26	6.23E-07
00:40	940.170	80.60	-0.27	6.37E-07
01:00	960.170	80.61	-0.28	6.50E-07
01:20	980.170	80.62	-0.29	6.64E-07
01:40	1000.200	80.63	-0.30	6.77E-07
02:40	1060.300	80.65	-0.32	7.18E-07
03:40	1120.300	80.68	-0.35	7.59E-07
04:40	1180.300	80.71	-0.38	7.99E-07
05:40	1240.300	80.73	-0.40	8.40E-07
06:40	1300.300	80.76	-0.43	8.80E-07
07:40	1360.200	80.79	-0.46	9.21E-07
08:40	1420.200	80.81	-0.48	9.62E-07
09:40	1480.200	80.84	-0.51	1.00E-06
10:40	1540.200	80.86	-0.53	1.04E-06
11:40	1600.300	80.88	-0.55	1.08E-06
12:40	1660.300	80.89	-0.56	1.12E-06
13:40	1720.200	80.89	-0.56	1.16E-06
14:40	1780.300	80.90	-0.57	1.21E-06
15:40	1840.300	80.92	-0.59	1.25E-06
16:40	1900.300	80.92	-0.59	1.29E-06
17:40	1960.200	80.94	-0.61	1.33E-06

18:40	2020.200	80.97	-0.64	1.37E-06
19:40	2080.200	80.99	-0.66	1.41E-06
20:40	2140.200	81.02	-0.69	1.45E-06
21:40	2200.300	81.05	-0.72	1.49E-06
22:40	2260.300	81.07	-0.74	1.53E-06
23:40	2320.200	81.10	-0.77	1.57E-06
00:40	2380.200	81.12	-0.79	1.61E-06
01:40	2440.200	81.14	-0.81	1.65E-06
02:40	2500.200	81.17	-0.84	1.69E-06
03:40	2560.200	81.19	-0.86	1.73E-06
04:40	2620.200	81.21	-0.88	1.77E-06
05:40	2680.200	81.23	-0.90	1.81E-06
06:40	2740.200	81.26	-0.93	1.86E-06
07:40	2800.200	81.27	-0.94	1.90E-06
08:40	2860.300	81.30	-0.97	1.94E-06
09:40	2920.300	81.32	-0.99	1.98E-06
10:40	2980.300	81.34	-1.01	2.02E-06
11:40	3040.200	81.36	-1.03	2.06E-06
12:40	3100.200	81.39	-1.06	2.10E-06
13:40	3160.300	81.41	-1.08	2.14E-06
14:40	3220.300	81.43	-1.10	2.18E-06
15:40	3280.200	81.45	-1.12	2.22E-06
16:40	3340.200	81.47	-1.14	2.26E-06
17:40	3400.300	81.49	-1.16	2.30E-06
18:40	3460.300	81.51	-1.18	2.34E-06
19:40	3520.300	81.53	-1.20	2.38E-06
20:40	3580.200	81.55	-1.22	2.42E-06
21:40	3640.200	81.57	-1.24	2.46E-06
22:40	3700.200	81.59	-1.26	2.51E-06
23:40	3760.200	81.61	-1.28	2.55E-06
00:40	3820.200	81.63	-1.30	2.59E-06
01:40	3880.200	81.65	-1.32	2.63E-06
02:40	3940.200	81.67	-1.34	2.67E-06
03:40	4000.200	81.68	-1.35	2.71E-06
04:40	4060.200	81.70	-1.37	2.75E-06
05:40	4120.200	81.72	-1.39	2.79E-06
06:40	4180.200	81.74	-1.41	2.83E-06
07:40	4240.300	81.76	-1.43	2.87E-06
08:40	4300.300	81.78	-1.45	2.91E-06
09:40	4360.700	81.80	-1.47	2.95E-06
10:40	4420.300	81.82	-1.49	2.99E-06
11:40	4480.300	81.84	-1.51	3.03E-06
12:40	4540.300	81.86	-1.53	3.07E-06
13:40	4600.300	81.87	-1.54	3.12E-06
14:40	4660.300	81.89	-1.56	3.16E-06
15:40	4720.300	81.90	-1.57	3.20E-06
16:40	4780.300	81.92	-1.59	3.24E-06
17:40	4840.300	81.91	-1.58	3.28E-06
18:40	4900.300	81.93	-1.60	3.32E-06
19:40	4960.300	81.95	-1.62	3.36E-06
20:40	5020.300	81.97	-1.64	3.40E-06
21:40	5080.300	81.99	-1.66	3.44E-06
22:40	5140.300	82.00	-1.67	3.48E-06
23:40	5200.300	82.02	-1.69	3.52E-06
00:40	5260.300	82.03	-1.70	3.56E-06
01:40	5320.300	82.05	-1.72	3.60E-06

02:40	5380.300	82.06	-1.73	3.64E-06
03:40	5440.300	82.07	-1.74	3.68E-06
04:40	5500.300	82.09	-1.76	3.72E-06
05:40	5560.300	82.10	-1.77	3.77E-06
06:40	5620.300	82.11	-1.78	3.81E-06
07:40	5680.300	82.14	-1.81	3.85E-06
08:40	5740.300	82.15	-1.82	3.89E-06
09:40	5800.300	82.17	-1.84	3.93E-06
10:40	5860.300	82.19	-1.86	3.97E-06
11:40	5920.300	82.20	-1.87	4.01E-06
12:40	5980.300	82.20	-1.87	4.05E-06
13:40	6040.300	82.22	-1.89	4.09E-06
14:40	6100.300	82.22	-1.89	4.13E-06
15:40	6160.500	82.23	-1.90	4.17E-06
16:40	6220.300	82.24	-1.91	4.21E-06
17:40	6280.300	82.25	-1.92	4.25E-06
18:40	6340.300	82.26	-1.93	4.29E-06
19:40	6400.400	82.27	-1.94	4.33E-06
20:40	6460.200	82.28	-1.95	4.37E-06
21:40	6520.200	82.29	-1.96	4.42E-06
22:40	6580.300	82.31	-1.98	4.46E-06
23:40	6640.300	82.32	-1.99	4.50E-06
00:40	6700.300	82.33	-2.00	4.54E-06
01:40	6760.300	82.32	-1.99	4.58E-06
02:40	6820.300	82.36	-2.03	4.62E-06
03:40	6880.300	82.37	-2.04	4.66E-06
04:40	6940.300	82.38	-2.05	4.70E-06
05:40	7000.300	82.39	-2.06	4.74E-06
06:40	7060.300	82.41	-2.08	4.78E-06
07:40	7120.300	82.41	-2.08	4.82E-06
08:40	7180.300	82.36	-2.03	4.86E-06
09:40	7240.300	82.29	-1.96	4.90E-06
10:40	7300.300	82.24	-1.91	4.94E-06
11:40	7360.300	82.13	-1.80	4.98E-06
12:40	7420.300	82.18	-1.85	5.02E-06
13:40	7480.300	82.21	-1.88	5.07E-06
14:40	7540.300	82.27	-1.94	5.11E-06
15:40	7600.300	82.26	-1.93	5.15E-06
16:40	7660.300	82.26	-1.93	5.19E-06
17:40	7720.300	82.26	-1.93	5.23E-06
18:40	7780.200	82.15	-1.82	5.27E-06
19:40	7840.200	82.12	-1.79	5.31E-06
20:40	7900.300	82.14	-1.81	5.35E-06
21:40	7960.300	82.07	-1.74	5.39E-06
22:40	8020.300	82.02	-1.69	5.43E-06
23:40	8080.300	81.94	-1.61	5.47E-06
00:40	8140.300	81.87	-1.54	5.51E-06
01:40	8200.300	81.83	-1.50	5.55E-06
02:40	8260.300	81.87	-1.54	5.59E-06
03:40	8320.300	81.84	-1.51	5.63E-06
04:40	8380.300	81.82	-1.49	5.67E-06
05:40	8440.300	81.82	-1.49	5.72E-06
06:40	8500.300	81.87	-1.54	5.76E-06
07:40	8560.200	81.92	-1.59	5.80E-06
08:40	8620.300	81.90	-1.57	5.84E-06
09:00	8640.600	81.90	-1.57	5.85E-06

## ADJUSTED DATA

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 10-1 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 7 INPUT 5  
 RADIUS: 1012.704 FEET  
 START DATE : 13-Oct-86  
 START TIME : 10:25  
 WATER START LEVEL: 80.33 FEET

TIME	E.T. (MIN)	LEVEL	Delta H	t/r <sup>2</sup>
10:25	8725.000	81.92	-1.59	5.91E-06
10:35	8735.071	81.93	-1.60	5.91E-06
10:45	8745.070	81.93	-1.60	5.92E-06
10:55	8755.072	81.92	-1.59	5.93E-06
11:05	8765.072	81.90	-1.57	5.94E-06
11:15	8775.072	81.88	-1.55	5.94E-06
11:25	8785.072	81.93	-1.60	5.95E-06
11:35	8795.072	81.95	-1.62	5.96E-06
11:45	8805.072	81.97	-1.64	5.96E-06
11:55	8815.102	81.98	-1.65	5.97E-06
12:05	8825.090	81.98	-1.65	5.98E-06
12:15	8835.090	82.01	-1.68	5.98E-06
12:25	8845.090	82.01	-1.68	5.99E-06
12:35	8855.090	82.04	-1.71	6.00E-06
12:45	8865.090	82.05	-1.72	6.00E-06
12:55	8875.120	82.08	-1.75	6.01E-06
13:04	8884.970	82.06	-1.73	6.02E-06
13:14	8894.970	82.08	-1.75	6.02E-06
13:25	8904.970	82.11	-1.78	6.03E-06
13:34	8914.970	82.14	-1.81	6.04E-06
13:45	8924.970	82.15	-1.82	6.04E-06
13:54	8934.970	82.17	-1.84	6.05E-06
14:05	8944.970	82.16	-1.83	6.06E-06
14:14	8955.020	82.18	-1.85	6.06E-06
14:25	8965.080	82.20	-1.87	6.07E-06
14:35	8975.080	82.22	-1.89	6.08E-06
14:45	8985.080	82.23	-1.90	6.08E-06
14:55	8995.080	82.25	-1.92	6.09E-06
15:05	9005.080	82.27	-1.94	6.10E-06
15:15	9015.080	82.28	-1.95	6.10E-06
15:25	9025.080	82.29	-1.96	6.11E-06
15:35	9035.080	82.29	-1.96	6.12E-06
15:45	9045.080	82.30	-1.97	6.12E-06
15:55	9055.080	82.30	-1.97	6.13E-06
16:04	9065.020	82.31	-1.98	6.14E-06
16:15	9075.020	82.32	-1.99	6.14E-06
16:25	9084.970	82.32	-1.99	6.15E-06
16:35	9095.080	82.33	-2.00	6.16E-06
16:45	9105.080	82.33	-2.00	6.17E-06
16:55	9115.080	82.35	-2.02	6.17E-06

## ADJUSTED DATA

17:05	9125.080	82.36	-2.03	6.18E-06
17:15	9135.080	82.35	-2.02	6.19E-06
17:25	9145.080	82.35	-2.02	6.19E-06
17:35	9155.080	82.33	-2.00	6.20E-06
17:45	9165.080	82.32	-1.99	6.21E-06
17:55	9175.080	82.34	-2.01	6.21E-06
18:05	9185.080	82.33	-2.00	6.22E-06
18:15	9195.080	82.33	-2.00	6.23E-06
18:25	9205.080	82.32	-1.99	6.23E-06
18:35	9215.080	82.31	-1.98	6.24E-06
18:45	9225.080	82.31	-1.98	6.25E-06
18:55	9235.080	82.30	-1.97	6.25E-06
19:05	9245.080	82.30	-1.97	6.26E-06
19:15	9255.080	82.29	-1.96	6.27E-06
19:25	9265.080	82.29	-1.96	6.27E-06
19:35	9275.070	82.29	-1.96	6.28E-06
19:45	9285.080	82.28	-1.95	6.29E-06
19:55	9295.080	82.29	-1.96	6.29E-06
20:05	9305.080	82.28	-1.95	6.30E-06
20:15	9315.080	82.28	-1.95	6.31E-06
20:25	9325.080	82.28	-1.95	6.31E-06
20:35	9335.080	82.28	-1.95	6.32E-06
20:45	9345.080	82.28	-1.95	6.33E-06
20:55	9355.080	82.27	-1.94	6.33E-06
21:05	9365.080	82.26	-1.93	6.34E-06
21:15	9375.080	82.26	-1.93	6.35E-06
21:25	9385.080	82.26	-1.93	6.35E-06
21:35	9395.080	82.26	-1.93	6.36E-06
21:45	9405.080	82.26	-1.93	6.37E-06
21:55	9415.080	82.26	-1.93	6.38E-06
22:05	9425.080	82.26	-1.93	6.38E-06
22:15	9435.080	82.25	-1.92	6.39E-06
22:25	9445.080	82.25	-1.92	6.40E-06
22:35	9455.080	82.25	-1.92	6.40E-06
22:45	9465.080	82.24	-1.91	6.41E-06
22:54	9475.020	82.23	-1.90	6.42E-06
23:05	9485.020	82.23	-1.90	6.42E-06
23:14	9495.020	82.22	-1.89	6.43E-06
23:25	9505.020	82.21	-1.88	6.44E-06
23:34	9515.020	82.21	-1.88	6.44E-06
23:45	9525.020	82.21	-1.88	6.45E-06
23:55	9535.020	82.21	-1.88	6.46E-06
00:05	9545.020	82.21	-1.88	6.46E-06
00:15	9555.020	82.21	-1.88	6.47E-06
00:25	9565.030	82.21	-1.88	6.48E-06
00:35	9575.030	82.21	-1.88	6.48E-06
00:44	9585.030	82.20	-1.87	6.49E-06
00:55	9595.030	82.20	-1.87	6.50E-06
01:04	9605.030	82.21	-1.88	6.50E-06
01:15	9615.030	82.21	-1.88	6.51E-06
01:25	9625.030	82.21	-1.88	6.52E-06
01:35	9635.030	82.20	-1.87	6.52E-06
01:45	9645.030	82.20	-1.87	6.53E-06
01:55	9655.030	82.20	-1.87	6.54E-06
02:05	9665.030	82.20	-1.87	6.54E-06
02:14	9675.030	82.20	-1.87	6.55E-06

## ADJUSTED DATA

02:25	9685.030	82.20	-1.87	6.56E-06
02:34	9695.030	82.20	-1.87	6.56E-06
02:45	9705.030	82.20	-1.87	6.57E-06
02:55	9715.030	82.21	-1.88	6.58E-06
03:04	9725.000	82.21	-1.88	6.59E-06
03:15	9735.000	82.21	-1.88	6.59E-06
03:24	9745.000	82.21	-1.88	6.60E-06
03:35	9755.100	82.21	-1.88	6.61E-06
03:44	9765.000	82.20	-1.87	6.61E-06
03:55	9775.000	82.20	-1.87	6.62E-06
04:04	9785.000	82.19	-1.86	6.63E-06
04:15	9795.000	82.19	-1.86	6.63E-06
04:25	9805.000	82.18	-1.85	6.64E-06
04:34	9815.000	82.17	-1.84	6.65E-06
04:45	9825.000	82.16	-1.83	6.65E-06
04:54	9835.000	82.15	-1.82	6.66E-06
05:05	9845.000	82.15	-1.82	6.67E-06
05:14	9855.000	82.14	-1.81	6.67E-06
05:25	9865.000	82.14	-1.81	6.68E-06
05:34	9875.000	82.13	-1.80	6.69E-06
05:45	9885.000	82.13	-1.80	6.69E-06
05:55	9895.000	82.12	-1.79	6.70E-06
06:04	9905.000	82.12	-1.79	6.71E-06
06:15	9915.000	82.12	-1.79	6.71E-06
06:24	9925.000	82.11	-1.78	6.72E-06
06:35	9935.000	82.11	-1.78	6.73E-06
06:44	9945.000	82.11	-1.78	6.73E-06
06:55	9955.000	82.10	-1.77	6.74E-06
07:05	9965.100	82.10	-1.77	6.75E-06
07:15	9975.100	82.10	-1.77	6.75E-06
07:25	9985.100	82.10	-1.77	6.76E-06
07:35	9995.100	82.11	-1.78	6.77E-06
07:45	10005.100	82.18	-1.85	6.77E-06
07:55	10015.100	82.16	-1.83	6.78E-06
08:05	10025.100	82.15	-1.82	6.79E-06
08:15	10035.100	82.15	-1.82	6.80E-06
08:25	10045.100	82.16	-1.83	6.80E-06
08:35	10055.100	82.17	-1.84	6.81E-06
08:45	10065.100	82.19	-1.86	6.82E-06
08:55	10075.000	82.20	-1.87	6.82E-06
09:04	10085.000	82.22	-1.89	6.83E-06
09:15	10095.000	82.24	-1.91	6.84E-06
09:24	10105.000	82.27	-1.94	6.84E-06
09:28	10108.200	82.28	-1.95	6.84E-06

TEST NAME: REI 10-1 RUN # 2  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 7 INPUT 5  
 RADIUS: 1012.704 FEET  
 START DATE: 07-Oct-86  
 START TIME: 11:10  
 WATER START LEVEL: 80.33 FEET  
 WATER STOP LEVEL: 83.05 FEET  
 TOTAL PUMPING TIME: 10210.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)	t/r2	t/t
11:10	0.017	-999.99	1083.04	1080.32	1.15E-11	6.01E+05
11:10	0.034	-999.99	1083.04	1080.32	2.30E-11	3.00E+05
11:10	0.050	-999.99	1083.04	1080.32	3.39E-11	2.04E+05
11:10	0.067	-999.99	1083.04	1080.32	4.54E-11	1.52E+05
11:10	0.084	-999.99	1083.04	1080.32	5.69E-11	1.22E+05
11:10	0.100	-999.99	1083.04	1080.32	6.77E-11	1.02E+05
11:10	0.117	-999.99	1083.04	1080.32	7.92E-11	8.73E+04
11:10	0.134	-999.99	1083.04	1080.32	9.07E-11	7.62E+04
11:10	0.150	-999.99	1083.04	1080.32	1.02E-10	6.81E+04
11:10	0.167	-999.99	1083.04	1080.32	1.13E-10	6.11E+04
11:10	0.257	83.05	0.00	2.72	1.74E-10	3.97E+04
11:10	0.341	83.05	0.00	2.72	2.31E-10	2.99E+04
11:10	0.424	83.05	0.00	2.72	2.87E-10	2.41E+04
11:10	0.507	83.05	0.00	2.72	3.43E-10	2.01E+04
11:10	0.591	83.05	0.00	2.72	4.00E-10	1.73E+04
11:10	0.674	83.05	0.00	2.72	4.56E-10	1.52E+04
11:10	0.757	83.05	0.00	2.72	5.13E-10	1.35E+04
11:10	0.841	83.05	0.00	2.72	5.69E-10	1.21E+04
11:10	0.924	83.05	0.00	2.72	6.26E-10	1.11E+04
11:11	1.007	83.05	0.00	2.72	6.82E-10	1.01E+04
11:11	1.413	83.06	-0.01	2.73	9.57E-10	7.23E+03
11:11	1.747	83.06	-0.01	2.73	1.18E-09	5.85E+03
11:12	2.080	83.06	-0.01	2.73	1.41E-09	4.91E+03
11:12	2.413	83.06	-0.01	2.73	1.63E-09	4.23E+03
11:12	2.747	83.07	-0.02	2.74	1.86E-09	3.72E+03
11:13	3.080	83.07	-0.02	2.74	2.09E-09	3.32E+03
11:13	3.413	83.07	-0.02	2.74	2.31E-09	2.99E+03
11:13	3.747	83.08	-0.03	2.75	2.54E-09	2.73E+03
11:14	4.080	83.08	-0.03	2.75	2.76E-09	2.50E+03
11:14	4.413	83.08	-0.03	2.75	2.99E-09	2.31E+03
11:14	4.747	83.09	-0.04	2.76	3.21E-09	2.15E+03
11:15	5.080	83.09	-0.04	2.76	3.44E-09	2.01E+03
11:15	5.413	83.09	-0.04	2.76	3.67E-09	1.89E+03
11:15	5.747	83.09	-0.04	2.76	3.89E-09	1.78E+03
11:16	6.080	83.10	-0.05	2.77	4.12E-09	1.68E+03
11:16	6.413	83.10	-0.05	2.77	4.34E-09	1.59E+03
11:16	6.747	83.10	-0.05	2.77	4.57E-09	1.51E+03
11:17	7.080	83.10	-0.05	2.77	4.79E-09	1.44E+03
11:17	7.413	83.11	-0.06	2.78	5.02E-09	1.38E+03
11:17	7.747	83.11	-0.06	2.78	5.25E-09	1.32E+03
11:18	8.080	83.11	-0.06	2.78	5.47E-09	1.26E+03
11:18	8.413	83.11	-0.06	2.78	5.70E-09	1.21E+03



11:18	8.747	83.11	-0.06	2.78	5.92E-09	1.17E+03
11:19	9.080	83.11	-0.06	2.78	6.15E-09	1.13E+03
11:19	9.413	83.12	-0.07	2.79	6.37E-09	1.09E+03
11:19	9.747	83.12	-0.07	2.79	6.60E-09	1.05E+03
11:20	10.080	83.12	-0.07	2.79	6.83E-09	1.01E+03
11:22	12.115	83.13	-0.08	2.80	8.20E-09	8.44E+02
11:24	14.115	83.15	-0.10	2.82	9.56E-09	7.24E+02
11:26	16.115	83.17	-0.12	2.84	1.09E-08	6.35E+02
11:28	18.115	83.18	-0.13	2.85	1.23E-08	5.65E+02
11:30	20.115	83.20	-0.15	2.87	1.36E-08	5.09E+02
11:32	22.115	83.22	-0.17	2.89	1.50E-08	4.63E+02
11:34	24.115	83.24	-0.19	2.91	1.63E-08	4.24E+02
11:36	26.115	83.26	-0.21	2.93	1.77E-08	3.92E+02
11:38	28.115	83.27	-0.22	2.94	1.90E-08	3.64E+02
11:40	30.115	83.28	-0.23	2.95	2.04E-08	3.40E+02
11:42	32.115	83.28	-0.23	2.95	2.17E-08	3.19E+02
11:44	34.115	83.29	-0.24	2.96	2.31E-08	3.00E+02
11:46	36.115	83.30	-0.25	2.97	2.45E-08	2.84E+02
11:48	38.115	83.32	-0.27	2.99	2.58E-08	2.69E+02
11:50	40.115	83.32	-0.27	2.99	2.72E-08	2.56E+02
11:52	42.115	83.35	-0.30	3.02	2.85E-08	2.43E+02
11:54	44.115	83.36	-0.31	3.03	2.99E-08	2.32E+02
11:56	46.115	83.38	-0.33	3.05	3.12E-08	2.22E+02
11:58	48.115	83.39	-0.34	3.06	3.26E-08	2.13E+02
12:00	50.115	83.40	-0.35	3.07	3.39E-08	2.05E+02
12:02	52.115	83.41	-0.36	3.08	3.53E-08	1.97E+02
12:04	54.115	83.41	-0.36	3.08	3.66E-08	1.90E+02
12:06	56.115	83.43	-0.38	3.10	3.80E-08	1.83E+02
12:08	58.115	83.44	-0.39	3.11	3.94E-08	1.77E+02
12:10	60.115	83.45	-0.40	3.12	4.07E-08	1.71E+02
12:12	62.102	83.47	-0.42	3.14	4.21E-08	1.65E+02
12:14	64.492	83.49	-0.44	3.16	4.37E-08	1.59E+02
12:16	66.188	83.50	-0.45	3.17	4.48E-08	1.55E+02
12:18	68.188	83.51	-0.46	3.18	4.62E-08	1.51E+02
12:20	70.188	83.52	-0.47	3.19	4.75E-08	1.46E+02
12:22	72.188	83.54	-0.49	3.21	4.89E-08	1.42E+02
12:24	74.188	83.56	-0.51	3.23	5.02E-08	1.39E+02
12:26	76.188	83.57	-0.52	3.24	5.16E-08	1.35E+02
12:28	78.188	83.58	-0.53	3.25	5.29E-08	1.32E+02
12:30	80.188	83.59	-0.54	3.26	5.43E-08	1.28E+02
12:32	82.188	83.60	-0.55	3.27	5.57E-08	1.25E+02
12:34	84.188	83.61	-0.56	3.28	5.70E-08	1.22E+02
12:36	86.188	83.62	-0.57	3.29	5.84E-08	1.19E+02
12:38	88.188	83.64	-0.59	3.31	5.97E-08	1.17E+02
12:40	90.188	83.66	-0.61	3.33	6.11E-08	1.14E+02
12:42	92.188	83.67	-0.62	3.34	6.24E-08	1.12E+02
12:44	94.188	83.68	-0.63	3.35	6.38E-08	1.09E+02
12:46	96.188	83.68	-0.63	3.35	6.51E-08	1.07E+02
12:48	98.188	83.69	-0.64	3.36	6.65E-08	1.05E+02
13:10	120.110	83.75	-0.70	3.42	8.13E-08	8.60E+01
13:30	140.110	83.79	-0.74	3.46	9.49E-08	7.39E+01
13:50	160.120	83.79	-0.74	3.46	1.08E-07	6.48E+01
14:10	180.120	83.93	-0.88	3.60	1.22E-07	5.77E+01
14:30	200.120	83.46	-0.41	3.13	1.36E-07	5.20E+01
14:50	220.120	83.16	-0.11	2.83	1.49E-07	4.74E+01
15:10	240.120	83.13	-0.08	2.80	1.63E-07	4.35E+01

15:30	260.120	83.12	-0.07	2.79	1.76E-07	4.03E+01
15:50	280.120	83.12	-0.07	2.79	1.90E-07	3.75E+01
16:10	300.120	83.11	-0.06	2.78	2.03E-07	3.50E+01
16:30	320.050	83.11	-0.06	2.78	2.17E-07	3.29E+01
16:49	340.050	83.10	-0.05	2.77	2.30E-07	3.10E+01
17:10	360.050	83.09	-0.04	2.76	2.44E-07	2.94E+01
17:30	380.050	83.09	-0.04	2.76	2.57E-07	2.79E+01
17:50	400.050	83.09	-0.04	2.76	2.71E-07	2.65E+01
18:10	420.050	83.08	-0.03	2.75	2.84E-07	2.53E+01
18:30	440.050	83.08	-0.03	2.75	2.98E-07	2.42E+01
18:50	460.050	83.08	-0.03	2.75	3.12E-07	2.32E+01
19:10	480.050	83.08	-0.03	2.75	3.25E-07	2.23E+01
19:30	500.050	83.08	-0.03	2.75	3.39E-07	2.14E+01
19:49	520.050	83.08	-0.03	2.75	3.52E-07	2.06E+01
20:10	540.050	83.08	-0.03	2.75	3.66E-07	1.99E+01
20:30	560.050	83.08	-0.03	2.75	3.79E-07	1.92E+01
20:50	580.050	83.07	-0.02	2.74	3.93E-07	1.86E+01
21:10	600.050	83.07	-0.02	2.74	4.06E-07	1.80E+01
21:30	620.050	83.06	-0.01	2.73	4.20E-07	1.75E+01
21:50	640.050	83.06	-0.01	2.73	4.33E-07	1.70E+01
22:10	660.050	83.06	-0.01	2.73	4.47E-07	1.65E+01
22:30	680.050	83.05	0.00	2.72	4.60E-07	1.60E+01
22:49	700.050	83.05	0.00	2.72	4.74E-07	1.56E+01
23:10	720.050	83.04	0.01	2.71	4.88E-07	1.52E+01
23:30	740.050	83.04	0.01	2.71	5.01E-07	1.48E+01
23:50	760.100	83.03	0.02	2.70	5.15E-07	1.44E+01
00:10	780.100	83.03	0.02	2.70	5.28E-07	1.41E+01
00:30	800.100	83.02	0.03	2.69	5.42E-07	1.38E+01
00:50	820.100	83.01	0.04	2.68	5.55E-07	1.35E+01
01:10	840.100	83.01	0.04	2.68	5.69E-07	1.32E+01
01:30	860.100	83.00	0.05	2.67	5.82E-07	1.29E+01
01:50	880.100	82.99	0.06	2.66	5.96E-07	1.26E+01
02:10	900.100	82.99	0.06	2.66	6.09E-07	1.23E+01
02:30	920.100	82.98	0.07	2.65	6.23E-07	1.21E+01
02:50	940.100	82.97	0.08	2.64	6.37E-07	1.19E+01
03:10	960.100	82.97	0.08	2.64	6.50E-07	1.16E+01
03:30	980.100	82.96	0.09	2.63	6.64E-07	1.14E+01
03:50	1000.100	82.95	0.10	2.62	6.77E-07	1.12E+01
04:50	1060.300	82.93	0.12	2.60	7.18E-07	1.06E+01
05:50	1120.300	82.91	0.14	2.58	7.59E-07	1.01E+01
06:50	1180.300	82.89	0.16	2.56	7.99E-07	9.65E+00
07:50	1240.300	82.87	0.18	2.54	8.40E-07	9.23E+00
08:50	1300.300	82.85	0.20	2.52	8.80E-07	8.85E+00
09:50	1360.300	82.84	0.21	2.51	9.21E-07	8.51E+00
10:50	1420.300	82.83	0.22	2.50	9.62E-07	8.19E+00
11:50	1480.300	82.80	0.25	2.47	1.00E-06	7.90E+00
12:50	1540.300	82.79	0.26	2.46	1.04E-06	7.63E+00
13:50	1600.300	82.77	0.28	2.44	1.08E-06	7.38E+00
14:50	1660.300	82.74	0.31	2.41	1.12E-06	7.15E+00
15:50	1720.100	82.71	0.34	2.38	1.16E-06	6.94E+00
16:50	1780.100	82.69	0.36	2.36	1.21E-06	6.74E+00
17:50	1840.100	82.67	0.38	2.34	1.25E-06	6.55E+00
18:50	1900.100	82.65	0.40	2.32	1.29E-06	6.37E+00
19:50	1960.100	82.63	0.42	2.30	1.33E-06	6.21E+00
20:50	2020.100	82.62	0.43	2.29	1.37E-06	6.05E+00
21:50	2080.100	82.60	0.45	2.27	1.41E-06	5.91E+00

22:50	2140.100	82.59	0.46	2.26	1.45E-06	5.77E+00
23:50	2200.100	82.58	0.47	2.25	1.49E-06	5.64E+00
00:50	2260.100	82.56	0.49	2.23	1.53E-06	5.52E+00
01:50	2320.100	82.54	0.51	2.21	1.57E-06	5.40E+00
02:50	2380.100	82.53	0.52	2.20	1.61E-06	5.29E+00
03:50	2440.100	82.51	0.54	2.18	1.65E-06	5.18E+00
04:50	2500.100	82.49	0.56	2.16	1.69E-06	5.08E+00
05:50	2560.100	82.47	0.58	2.14	1.73E-06	4.99E+00
06:50	2620.100	82.46	0.59	2.13	1.77E-06	4.90E+00
07:50	2680.100	82.44	0.61	2.11	1.81E-06	4.81E+00
08:50	2740.200	82.42	0.63	2.09	1.86E-06	4.73E+00
09:50	2800.200	82.41	0.64	2.08	1.90E-06	4.65E+00
10:50	2860.200	82.39	0.66	2.06	1.94E-06	4.57E+00
11:50	2920.100	82.37	0.68	2.04	1.98E-06	4.50E+00
12:50	2980.200	82.37	0.68	2.04	2.02E-06	4.43E+00
13:50	3040.200	82.34	0.71	2.01	2.06E-06	4.36E+00
14:50	3100.200	82.33	0.72	2.00	2.10E-06	4.29E+00
15:50	3160.200	82.31	0.74	1.98	2.14E-06	4.23E+00
16:50	3220.200	82.29	0.76	1.96	2.18E-06	4.17E+00
17:50	3280.200	82.27	0.78	1.94	2.22E-06	4.11E+00
18:50	3340.200	82.26	0.79	1.93	2.26E-06	4.06E+00
19:50	3400.200	82.26	0.79	1.93	2.30E-06	4.00E+00
20:50	3460.200	82.26	0.79	1.93	2.34E-06	3.95E+00
21:50	3520.200	82.25	0.80	1.92	2.38E-06	3.90E+00
22:50	3580.200	82.24	0.81	1.91	2.42E-06	3.85E+00
23:50	3640.200	82.23	0.82	1.90	2.46E-06	3.80E+00
00:50	3700.200	82.21	0.84	1.88	2.51E-06	3.76E+00
01:50	3760.200	82.19	0.86	1.86	2.55E-06	3.72E+00
02:50	3820.200	82.17	0.88	1.84	2.59E-06	3.67E+00
03:50	3880.200	82.16	0.89	1.83	2.63E-06	3.63E+00
04:50	3940.200	82.14	0.91	1.81	2.67E-06	3.59E+00
05:50	4000.200	82.12	0.93	1.79	2.71E-06	3.55E+00
06:50	4060.200	82.10	0.95	1.77	2.75E-06	3.51E+00
07:50	4120.200	82.10	0.95	1.77	2.79E-06	3.48E+00
08:50	4180.200	82.08	0.97	1.75	2.83E-06	3.44E+00
09:50	4240.200	82.07	0.98	1.74	2.87E-06	3.41E+00
10:50	4300.200	-999.99	1083.04	1080.32	2.91E-06	3.37E+00
11:04	4314.800	-999.99	1083.04	1080.32	2.92E-06	3.37E+00

## ADJUSTED DATA

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14 1  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : F 10-4 INPUT 8  
RADIUS: 20.053 FEET  
START DATE : 13-Oct-86  
START TIME : 10:25  
WATER START LEVEL: 38.82 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
10:25	8725.000	38.74	0.08
10:35	8735.071	38.74	0.08
10:45	8745.070	38.74	0.08
10:55	8755.072	38.74	0.08
11:05	8765.072	38.74	0.08
11:15	8775.072	38.74	0.08
11:25	8785.072	38.74	0.08
11:35	8795.072	38.74	0.08
11:45	8805.072	38.74	0.08
11:55	8815.102	38.74	0.08
12:05	8825.090	38.74	0.08
12:15	8835.090	38.74	0.08
12:25	8845.090	38.74	0.08
12:35	8855.090	38.73	0.09
12:45	8865.090	38.73	0.09
12:55	8875.120	38.73	0.09
13:04	8884.970	38.73	0.09
13:14	8894.970	38.73	0.09
13:25	8904.970	38.73	0.09
13:34	8914.970	38.73	0.09
13:45	8924.970	38.73	0.09
13:54	8934.970	38.73	0.09
14:05	8944.970	38.73	0.09
14:14	8955.020	38.73	0.09
14:25	8965.080	38.73	0.09
14:35	8975.080	38.73	0.09
14:45	8985.080	38.73	0.09
14:55	8995.080	38.73	0.09
15:05	9005.080	38.73	0.09
15:15	9015.080	38.73	0.09
15:25	9025.080	38.73	0.09
15:35	9035.080	38.73	0.09
15:45	9045.080	38.73	0.09
15:55	9055.080	38.73	0.09
16:04	9065.020	38.73	0.09
16:15	9075.020	38.73	0.09
16:25	9084.970	38.73	0.09
16:35	9095.080	38.73	0.09
16:45	9105.080	38.73	0.09
16:55	9115.080	38.73	0.09

## ADJUSTED DATA

17:05	9125.080	38.73	0.09
17:15	9135.080	38.73	0.09
17:25	9145.080	38.72	0.10
17:35	9155.080	38.72	0.10
17:45	9165.080	38.72	0.10
17:55	9175.080	38.72	0.10
18:05	9185.080	38.72	0.10
18:15	9195.080	38.72	0.10
18:25	9205.080	38.72	0.10
18:35	9215.080	38.72	0.10
18:45	9225.080	38.72	0.10
18:55	9235.080	38.72	0.10
19:05	9245.080	38.72	0.10
19:15	9255.080	38.72	0.10
19:25	9265.080	38.72	0.10
19:35	9275.070	38.72	0.10
19:45	9285.080	38.72	0.10
19:55	9295.080	38.72	0.10
20:05	9305.080	38.72	0.10
20:15	9315.080	38.72	0.10
20:25	9325.080	38.72	0.10
20:35	9335.080	38.72	0.10
20:45	9345.080	38.72	0.10
20:55	9355.080	38.72	0.10
21:05	9365.080	38.72	0.10
21:15	9375.080	38.72	0.10
21:25	9385.080	38.72	0.10
21:35	9395.080	38.72	0.10
21:45	9405.080	38.72	0.10
21:55	9415.080	38.72	0.10
22:05	9425.080	38.72	0.10
22:15	9435.080	38.72	0.10
22:25	9445.080	38.72	0.10
22:35	9455.080	38.72	0.10
22:45	9465.080	38.72	0.10
22:54	9475.020	38.72	0.10
23:05	9485.020	38.71	0.11
23:14	9495.020	38.72	0.10
23:25	9505.020	38.72	0.10
23:34	9515.020	38.71	0.11
23:45	9525.020	38.71	0.11
23:55	9535.020	38.71	0.11
00:05	9545.020	38.71	0.11
00:15	9555.020	38.71	0.11
00:25	9565.030	38.71	0.11
00:35	9575.030	38.71	0.11
00:44	9585.030	38.71	0.11
00:55	9595.030	38.71	0.11
01:04	9605.030	38.71	0.11
01:15	9615.030	38.71	0.11
01:25	9625.030	38.71	0.11
01:35	9635.030	38.71	0.11
01:45	9645.030	38.71	0.11
01:55	9655.030	38.71	0.11
02:05	9665.030	38.71	0.11
02:14	9675.030	38.71	0.11

## ADJUSTED DATA

02:25	9685.030	38.71	0.11
02:34	9695.030	38.71	0.11
02:45	9705.030	38.71	0.11
02:55	9715.030	38.71	0.11
03:04	9725.000	38.71	0.11
03:15	9735.000	38.71	0.11
03:24	9745.000	38.71	0.11
03:35	9755.100	38.71	0.11
03:44	9765.000	38.71	0.11
03:55	9775.000	38.71	0.11
04:04	9785.000	38.71	0.11
04:15	9795.000	38.71	0.11
04:25	9805.000	38.71	0.11
04:34	9815.000	38.71	0.11
04:45	9825.000	38.71	0.11
04:54	9835.000	38.71	0.11
05:05	9845.000	38.71	0.11
05:14	9855.000	38.71	0.11
05:25	9865.000	38.70	0.12
05:34	9875.000	38.70	0.12
05:45	9885.000	38.70	0.12
05:55	9895.000	38.70	0.12
06:04	9905.000	38.70	0.12
06:15	9915.000	38.70	0.12
06:24	9925.000	38.70	0.12
06:35	9935.000	38.70	0.12
06:44	9945.000	38.70	0.12
06:55	9955.000	38.70	0.12
07:05	9965.100	38.70	0.12
07:15	9975.100	38.70	0.12
07:25	9985.100	38.70	0.12
07:35	9995.100	38.70	0.12
07:45	10005.100	38.70	0.12
07:55	10015.100	38.70	0.12
08:05	10025.100	38.70	0.12
08:15	10035.100	38.70	0.12
08:25	10045.100	38.70	0.12
08:35	10055.100	38.70	0.12
08:45	10065.100	38.70	0.12
08:55	10075.000	38.70	0.12
09:04	10085.000	38.70	0.12
09:15	10095.000	38.70	0.12
09:24	10105.000	38.70	0.12
09:28	10108.200	38.70	0.12

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 2  
 TEST TYPE: RECOVERY  
 WELL NUMBER: P 10-4 INPUT 8  
 RADIUS: 20.053 FEET  
 START DATE: 07-Oct-86  
 START TIME: 11:10  
 WATER START LEVEL: 38.82 FEET  
 WATER STOP LEVEL: 38.76 FEET  
 TOTAL PUMPING TIME: 10210.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
11:10	0.017	-999.99	1038.75	1038.81
11:10	0.034	-999.99	1038.75	1038.81
11:10	0.050	-999.99	1038.75	1038.81
11:10	0.067	-999.99	1038.75	1038.81
11:10	0.084	-999.99	1038.75	1038.81
11:10	0.100	-999.99	1038.75	1038.81
11:10	0.117	-999.99	1038.75	1038.81
11:10	0.134	-999.99	1038.75	1038.81
11:10	0.150	-999.99	1038.75	1038.81
11:10	0.167	-999.99	1038.75	1038.81
11:10	0.257	38.76	0.00	0.06
11:10	0.341	38.76	0.00	0.06
11:10	0.424	38.76	0.00	0.06
11:10	0.507	38.76	0.00	0.06
11:10	0.591	38.76	0.00	0.06
11:10	0.674	38.76	0.00	0.06
11:10	0.757	38.76	0.00	0.06
11:10	0.841	38.76	0.00	0.06
11:10	0.924	38.76	0.00	0.06
11:11	1.007	38.76	0.00	0.06
11:11	1.413	38.76	0.00	0.06
11:11	1.747	38.76	0.00	0.06
11:12	2.080	38.76	0.00	0.06
11:12	2.413	38.76	0.00	0.06
11:12	2.747	38.76	0.00	0.06
11:13	3.080	38.76	0.00	0.06
11:13	3.413	38.76	0.00	0.06
11:13	3.747	38.76	0.00	0.06
11:14	4.080	38.76	0.00	0.06
11:14	4.413	38.76	0.00	0.06
11:14	4.747	38.76	0.00	0.06
11:15	5.080	38.76	0.00	0.06
11:15	5.413	38.76	0.00	0.06
11:15	5.747	38.76	0.00	0.06
11:16	6.080	38.76	0.00	0.06
11:16	6.413	38.76	0.00	0.06
11:16	6.747	38.76	0.00	0.06
11:17	7.080	38.76	0.00	0.06
11:17	7.413	38.76	0.00	0.06
11:17	7.747	38.76	0.00	0.06

11:18	8.080	38.76	0.00	0.06
11:18	8.413	38.76	0.00	0.06
11:18	8.747	38.76	0.00	0.06
11:19	9.080	38.76	0.00	0.06
11:19	9.413	38.76	0.00	0.06
11:19	9.747	38.76	0.00	0.06
11:20	10.080	38.76	0.00	0.06
11:22	12.115	38.76	0.00	0.06
11:24	14.115	38.76	0.00	0.06
11:26	16.115	38.76	0.00	0.06
11:28	18.115	38.76	0.00	0.06
11:30	20.115	38.76	0.00	0.06
11:32	22.115	38.76	0.00	0.06
11:34	24.115	38.76	0.00	0.06
11:36	26.115	38.76	0.00	0.06
11:38	28.115	38.76	0.00	0.06
11:40	30.115	38.76	0.00	0.06
11:42	32.115	38.76	0.00	0.06
11:44	34.115	38.76	0.00	0.06
11:46	36.115	38.76	0.00	0.06
11:48	38.115	38.76	0.00	0.06
11:50	40.115	38.76	0.00	0.06
11:52	42.115	38.76	0.00	0.06
11:54	44.115	38.76	0.00	0.06
11:56	46.115	38.76	0.00	0.06
11:58	48.115	38.76	0.00	0.06
12:00	50.115	38.76	0.00	0.06
12:02	52.115	38.76	0.00	0.06
12:04	54.115	38.76	0.00	0.06
12:06	56.115	38.76	0.00	0.06
12:08	58.115	38.76	0.00	0.06
12:10	60.115	38.76	0.00	0.06
12:12	62.102	38.76	0.00	0.06
12:14	64.492	38.76	0.00	0.06
12:16	66.188	38.76	0.00	0.06
12:18	68.188	38.76	0.00	0.06
12:20	70.188	38.76	0.00	0.06
12:22	72.188	38.76	0.00	0.06
12:24	74.188	38.76	0.00	0.06
12:26	76.188	38.76	0.00	0.06
12:28	78.188	38.76	0.00	0.06
12:30	80.188	38.76	0.00	0.06
12:32	82.188	38.76	0.00	0.06
12:34	84.188	38.76	0.00	0.06
12:36	86.188	38.76	0.00	0.06
12:38	88.188	38.76	0.00	0.06
12:40	90.188	38.76	0.00	0.06
12:42	92.188	38.76	0.00	0.06
12:44	94.188	38.76	0.00	0.06
12:46	96.188	38.76	0.00	0.06
12:48	98.188	38.76	0.00	0.06
13:10	120.110	38.76	0.00	0.06
13:30	140.110	38.76	0.00	0.06
13:50	160.120	38.76	0.00	0.06
14:10	180.120	38.76	0.00	0.06
14:30	200.120	38.76	0.00	0.06



14:50	220.120	38.75	0.01	0.07
15:10	240.120	38.75	0.01	0.07
15:30	260.120	38.76	0.00	0.06
15:50	280.120	38.76	0.00	0.06
16:10	300.120	38.76	0.00	0.06
16:30	320.050	38.76	0.00	0.06
16:49	340.050	38.76	0.00	0.06
17:10	360.050	38.76	0.00	0.06
17:30	380.050	38.76	0.00	0.06
17:50	400.050	38.76	0.00	0.06
18:10	420.050	38.76	0.00	0.06
18:30	440.050	38.76	0.00	0.06
18:50	460.050	38.76	0.00	0.06
19:10	480.050	38.76	0.00	0.06
19:30	500.050	38.76	0.00	0.06
19:49	520.050	38.75	0.01	0.07
20:10	540.050	38.76	0.00	0.06
20:30	560.050	38.76	0.00	0.06
20:50	580.050	38.76	0.00	0.06
21:10	600.050	38.76	0.00	0.06
21:30	620.050	38.76	0.00	0.06
21:50	640.050	38.75	0.01	0.07
22:10	660.050	38.75	0.01	0.07
22:30	680.050	38.75	0.01	0.07
22:49	700.050	38.75	0.01	0.07
23:10	720.050	38.75	0.01	0.07
23:30	740.050	38.76	0.00	0.06
23:50	760.100	38.76	0.00	0.06
00:10	780.100	38.75	0.01	0.07
00:30	800.100	38.76	0.00	0.06
00:50	820.100	38.76	0.00	0.06
01:10	840.100	38.76	0.00	0.06
01:30	860.100	38.76	0.00	0.06
01:50	880.100	38.76	0.00	0.06
02:10	900.100	38.76	0.00	0.06
02:30	920.100	38.76	0.00	0.06
02:50	940.100	38.76	0.00	0.06
03:10	960.100	38.76	0.00	0.06
03:30	980.100	38.76	0.00	0.06
03:50	1000.100	38.75	0.01	0.07
04:50	1060.300	38.75	0.01	0.07
05:50	1120.300	38.75	0.01	0.07
06:50	1180.300	38.75	0.01	0.07
07:50	1240.300	38.75	0.01	0.07
08:50	1300.300	38.76	0.00	0.06
09:50	1360.300	38.76	0.00	0.06
10:50	1420.300	38.76	0.00	0.06
11:50	1480.300	38.76	0.00	0.06
12:50	1540.300	38.76	0.00	0.06
13:50	1600.300	38.76	0.00	0.06
14:50	1660.300	38.76	0.00	0.06
15:50	1720.100	38.76	0.00	0.06
16:50	1780.100	38.76	0.00	0.06
17:50	1840.100	38.76	0.00	0.06
18:50	1900.100	38.76	0.00	0.06
19:50	1960.100	38.76	0.00	0.06

20:50	2020.100	38.76	0.00	0.06
21:50	2080.100	38.76	0.00	0.06
22:50	2140.100	38.76	0.00	0.06
23:50	2200.100	38.76	0.00	0.06
00:50	2260.100	38.76	0.00	0.06
01:50	2320.100	38.76	0.00	0.06
02:50	2380.100	38.76	0.00	0.06
03:50	2440.100	38.76	0.00	0.06
04:50	2500.100	38.76	0.00	0.06
05:50	2560.100	38.76	0.00	0.06
06:50	2620.100	38.76	0.00	0.06
07:50	2680.100	38.76	0.00	0.06
08:50	2740.200	38.76	0.00	0.06
09:50	2800.200	38.76	0.00	0.06
10:50	2860.200	38.76	0.00	0.06
11:50	2920.100	38.76	0.00	0.06
12:50	2980.200	38.77	-0.01	0.05
13:50	3040.200	38.76	0.00	0.06
14:50	3100.200	38.77	-0.01	0.05
15:50	3160.200	38.77	-0.01	0.05
16:50	3220.200	38.77	-0.01	0.05
17:50	3280.200	38.77	-0.01	0.05
18:50	3340.200	38.77	-0.01	0.05
19:50	3400.200	38.76	0.00	0.06
20:50	3460.200	38.76	0.00	0.06
21:50	3520.200	38.76	0.00	0.06
22:50	3580.200	38.76	0.00	0.06
23:50	3640.200	38.77	-0.01	0.05
00:50	3700.200	38.77	-0.01	0.05
01:50	3760.200	38.77	-0.01	0.05
02:50	3820.200	38.77	-0.01	0.05
03:50	3880.200	38.77	-0.01	0.05
04:50	3940.200	38.77	-0.01	0.05
05:50	4000.200	38.77	-0.01	0.05
06:50	4060.200	38.77	-0.01	0.05
07:50	4120.200	38.77	-0.01	0.05
08:50	4180.200	38.77	-0.01	0.05
09:50	4240.200	-999.99	1038.75	1038.81
10:50	4300.200	-999.99	1038.75	1038.81
11:04	4314.800	-999.99	1038.75	1038.81

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : REI 10-2 INPUT 9  
RADIUS: 25.391 FEET  
START DATE : 07-Oct-86  
START TIME : 09:00  
WATER START LEVEL: 5.78 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
09:00	0.000	5.78	0.00
09:00	0.017	-99.99	105.77
09:00	0.034	-99.99	105.77
09:00	0.050	-99.99	105.77
09:00	0.067	-99.99	105.77
09:00	0.084	-99.99	105.77
09:00	0.100	-99.99	105.77
09:00	0.117	-99.99	105.77
09:00	0.134	-99.99	105.77
09:00	0.150	-99.99	105.77
09:00	0.167	-99.99	105.77
09:00	0.257	5.78	0.00
09:00	0.340	5.78	0.00
09:00	0.424	5.78	0.00
09:00	0.507	5.78	0.00
09:00	0.590	5.78	0.00
09:00	0.674	5.78	0.00
09:00	0.757	5.78	0.00
09:00	0.840	5.78	0.00
09:00	0.924	5.78	0.00
09:01	1.007	5.78	0.00
09:01	1.414	5.78	0.00
09:01	1.748	5.78	0.00
09:02	2.081	5.78	0.00
09:02	2.414	5.78	0.00
09:02	2.748	5.78	0.00
09:03	3.081	5.78	0.00
09:03	3.415	5.78	0.00
09:03	3.748	5.78	0.00
09:04	4.081	5.78	0.00
09:04	4.414	5.78	0.00
09:04	4.748	5.78	0.00
09:05	5.081	5.78	0.00
09:05	5.414	5.78	0.00
09:05	5.748	5.78	0.00
09:06	6.081	5.78	0.00
09:06	6.415	5.78	0.00
09:06	6.748	5.78	0.00
09:07	7.081	5.78	0.00
09:07	7.415	5.78	0.00
09:07	7.748	5.78	0.00

09:08	8.081	5.78	0.00
09:08	8.415	5.78	0.00
09:08	8.748	5.78	0.00
09:09	9.081	5.78	0.00
09:09	9.414	5.78	0.00
09:09	9.748	5.78	0.00
09:10	10.081	5.78	0.00
09:12	12.108	5.78	0.00
09:14	14.152	5.78	0.00
09:16	16.152	5.77	0.01
09:18	18.152	5.77	0.01
09:20	20.152	5.77	0.01
09:22	22.152	5.77	0.01
09:24	24.152	5.77	0.01
09:26	26.152	5.77	0.01
09:28	28.215	5.77	0.01
09:30	30.197	5.77	0.01
09:32	32.197	5.77	0.01
09:34	34.197	5.77	0.01
09:36	36.197	5.77	0.01
09:38	38.197	5.77	0.01
09:40	40.197	5.77	0.01
09:42	42.197	5.77	0.01
09:44	44.197	5.77	0.01
09:46	46.197	5.77	0.01
09:48	48.197	5.77	0.01
09:50	50.197	5.77	0.01
09:52	52.197	5.77	0.01
09:54	54.197	5.77	0.01
09:56	56.217	5.77	0.01
09:58	58.100	5.77	0.01
10:00	60.245	5.77	0.01
10:02	62.245	5.77	0.01
10:04	64.245	5.77	0.01
10:06	66.245	5.77	0.01
10:08	68.245	5.77	0.01
10:10	70.245	5.77	0.01
10:12	72.245	5.77	0.01
10:14	74.245	5.77	0.01
10:16	76.245	5.77	0.01
10:18	78.245	5.77	0.01
10:20	80.245	5.77	0.01
10:22	82.245	5.77	0.01
10:24	84.245	5.77	0.01
10:26	86.245	5.77	0.01
10:28	88.245	5.77	0.01
10:30	90.245	5.77	0.01
10:32	92.245	5.77	0.01
10:34	94.245	5.77	0.01
10:36	96.245	5.77	0.01
10:38	98.245	5.77	0.01
11:00	120.210	5.77	0.01
11:20	140.210	5.77	0.01
11:40	160.210	5.77	0.01
12:00	180.220	5.77	0.01
12:20	200.220	5.76	0.02

12:40	220.220	5.76	0.02
13:00	240.220	5.76	0.02
13:20	260.220	5.75	0.03
13:40	280.230	5.73	0.05
14:00	300.230	5.72	0.06
14:20	320.230	5.72	0.06
14:40	340.180	5.71	0.07
15:00	360.100	5.71	0.07
15:20	380.100	5.70	0.08
15:40	400.100	5.69	0.09
16:00	420.170	5.68	0.10
16:20	440.250	5.68	0.10
16:40	460.200	5.67	0.11
17:00	480.170	5.67	0.11
17:20	500.170	5.67	0.11
17:40	520.130	5.67	0.11
18:00	540.120	5.67	0.11
18:20	560.220	5.66	0.12
18:40	580.080	5.67	0.11
19:00	600.220	5.67	0.11
19:20	620.230	5.68	0.10
19:40	640.220	5.68	0.10
20:00	660.220	5.68	0.10
20:20	680.130	5.69	0.09
20:40	700.120	5.69	0.09
21:00	720.230	5.69	0.09
21:20	740.300	5.69	0.09
21:40	760.230	5.69	0.09
22:00	780.230	5.69	0.09
22:20	800.230	5.69	0.09
22:40	820.180	5.70	0.08
23:00	840.570	5.70	0.08
23:20	860.180	5.70	0.08
23:40	880.080	5.70	0.08
00:00	900.170	5.70	0.08
00:20	920.170	5.69	0.09
00:40	940.170	5.69	0.09
01:00	960.170	5.69	0.09
01:20	980.170	5.68	0.10
01:40	1000.200	5.67	0.11
02:40	1060.300	5.66	0.12
03:40	1120.300	5.65	0.13
04:40	1180.300	5.64	0.14
05:40	1240.300	5.64	0.14
06:40	1300.300	5.64	0.14
07:40	1360.200	5.64	0.14
08:40	1420.200	5.64	0.14
09:40	1480.200	5.66	0.12
10:40	1540.200	5.65	0.13
11:40	1600.300	5.65	0.13
12:40	1660.300	5.64	0.14
13:40	1720.200	5.64	0.14
14:40	1780.300	5.61	0.17
15:40	1840.300	5.59	0.19
16:40	1900.300	5.59	0.19
17:40	1960.200	5.57	0.21

18:40	2020.200	5.57	0.21
19:40	2080.200	5.57	0.21
20:40	2140.200	5.57	0.21
21:40	2200.300	5.58	0.20
22:40	2260.300	5.58	0.20
23:40	2320.200	5.57	0.21
00:40	2380.200	5.57	0.21
01:40	2440.200	5.55	0.23
02:40	2500.200	5.55	0.23
03:40	2560.200	5.55	0.23
04:40	2620.200	5.53	0.25
05:40	2680.200	5.54	0.24
06:40	2740.200	5.54	0.24
07:40	2800.200	5.55	0.23
08:40	2860.300	5.56	0.22
09:40	2920.300	5.57	0.21
10:40	2980.300	5.58	0.20
11:40	3040.200	5.59	0.19
12:40	3100.200	5.56	0.22
13:40	3160.300	5.56	0.22
14:40	3220.300	5.53	0.25
15:40	3280.200	5.53	0.25
16:40	3340.200	5.52	0.26
17:40	3400.300	5.52	0.26
18:40	3460.300	5.52	0.26
19:40	3520.300	5.53	0.25
20:40	3580.200	5.53	0.25
21:40	3640.200	5.55	0.23
22:40	3700.200	5.55	0.23
23:40	3760.200	5.55	0.23
00:40	3820.200	5.54	0.24
01:40	3880.200	5.53	0.25
02:40	3940.200	5.53	0.25
03:40	4000.200	5.53	0.25
04:40	4060.200	5.52	0.26
05:40	4120.200	5.51	0.27
06:40	4180.200	5.52	0.26
07:40	4240.300	5.52	0.26
08:40	4300.300	5.53	0.25
09:40	4360.700	5.54	0.24
10:40	4420.300	5.53	0.25
11:40	4480.300	5.52	0.26
12:40	4540.300	5.51	0.27
13:40	4600.300	5.50	0.28
14:40	4660.300	5.48	0.30
15:40	4720.300	5.40	0.38
16:40	4780.300	5.42	0.36
17:40	4840.300	5.41	0.37
18:40	4900.300	5.41	0.37
19:40	4960.300	5.42	0.36
20:40	5020.300	5.43	0.35
21:40	5080.300	5.43	0.35
22:40	5140.300	5.44	0.34
23:40	5200.300	5.44	0.34
00:40	5260.300	5.43	0.35
01:40	5320.300	5.42	0.36

02:40	5380.300	5.41	0.37
03:40	5440.300	5.41	0.37
04:40	5500.300	5.39	0.39
05:40	5560.300	5.39	0.39
06:40	5620.300	5.40	0.38
07:40	5680.300	5.42	0.36
08:40	5740.300	5.42	0.36
09:40	5800.300	5.43	0.35
10:40	5860.300	5.44	0.34
11:40	5920.300	5.46	0.32
12:40	5980.300	5.46	0.32
13:40	6040.300	5.44	0.34
14:40	6100.300	5.41	0.37
15:40	6160.500	5.39	0.39
16:40	6220.300	5.38	0.40
17:40	6280.300	5.38	0.40
18:40	6340.300	5.41	0.37
19:40	6400.400	5.41	0.37
20:40	6460.200	5.41	0.37
21:40	6520.200	5.42	0.36
22:40	6580.300	5.42	0.36
23:40	6640.300	5.42	0.36
00:40	6700.300	5.42	0.36
01:40	6760.300	5.43	0.35
02:40	6820.300	5.41	0.37
03:40	6880.300	5.39	0.39
04:40	6940.300	5.37	0.41
05:40	7000.300	5.37	0.41
06:40	7060.300	5.37	0.41
07:40	7120.300	5.40	0.38
08:40	7180.300	5.45	0.33
09:40	7240.300	5.47	0.31
10:40	7300.300	5.46	0.32
11:40	7360.300	5.44	0.34
12:40	7420.300	5.42	0.36
13:40	7480.300	5.39	0.39
14:40	7540.300	5.34	0.44
15:40	7600.300	5.31	0.47
16:40	7660.300	5.27	0.51
17:40	7720.300	5.24	0.54
18:40	7780.200	5.22	0.56
19:40	7840.200	5.21	0.57
20:40	7900.300	5.18	0.60
21:40	7960.300	5.17	0.61
22:40	8020.300	5.15	0.63
23:40	8080.300	5.13	0.65
00:40	8140.300	5.10	0.68
01:40	8200.300	5.06	0.72
02:40	8260.300	5.04	0.74
03:40	8320.300	5.01	0.77
04:40	8380.300	4.99	0.79
05:40	8440.300	4.97	0.81
06:40	8500.300	4.96	0.82
07:40	8560.200	4.95	0.83
08:40	8620.300	4.97	0.81
09:00	8640.600	4.97	0.81

## ADJUSTED DATA

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : REI 10-2 INPUT 9  
RADIUS: 25.391 FEET  
START DATE : 13-Oct-86  
START TIME : 10:25  
WATER START LEVEL: 5.78 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
10:25	8725.000	4.95	0.83
10:35	8735.071	4.94	0.84
10:45	8745.070	4.94	0.84
10:55	8755.072	4.94	0.84
11:05	8765.072	4.95	0.83
11:15	8775.072	4.96	0.82
11:25	8785.072	4.96	0.82
11:35	8795.072	4.94	0.84
11:45	8805.072	4.94	0.84
11:55	8815.102	4.94	0.84
12:05	8825.090	4.94	0.84
12:15	8835.090	4.93	0.85
12:25	8845.090	4.94	0.84
12:35	8855.090	4.93	0.85
12:45	8865.090	4.92	0.86
12:55	8875.120	4.92	0.86
13:04	8884.970	4.93	0.85
13:14	8894.970	4.92	0.86
13:25	8904.970	4.92	0.86
13:34	8914.970	4.90	0.88
13:45	8924.970	4.90	0.88
13:54	8934.970	4.89	0.89
14:05	8944.970	4.90	0.88
14:14	8955.020	4.89	0.89
14:25	8965.080	4.89	0.89
14:35	8975.080	4.88	0.90
14:45	8985.080	4.88	0.90
14:55	8995.080	4.89	0.89
15:05	9005.080	4.88	0.90
15:15	9015.080	4.87	0.91
15:25	9025.080	4.86	0.92
15:35	9035.080	4.86	0.92
15:45	9045.080	4.85	0.93
15:55	9055.080	4.85	0.93
16:04	9065.020	4.85	0.93
16:15	9075.020	4.85	0.93
16:25	9084.970	4.85	0.93
16:35	9095.080	4.84	0.94
16:45	9105.080	4.84	0.94
16:55	9115.080	4.83	0.95



## ADJUSTED DATA

17:05	9125.080	4.83	0.95
17:15	9135.080	4.83	0.95
17:25	9145.080	4.83	0.95
17:35	9155.080	4.83	0.95
17:45	9165.080	4.83	0.95
17:55	9175.080	4.82	0.96
18:05	9185.080	4.82	0.96
18:15	9195.080	4.81	0.97
18:25	9205.080	4.80	0.98
18:35	9215.080	4.81	0.97
18:45	9225.080	4.81	0.97
18:55	9235.080	4.80	0.98
19:05	9245.080	4.80	0.98
19:15	9255.080	4.80	0.98
19:25	9265.080	4.80	0.98
19:35	9275.070	4.80	0.98
19:45	9285.080	4.80	0.98
19:55	9295.080	4.80	0.98
20:05	9305.080	4.79	0.99
20:15	9315.080	4.79	0.99
20:25	9325.080	4.79	0.99
20:35	9335.080	4.79	0.99
20:45	9345.080	4.79	0.99
20:55	9355.080	4.80	0.98
21:05	9365.080	4.80	0.98
21:15	9375.080	4.80	0.98
21:25	9385.080	4.80	0.98
21:35	9395.080	4.80	0.98
21:45	9405.080	4.80	0.98
21:55	9415.080	4.80	0.98
22:05	9425.080	4.80	0.98
22:15	9435.080	4.80	0.98
22:25	9445.080	4.80	0.98
22:35	9455.080	4.80	0.98
22:45	9465.080	4.80	0.98
22:54	9475.020	4.80	0.98
23:05	9485.020	4.80	0.98
23:14	9495.020	4.80	0.98
23:25	9505.020	4.80	0.98
23:34	9515.020	4.79	0.99
23:45	9525.020	4.80	0.98
23:55	9535.020	4.79	0.99
00:05	9545.020	4.79	0.99
00:15	9555.020	4.78	1.00
00:25	9565.030	4.79	0.99
00:35	9575.030	4.78	1.00
00:44	9585.030	4.78	1.00
00:55	9595.030	4.78	1.00
01:04	9605.030	4.78	1.00
01:15	9615.030	4.78	1.00
01:25	9625.030	4.78	1.00
01:35	9635.030	4.78	1.00
01:45	9645.030	4.78	1.00
01:55	9655.030	4.78	1.00
02:05	9665.030	4.78	1.00
02:14	9675.030	4.78	1.00

## ADJUSTED DATA

02:25	9685.030	4.78	1.00
02:34	9695.030	4.78	1.00
02:45	9705.030	4.78	1.00
02:55	9715.030	4.78	1.00
03:04	9725.000	4.78	1.00
03:15	9735.000	4.78	1.00
03:24	9745.000	4.78	1.00
03:35	9755.100	4.79	0.99
03:44	9765.000	4.78	1.00
03:55	9775.000	4.78	1.00
04:04	9785.000	4.78	1.00
04:15	9795.000	4.78	1.00
04:25	9805.000	4.78	1.00
04:34	9815.000	4.78	1.00
04:45	9825.000	4.78	1.00
04:54	9835.000	4.78	1.00
05:05	9845.000	4.78	1.00
05:14	9855.000	4.78	1.00
05:25	9865.000	4.78	1.00
05:34	9875.000	4.78	1.00
05:45	9885.000	4.78	1.00
05:55	9895.000	4.78	1.00
06:04	9905.000	4.78	1.00
06:15	9915.000	4.78	1.00
06:24	9925.000	4.78	1.00
06:35	9935.000	4.78	1.00
06:44	9945.000	4.78	1.00
06:55	9955.000	4.79	0.99
07:05	9965.100	4.79	0.99
07:15	9975.100	4.79	0.99
07:25	9985.100	4.80	0.98
07:35	9995.100	4.80	0.98
07:45	10005.100	4.80	0.98
07:55	10015.100	4.80	0.98
08:05	10025.100	4.81	0.97
08:15	10035.100	4.81	0.97
08:25	10045.100	4.81	0.97
08:35	10055.100	4.82	0.96
08:45	10065.100	4.83	0.95
08:55	10075.000	4.82	0.96
09:04	10085.000	4.83	0.95
09:15	10095.000	4.83	0.95
09:24	10105.000	4.83	0.95
09:28	10108.200	4.83	0.95

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 2  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 10-2 INPUT 9  
 RADIUS: 25.391 FEET  
 START DATE: 07-Oct-86  
 START TIME: 11:10  
 WATER START LEVEL: 5.78 FEET  
 WATER STOP LEVEL: 5.01 FEET  
 TOTAL PUMPING TIME: 10210.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
11:10	0.017	-999.99	1005.00	1005.77
11:10	0.034	-999.99	1005.00	1005.77
11:10	0.050	-999.99	1005.00	1005.77
11:10	0.067	-999.99	1005.00	1005.77
11:10	0.084	-999.99	1005.00	1005.77
11:10	0.100	-999.99	1005.00	1005.77
11:10	0.117	-999.99	1005.00	1005.77
11:10	0.134	-999.99	1005.00	1005.77
11:10	0.150	-999.99	1005.00	1005.77
11:10	0.167	-999.99	1005.00	1005.77
11:10	0.257	5.01	0.00	0.77
11:10	0.341	5.01	0.00	0.77
11:10	0.424	5.01	0.00	0.77
11:10	0.507	5.01	0.00	0.77
11:10	0.591	5.01	0.00	0.77
11:10	0.674	5.01	0.00	0.77
11:10	0.757	5.01	0.00	0.77
11:10	0.841	5.01	0.00	0.77
11:10	0.924	5.01	0.00	0.77
11:11	1.007	5.01	0.00	0.77
11:11	1.413	5.01	0.00	0.77
11:11	1.747	5.01	0.00	0.77
11:12	2.080	5.01	0.00	0.77
11:12	2.413	5.02	-0.01	0.76
11:12	2.747	5.02	-0.01	0.76
11:13	3.080	5.03	-0.02	0.75
11:13	3.413	5.03	-0.02	0.75
11:13	3.747	5.03	-0.02	0.75
11:14	4.080	5.03	-0.02	0.75
11:14	4.413	5.03	-0.02	0.75
11:14	4.747	5.02	-0.01	0.76
11:15	5.080	5.02	-0.01	0.76
11:15	5.413	5.01	0.00	0.77
11:15	5.747	5.01	0.00	0.77
11:16	6.080	5.01	0.00	0.77
11:16	6.413	5.02	-0.01	0.76
11:16	6.747	5.02	-0.01	0.76
11:17	7.080	5.02	-0.01	0.76

11:17	7.413	5.02	-0.01	0.76
11:17	7.747	5.02	-0.01	0.76
11:18	8.080	5.02	-0.01	0.76
11:18	8.413	5.02	-0.01	0.76
11:18	8.747	5.02	-0.01	0.76
11:19	9.080	5.02	-0.01	0.76
11:19	9.413	5.02	-0.01	0.76
11:19	9.747	5.02	-0.01	0.76
11:20	10.080	5.02	-0.01	0.76
11:22	12.115	5.02	-0.01	0.76
11:24	14.115	5.03	-0.02	0.75
11:26	16.115	5.04	-0.03	0.74
11:28	18.115	5.03	-0.02	0.75
11:30	20.115	5.04	-0.03	0.74
11:32	22.115	5.04	-0.03	0.74
11:34	24.115	5.03	-0.02	0.75
11:36	26.115	5.03	-0.02	0.75
11:38	28.115	5.03	-0.02	0.75
11:40	30.115	5.02	-0.01	0.76
11:42	32.115	5.02	-0.01	0.76
11:44	34.115	5.02	-0.01	0.76
11:46	36.115	5.04	-0.03	0.74
11:48	38.115	5.04	-0.03	0.74
11:50	40.115	5.04	-0.03	0.74
11:52	42.115	5.05	-0.04	0.73
11:54	44.115	5.04	-0.03	0.74
11:56	46.115	5.04	-0.03	0.74
11:58	48.115	5.03	-0.02	0.75
12:00	50.115	5.03	-0.02	0.75
12:02	52.115	5.03	-0.02	0.75
12:04	54.115	5.03	-0.02	0.75
12:06	56.115	5.04	-0.03	0.74
12:08	58.115	5.04	-0.03	0.74
12:10	60.115	5.05	-0.04	0.73
12:12	62.102	5.04	-0.03	0.74
12:14	64.492	5.04	-0.03	0.74
12:16	66.188	5.03	-0.02	0.75
12:18	68.188	5.04	-0.03	0.74
12:20	70.188	5.04	-0.03	0.74
12:22	72.188	5.04	-0.03	0.74
12:24	74.188	5.04	-0.03	0.74
12:26	76.188	5.03	-0.02	0.75
12:28	78.188	5.03	-0.02	0.75
12:30	80.188	5.03	-0.02	0.75
12:32	82.188	5.03	-0.02	0.75
12:34	84.188	5.02	-0.01	0.76
12:36	86.188	5.02	-0.01	0.76
12:38	88.188	5.04	-0.03	0.74
12:40	90.188	5.03	-0.02	0.75
12:42	92.188	5.03	-0.02	0.75
12:44	94.188	5.02	-0.01	0.76
12:46	96.188	5.02	-0.01	0.76
12:48	98.188	5.01	0.00	0.77
13:10	120.110	5.03	-0.02	0.75
13:30	140.110	5.02	-0.01	0.76
13:50	160.120	5.02	-0.01	0.76

14:10	180.120	5.00	0.01	0.78
14:30	200.120	4.99	0.02	0.79
14:50	220.120	4.99	0.02	0.79
15:10	240.120	4.98	0.03	0.80
15:30	260.120	4.99	0.02	0.79
15:50	280.120	4.98	0.03	0.80
16:10	300.120	4.97	0.04	0.81
16:30	320.050	4.97	0.04	0.81
16:49	340.050	4.97	0.04	0.81
17:10	360.050	4.97	0.04	0.81
17:30	380.050	4.97	0.04	0.81
17:50	400.050	4.98	0.03	0.80
18:10	420.050	4.98	0.03	0.80
18:30	440.050	4.98	0.03	0.80
18:50	460.050	4.99	0.02	0.79
19:10	480.050	4.99	0.02	0.79
19:30	500.050	5.00	0.01	0.78
19:49	520.050	5.01	0.00	0.77
20:10	540.050	5.02	-0.01	0.76
20:30	560.050	5.03	-0.02	0.75
20:50	580.050	5.04	-0.03	0.74
21:10	600.050	5.04	-0.03	0.74
21:30	620.050	5.05	-0.04	0.73
21:50	640.050	5.06	-0.05	0.72
22:10	660.050	5.06	-0.05	0.72
22:30	680.050	5.07	-0.06	0.71
22:49	700.050	5.08	-0.07	0.70
23:10	720.050	5.08	-0.07	0.70
23:30	740.050	5.08	-0.07	0.70
23:50	760.100	5.09	-0.08	0.69
00:10	780.100	5.09	-0.08	0.69
00:30	800.100	5.10	-0.09	0.68
00:50	820.100	5.10	-0.09	0.68
01:10	840.100	5.10	-0.09	0.68
01:30	860.100	5.10	-0.09	0.68
01:50	880.100	5.10	-0.09	0.68
02:10	900.100	5.11	-0.10	0.67
02:30	920.100	5.11	-0.10	0.67
02:50	940.100	5.12	-0.11	0.66
03:10	960.100	5.12	-0.11	0.66
03:30	980.100	5.13	-0.12	0.65
03:50	1000.100	5.13	-0.12	0.65
04:50	1060.300	5.13	-0.12	0.65
05:50	1120.300	5.15	-0.14	0.63
06:50	1180.300	5.16	-0.15	0.62
07:50	1240.300	5.18	-0.17	0.60
08:50	1300.300	5.21	-0.20	0.57
09:50	1360.300	5.23	-0.22	0.55
10:50	1420.300	5.24	-0.23	0.54
11:50	1480.300	5.24	-0.23	0.54
12:50	1540.300	5.23	-0.22	0.55
13:50	1600.300	5.21	-0.20	0.57
14:50	1660.300	5.18	-0.17	0.60
15:50	1720.100	5.16	-0.15	0.62
16:50	1780.100	5.16	-0.15	0.62
17:50	1840.100	5.16	-0.15	0.62

18:50	1900.100	5.16	-0.15	0.62
19:50	1960.100	5.18	-0.17	0.60
20:50	2020.100	5.20	-0.19	0.58
21:50	2080.100	5.21	-0.20	0.57
22:50	2140.100	5.23	-0.22	0.55
23:50	2200.100	5.24	-0.23	0.54
00:50	2260.100	5.24	-0.23	0.54
01:50	2320.100	5.24	-0.23	0.54
02:50	2380.100	5.24	-0.23	0.54
03:50	2440.100	5.24	-0.23	0.54
04:50	2500.100	5.24	-0.23	0.54
05:50	2560.100	5.24	-0.23	0.54
06:50	2620.100	5.25	-0.24	0.53
07:50	2680.100	5.26	-0.25	0.52
08:50	2740.200	5.27	-0.26	0.51
09:50	2800.200	5.28	-0.27	0.50
10:50	2860.200	5.29	-0.28	0.49
11:50	2920.100	5.28	-0.27	0.50
12:50	2980.200	5.26	-0.25	0.52
13:50	3040.200	5.21	-0.20	0.57
14:50	3100.200	5.21	-0.20	0.57
15:50	3160.200	5.17	-0.16	0.61
16:50	3220.200	5.15	-0.14	0.63
17:50	3280.200	5.15	-0.14	0.63
18:50	3340.200	5.15	-0.14	0.63
19:50	3400.200	5.17	-0.16	0.61
20:50	3460.200	5.18	-0.17	0.60
21:50	3520.200	5.19	-0.18	0.59
22:50	3580.200	5.19	-0.18	0.59
23:50	3640.200	5.20	-0.19	0.58
00:50	3700.200	5.19	-0.18	0.59
01:50	3760.200	5.19	-0.18	0.59
02:50	3820.200	5.19	-0.18	0.59
03:50	3880.200	5.19	-0.18	0.59
04:50	3940.200	5.19	-0.18	0.59
05:50	4000.200	5.19	-0.18	0.59
06:50	4060.200	5.21	-0.20	0.57
07:50	4120.200	5.21	-0.20	0.57
08:50	4180.200	5.26	-0.25	0.52
09:50	4240.200	-999.99	1005.00	1005.77
10:50	4300.200	-999.99	1005.00	1005.77
11:04	4314.800	-999.99	1005.00	1005.77

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : REI 10-3 INPUT 10  
RADIUS: 63.843 FEET  
START DATE : 07-Oct-86  
START TIME : 09:00  
WATER START LEVEL: 7.14 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
09:00	0.000	7.14	0.00
09:00	0.017	-99.99	107.13
09:00	0.034	-99.99	107.13
09:00	0.050	-99.99	107.13
09:00	0.067	-99.99	107.13
09:00	0.084	-99.99	107.13
09:00	0.100	-99.99	107.13
09:00	0.117	-99.99	107.13
09:00	0.134	-99.99	107.13
09:00	0.150	-99.99	107.13
09:00	0.167	-99.99	107.13
09:00	0.257	7.14	0.00
09:00	0.340	7.14	0.00
09:00	0.424	7.14	0.00
09:00	0.507	7.14	0.00
09:00	0.590	7.14	0.00
09:00	0.674	7.14	0.00
09:00	0.757	7.14	0.00
09:00	0.840	7.14	0.00
09:00	0.924	7.14	0.00
09:01	1.007	7.14	0.00
09:01	1.414	7.14	0.00
09:01	1.748	7.14	0.00
09:02	2.081	7.14	0.00
09:02	2.414	7.14	0.00
09:02	2.748	7.14	0.00
09:03	3.081	7.14	0.00
09:03	3.415	7.14	0.00
09:03	3.748	7.14	0.00
09:04	4.081	7.14	0.00
09:04	4.414	7.14	0.00
09:04	4.748	7.14	0.00
09:05	5.081	7.13	0.01
09:05	5.414	7.13	0.01
09:05	5.748	7.13	0.01
09:06	6.081	7.13	0.01
09:06	6.415	7.13	0.01
09:06	6.748	7.13	0.01
09:07	7.081	7.13	0.01
09:07	7.415	7.13	0.01
09:07	7.748	7.13	0.01

09:08	8.081	7.13	0.01
09:08	8.415	7.13	0.01
09:08	8.748	7.13	0.01
09:09	9.081	7.13	0.01
09:09	9.414	7.13	0.01
09:09	9.748	7.13	0.01
09:10	10.081	7.13	0.01
09:12	12.108	7.13	0.01
09:14	14.152	7.13	0.01
09:16	16.152	7.13	0.01
09:18	18.152	7.13	0.01
09:20	20.152	7.13	0.01
09:22	22.152	7.13	0.01
09:24	24.152	7.13	0.01
09:26	26.152	7.13	0.01
09:28	28.215	7.13	0.01
09:30	30.197	7.13	0.01
09:32	32.197	7.13	0.01
09:34	34.197	7.13	0.01
09:36	36.197	7.13	0.01
09:38	38.197	7.13	0.01
09:40	40.197	7.13	0.01
09:42	42.197	7.13	0.01
09:44	44.197	7.13	0.01
09:46	46.197	7.13	0.01
09:48	48.197	7.13	0.01
09:50	50.197	7.13	0.01
09:52	52.197	7.13	0.01
09:54	54.197	7.14	0.00
09:56	56.217	7.13	0.01
09:58	58.100	7.13	0.01
10:00	60.245	7.13	0.01
10:02	62.245	7.14	0.00
10:04	64.245	7.13	0.01
10:06	66.245	7.14	0.00
10:08	68.245	7.13	0.01
10:10	70.245	7.13	0.01
10:12	72.245	7.14	0.00
10:14	74.245	7.13	0.01
10:16	76.245	7.13	0.01
10:18	78.245	7.14	0.00
10:20	80.245	7.13	0.01
10:22	82.245	7.13	0.01
10:24	84.245	7.14	0.00
10:26	86.245	7.14	0.00
10:28	88.245	7.14	0.00
10:30	90.245	7.13	0.01
10:32	92.245	7.13	0.01
10:34	94.245	7.13	0.01
10:36	96.245	7.13	0.01
10:38	98.245	7.13	0.01
11:00	120.210	7.14	0.00
11:20	140.210	7.14	0.00
11:40	160.210	7.13	0.01
12:00	180.220	7.13	0.01
12:20	200.220	7.13	0.01



12:40	220.220	7.12	0.02
13:00	240.220	7.11	0.03
13:20	260.220	7.11	0.03
13:40	280.230	7.09	0.05
14:00	300.230	7.08	0.06
14:20	320.230	7.07	0.07
14:40	340.180	7.07	0.07
15:00	360.100	7.07	0.07
15:20	380.100	7.06	0.08
15:40	400.100	7.06	0.08
16:00	420.170	7.05	0.09
16:20	440.250	7.05	0.09
16:40	460.200	7.04	0.10
17:00	480.170	7.04	0.10
17:20	500.170	7.04	0.10
17:40	520.130	7.04	0.10
18:00	540.120	7.04	0.10
18:20	560.220	7.04	0.10
18:40	580.080	7.04	0.10
19:00	600.220	7.05	0.09
19:20	620.230	7.05	0.09
19:40	640.220	7.06	0.08
20:00	660.220	7.06	0.08
20:20	680.130	7.06	0.08
20:40	700.120	7.06	0.08
21:00	720.230	7.06	0.08
21:20	740.300	7.06	0.08
21:40	760.230	7.06	0.08
22:00	780.230	7.07	0.07
22:20	800.230	7.07	0.07
22:40	820.180	7.08	0.06
23:00	840.570	7.08	0.06
23:20	860.180	7.07	0.07
23:40	880.080	7.07	0.07
00:00	900.170	7.07	0.07
00:20	920.170	7.07	0.07
00:40	940.170	7.06	0.08
01:00	960.170	7.05	0.09
01:20	980.170	7.04	0.10
01:40	1000.200	7.04	0.10
02:40	1060.300	7.04	0.10
03:40	1120.300	7.02	0.12
04:40	1180.300	7.02	0.12
05:40	1240.300	7.02	0.12
06:40	1300.300	7.02	0.12
07:40	1360.200	7.02	0.12
08:40	1420.200	7.03	0.11
09:40	1480.200	7.05	0.09
10:40	1540.200	7.05	0.09
11:40	1600.300	7.04	0.10
12:40	1660.300	7.04	0.10
13:40	1720.200	7.02	0.12
14:40	1780.300	7.00	0.14
15:40	1840.300	6.98	0.16
16:40	1900.300	6.97	0.17
17:40	1960.200	6.97	0.17

18:40	2020.200	6.97	0.17
19:40	2080.200	6.97	0.17
20:40	2140.200	6.98	0.16
21:40	2200.300	6.99	0.15
22:40	2260.300	6.99	0.15
23:40	2320.200	6.98	0.16
00:40	2380.200	6.97	0.17
01:40	2440.200	6.95	0.19
02:40	2500.200	6.95	0.19
03:40	2560.200	6.94	0.20
04:40	2620.200	6.93	0.21
05:40	2680.200	6.94	0.20
06:40	2740.200	6.95	0.19
07:40	2800.200	6.96	0.18
08:40	2860.300	6.98	0.16
09:40	2920.300	7.00	0.14
10:40	2980.300	7.00	0.14
11:40	3040.200	7.00	0.14
12:40	3100.200	6.99	0.15
13:40	3160.300	6.98	0.16
14:40	3220.300	6.95	0.19
15:40	3280.200	6.95	0.19
16:40	3340.200	6.94	0.20
17:40	3400.300	6.95	0.19
18:40	3460.300	6.95	0.19
19:40	3520.300	6.96	0.18
20:40	3580.200	6.97	0.17
21:40	3640.200	6.98	0.16
22:40	3700.200	6.98	0.16
23:40	3760.200	6.98	0.16
00:40	3820.200	6.97	0.17
01:40	3880.200	6.97	0.17
02:40	3940.200	6.96	0.18
03:40	4000.200	6.95	0.19
04:40	4060.200	6.95	0.19
05:40	4120.200	6.95	0.19
06:40	4180.200	6.95	0.19
07:40	4240.300	6.96	0.18
08:40	4300.300	6.96	0.18
09:40	4360.700	6.98	0.16
10:40	4420.300	6.97	0.17
11:40	4480.300	6.97	0.17
12:40	4540.300	6.95	0.19
13:40	4600.300	6.92	0.22
14:40	4660.300	6.90	0.24
15:40	4720.300	6.87	0.27
16:40	4780.300	6.87	0.27
17:40	4840.300	6.86	0.28
18:40	4900.300	6.87	0.27
19:40	4960.300	6.87	0.27
20:40	5020.300	6.89	0.25
21:40	5080.300	6.89	0.25
22:40	5140.300	6.90	0.24
23:40	5200.300	6.90	0.24
00:40	5260.300	6.88	0.26
01:40	5320.300	6.87	0.27

02:40	5380.300	6.86	0.28
03:40	5440.300	6.85	0.29
04:40	5500.300	6.84	0.30
05:40	5560.300	6.84	0.30
06:40	5620.300	6.87	0.27
07:40	5680.300	6.88	0.26
08:40	5740.300	6.87	0.27
09:40	5800.300	6.89	0.25
10:40	5860.300	6.90	0.24
11:40	5920.300	6.93	0.21
12:40	5980.300	6.90	0.24
13:40	6040.300	6.90	0.24
14:40	6100.300	6.84	0.30
15:40	6160.500	6.82	0.32
16:40	6220.300	6.84	0.30
17:40	6280.300	6.84	0.30
18:40	6340.300	6.88	0.26
19:40	6400.400	6.88	0.26
20:40	6460.200	6.89	0.25
21:40	6520.200	6.89	0.25
22:40	6580.300	6.89	0.25
23:40	6640.300	6.89	0.25
00:40	6700.300	6.89	0.25
01:40	6760.300	6.89	0.25
02:40	6820.300	6.88	0.26
03:40	6880.300	6.86	0.28
04:40	6940.300	6.84	0.30
05:40	7000.300	6.83	0.31
06:40	7060.300	6.86	0.28
07:40	7120.300	6.90	0.24
08:40	7180.300	6.95	0.19
09:40	7240.300	6.96	0.18
10:40	7300.300	6.93	0.21
11:40	7360.300	6.92	0.22
12:40	7420.300	6.89	0.25
13:40	7480.300	6.86	0.28
14:40	7540.300	6.80	0.34
15:40	7600.300	6.76	0.38
16:40	7660.300	6.72	0.42
17:40	7720.300	6.69	0.45
18:40	7780.200	6.66	0.48
19:40	7840.200	6.67	0.47
20:40	7900.300	6.64	0.50
21:40	7960.300	6.63	0.51
22:40	8020.300	6.62	0.52
23:40	8080.300	6.60	0.54
00:40	8140.300	6.56	0.58
01:40	8200.300	6.53	0.61
02:40	8260.300	6.52	0.62
03:40	8320.300	6.49	0.65
04:40	8380.300	6.47	0.67
05:40	8440.300	6.46	0.68
06:40	8500.300	6.46	0.68
07:40	8560.200	6.45	0.69
08:40	8620.300	6.47	0.67
09:00	8640.600	6.48	0.66

## ADJUSTED DATA

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : REI 10-3 INPUT 10  
RADIUS: 63.843 FEET  
START DATE : 13-Oct-86  
START TIME : 10:25  
WATER START LEVEL: 7.14 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
10:25	8725.000	6.45	0.69
10:35	8735.071	6.44	0.70
10:45	8745.070	6.44	0.70
10:55	8755.072	6.43	0.71
11:05	8765.072	6.43	0.71
11:15	8775.072	6.45	0.69
11:25	8785.072	6.45	0.69
11:35	8795.072	6.44	0.70
11:45	8805.072	6.42	0.72
11:55	8815.102	6.42	0.72
12:05	8825.090	6.42	0.72
12:15	8835.090	6.42	0.72
12:25	8845.090	6.41	0.73
12:35	8855.090	6.42	0.72
12:45	8865.090	6.40	0.74
12:55	8875.120	6.40	0.74
13:04	8884.970	6.40	0.74
13:14	8894.970	6.40	0.74
13:25	8904.970	6.40	0.74
13:34	8914.970	6.40	0.74
13:45	8924.970	6.39	0.75
13:54	8934.970	6.37	0.77
14:05	8944.970	6.38	0.76
14:14	8955.020	6.37	0.77
14:25	8965.080	6.37	0.77
14:35	8975.080	6.36	0.78
14:45	8985.080	6.36	0.78
14:55	8995.080	6.36	0.78
15:05	9005.080	6.36	0.78
15:15	9015.080	6.35	0.79
15:25	9025.080	6.35	0.79
15:35	9035.080	6.34	0.80
15:45	9045.080	6.34	0.80
15:55	9055.080	6.33	0.81
16:04	9065.020	6.33	0.81
16:15	9075.020	6.33	0.81
16:25	9084.970	6.33	0.81
16:35	9095.080	6.33	0.81
16:45	9105.080	6.32	0.82
16:55	9115.080	6.32	0.82

## ADJUSTED DATA

17:05	9125.080	6.31	0.83
17:15	9135.080	6.31	0.83
17:25	9145.080	6.31	0.83
17:35	9155.080	6.31	0.83
17:45	9165.080	6.31	0.83
17:55	9175.080	6.31	0.83
18:05	9185.080	6.31	0.83
18:15	9195.080	6.30	0.84
18:25	9205.080	6.30	0.84
18:35	9215.080	6.30	0.84
18:45	9225.080	6.30	0.84
18:55	9235.080	6.29	0.85
19:05	9245.080	6.29	0.85
19:15	9255.080	6.29	0.85
19:25	9265.080	6.29	0.85
19:35	9275.070	6.29	0.85
19:45	9285.080	6.29	0.85
19:55	9295.080	6.29	0.85
20:05	9305.080	6.29	0.85
20:15	9315.080	6.29	0.85
20:25	9325.080	6.29	0.85
20:35	9335.080	6.29	0.85
20:45	9345.080	6.29	0.85
20:55	9355.080	6.29	0.85
21:05	9365.080	6.29	0.85
21:15	9375.080	6.30	0.84
21:25	9385.080	6.30	0.84
21:35	9395.080	6.30	0.84
21:45	9405.080	6.30	0.84
21:55	9415.080	6.30	0.84
22:05	9425.080	6.30	0.84
22:15	9435.080	6.30	0.84
22:25	9445.080	6.30	0.84
22:35	9455.080	6.30	0.84
22:45	9465.080	6.30	0.84
22:54	9475.020	6.29	0.85
23:05	9485.020	6.29	0.85
23:14	9495.020	6.29	0.85
23:25	9505.020	6.29	0.85
23:34	9515.020	6.28	0.86
23:45	9525.020	6.29	0.85
23:55	9535.020	6.28	0.86
00:05	9545.020	6.28	0.86
00:15	9555.020	6.28	0.86
00:25	9565.030	6.28	0.86
00:35	9575.030	6.27	0.87
00:44	9585.030	6.27	0.87
00:55	9595.030	6.27	0.87
01:04	9605.030	6.27	0.87
01:15	9615.030	6.27	0.87
01:25	9625.030	6.27	0.87
01:35	9635.030	6.27	0.87
01:45	9645.030	6.27	0.87
01:55	9655.030	6.27	0.87
02:05	9665.030	6.27	0.87
02:14	9675.030	6.27	0.87

## ADJUSTED DATA

02:25	9685.030	6.27	0.87
02:34	9695.030	6.27	0.87
02:45	9705.030	6.28	0.86
02:55	9715.030	6.28	0.86
03:04	9725.000	6.28	0.86
03:15	9735.000	6.28	0.86
03:24	9745.000	6.28	0.86
03:35	9755.100	6.27	0.87
03:44	9765.000	6.27	0.87
03:55	9775.000	6.27	0.87
04:04	9785.000	6.27	0.87
04:15	9795.000	6.27	0.87
04:25	9805.000	6.27	0.87
04:34	9815.000	6.27	0.87
04:45	9825.000	6.27	0.87
04:54	9835.000	6.27	0.87
05:05	9845.000	6.27	0.87
05:14	9855.000	6.27	0.87
05:25	9865.000	6.27	0.87
05:34	9875.000	6.27	0.87
05:45	9885.000	6.28	0.86
05:55	9895.000	6.28	0.86
06:04	9905.000	6.27	0.87
06:15	9915.000	6.28	0.86
06:24	9925.000	6.28	0.86
06:35	9935.000	6.28	0.86
06:44	9945.000	6.28	0.86
06:55	9955.000	6.28	0.86
07:05	9965.100	6.28	0.86
07:15	9975.100	6.29	0.85
07:25	9985.100	6.29	0.85
07:35	9995.100	6.29	0.85
07:45	10005.100	6.29	0.85
07:55	10015.100	6.29	0.85
08:05	10025.100	6.30	0.84
08:15	10035.100	6.31	0.83
08:25	10045.100	6.31	0.83
08:35	10055.100	6.32	0.82
08:45	10065.100	6.32	0.82
08:55	10075.000	6.32	0.82
09:04	10085.000	6.33	0.81
09:15	10095.000	6.33	0.81
09:24	10105.000	6.33	0.81
09:28	10108.200	6.33	0.81

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 2  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 10-3 INPUT 10  
 RADIUS: 63.843 FEET  
 START DATE: 07-Oct-86  
 START TIME: 11:10  
 WATER START LEVEL: 7.14 FEET  
 WATER STOP LEVEL: 6.39 FEET  
 TOTAL PUMPING TIME: 10210.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
11:10	0.017	-999.99	1006.38	1007.13
11:10	0.034	-999.99	1006.38	1007.13
11:10	0.050	-999.99	1006.38	1007.13
11:10	0.067	-999.99	1006.38	1007.13
11:10	0.084	-999.99	1006.38	1007.13
11:10	0.100	-999.99	1006.38	1007.13
11:10	0.117	-999.99	1006.38	1007.13
11:10	0.134	-999.99	1006.38	1007.13
11:10	0.150	-999.99	1006.38	1007.13
11:10	0.167	-999.99	1006.38	1007.13
11:10	0.257	6.39	0.00	0.75
11:10	0.341	6.39	0.00	0.75
11:10	0.424	6.39	0.00	0.75
11:10	0.507	6.39	0.00	0.75
11:10	0.591	6.39	0.00	0.75
11:10	0.674	6.39	0.00	0.75
11:10	0.757	6.39	0.00	0.75
11:10	0.841	6.39	0.00	0.75
11:10	0.924	6.39	0.00	0.75
11:11	1.007	6.39	0.00	0.75
11:11	1.413	6.39	0.00	0.75
11:11	1.747	6.39	0.00	0.75
11:12	2.080	6.39	0.00	0.75
11:12	2.413	6.39	0.00	0.75
11:12	2.747	6.39	0.00	0.75
11:13	3.080	6.39	0.00	0.75
11:13	3.413	6.39	0.00	0.75
11:13	3.747	6.39	0.00	0.75
11:14	4.080	6.39	0.00	0.75
11:14	4.413	6.39	0.00	0.75
11:14	4.747	6.39	0.00	0.75
11:15	5.080	6.39	0.00	0.75
11:15	5.413	6.39	0.00	0.75
11:15	5.747	6.39	0.00	0.75
11:16	6.080	6.39	0.00	0.75
11:16	6.413	6.39	0.00	0.75
11:16	6.747	6.39	0.00	0.75
11:17	7.080	6.39	0.00	0.75

11:17	7.413	6.39	0.00	0.75
11:17	7.747	6.39	0.00	0.75
11:18	8.080	6.39	0.00	0.75
11:18	8.413	6.38	0.01	0.76
11:18	8.747	6.39	0.00	0.75
11:19	9.080	6.39	0.00	0.75
11:19	9.413	6.39	0.00	0.75
11:19	9.747	6.39	0.00	0.75
11:20	10.080	6.39	0.00	0.75
11:22	12.115	6.40	-0.01	0.74
11:24	14.115	6.40	-0.01	0.74
11:26	16.115	6.40	-0.01	0.74
11:28	18.115	6.40	-0.01	0.74
11:30	20.115	6.40	-0.01	0.74
11:32	22.115	6.40	-0.01	0.74
11:34	24.115	6.40	-0.01	0.74
11:36	26.115	6.40	-0.01	0.74
11:38	28.115	6.40	-0.01	0.74
11:40	30.115	6.40	-0.01	0.74
11:42	32.115	6.40	-0.01	0.74
11:44	34.115	6.40	-0.01	0.74
11:46	36.115	6.40	-0.01	0.74
11:48	38.115	6.40	-0.01	0.74
11:50	40.115	6.40	-0.01	0.74
11:52	42.115	6.41	-0.02	0.73
11:54	44.115	6.40	-0.01	0.74
11:56	46.115	6.40	-0.01	0.74
11:58	48.115	6.40	-0.01	0.74
12:00	50.115	6.40	-0.01	0.74
12:02	52.115	6.40	-0.01	0.74
12:04	54.115	6.40	-0.01	0.74
12:06	56.115	6.40	-0.01	0.74
12:08	58.115	6.40	-0.01	0.74
12:10	60.115	6.40	-0.01	0.74
12:12	62.102	6.40	-0.01	0.74
12:14	64.492	6.40	-0.01	0.74
12:16	66.188	6.39	0.00	0.75
12:18	68.188	6.39	0.00	0.75
12:20	70.188	6.39	0.00	0.75
12:22	72.188	6.39	0.00	0.75
12:24	74.188	6.39	0.00	0.75
12:26	76.188	6.39	0.00	0.75
12:28	78.188	6.39	0.00	0.75
12:30	80.188	6.39	0.00	0.75
12:32	82.188	6.39	0.00	0.75
12:34	84.188	6.39	0.00	0.75
12:36	86.188	6.39	0.00	0.75
12:38	88.188	6.39	0.00	0.75
12:40	90.188	6.39	0.00	0.75
12:42	92.188	6.39	0.00	0.75
12:44	94.188	6.39	0.00	0.75
12:46	96.188	6.39	0.00	0.75
12:48	98.188	6.39	0.00	0.75
13:10	120.110	6.38	0.01	0.76
13:30	140.110	6.38	0.01	0.76
13:50	160.120	6.37	0.02	0.77



14:10	180.120	6.36	0.03	0.78
14:30	200.120	6.35	0.04	0.79
14:50	220.120	6.35	0.04	0.79
15:10	240.120	6.34	0.05	0.80
15:30	260.120	6.34	0.05	0.80
15:50	280.120	6.34	0.05	0.80
16:10	300.120	6.34	0.05	0.80
16:30	320.050	6.34	0.05	0.80
16:49	340.050	6.34	0.05	0.80
17:10	360.050	6.34	0.05	0.80
17:30	380.050	6.35	0.04	0.79
17:50	400.050	6.35	0.04	0.79
18:10	420.050	6.35	0.04	0.79
18:30	440.050	6.36	0.03	0.78
18:50	460.050	6.37	0.02	0.77
19:10	480.050	6.37	0.02	0.77
19:30	500.050	6.38	0.01	0.76
19:49	520.050	6.39	0.00	0.75
20:10	540.050	6.39	0.00	0.75
20:30	560.050	6.41	-0.02	0.73
20:50	580.050	6.42	-0.03	0.72
21:10	600.050	6.42	-0.03	0.72
21:30	620.050	6.43	-0.04	0.71
21:50	640.050	6.43	-0.04	0.71
22:10	660.050	6.44	-0.05	0.70
22:30	680.050	6.45	-0.06	0.69
22:49	700.050	6.45	-0.06	0.69
23:10	720.050	6.46	-0.07	0.68
23:30	740.050	6.46	-0.07	0.68
23:50	760.100	6.46	-0.07	0.68
00:10	780.100	6.47	-0.08	0.67
00:30	800.100	6.47	-0.08	0.67
00:50	820.100	6.47	-0.08	0.67
01:10	840.100	6.47	-0.08	0.67
01:30	860.100	6.47	-0.08	0.67
01:50	880.100	6.48	-0.09	0.66
02:10	900.100	6.48	-0.09	0.66
02:30	920.100	6.49	-0.10	0.65
02:50	940.100	6.49	-0.10	0.65
03:10	960.100	6.50	-0.11	0.64
03:30	980.100	6.49	-0.10	0.65
03:50	1000.100	6.50	-0.11	0.64
04:50	1060.300	6.50	-0.11	0.64
05:50	1120.300	6.52	-0.13	0.62
06:50	1180.300	6.54	-0.15	0.60
07:50	1240.300	6.55	-0.16	0.59
08:50	1300.300	6.58	-0.19	0.56
09:50	1360.300	6.60	-0.21	0.54
10:50	1420.300	6.61	-0.22	0.53
11:50	1480.300	6.61	-0.22	0.53
12:50	1540.300	6.59	-0.20	0.55
13:50	1600.300	6.57	-0.18	0.57
14:50	1660.300	6.54	-0.15	0.60
15:50	1720.100	6.53	-0.14	0.61
16:50	1780.100	6.53	-0.14	0.61
17:50	1840.100	6.53	-0.14	0.61

18:50	1900.100	6.54	-0.15	0.60
19:50	1960.100	6.56	-0.17	0.58
20:50	2020.100	6.58	-0.19	0.56
21:50	2080.100	6.59	-0.20	0.55
22:50	2140.100	6.60	-0.21	0.54
23:50	2200.100	6.62	-0.23	0.52
00:50	2260.100	6.61	-0.22	0.53
01:50	2320.100	6.61	-0.22	0.53
02:50	2380.100	6.61	-0.22	0.53
03:50	2440.100	6.60	-0.21	0.54
04:50	2500.100	6.61	-0.22	0.53
05:50	2560.100	6.61	-0.22	0.53
06:50	2620.100	6.63	-0.24	0.51
07:50	2680.100	6.63	-0.24	0.51
08:50	2740.200	6.64	-0.25	0.50
09:50	2800.200	6.65	-0.26	0.49
10:50	2860.200	6.65	-0.26	0.49
11:50	2920.100	6.65	-0.26	0.49
12:50	2980.200	6.63	-0.24	0.51
13:50	3040.200	6.59	-0.20	0.55
14:50	3100.200	6.56	-0.17	0.58
15:50	3160.200	6.54	-0.15	0.60
16:50	3220.200	6.54	-0.15	0.60
17:50	3280.200	6.53	-0.14	0.61
18:50	3340.200	6.54	-0.15	0.60
19:50	3400.200	6.55	-0.16	0.59
20:50	3460.200	6.56	-0.17	0.58
21:50	3520.200	6.57	-0.18	0.57
22:50	3580.200	6.58	-0.19	0.56
23:50	3640.200	6.58	-0.19	0.56
00:50	3700.200	6.58	-0.19	0.56
01:50	3760.200	6.58	-0.19	0.56
02:50	3820.200	6.58	-0.19	0.56
03:50	3880.200	6.58	-0.19	0.56
04:50	3940.200	6.57	-0.18	0.57
05:50	4000.200	6.57	-0.18	0.57
06:50	4060.200	6.59	-0.20	0.55
07:50	4120.200	6.60	-0.21	0.54
08:50	4180.200	6.62	-0.23	0.52
09:50	4240.200	-999.99	1006.38	1007.13
10:50	4300.200	-999.99	1006.38	1007.13
11:04	4314.800	-999.99	1006.38	1007.13

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 10-1 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 10-4 INPUT 11  
 RADIUS: 34.651 FEET  
 START DATE : 07-Oct-86  
 START TIME : 09:00  
 WATER START LEVEL: 7.66 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
09:00	0.000	7.66	0.00
09:00	0.017	-99.99	107.65
09:00	0.034	-99.99	107.65
09:00	0.050	-99.99	107.65
09:00	0.067	-99.99	107.65
09:00	0.084	-99.99	107.65
09:00	0.100	-99.99	107.65
09:00	0.117	-99.99	107.65
09:00	0.134	-99.99	107.65
09:00	0.150	-99.99	107.65
09:00	0.167	-99.99	107.65
09:00	0.257	7.66	0.00
09:00	0.340	7.66	0.00
09:00	0.424	7.66	0.00
09:00	0.507	7.66	0.00
09:00	0.590	7.66	0.00
09:00	0.674	7.66	0.00
09:00	0.757	7.66	0.00
09:00	0.840	7.66	0.00
09:00	0.924	7.66	0.00
09:01	1.007	7.66	0.00
09:01	1.414	7.66	0.00
09:01	1.748	7.66	0.00
09:02	2.081	7.66	0.00
09:02	2.414	7.66	0.00
09:02	2.748	7.66	0.00
09:03	3.081	7.66	0.00
09:03	3.415	7.66	0.00
09:03	3.748	7.66	0.00
09:04	4.081	7.66	0.00
09:04	4.414	7.66	0.00
09:04	4.748	7.66	0.00
09:05	5.081	7.66	0.00
09:05	5.414	7.66	0.00
09:05	5.748	7.66	0.00
09:06	6.081	7.66	0.00
09:06	6.415	7.66	0.00
09:06	6.748	7.66	0.00
09:07	7.081	7.66	0.00
09:07	7.415	7.66	0.00
09:07	7.748	7.66	0.00

09:08	8.081	7.66	0.00
09:08	8.415	7.66	0.00
09:08	8.748	7.66	0.00
09:09	9.081	7.66	0.00
09:09	9.414	7.66	0.00
09:09	9.748	7.66	0.00
09:10	10.081	7.66	0.00
09:12	12.108	7.66	0.00
09:14	14.152	7.66	0.00
09:16	16.152	7.66	0.00
09:18	18.152	7.66	0.00
09:20	20.152	7.66	0.00
09:22	22.152	7.66	0.00
09:24	24.152	7.66	0.00
09:26	26.152	7.66	0.00
09:28	28.215	7.66	0.00
09:30	30.197	7.65	0.01
09:32	32.197	7.66	0.00
09:34	34.197	7.66	0.00
09:36	36.197	7.66	0.00
09:38	38.197	7.66	0.00
09:40	40.197	7.66	0.00
09:42	42.197	7.66	0.00
09:44	44.197	7.66	0.00
09:46	46.197	7.66	0.00
09:48	48.197	7.66	0.00
09:50	50.197	7.66	0.00
09:52	52.197	7.66	0.00
09:54	54.197	7.66	0.00
09:56	56.217	7.65	0.01
09:58	58.100	7.65	0.01
10:00	60.245	7.65	0.01
10:02	62.245	7.65	0.01
10:04	64.245	7.65	0.01
10:06	66.245	7.65	0.01
10:08	68.245	7.65	0.01
10:10	70.245	7.65	0.01
10:12	72.245	7.65	0.01
10:14	74.245	7.65	0.01
10:16	76.245	7.65	0.01
10:18	78.245	7.65	0.01
10:20	80.245	7.65	0.01
10:22	82.245	7.65	0.01
10:24	84.245	7.65	0.01
10:26	86.245	7.65	0.01
10:28	88.245	7.65	0.01
10:30	90.245	7.65	0.01
10:32	92.245	7.65	0.01
10:34	94.245	7.65	0.01
10:36	96.245	7.64	0.02
10:38	98.245	7.64	0.02
11:00	120.210	7.64	0.02
11:20	140.210	7.63	0.03
11:40	160.210	7.62	0.04
12:00	180.220	7.61	0.05
12:20	200.220	7.60	0.06

12:40	220.220	7.58	0.08
13:00	240.220	7.57	0.09
13:20	260.220	7.55	0.11
13:40	280.230	7.53	0.13
14:00	300.230	7.50	0.16
14:20	320.230	7.50	0.16
14:40	340.180	7.49	0.17
15:00	360.100	7.48	0.18
15:20	380.100	7.46	0.20
15:40	400.100	7.45	0.21
16:00	420.170	7.44	0.22
16:20	440.250	7.43	0.23
16:40	460.200	7.42	0.24
17:00	480.170	7.41	0.25
17:20	500.170	7.41	0.25
17:40	520.130	7.40	0.26
18:00	540.120	7.40	0.26
18:20	560.220	7.39	0.27
18:40	580.080	7.39	0.27
19:00	600.220	7.39	0.27
19:20	620.230	7.39	0.27
19:40	640.220	7.39	0.27
20:00	660.220	7.38	0.28
20:20	680.130	7.38	0.28
20:40	700.120	7.38	0.28
21:00	720.230	7.38	0.28
21:20	740.300	7.38	0.28
21:40	760.230	7.39	0.27
22:00	780.230	7.39	0.27
22:20	800.230	7.39	0.27
22:40	820.180	7.40	0.26
23:00	840.570	7.39	0.27
23:20	860.180	7.38	0.28
23:40	880.080	7.38	0.28
00:00	900.170	7.38	0.28
00:20	920.170	7.38	0.28
00:40	940.170	7.38	0.28
01:00	960.170	7.37	0.29
01:20	980.170	7.36	0.30
01:40	1000.200	7.36	0.30
02:40	1060.300	7.35	0.31
03:40	1120.300	7.35	0.31
04:40	1180.300	7.34	0.32
05:40	1240.300	7.35	0.31
06:40	1300.300	7.35	0.31
07:40	1360.200	7.35	0.31
08:40	1420.200	7.36	0.30
09:40	1480.200	7.38	0.28
10:40	1540.200	7.38	0.28
11:40	1600.300	7.39	0.27
12:40	1660.300	7.39	0.27
13:40	1720.200	7.37	0.29
14:40	1780.300	7.35	0.31
15:40	1840.300	7.34	0.32
16:40	1900.300	7.32	0.34
17:40	1960.200	7.32	0.34

18:40	2020.200	7.32	0.34
19:40	2080.200	7.32	0.34
20:40	2140.200	7.33	0.33
21:40	2200.300	7.34	0.32
22:40	2260.300	7.34	0.32
23:40	2320.200	7.33	0.33
00:40	2380.200	7.32	0.34
01:40	2440.200	7.31	0.35
02:40	2500.200	7.31	0.35
03:40	2560.200	7.30	0.36
04:40	2620.200	7.29	0.37
05:40	2680.200	7.30	0.36
06:40	2740.200	7.30	0.36
07:40	2800.200	7.32	0.34
08:40	2860.300	7.33	0.33
09:40	2920.300	7.35	0.31
10:40	2980.300	7.36	0.30
11:40	3040.200	7.36	0.30
12:40	3100.200	7.33	0.33
13:40	3160.300	7.33	0.33
14:40	3220.300	7.30	0.36
15:40	3280.200	7.31	0.35
16:40	3340.200	7.28	0.38
17:40	3400.300	7.29	0.37
18:40	3460.300	7.30	0.36
19:40	3520.300	7.31	0.35
20:40	3580.200	7.32	0.34
21:40	3640.200	7.33	0.33
22:40	3700.200	7.33	0.33
23:40	3760.200	7.33	0.33
00:40	3820.200	7.32	0.34
01:40	3880.200	7.31	0.35
02:40	3940.200	7.31	0.35
03:40	4000.200	7.30	0.36
04:40	4060.200	7.29	0.37
05:40	4120.200	7.30	0.36
06:40	4180.200	7.31	0.35
07:40	4240.300	7.32	0.34
08:40	4300.300	7.32	0.34
09:40	4360.700	7.34	0.32
10:40	4420.300	7.33	0.33
11:40	4480.300	7.33	0.33
12:40	4540.300	7.31	0.35
13:40	4600.300	7.29	0.37
14:40	4660.300	7.28	0.38
15:40	4720.300	7.19	0.47
16:40	4780.300	7.23	0.43
17:40	4840.300	7.22	0.44
18:40	4900.300	7.22	0.44
19:40	4960.300	7.23	0.43
20:40	5020.300	7.23	0.43
21:40	5080.300	7.25	0.41
22:40	5140.300	7.24	0.42
23:40	5200.300	7.25	0.41
00:40	5260.300	7.24	0.42
01:40	5320.300	7.22	0.44

02:40	5380.300	7.22	0.44
03:40	5440.300	7.22	0.44
04:40	5500.300	7.20	0.46
05:40	5560.300	7.20	0.46
06:40	5620.300	7.22	0.44
07:40	5680.300	7.23	0.43
08:40	5740.300	7.22	0.44
09:40	5800.300	7.25	0.41
10:40	5860.300	7.26	0.40
11:40	5920.300	7.28	0.38
12:40	5980.300	7.27	0.39
13:40	6040.300	7.26	0.40
14:40	6100.300	7.20	0.46
15:40	6160.500	7.19	0.47
16:40	6220.300	7.19	0.47
17:40	6280.300	7.20	0.46
18:40	6340.300	7.24	0.42
19:40	6400.400	7.23	0.43
20:40	6460.200	7.24	0.42
21:40	6520.200	7.24	0.42
22:40	6580.300	7.24	0.42
23:40	6640.300	7.24	0.42
00:40	6700.300	7.24	0.42
01:40	6760.300	7.25	0.41
02:40	6820.300	7.23	0.43
03:40	6880.300	7.22	0.44
04:40	6940.300	7.20	0.46
05:40	7000.300	7.19	0.47
06:40	7060.300	7.22	0.44
07:40	7120.300	7.26	0.40
08:40	7180.300	7.31	0.35
09:40	7240.300	7.32	0.34
10:40	7300.300	7.31	0.35
11:40	7360.300	7.31	0.35
12:40	7420.300	7.30	0.36
13:40	7480.300	7.28	0.38
14:40	7540.300	7.24	0.42
15:40	7600.300	7.22	0.44
16:40	7660.300	7.20	0.46
17:40	7720.300	7.16	0.50
18:40	7780.200	7.16	0.50
19:40	7840.200	7.16	0.50
20:40	7900.300	7.13	0.53
21:40	7960.300	7.12	0.54
22:40	8020.300	7.10	0.56
23:40	8080.300	7.08	0.58
00:40	8140.300	7.04	0.62
01:40	8200.300	7.01	0.65
02:40	8260.300	6.98	0.68
03:40	8320.300	6.95	0.71
04:40	8380.300	6.92	0.74
05:40	8440.300	6.90	0.76
06:40	8500.300	6.90	0.76
07:40	8560.200	6.89	0.77
08:40	8620.300	6.90	0.76
09:00	8640.600	6.90	0.76

## ADJUSTED DATA

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : REI 10-4 INPUT 11  
RADIUS: 34.651 FEET  
START DATE : 13-Oct-86  
START TIME : 10:25  
WATER START LEVEL: 7.66 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
10:25	8725.000	6.89	0.77
10:35	8735.071	6.88	0.78
10:45	8745.070	6.88	0.78
10:55	8755.072	6.88	0.78
11:05	8765.072	6.89	0.77
11:15	8775.072	6.91	0.75
11:25	8785.072	6.88	0.78
11:35	8795.072	6.87	0.79
11:45	8805.072	6.86	0.80
11:55	8815.102	6.86	0.80
12:05	8825.090	6.87	0.79
12:15	8835.090	6.86	0.80
12:25	8845.090	6.86	0.80
12:35	8855.090	6.85	0.81
12:45	8865.090	6.84	0.82
12:55	8875.120	6.84	0.82
13:04	8884.970	6.86	0.80
13:14	8894.970	6.85	0.81
13:25	8904.970	6.84	0.82
13:34	8914.970	6.83	0.83
13:45	8924.970	6.83	0.83
13:54	8934.970	6.81	0.85
14:05	8944.970	6.83	0.83
14:14	8955.020	6.82	0.84
14:25	8965.080	6.81	0.85
14:35	8975.080	6.80	0.86
14:45	8985.080	6.81	0.85
14:55	8995.080	6.81	0.85
15:05	9005.080	6.80	0.86
15:15	9015.080	6.79	0.87
15:25	9025.080	6.79	0.87
15:35	9035.080	6.79	0.87
15:45	9045.080	6.78	0.88
15:55	9055.080	6.77	0.89
16:04	9065.020	6.77	0.89
16:15	9075.020	6.77	0.89
16:25	9084.970	6.77	0.89
16:35	9095.080	6.76	0.90
16:45	9105.080	6.75	0.91
16:55	9115.080	6.75	0.91



## ADJUSTED DATA

17:05	9125.080	6.74	0.92
17:15	9135.080	6.74	0.92
17:25	9145.080	6.75	0.91
17:35	9155.080	6.75	0.91
17:45	9165.080	6.76	0.90
17:55	9175.080	6.74	0.92
18:05	9185.080	6.74	0.92
18:15	9195.080	6.73	0.93
18:25	9205.080	6.72	0.94
18:35	9215.080	6.73	0.93
18:45	9225.080	6.73	0.93
18:55	9235.080	6.72	0.94
19:05	9245.080	6.72	0.94
19:15	9255.080	6.72	0.94
19:25	9265.080	6.72	0.94
19:35	9275.070	6.72	0.94
19:45	9285.080	6.72	0.94
19:55	9295.080	6.72	0.94
20:05	9305.080	6.72	0.94
20:15	9315.080	6.71	0.95
20:25	9325.080	6.72	0.94
20:35	9335.080	6.72	0.94
20:45	9345.080	6.72	0.94
20:55	9355.080	6.72	0.94
21:05	9365.080	6.73	0.93
21:15	9375.080	6.73	0.93
21:25	9385.080	6.73	0.93
21:35	9395.080	6.72	0.94
21:45	9405.080	6.73	0.93
21:55	9415.080	6.72	0.94
22:05	9425.080	6.72	0.94
22:15	9435.080	6.72	0.94
22:25	9445.080	6.72	0.94
22:35	9455.080	6.72	0.94
22:45	9465.080	6.72	0.94
22:54	9475.020	6.72	0.94
23:05	9485.020	6.72	0.94
23:14	9495.020	6.72	0.94
23:25	9505.020	6.71	0.95
23:34	9515.020	6.71	0.95
23:45	9525.020	6.71	0.95
23:55	9535.020	6.71	0.95
00:05	9545.020	6.70	0.96
00:15	9555.020	6.70	0.96
00:25	9565.030	6.70	0.96
00:35	9575.030	6.70	0.96
00:44	9585.030	6.70	0.96
00:55	9595.030	6.70	0.96
01:04	9605.030	6.70	0.96
01:15	9615.030	6.69	0.97
01:25	9625.030	6.69	0.97
01:35	9635.030	6.70	0.96
01:45	9645.030	6.70	0.96
01:55	9655.030	6.70	0.96
02:05	9665.030	6.70	0.96
02:14	9675.030	6.70	0.96

## ADJUSTED DATA

02:25	9685.030	6.69	0.97
02:34	9695.030	6.69	0.97
02:45	9705.030	6.70	0.96
02:55	9715.030	6.70	0.96
03:04	9725.000	6.70	0.96
03:15	9735.000	6.69	0.97
03:24	9745.000	6.69	0.97
03:35	9755.100	6.69	0.97
03:44	9765.000	6.68	0.98
03:55	9775.000	6.68	0.98
04:04	9785.000	6.68	0.98
04:15	9795.000	6.68	0.98
04:25	9805.000	6.68	0.98
04:34	9815.000	6.68	0.98
04:45	9825.000	6.68	0.98
04:54	9835.000	6.68	0.98
05:05	9845.000	6.68	0.98
05:14	9855.000	6.68	0.98
05:25	9865.000	6.68	0.98
05:34	9875.000	6.68	0.98
05:45	9885.000	6.68	0.98
05:55	9895.000	6.68	0.98
06:04	9905.000	6.68	0.98
06:15	9915.000	6.68	0.98
06:24	9925.000	6.68	0.98
06:35	9935.000	6.68	0.98
06:44	9945.000	6.68	0.98
06:55	9955.000	6.68	0.98
07:05	9965.100	6.69	0.97
07:15	9975.100	6.69	0.97
07:25	9985.100	6.69	0.97
07:35	9995.100	6.70	0.96
07:45	10005.100	6.70	0.96
07:55	10015.100	6.70	0.96
08:05	10025.100	6.70	0.96
08:15	10035.100	6.71	0.95
08:25	10045.100	6.72	0.94
08:35	10055.100	6.72	0.94
08:45	10065.100	6.72	0.94
08:55	10075.000	6.72	0.94
09:04	10085.000	6.73	0.93
09:15	10095.000	6.73	0.93
09:24	10105.000	6.72	0.94
09:28	10108.200	6.72	0.94

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 2  
 TEST TYPE: RECOVERY  
 WELL NUMBER: REI 10-4 INPUT 11  
 RADIUS: 34.651 FEET  
 START DATE: 07-Oct-86  
 START TIME: 11:10  
 WATER START LEVEL: 7.66 FEET  
 WATER STOP LEVEL: 6.87 FEET  
 TOTAL PUMPING TIME: 10210.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
11:10	0.017	-999.99	1006.86	1007.65
11:10	0.034	-999.99	1006.86	1007.65
11:10	0.050	-999.99	1006.86	1007.65
11:10	0.067	-999.99	1006.86	1007.65
11:10	0.084	-999.99	1006.86	1007.65
11:10	0.100	-999.99	1006.86	1007.65
11:10	0.117	-999.99	1006.86	1007.65
11:10	0.134	-999.99	1006.86	1007.65
11:10	0.150	-999.99	1006.86	1007.65
11:10	0.167	-999.99	1006.86	1007.65
11:10	0.257	6.87	0.00	0.79
11:10	0.341	6.87	0.00	0.79
11:10	0.424	6.87	0.00	0.79
11:10	0.507	6.87	0.00	0.79
11:10	0.591	6.87	0.00	0.79
11:10	0.674	6.87	0.00	0.79
11:10	0.757	6.87	0.00	0.79
11:10	0.841	6.87	0.00	0.79
11:10	0.924	6.87	0.00	0.79
11:11	1.007	6.87	0.00	0.79
11:11	1.413	6.88	-0.01	0.78
11:11	1.747	6.87	0.00	0.79
11:12	2.080	6.88	-0.01	0.78
11:12	2.413	6.88	-0.01	0.78
11:12	2.747	6.88	-0.01	0.78
11:13	3.080	6.89	-0.02	0.77
11:13	3.413	6.89	-0.02	0.77
11:13	3.747	6.89	-0.02	0.77
11:14	4.080	6.88	-0.01	0.78
11:14	4.413	6.88	-0.01	0.78
11:14	4.747	6.87	0.00	0.79
11:15	5.080	6.87	0.00	0.79
11:15	5.413	6.87	0.00	0.79
11:15	5.747	6.87	0.00	0.79
11:16	6.080	6.87	0.00	0.79
11:16	6.413	6.87	0.00	0.79
11:16	6.747	6.87	0.00	0.79
11:17	7.080	6.87	0.00	0.79

11:17	7.413	6.87	0.00	0.79
11:17	7.747	6.88	-0.01	0.78
11:18	8.080	6.87	0.00	0.79
11:18	8.413	6.87	0.00	0.79
11:18	8.747	6.87	0.00	0.79
11:19	9.080	6.87	0.00	0.79
11:19	9.413	6.87	0.00	0.79
11:19	9.747	6.87	0.00	0.79
11:20	10.080	6.87	0.00	0.79
11:22	12.115	6.88	-0.01	0.78
11:24	14.115	6.88	-0.01	0.78
11:26	16.115	6.89	-0.02	0.77
11:28	18.115	6.88	-0.01	0.78
11:30	20.115	6.89	-0.02	0.77
11:32	22.115	6.89	-0.02	0.77
11:34	24.115	6.88	-0.01	0.78
11:36	26.115	6.88	-0.01	0.78
11:38	28.115	6.87	0.00	0.79
11:40	30.115	6.87	0.00	0.79
11:42	32.115	6.87	0.00	0.79
11:44	34.115	6.87	0.00	0.79
11:46	36.115	6.88	-0.01	0.78
11:48	38.115	6.88	-0.01	0.78
11:50	40.115	6.89	-0.02	0.77
11:52	42.115	6.89	-0.02	0.77
11:54	44.115	6.88	-0.01	0.78
11:56	46.115	6.88	-0.01	0.78
11:58	48.115	6.87	0.00	0.79
12:00	50.115	6.87	0.00	0.79
12:02	52.115	6.87	0.00	0.79
12:04	54.115	6.87	0.00	0.79
12:06	56.115	6.87	0.00	0.79
12:08	58.115	6.88	-0.01	0.78
12:10	60.115	6.88	-0.01	0.78
12:12	62.102	6.88	-0.01	0.78
12:14	64.492	6.87	0.00	0.79
12:16	66.188	6.87	0.00	0.79
12:18	68.188	6.87	0.00	0.79
12:20	70.188	6.87	0.00	0.79
12:22	72.188	6.88	-0.01	0.78
12:24	74.188	6.87	0.00	0.79
12:26	76.188	6.87	0.00	0.79
12:28	78.188	6.87	0.00	0.79
12:30	80.188	6.86	0.01	0.80
12:32	82.188	6.86	0.01	0.80
12:34	84.188	6.86	0.01	0.80
12:36	86.188	6.86	0.01	0.80
12:38	88.188	6.88	-0.01	0.78
12:40	90.188	6.86	0.01	0.80
12:42	92.188	6.87	0.00	0.79
12:44	94.188	6.87	0.00	0.79
12:46	96.188	6.86	0.01	0.80
12:48	98.188	6.85	0.02	0.81
13:10	120.110	6.86	0.01	0.80
13:30	140.110	6.85	0.02	0.81
13:50	160.120	6.85	0.02	0.81

14:10	180.120	6.83	0.04	0.83
14:30	200.120	6.83	0.04	0.83
14:50	220.120	6.81	0.06	0.85
15:10	240.120	6.80	0.07	0.86
15:30	260.120	6.82	0.05	0.84
15:50	280.120	6.82	0.05	0.84
16:10	300.120	6.81	0.06	0.85
16:30	320.050	6.82	0.05	0.84
16:49	340.050	6.80	0.07	0.86
17:10	360.050	6.81	0.06	0.85
17:30	380.050	6.81	0.06	0.85
17:50	400.050	6.82	0.05	0.84
18:10	420.050	6.82	0.05	0.84
18:30	440.050	6.82	0.05	0.84
18:50	460.050	6.83	0.04	0.83
19:10	480.050	6.83	0.04	0.83
19:30	500.050	6.84	0.03	0.82
19:49	520.050	6.85	0.02	0.81
20:10	540.050	6.86	0.01	0.80
20:30	560.050	6.87	0.00	0.79
20:50	580.050	6.88	-0.01	0.78
21:10	600.050	6.89	-0.02	0.77
21:30	620.050	6.89	-0.02	0.77
21:50	640.050	6.90	-0.03	0.76
22:10	660.050	6.90	-0.03	0.76
22:30	680.050	6.91	-0.04	0.75
22:49	700.050	6.91	-0.04	0.75
23:10	720.050	6.92	-0.05	0.74
23:30	740.050	6.93	-0.06	0.73
23:50	760.100	6.93	-0.06	0.73
00:10	780.100	6.93	-0.06	0.73
00:30	800.100	6.94	-0.07	0.72
00:50	820.100	6.94	-0.07	0.72
01:10	840.100	6.94	-0.07	0.72
01:30	860.100	6.95	-0.08	0.71
01:50	880.100	6.95	-0.08	0.71
02:10	900.100	6.95	-0.08	0.71
02:30	920.100	6.96	-0.09	0.70
02:50	940.100	6.96	-0.09	0.70
03:10	960.100	6.96	-0.09	0.70
03:30	980.100	6.97	-0.10	0.69
03:50	1000.100	6.97	-0.10	0.69
04:50	1060.300	6.98	-0.11	0.68
05:50	1120.300	6.99	-0.12	0.67
06:50	1180.300	7.01	-0.14	0.65
07:50	1240.300	7.03	-0.16	0.63
08:50	1300.300	7.07	-0.20	0.59
09:50	1360.300	7.10	-0.23	0.56
10:50	1420.300	7.10	-0.23	0.56
11:50	1480.300	7.10	-0.23	0.56
12:50	1540.300	7.08	-0.21	0.58
13:50	1600.300	7.05	-0.18	0.61
14:50	1660.300	7.03	-0.16	0.63
15:50	1720.100	7.03	-0.16	0.63
16:50	1780.100	7.03	-0.16	0.63
17:50	1840.100	7.03	-0.16	0.63

18:50	1900.100	7.03	-0.16	0.63
19:50	1960.100	7.05	-0.18	0.61
20:50	2020.100	7.07	-0.20	0.59
21:50	2080.100	7.08	-0.21	0.58
22:50	2140.100	7.10	-0.23	0.56
23:50	2200.100	7.11	-0.24	0.55
00:50	2260.100	7.11	-0.24	0.55
01:50	2320.100	7.11	-0.24	0.55
02:50	2380.100	7.10	-0.23	0.56
03:50	2440.100	7.10	-0.23	0.56
04:50	2500.100	7.11	-0.24	0.55
05:50	2560.100	7.12	-0.25	0.54
06:50	2620.100	7.12	-0.25	0.54
07:50	2680.100	7.14	-0.27	0.52
08:50	2740.200	7.15	-0.28	0.51
09:50	2800.200	7.17	-0.30	0.49
10:50	2860.200	7.16	-0.29	0.50
11:50	2920.100	7.15	-0.28	0.51
12:50	2980.200	7.13	-0.26	0.53
13:50	3040.200	7.07	-0.20	0.59
14:50	3100.200	7.08	-0.21	0.58
15:50	3160.200	7.04	-0.17	0.62
16:50	3220.200	7.03	-0.16	0.63
17:50	3280.200	7.03	-0.16	0.63
18:50	3340.200	7.03	-0.16	0.63
19:50	3400.200	7.05	-0.18	0.61
20:50	3460.200	7.06	-0.19	0.60
21:50	3520.200	7.07	-0.20	0.59
22:50	3580.200	7.08	-0.21	0.58
23:50	3640.200	7.07	-0.20	0.59
00:50	3700.200	7.07	-0.20	0.59
01:50	3760.200	7.07	-0.20	0.59
02:50	3820.200	7.07	-0.20	0.59
03:50	3880.200	7.07	-0.20	0.59
04:50	3940.200	7.07	-0.20	0.59
05:50	4000.200	7.07	-0.20	0.59
06:50	4060.200	7.08	-0.21	0.58
07:50	4120.200	7.10	-0.23	0.56
08:50	4180.200	7.12	-0.25	0.54
09:50	4240.200	-999.99	1006.86	1007.65
10:50	4300.200	-999.99	1006.86	1007.65
11:04	4314.800	-999.99	1006.86	1007.65

12:40	220.220	38.82	0.00
13:00	240.220	38.82	0.00
13:20	260.220	38.82	0.00
13:40	280.230	38.82	0.00
14:00	300.230	38.82	0.00
14:20	320.230	38.82	0.00
14:40	340.180	38.82	0.00
15:00	360.100	38.80	0.02
15:20	380.100	38.82	0.00
15:40	400.100	38.82	0.00
16:00	420.170	38.82	0.00
16:20	440.250	38.82	0.00
16:40	460.200	38.82	0.00
17:00	480.170	38.82	0.00
17:20	500.170	38.82	0.00
17:40	520.130	38.82	0.00
18:00	540.120	38.82	0.00
18:20	560.220	38.82	0.00
18:40	580.080	38.82	0.00
19:00	600.220	38.82	0.00
19:20	620.230	38.82	0.00
19:40	640.220	38.82	0.00
20:00	660.220	38.82	0.00
20:20	680.130	38.82	0.00
20:40	700.120	38.82	0.00
21:00	720.230	38.82	0.00
21:20	740.300	38.82	0.00
21:40	760.230	38.82	0.00
22:00	780.230	38.82	0.00
22:20	800.230	38.82	0.00
22:40	820.180	38.82	0.00
23:00	840.570	38.82	0.00
23:20	860.180	38.82	0.00
23:40	880.080	38.82	0.00
00:00	900.170	38.82	0.00
00:20	920.170	38.82	0.00
00:40	940.170	38.82	0.00
01:00	960.170	38.82	0.00
01:20	980.170	38.82	0.00
01:40	1000.200	38.82	0.00
02:40	1060.300	38.82	0.00
03:40	1120.300	38.82	0.00
04:40	1180.300	38.82	0.00
05:40	1240.300	38.82	0.00
06:40	1300.300	38.83	-0.01
07:40	1360.200	38.83	-0.01
08:40	1420.200	38.83	-0.01
09:40	1480.200	38.83	-0.01
10:40	1540.200	38.83	-0.01
11:40	1600.300	38.83	-0.01
12:40	1660.300	38.83	-0.01
13:40	1720.200	38.83	-0.01
14:40	1780.300	38.83	-0.01
15:40	1840.300	38.82	0.00
16:40	1900.300	38.82	0.00
17:40	1960.200	38.81	0.01

18:40	2020.200	38.81	0.01
19:40	2080.200	38.81	0.01
20:40	2140.200	38.81	0.01
21:40	2200.300	38.81	0.01
22:40	2260.300	38.81	0.01
23:40	2320.200	38.81	0.01
00:40	2380.200	38.81	0.01
01:40	2440.200	38.81	0.01
02:40	2500.200	38.81	0.01
03:40	2560.200	38.82	0.00
04:40	2620.200	38.81	0.01
05:40	2680.200	38.81	0.01
06:40	2740.200	38.82	0.00
07:40	2800.200	38.82	0.00
08:40	2860.300	38.82	0.00
09:40	2920.300	38.81	0.01
10:40	2980.300	38.81	0.01
11:40	3040.200	38.81	0.01
12:40	3100.200	38.81	0.01
13:40	3160.300	38.81	0.01
14:40	3220.300	38.82	0.00
15:40	3280.200	38.82	0.00
16:40	3340.200	38.81	0.01
17:40	3400.300	38.81	0.01
18:40	3460.300	38.81	0.01
19:40	3520.300	38.81	0.01
20:40	3580.200	38.82	0.00
21:40	3640.200	38.81	0.01
22:40	3700.200	38.81	0.01
23:40	3760.200	38.81	0.01
00:40	3820.200	38.81	0.01
01:40	3880.200	38.81	0.01
02:40	3940.200	38.81	0.01
03:40	4000.200	38.81	0.01
04:40	4060.200	38.81	0.01
05:40	4120.200	38.81	0.01
06:40	4180.200	38.81	0.01
07:40	4240.300	38.81	0.01
08:40	4300.300	38.81	0.01
09:40	4360.700	38.81	0.01
10:40	4420.300	38.81	0.01
11:40	4480.300	38.81	0.01
12:40	4540.300	38.81	0.01
13:40	4600.300	38.81	0.01
14:40	4660.300	38.81	0.01
15:40	4720.300	38.81	0.01
16:40	4780.300	38.81	0.01
17:40	4840.300	38.81	0.01
18:40	4900.300	38.81	0.01
19:40	4960.300	38.81	0.01
20:40	5020.300	38.81	0.01
21:40	5080.300	38.81	0.01
22:40	5140.300	38.81	0.01
23:40	5200.300	38.81	0.01
00:40	5260.300	38.80	0.02
01:40	5320.300	38.81	0.01



02:40	5380.300	38.81	0.01
03:40	5440.300	38.81	0.01
04:40	5500.300	38.80	0.02
05:40	5560.300	38.80	0.02
06:40	5620.300	38.80	0.02
07:40	5680.300	38.81	0.01
08:40	5740.300	38.81	0.01
09:40	5800.300	38.81	0.01
10:40	5860.300	38.81	0.01
11:40	5920.300	38.81	0.01
12:40	5980.300	38.81	0.01
13:40	6040.300	38.81	0.01
14:40	6100.300	38.81	0.01
15:40	6160.500	38.81	0.01
16:40	6220.300	38.80	0.02
17:40	6280.300	38.81	0.01
18:40	6340.300	38.81	0.01
19:40	6400.400	38.81	0.01
20:40	6460.200	38.80	0.02
21:40	6520.200	38.80	0.02
22:40	6580.300	38.80	0.02
23:40	6640.300	38.80	0.02
00:40	6700.300	38.80	0.02
01:40	6760.300	38.80	0.02
02:40	6820.300	38.81	0.01
03:40	6880.300	38.81	0.01
04:40	6940.300	38.81	0.01
05:40	7000.300	38.81	0.01
06:40	7060.300	38.82	0.00
07:40	7120.300	38.82	0.00
08:40	7180.300	38.81	0.01
09:40	7240.300	38.80	0.02
10:40	7300.300	38.79	0.03
11:40	7360.300	38.78	0.04
12:40	7420.300	38.78	0.04
13:40	7480.300	38.78	0.04
14:40	7540.300	38.78	0.04
15:40	7600.300	38.77	0.05
16:40	7660.300	38.77	0.05
17:40	7720.300	38.77	0.05
18:40	7780.200	38.77	0.05
19:40	7840.200	38.76	0.06
20:40	7900.300	38.76	0.06
21:40	7960.300	38.76	0.06
22:40	8020.300	38.76	0.06
23:40	8080.300	38.76	0.06
00:40	8140.300	38.75	0.07
01:40	8200.300	38.75	0.07
02:40	8260.300	38.75	0.07
03:40	8320.300	38.75	0.07
04:40	8380.300	38.75	0.07
05:40	8440.300	38.75	0.07
06:40	8500.300	38.74	0.08
07:40	8560.200	38.75	0.07
08:40	8620.300	38.74	0.08
09:00	8640.600	38.74	0.08

20:50	2020.100	39.64	0.01	0.08
21:50	2080.100	39.64	0.01	0.08
22:50	2140.100	39.64	0.01	0.08
23:50	2200.100	39.64	0.01	0.08
00:50	2260.100	39.64	0.01	0.08
01:50	2320.100	39.64	0.01	0.08
02:50	2380.100	39.64	0.01	0.08
03:50	2440.100	39.64	0.01	0.08
04:50	2500.100	39.64	0.01	0.08
05:50	2560.100	39.64	0.01	0.08
06:50	2620.100	39.64	0.01	0.08
07:50	2680.100	39.64	0.01	0.08
08:50	2740.200	39.64	0.01	0.08
09:50	2800.200	39.64	0.01	0.08
10:50	2860.200	39.64	0.01	0.08
11:50	2920.100	39.64	0.01	0.08
12:50	2980.200	39.64	0.01	0.08
13:50	3040.200	39.64	0.01	0.08
14:50	3100.200	39.64	0.01	0.08
15:50	3160.200	39.64	0.01	0.08
16:50	3220.200	39.64	0.01	0.08
17:50	3280.200	39.64	0.01	0.08
18:50	3340.200	39.64	0.01	0.08
19:50	3400.200	39.64	0.01	0.08
20:50	3460.200	39.63	0.02	0.09
21:50	3520.200	39.64	0.01	0.08
22:50	3580.200	39.64	0.01	0.08
23:50	3640.200	39.64	0.01	0.08
00:50	3700.200	39.64	0.01	0.08
01:50	3760.200	39.63	0.02	0.09
02:50	3820.200	39.64	0.01	0.08
03:50	3880.200	39.64	0.01	0.08
04:50	3940.200	39.64	0.01	0.08
05:50	4000.200	39.63	0.02	0.09
06:50	4060.200	39.63	0.02	0.09
07:50	4120.200	39.63	0.02	0.09
08:50	4180.200	39.64	0.01	0.08
09:50	4240.200	-999.99	1039.64	1039.71
10:50	4300.200	-999.99	1039.64	1039.71
11:04	4314.800	-999.99	1039.64	1039.71

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME : REI 10-1 RUN # 2  
 TEST TYPE : DRAWDOWN  
 WELL NUMBER : REI 12-1  
 RADIUS: 1492.112 FEET  
 START DATE : 07-Oct-86  
 START TIME : 09:00  
 WATER START LEVEL: 77.64 FEET

TIME	ELAPSED TIME (MIN)	WATER LEVEL (FEET)	DELTA HEAD (FEET)	t/r2
09:29	29.0	77.64	0.00	9.05E-09
11:22	142.0	77.66	-0.02	4.43E-08
13:16	256.0	77.81	-0.17	7.98E-08
15:23	383.0	78.08	-0.44	1.19E-07
19:26	626.0	78.71	-1.07	1.95E-07
22:05	785.0	79.11	-1.47	2.45E-07
23:24	864.0	79.39	-1.75	2.69E-07
01:08	968.0	79.59	-1.95	3.02E-07
03:25	1105.0	79.95	-2.31	3.45E-07
05:15	1215.0	80.23	-2.59	3.79E-07
07:26	1346.0	80.54	-2.90	4.20E-07
09:50	1490.0	80.88	-3.24	4.65E-07
11:37	1597.0	81.25	-3.61	4.98E-07
13:45	1725.0	81.34	-3.70	5.38E-07
15:35	1835.0	81.59	-3.95	5.72E-07
17:31	1951.0	81.77	-4.13	6.09E-07
19:43	2083.0	81.82	-4.18	6.50E-07
21:25	2185.0	82.22	-4.58	6.82E-07
23:27	2307.0	82.38	-4.74	7.20E-07
01:26	2426.0	82.59	-4.95	7.57E-07
03:52	2572.0	82.86	-5.22	8.02E-07
05:25	2665.0	82.96	-5.32	8.31E-07
07:05	2765.0	83.12	-5.48	8.62E-07
09:34	2914.0	83.35	-5.71	9.09E-07
11:43	3043.0	83.53	-5.89	9.49E-07
13:37	3157.0	83.69	-6.05	9.85E-07
15:55	3295.0	83.89	-6.25	1.03E-06
17:30	3390.0	84.02	-6.38	1.06E-06
20:00	3540.0	84.19	-6.55	1.10E-06
21:32	3632.0	84.34	-6.70	1.13E-06
23:54	3774.0	84.45	-6.81	1.18E-06
03:42	4002.0	84.72	-7.08	1.25E-06
07:22	4222.0	84.96	-7.32	1.32E-06
09:40	4360.0	85.11	-7.47	1.36E-06
11:36	4476.0	85.22	-7.58	1.40E-06
13:56	4616.0	85.35	-7.71	1.44E-06
15:44	4724.0	85.46	-7.82	1.47E-06
17:30	4830.0	85.56	-7.92	1.51E-06
19:28	4948.0	85.68	-8.04	1.54E-06

21:29	5069.0	85.73	-8.09	1.58E-06
23:33	5193.0	85.88	-8.24	1.62E-06
03:38	5437.0	86.03	-8.39	1.70E-06
07:18	5657.0	86.21	-8.57	1.76E-06
09:31	5790.0	86.33	-8.69	1.81E-06
11:35	5914.0	86.39	-8.75	1.84E-06
15:27	6146.0	86.67	-9.03	1.92E-06
17:46	6285.0	86.69	-9.05	1.96E-06
19:39	6398.0	86.78	-9.14	2.00E-06
22:00	6539.0	86.84	-9.20	2.04E-06
23:29	6628.0	86.86	-9.22	2.07E-06
02:01	6780.0	87.02	-9.38	2.11E-06
03:51	6890.0	87.02	-9.38	2.15E-06
05:45	7004.0	87.13	-9.49	2.18E-06
07:46	7125.0	87.13	-9.49	2.22E-06
09:48	7247.0	87.13	-9.49	2.26E-06
11:42	7361.0	87.43	-9.79	2.30E-06
13:34	7473.0	87.13	-9.49	2.33E-06
15:38	7597.0	87.15	-9.51	2.37E-06
17:38	7717.0	87.61	-9.97	2.41E-06
23:55	8094.0	87.72	-10.08	2.52E-06
07:27	8546.0	87.57	-9.93	2.67E-06
14:53	8992.0	87.73	-10.09	2.80E-06
19:55	9294.0	87.87	-10.23	2.90E-06
23:44	9523.0	87.98	-10.34	2.97E-06
03:53	9772.0	88.13	-10.49	3.05E-06
07:25	9984.0	88.22	-10.58	3.11E-06
09:33	10112.0	88.30	-10.66	3.15E-06

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : P 10-2 INPUT 6  
RADIUS: 20.845 FEET  
START DATE : 07-Oct-86  
START TIME : 09:00  
WATER START LEVEL: 46.06 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
09:00	0.000	46.06	0.00
09:00	0.017	-99.99	146.05
09:00	0.034	-99.99	146.05
09:00	0.050	-99.99	146.05
09:00	0.067	-99.99	146.05
09:00	0.084	-99.99	146.05
09:00	0.100	-99.99	146.05
09:00	0.117	-99.99	146.05
09:00	0.134	-99.99	146.05
09:00	0.150	-99.99	146.05
09:00	0.167	-99.99	146.05
09:00	0.257	46.05	0.01
09:00	0.340	46.05	0.01
09:00	0.424	46.05	0.01
09:00	0.507	46.05	0.01
09:00	0.590	46.05	0.01
09:00	0.674	46.05	0.01
09:00	0.757	46.05	0.01
09:00	0.840	46.05	0.01
09:00	0.924	46.04	0.02
09:01	1.007	46.04	0.02
09:01	1.414	46.04	0.02
09:01	1.748	46.03	0.03
09:02	2.081	46.03	0.03
09:02	2.414	46.03	0.03
09:02	2.748	46.02	0.04
09:03	3.081	46.02	0.04
09:03	3.415	46.01	0.05
09:03	3.748	46.01	0.05
09:04	4.081	46.01	0.05
09:04	4.414	46.01	0.05
09:04	4.748	46.01	0.05
09:05	5.081	46.00	0.06
09:05	5.414	46.00	0.06
09:05	5.748	46.00	0.06
09:06	6.081	46.00	0.06
09:06	6.415	46.00	0.06
09:06	6.748	46.00	0.06
09:07	7.081	45.99	0.07
09:07	7.415	45.99	0.07
09:07	7.748	45.99	0.07

09:08	8.081	45.99	0.07
09:08	8.415	45.99	0.07
09:08	8.748	45.99	0.07
09:09	9.081	45.99	0.07
09:09	9.414	45.99	0.07
09:09	9.748	45.99	0.07
09:10	10.081	45.99	0.07
09:12	12.108	45.98	0.08
09:14	14.152	45.98	0.08
09:16	16.152	45.98	0.08
09:18	18.152	45.98	0.08
09:20	20.152	45.97	0.09
09:22	22.152	45.97	0.09
09:24	24.152	45.97	0.09
09:26	26.152	45.98	0.08
09:28	28.215	45.98	0.08
09:30	30.197	45.98	0.08
09:32	32.197	45.98	0.08
09:34	34.197	45.99	0.07
09:36	36.197	45.99	0.07
09:38	38.197	45.99	0.07
09:40	40.197	45.99	0.07
09:42	42.197	45.99	0.07
09:44	44.197	45.99	0.07
09:46	46.197	45.99	0.07
09:48	48.197	45.99	0.07
09:50	50.197	45.99	0.07
09:52	52.197	45.99	0.07
09:54	54.197	45.99	0.07
09:56	56.217	45.98	0.08
09:58	58.100	45.98	0.08
10:00	60.245	45.97	0.09
10:02	62.245	45.97	0.09
10:04	64.245	45.97	0.09
10:06	66.245	45.97	0.09
10:08	68.245	45.97	0.09
10:10	70.245	45.96	0.10
10:12	72.245	45.96	0.10
10:14	74.245	45.97	0.09
10:16	76.245	45.97	0.09
10:18	78.245	45.97	0.09
10:20	80.245	45.97	0.09
10:22	82.245	45.98	0.08
10:24	84.245	45.98	0.08
10:26	86.245	45.98	0.08
10:28	88.245	45.99	0.07
10:30	90.245	45.99	0.07
10:32	92.245	45.98	0.08
10:34	94.245	45.99	0.07
10:36	96.245	45.98	0.08
10:38	98.245	45.98	0.08
11:00	120.210	45.96	0.10
11:20	140.210	45.97	0.09
11:40	160.210	45.98	0.08
12:00	180.220	45.99	0.07
12:20	200.220	45.96	0.10

12:40	220.220	45.97	0.09
13:00	240.220	45.99	0.07
13:20	260.220	45.99	0.07
13:40	280.230	45.96	0.10
14:00	300.230	46.00	0.06
14:20	320.230	45.94	0.12
14:40	340.180	45.96	0.10
15:00	360.100	45.99	0.07
15:20	380.100	45.97	0.09
15:40	400.100	45.96	0.10
16:00	420.170	45.89	0.17
16:20	440.250	45.88	0.18
16:40	460.200	45.90	0.16
17:00	480.170	45.92	0.14
17:20	500.170	45.92	0.14
17:40	520.130	45.90	0.16
18:00	540.120	45.93	0.13
18:20	560.220	45.93	0.13
18:40	580.080	45.93	0.13
19:00	600.220	45.93	0.13
19:20	620.230	45.93	0.13
19:40	640.220	45.94	0.12
20:00	660.220	45.94	0.12
20:20	680.130	45.95	0.11
20:40	700.120	45.95	0.11
21:00	720.230	45.90	0.16
21:20	740.300	45.90	0.16
21:40	760.230	45.92	0.14
22:00	780.230	45.92	0.14
22:20	800.230	45.92	0.14
22:40	820.180	45.92	0.14
23:00	840.570	45.94	0.12
23:20	860.180	45.94	0.12
23:40	880.080	45.93	0.13
00:00	900.170	45.94	0.12
00:20	920.170	45.94	0.12
00:40	940.170	45.94	0.12
01:00	960.170	45.94	0.12
01:20	980.170	45.94	0.12
01:40	1000.200	45.94	0.12
02:40	1060.300	45.94	0.12
03:40	1120.300	45.94	0.12
04:40	1180.300	45.96	0.10
05:40	1240.300	45.95	0.11
06:40	1300.300	46.01	0.05
07:40	1360.200	45.94	0.12
08:40	1420.200	45.95	0.11
09:40	1480.200	45.99	0.07
10:40	1540.200	45.93	0.13
11:40	1600.300	45.94	0.12
12:40	1660.300	45.89	0.17
13:40	1720.200	45.87	0.19
14:40	1780.300	45.98	0.08
15:40	1840.300	45.98	0.08
16:40	1900.300	45.96	0.10
17:40	1960.200	45.95	0.11

18:40	2020.200	45.90	0.16
19:40	2080.200	45.83	0.23
20:40	2140.200	45.80	0.26
21:40	2200.300	45.77	0.29
22:40	2260.300	45.78	0.28
23:40	2320.200	45.87	0.19
00:40	2380.200	45.88	0.18
01:40	2440.200	45.83	0.23
02:40	2500.200	45.76	0.30
03:40	2560.200	45.84	0.22
04:40	2620.200	45.68	0.38
05:40	2680.200	45.67	0.39
06:40	2740.200	45.75	0.31
07:40	2800.200	45.83	0.23
08:40	2860.300	45.77	0.29
09:40	2920.300	45.74	0.32
10:40	2980.300	45.80	0.26
11:40	3040.200	45.84	0.22
12:40	3100.200	45.87	0.19
13:40	3160.300	45.82	0.24
14:40	3220.300	45.80	0.26
15:40	3280.200	45.83	0.23
16:40	3340.200	45.83	0.23
17:40	3400.300	45.78	0.28
18:40	3460.300	45.80	0.26
19:40	3520.300	45.79	0.27
20:40	3580.200	45.80	0.26
21:40	3640.200	45.81	0.25
22:40	3700.200	45.81	0.25
23:40	3760.200	45.86	0.20
00:40	3820.200	45.91	0.15
01:40	3880.200	45.91	0.15
02:40	3940.200	45.90	0.16
03:40	4000.200	45.89	0.17
04:40	4060.200	45.88	0.18
05:40	4120.200	45.86	0.20
06:40	4180.200	45.85	0.21
07:40	4240.300	45.82	0.24
08:40	4300.300	45.83	0.23
09:40	4360.700	45.89	0.17
10:40	4420.300	45.87	0.19
11:40	4480.300	45.82	0.24
12:40	4540.300	45.90	0.16
13:40	4600.300	45.86	0.20
14:40	4660.300	45.87	0.19
15:40	4720.300	45.78	0.28
16:40	4780.300	45.86	0.20
17:40	4840.300	45.81	0.25
18:40	4900.300	45.82	0.24
19:40	4960.300	45.82	0.24
20:40	5020.300	45.85	0.21
21:40	5080.300	45.83	0.23
22:40	5140.300	45.84	0.22
23:40	5200.300	45.85	0.21
00:40	5260.300	45.86	0.20
01:40	5320.300	45.86	0.20



02:40	5380.300	45.85	0.21
03:40	5440.300	45.87	0.19
04:40	5500.300	45.88	0.18
05:40	5560.300	45.87	0.19
06:40	5620.300	45.85	0.21
07:40	5680.300	45.85	0.21
08:40	5740.300	45.91	0.15
09:40	5800.300	45.96	0.10
10:40	5860.300	45.95	0.11
11:40	5920.300	45.91	0.15
12:40	5980.300	45.96	0.10
13:40	6040.300	45.93	0.13
14:40	6100.300	46.06	0.00
15:40	6160.500	46.07	-0.01
16:40	6220.300	46.03	0.03
17:40	6280.300	45.85	0.21
18:40	6340.300	45.83	0.23
19:40	6400.400	45.81	0.25
20:40	6460.200	45.86	0.20
21:40	6520.200	45.89	0.17
22:40	6580.300	45.90	0.16
23:40	6640.300	45.90	0.16
00:40	6700.300	45.91	0.15
01:40	6760.300	45.91	0.15
02:40	6820.300	45.93	0.13
03:40	6880.300	45.96	0.10
04:40	6940.300	45.98	0.08
05:40	7000.300	45.99	0.07
06:40	7060.300	45.93	0.13
07:40	7120.300	45.71	0.35
08:40	7180.300	45.58	0.48
09:40	7240.300	45.56	0.50
10:40	7300.300	45.57	0.49
11:40	7360.300	45.54	0.52
12:40	7420.300	45.46	0.60
13:40	7480.300	45.40	0.66
14:40	7540.300	45.34	0.72
15:40	7600.300	45.22	0.84
16:40	7660.300	45.15	0.91
17:40	7720.300	45.14	0.92
18:40	7780.200	45.05	1.01
19:40	7840.200	45.00	1.06
20:40	7900.300	45.02	1.04
21:40	7960.300	45.02	1.04
22:40	8020.300	45.03	1.03
23:40	8080.300	45.08	0.98
00:40	8140.300	45.07	0.99
01:40	8200.300	45.10	0.96
02:40	8260.300	45.15	0.91
03:40	8320.300	45.19	0.87
04:40	8380.300	45.22	0.84
05:40	8440.300	45.28	0.78
06:40	8500.300	45.35	0.71
07:40	8560.200	45.39	0.67
08:40	8620.300	45.36	0.70
09:00	8640.600	45.37	0.69

## ADJUSTED DATA

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : P 10-2 INPUT 6  
RADIUS: 20.854 FEET  
START DATE : 13-Oct-86  
START TIME : 10:25  
WATER START LEVEL: 46.06 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
10:25	8725.000	45.38	0.68
10:35	8735.071	45.39	0.67
10:45	8745.070	45.40	0.66
10:55	8755.072	45.41	0.65
11:05	8765.072	45.39	0.67
11:15	8775.072	45.38	0.68
11:25	8785.072	45.46	0.60
11:35	8795.072	45.47	0.59
11:45	8805.072	45.49	0.57
11:55	8815.102	45.51	0.55
12:05	8825.090	45.50	0.56
12:15	8835.090	45.52	0.54
12:25	8845.090	45.51	0.55
12:35	8855.090	45.51	0.55
12:45	8865.090	45.53	0.53
12:55	8875.120	45.56	0.50
13:04	8884.970	45.52	0.54
13:14	8894.970	45.51	0.55
13:25	8904.970	45.53	0.53
13:34	8914.970	45.56	0.50
13:45	8924.970	45.57	0.49
13:54	8934.970	45.57	0.49
14:05	8944.970	45.55	0.51
14:14	8955.020	45.55	0.51
14:25	8965.080	45.58	0.48
14:35	8975.080	45.59	0.47
14:45	8985.080	45.58	0.48
14:55	8995.080	45.60	0.46
15:05	9005.080	45.58	0.48
15:15	9015.080	45.57	0.49
15:25	9025.080	45.56	0.50
15:35	9035.080	45.57	0.49
15:45	9045.080	45.56	0.50
15:55	9055.080	45.55	0.51
16:04	9065.020	45.55	0.51
16:15	9075.020	45.57	0.49
16:25	9084.970	45.54	0.52
16:35	9095.080	45.55	0.51
16:45	9105.080	45.56	0.50
16:55	9115.080	45.59	0.47

## ADJUSTED DATA

17:05	9125.080	45.57	0.49
17:15	9135.080	45.57	0.49
17:25	9145.080	45.57	0.49
17:35	9155.080	45.55	0.51
17:45	9165.080	45.55	0.51
17:55	9175.080	45.57	0.49
18:05	9185.080	45.56	0.50
18:15	9195.080	45.57	0.49
18:25	9205.080	45.56	0.50
18:35	9215.080	45.55	0.51
18:45	9225.080	45.56	0.50
18:55	9235.080	45.56	0.50
19:05	9245.080	45.55	0.51
19:15	9255.080	45.55	0.51
19:25	9265.080	45.55	0.51
19:35	9275.070	45.54	0.52
19:45	9285.080	45.54	0.52
19:55	9295.080	45.55	0.51
20:05	9305.080	45.55	0.51
20:15	9315.080	45.55	0.51
20:25	9325.080	45.55	0.51
20:35	9335.080	45.55	0.51
20:45	9345.080	45.55	0.51
20:55	9355.080	45.55	0.51
21:05	9365.080	45.54	0.52
21:15	9375.080	45.55	0.51
21:25	9385.080	45.55	0.51
21:35	9395.080	45.55	0.51
21:45	9405.080	45.55	0.51
21:55	9415.080	45.55	0.51
22:05	9425.080	45.54	0.52
22:15	9435.080	45.54	0.52
22:25	9445.080	45.55	0.51
22:35	9455.080	45.55	0.51
22:45	9465.080	45.55	0.51
22:54	9475.020	45.55	0.51
23:05	9485.020	45.54	0.52
23:14	9495.020	45.53	0.53
23:25	9505.020	45.52	0.54
23:34	9515.020	45.50	0.56
23:45	9525.020	45.51	0.55
23:55	9535.020	45.51	0.55
00:05	9545.020	45.51	0.55
00:15	9555.020	45.52	0.54
00:25	9565.030	45.53	0.53
00:35	9575.030	45.52	0.54
00:44	9585.030	45.51	0.55
00:55	9595.030	45.52	0.54
01:04	9605.030	45.54	0.52
01:15	9615.030	45.54	0.52
01:25	9625.030	45.53	0.53
01:35	9635.030	45.53	0.53
01:45	9645.030	45.53	0.53
01:55	9655.030	45.53	0.53
02:05	9665.030	45.54	0.52
02:14	9675.030	45.55	0.51

## ADJUSTED DATA

02:25	9685.030	45.55	0.51
02:34	9695.030	45.55	0.51
02:45	9705.030	45.55	0.51
02:55	9715.030	45.55	0.51
03:04	9725.000	45.56	0.50
03:15	9735.000	45.56	0.50
03:24	9745.000	45.56	0.50
03:35	9755.100	45.55	0.51
03:44	9765.000	45.55	0.51
03:55	9775.000	45.55	0.51
04:04	9785.000	45.54	0.52
04:15	9795.000	45.53	0.53
04:25	9805.000	45.53	0.53
04:34	9815.000	45.53	0.53
04:45	9825.000	45.53	0.53
04:54	9835.000	45.52	0.54
05:05	9845.000	45.52	0.54
05:14	9855.000	45.52	0.54
05:25	9865.000	45.53	0.53
05:34	9875.000	45.52	0.54
05:45	9885.000	45.53	0.53
05:55	9895.000	45.53	0.53
06:04	9905.000	45.54	0.52
06:15	9915.000	45.54	0.52
06:24	9925.000	45.53	0.53
06:35	9935.000	45.54	0.52
06:44	9945.000	45.55	0.51
06:55	9955.000	45.55	0.51
07:05	9965.100	45.55	0.51
07:15	9975.100	45.55	0.51
07:25	9985.100	45.55	0.51
07:35	9995.100	45.55	0.51
07:45	10005.100	45.55	0.51
07:55	10015.100	45.55	0.51
08:05	10025.100	45.55	0.51
08:15	10035.100	45.57	0.49
08:25	10045.100	45.58	0.48
08:35	10055.100	45.61	0.45
08:45	10065.100	45.63	0.43
08:55	10075.000	45.64	0.42
09:04	10085.000	45.68	0.38
09:15	10095.000	45.67	0.39
09:24	10105.000	45.69	0.37
09:28	10108.200	45.70	0.36

PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 2  
 TEST TYPE: RECOVERY  
 WELL NUMBER: P 10-2 INPUT 6  
 RADIUS: 20.854 FEET  
 START DATE: 07-Oct-86  
 START TIME: 11:10  
 WATER START LEVEL: 46.06 FEET  
 WATER STOP LEVEL: 45.83 FEET  
 TOTAL PUMPING TIME: 10210.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
11:10	0.017	-999.99	1045.82	1046.05
11:10	0.034	-999.99	1045.82	1046.05
11:10	0.050	-999.99	1045.82	1046.05
11:10	0.067	-999.99	1045.82	1046.05
11:10	0.084	-999.99	1045.82	1046.05
11:10	0.100	-999.99	1045.82	1046.05
11:10	0.117	-999.99	1045.82	1046.05
11:10	0.134	-999.99	1045.82	1046.05
11:10	0.150	-999.99	1045.82	1046.05
11:10	0.167	-999.99	1045.82	1046.05
11:10	0.257	45.83	0.00	0.23
11:10	0.341	45.83	0.00	0.23
11:10	0.424	45.83	0.00	0.23
11:10	0.507	45.83	0.00	0.23
11:10	0.591	45.83	0.00	0.23
11:10	0.674	45.83	0.00	0.23
11:10	0.757	45.83	0.00	0.23
11:10	0.841	45.83	0.00	0.23
11:10	0.924	45.83	0.00	0.23
11:11	1.007	45.84	-0.01	0.22
11:11	1.413	45.84	-0.01	0.22
11:11	1.747	45.85	-0.02	0.21
11:12	2.080	45.85	-0.02	0.21
11:12	2.413	45.86	-0.03	0.20
11:12	2.747	45.87	-0.04	0.19
11:13	3.080	45.88	-0.05	0.18
11:13	3.413	45.89	-0.06	0.17
11:13	3.747	45.89	-0.06	0.17
11:14	4.080	45.90	-0.07	0.16
11:14	4.413	45.90	-0.07	0.16
11:14	4.747	45.90	-0.07	0.16
11:15	5.080	45.90	-0.07	0.16
11:15	5.413	45.90	-0.07	0.16
11:15	5.747	45.91	-0.08	0.15
11:16	6.080	45.91	-0.08	0.15
11:16	6.413	45.91	-0.08	0.15
11:16	6.747	45.91	-0.08	0.15
11:17	7.080	45.91	-0.08	0.15
11:17	7.413	45.91	-0.08	0.15
11:17	7.747	45.91	-0.08	0.15

11:18	8.080	45.91	-0.08	0.15
11:18	8.413	45.91	-0.08	0.15
11:18	8.747	45.90	-0.07	0.16
11:19	9.080	45.90	-0.07	0.16
11:19	9.413	45.90	-0.07	0.16
11:19	9.747	45.90	-0.07	0.16
11:20	10.080	45.90	-0.07	0.16
11:22	12.115	45.86	-0.03	0.20
11:24	14.115	45.92	-0.09	0.14
11:26	16.115	45.94	-0.11	0.12
11:28	18.115	45.94	-0.11	0.12
11:30	20.115	45.95	-0.12	0.11
11:32	22.115	45.97	-0.14	0.09
11:34	24.115	45.98	-0.15	0.08
11:36	26.115	45.98	-0.15	0.08
11:38	28.115	45.97	-0.14	0.09
11:40	30.115	45.96	-0.13	0.10
11:42	32.115	45.94	-0.11	0.12
11:44	34.115	45.94	-0.11	0.12
11:46	36.115	45.94	-0.11	0.12
11:48	38.115	45.97	-0.14	0.09
11:50	40.115	45.97	-0.14	0.09
11:52	42.115	46.01	-0.18	0.05
11:54	44.115	46.02	-0.19	0.04
11:56	46.115	46.03	-0.20	0.03
11:58	48.115	46.03	-0.20	0.03
12:00	50.115	46.05	-0.22	0.01
12:02	52.115	46.01	-0.18	0.05
12:04	54.115	46.00	-0.17	0.06
12:06	56.115	46.00	-0.17	0.06
12:08	58.115	46.01	-0.18	0.05
12:10	60.115	46.04	-0.21	0.02
12:12	62.102	46.06	-0.23	0.00
12:14	64.492	46.07	-0.24	0.01
12:16	66.188	46.06	-0.23	0.00
12:18	68.188	46.06	-0.23	0.00
12:20	70.188	46.07	-0.24	0.01
12:22	72.188	46.08	-0.25	0.02
12:24	74.188	46.10	-0.27	0.04
12:26	76.188	46.09	-0.26	0.03
12:28	78.188	46.09	-0.26	0.03
12:30	80.188	46.08	-0.25	0.02
12:32	82.188	46.07	-0.24	0.01
12:34	84.188	46.05	-0.22	0.01
12:36	86.188	46.05	-0.22	0.01
12:38	88.188	46.07	-0.24	0.01
12:40	90.188	46.07	-0.24	0.01
12:42	92.188	46.06	-0.23	0.00
12:44	94.188	46.07	-0.24	0.01
12:46	96.188	46.06	-0.23	0.00
12:48	98.188	46.04	-0.21	0.02
13:10	120.110	46.03	-0.20	0.03
13:30	140.110	46.00	-0.17	0.06
13:50	160.120	46.05	-0.22	0.01
14:10	180.120	46.05	-0.22	0.01
14:30	200.120	46.06	-0.23	0.00

14:50	220.120	46.02	-0.19	0.04
15:10	240.120	45.99	-0.16	0.07
15:30	260.120	45.96	-0.13	0.10
15:50	280.120	45.94	-0.11	0.12
16:10	300.120	45.89	-0.06	0.17
16:30	320.050	45.87	-0.04	0.19
16:49	340.050	45.83	0.00	0.23
17:10	360.050	45.79	0.04	0.27
17:30	380.050	45.77	0.06	0.29
17:50	400.050	45.74	0.09	0.32
18:10	420.050	45.72	0.11	0.34
18:30	440.050	45.72	0.11	0.34
18:50	460.050	45.72	0.11	0.34
19:10	480.050	45.74	0.09	0.32
19:30	500.050	45.74	0.09	0.32
19:49	520.050	45.74	0.09	0.32
20:10	540.050	45.74	0.09	0.32
20:30	560.050	45.73	0.10	0.33
20:50	580.050	45.73	0.10	0.33
21:10	600.050	45.74	0.09	0.32
21:30	620.050	45.73	0.10	0.33
21:50	640.050	45.73	0.10	0.33
22:10	660.050	45.72	0.11	0.34
22:30	680.050	45.71	0.12	0.35
22:49	700.050	45.71	0.12	0.35
23:10	720.050	45.70	0.13	0.36
23:30	740.050	45.69	0.14	0.37
23:50	760.100	45.67	0.16	0.39
00:10	780.100	45.65	0.18	0.41
00:30	800.100	45.66	0.17	0.40
00:50	820.100	45.66	0.17	0.40
01:10	840.100	45.67	0.16	0.39
01:30	860.100	45.67	0.16	0.39
01:50	880.100	45.67	0.16	0.39
02:10	900.100	45.67	0.16	0.39
02:30	920.100	45.67	0.16	0.39
02:50	940.100	45.67	0.16	0.39
03:10	960.100	45.69	0.14	0.37
03:30	980.100	45.70	0.13	0.36
03:50	1000.100	45.70	0.13	0.36
04:50	1060.300	45.71	0.12	0.35
05:50	1120.300	45.72	0.11	0.34
06:50	1180.300	45.71	0.12	0.35
07:50	1240.300	45.66	0.17	0.40
08:50	1300.300	45.72	0.11	0.34
09:50	1360.300	45.89	-0.06	0.17
10:50	1420.300	46.10	-0.27	0.04
11:50	1480.300	46.24	-0.41	0.18
12:50	1540.300	46.25	-0.42	0.19
13:50	1600.300	46.24	-0.41	0.18
14:50	1660.300	46.17	-0.34	0.11
15:50	1720.100	46.09	-0.26	0.03
16:50	1780.100	45.96	-0.13	0.10
17:50	1840.100	45.87	-0.04	0.19
18:50	1900.100	45.80	0.03	0.26
19:50	1960.100	45.70	0.13	0.36

20:50	2020.100	45.62	0.21	0.44
21:50	2080.100	45.60	0.23	0.46
22:50	2140.100	45.58	0.25	0.48
23:50	2200.100	45.58	0.25	0.48
00:50	2260.100	45.61	0.22	0.45
01:50	2320.100	45.64	0.19	0.42
02:50	2380.100	45.68	0.15	0.38
03:50	2440.100	45.70	0.13	0.36
04:50	2500.100	45.71	0.12	0.35
05:50	2560.100	45.72	0.11	0.34
06:50	2620.100	45.73	0.10	0.33
07:50	2680.100	45.75	0.08	0.31
08:50	2740.200	45.87	-0.04	0.19
09:50	2800.200	46.04	-0.21	0.02
10:50	2860.200	46.25	-0.42	0.19
11:50	2920.100	46.40	-0.57	0.34
12:50	2980.200	46.14	-0.31	0.08
13:50	3040.200	45.90	-0.07	0.16
14:50	3100.200	45.92	-0.09	0.14
15:50	3160.200	45.91	-0.08	0.15
16:50	3220.200	45.92	-0.09	0.14
17:50	3280.200	45.92	-0.09	0.14
18:50	3340.200	45.92	-0.09	0.14
19:50	3400.200	45.92	-0.09	0.14
20:50	3460.200	45.92	-0.09	0.14
21:50	3520.200	45.92	-0.09	0.14
22:50	3580.200	45.92	-0.09	0.14
23:50	3640.200	45.93	-0.10	0.13
00:50	3700.200	45.93	-0.10	0.13
01:50	3760.200	45.93	-0.10	0.13
02:50	3820.200	45.93	-0.10	0.13
03:50	3880.200	45.93	-0.10	0.13
04:50	3940.200	45.92	-0.09	0.14
05:50	4000.200	45.92	-0.09	0.14
06:50	4060.200	45.92	-0.09	0.14
07:50	4120.200	45.92	-0.09	0.14
08:50	4180.200	45.93	-0.10	0.13
09:50	4240.200	-999.99	1045.82	1046.05
10:50	4300.200	-999.99	1045.82	1046.05
11:04	4314.800	-999.99	1045.82	1046.05



PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : P 10-3 INPUT 7  
RADIUS: 20.220 FEET  
START DATE : 07-Oct-86  
START TIME : 09:00  
WATER START LEVEL: 39.72 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
09:00	0.000	39.72	0.00
09:00	0.017	-99.99	139.71
09:00	0.034	-99.99	139.71
09:00	0.050	-99.99	139.71
09:00	0.067	-99.99	139.71
09:00	0.084	-99.99	139.71
09:00	0.100	-99.99	139.71
09:00	0.117	-99.99	139.71
09:00	0.134	-99.99	139.71
09:00	0.150	-99.99	139.71
09:00	0.167	-99.99	139.71
09:00	0.257	39.72	0.00
09:00	0.340	39.72	0.00
09:00	0.424	39.72	0.00
09:00	0.507	39.72	0.00
09:00	0.590	39.72	0.00
09:00	0.674	39.72	0.00
09:00	0.757	39.72	0.00
09:00	0.840	39.72	0.00
09:00	0.924	39.72	0.00
09:01	1.007	39.72	0.00
09:01	1.414	39.72	0.00
09:01	1.748	39.72	0.00
09:02	2.081	39.72	0.00
09:02	2.414	39.72	0.00
09:02	2.748	39.72	0.00
09:03	3.081	39.72	0.00
09:03	3.415	39.72	0.00
09:03	3.748	39.72	0.00
09:04	4.081	39.72	0.00
09:04	4.414	39.72	0.00
09:04	4.748	39.72	0.00
09:05	5.081	39.72	0.00
09:05	5.414	39.72	0.00
09:05	5.748	39.72	0.00
09:06	6.081	39.72	0.00
09:06	6.415	39.72	0.00
09:06	6.748	39.72	0.00
09:07	7.081	39.72	0.00
09:07	7.415	39.72	0.00
09:07	7.748	39.72	0.00

09:08	8.081	39.72	0.00
09:08	8.415	39.72	0.00
09:08	8.748	39.69	0.03
09:09	9.081	39.72	0.00
09:09	9.414	39.72	0.00
09:09	9.748	39.72	0.00
09:10	10.081	39.72	0.00
09:12	12.108	39.72	0.00
09:14	14.152	39.72	0.00
09:16	16.152	39.72	0.00
09:18	18.152	39.72	0.00
09:20	20.152	39.72	0.00
09:22	22.152	39.72	0.00
09:24	24.152	39.72	0.00
09:26	26.152	39.72	0.00
09:28	28.215	39.72	0.00
09:30	30.197	39.72	0.00
09:32	32.197	39.72	0.00
09:34	34.197	39.72	0.00
09:36	36.197	39.72	0.00
09:38	38.197	39.72	0.00
09:40	40.197	39.72	0.00
09:42	42.197	39.72	0.00
09:44	44.197	39.72	0.00
09:46	46.197	39.72	0.00
09:48	48.197	39.72	0.00
09:50	50.197	39.72	0.00
09:52	52.197	39.72	0.00
09:54	54.197	39.72	0.00
09:56	56.217	39.72	0.00
09:58	58.100	39.72	0.00
10:00	60.245	39.72	0.00
10:02	62.245	39.72	0.00
10:04	64.245	39.72	0.00
10:06	66.245	39.72	0.00
10:08	68.245	39.72	0.00
10:10	70.245	39.72	0.00
10:12	72.245	39.72	0.00
10:14	74.245	39.72	0.00
10:16	76.245	39.72	0.00
10:18	78.245	39.72	0.00
10:20	80.245	39.72	0.00
10:22	82.245	39.72	0.00
10:24	84.245	39.72	0.00
10:26	86.245	39.72	0.00
10:28	88.245	39.72	0.00
10:30	90.245	39.72	0.00
10:32	92.245	39.72	0.00
10:34	94.245	39.72	0.00
10:36	96.245	39.72	0.00
10:38	98.245	39.72	0.00
11:00	120.210	39.72	0.00
11:20	140.210	39.72	0.00
11:40	160.210	39.72	0.00
12:00	180.220	39.72	0.00
12:20	200.220	39.72	0.00

12:40	220.220	39.72	0.00
13:00	240.220	39.72	0.00
13:20	260.220	39.72	0.00
13:40	280.230	39.72	0.00
14:00	300.230	39.72	0.00
14:20	320.230	39.72	0.00
14:40	340.180	39.72	0.00
15:00	360.100	39.72	0.00
15:20	380.100	39.72	0.00
15:40	400.100	39.72	0.00
16:00	420.170	39.72	0.00
16:20	440.250	39.72	0.00
16:40	460.200	39.72	0.00
17:00	480.170	39.72	0.00
17:20	500.170	39.72	0.00
17:40	520.130	39.72	0.00
18:00	540.120	39.72	0.00
18:20	560.220	39.72	0.00
18:40	580.080	39.72	0.00
19:00	600.220	39.72	0.00
19:20	620.230	39.72	0.00
19:40	640.220	39.72	0.00
20:00	660.220	39.72	0.00
20:20	680.130	39.72	0.00
20:40	700.120	39.72	0.00
21:00	720.230	39.72	0.00
21:20	740.300	39.72	0.00
21:40	760.230	39.72	0.00
22:00	780.230	39.72	0.00
22:20	800.230	39.72	0.00
22:40	820.180	39.72	0.00
23:00	840.570	39.72	0.00
23:20	860.180	39.72	0.00
23:40	880.080	39.72	0.00
00:00	900.170	39.72	0.00
00:20	920.170	39.72	0.00
00:40	940.170	39.72	0.00
01:00	960.170	39.72	0.00
01:20	980.170	39.72	0.00
01:40	1000.200	39.72	0.00
02:40	1060.300	39.72	0.00
03:40	1120.300	39.72	0.00
04:40	1180.300	39.72	0.00
05:40	1240.300	39.72	0.00
06:40	1300.300	39.72	0.00
07:40	1360.200	39.72	0.00
08:40	1420.200	39.72	0.00
09:40	1480.200	39.72	0.00
10:40	1540.200	39.72	0.00
11:40	1600.300	39.72	0.00
12:40	1660.300	39.72	0.00
13:40	1720.200	39.72	0.00
14:40	1780.300	39.72	0.00
15:40	1840.300	39.72	0.00
16:40	1900.300	39.72	0.00
17:40	1960.200	39.71	0.01

18:40	2020.200	39.71	0.01
19:40	2080.200	39.71	0.01
20:40	2140.200	39.72	0.00
21:40	2200.300	39.71	0.01
22:40	2260.300	39.71	0.01
23:40	2320.200	39.71	0.01
00:40	2380.200	39.71	0.01
01:40	2440.200	39.71	0.01
02:40	2500.200	39.71	0.01
03:40	2560.200	39.72	0.00
04:40	2620.200	39.71	0.01
05:40	2680.200	39.71	0.01
06:40	2740.200	39.71	0.01
07:40	2800.200	39.71	0.01
08:40	2860.300	39.71	0.01
09:40	2920.300	39.71	0.01
10:40	2980.300	39.71	0.01
11:40	3040.200	39.71	0.01
12:40	3100.200	39.71	0.01
13:40	3160.300	39.71	0.01
14:40	3220.300	39.71	0.01
15:40	3280.200	39.71	0.01
16:40	3340.200	39.71	0.01
17:40	3400.300	39.71	0.01
18:40	3460.300	39.71	0.01
19:40	3520.300	39.71	0.01
20:40	3580.200	39.71	0.01
21:40	3640.200	39.71	0.01
22:40	3700.200	39.71	0.01
23:40	3760.200	39.71	0.01
00:40	3820.200	39.71	0.01
01:40	3880.200	39.71	0.01
02:40	3940.200	39.71	0.01
03:40	4000.200	39.71	0.01
04:40	4060.200	39.71	0.01
05:40	4120.200	39.71	0.01
06:40	4180.200	39.70	0.02
07:40	4240.300	39.71	0.01
08:40	4300.300	39.70	0.02
09:40	4360.700	39.71	0.01
10:40	4420.300	39.70	0.02
11:40	4480.300	39.70	0.02
12:40	4540.300	39.70	0.02
13:40	4600.300	39.70	0.02
14:40	4660.300	39.70	0.02
15:40	4720.300	39.70	0.02
16:40	4780.300	39.70	0.02
17:40	4840.300	39.70	0.02
18:40	4900.300	39.70	0.02
19:40	4960.300	39.70	0.02
20:40	5020.300	39.70	0.02
21:40	5080.300	39.70	0.02
22:40	5140.300	39.70	0.02
23:40	5200.300	39.70	0.02
00:40	5260.300	39.69	0.03
01:40	5320.300	39.70	0.02

02:40	5380.300	39.69	0.03
03:40	5440.300	39.70	0.02
04:40	5500.300	39.70	0.02
05:40	5560.300	39.69	0.03
06:40	5620.300	39.70	0.02
07:40	5680.300	39.70	0.02
08:40	5740.300	39.69	0.03
09:40	5800.300	39.70	0.02
10:40	5860.300	39.69	0.03
11:40	5920.300	39.69	0.03
12:40	5980.300	39.69	0.03
13:40	6040.300	39.69	0.03
14:40	6100.300	39.69	0.03
15:40	6160.500	39.69	0.03
16:40	6220.300	39.69	0.03
17:40	6280.300	39.69	0.03
18:40	6340.300	39.69	0.03
19:40	6400.400	39.69	0.03
20:40	6460.200	39.69	0.03
21:40	6520.200	39.69	0.03
22:40	6580.300	39.69	0.03
23:40	6640.300	39.69	0.03
00:40	6700.300	39.69	0.03
01:40	6760.300	39.69	0.03
02:40	6820.300	39.69	0.03
03:40	6880.300	39.70	0.02
04:40	6940.300	39.69	0.03
05:40	7000.300	39.69	0.03
06:40	7060.300	39.69	0.03
07:40	7120.300	39.66	0.06
08:40	7180.300	39.59	0.13
09:40	7240.300	39.58	0.14
10:40	7300.300	39.58	0.14
11:40	7360.300	39.58	0.14
12:40	7420.300	39.58	0.14
13:40	7480.300	39.58	0.14
14:40	7540.300	39.58	0.14
15:40	7600.300	39.57	0.15
16:40	7660.300	39.57	0.15
17:40	7720.300	39.57	0.15
18:40	7780.200	39.57	0.15
19:40	7840.200	39.57	0.15
20:40	7900.300	39.57	0.15
21:40	7960.300	39.57	0.15
22:40	8020.300	39.59	0.13
23:40	8080.300	39.59	0.13
00:40	8140.300	39.59	0.13
01:40	8200.300	39.59	0.13
02:40	8260.300	39.59	0.13
03:40	8320.300	39.59	0.13
04:40	8380.300	39.59	0.13
05:40	8440.300	39.59	0.13
06:40	8500.300	39.59	0.13
07:40	8560.200	39.59	0.13
08:40	8620.300	39.59	0.13
09:00	8640.600	39.58	0.14

## ADJUSTED DATA

PROJECT NAME : FRENCH LTD.  
PROJECT NUMBER : 275-14  
TEST NAME : REI 10-1 RUN # 2  
TEST TYPE : DRAWDOWN  
WELL NUMBER : P 10-3 INPUT 7  
RADIUS: 20.220 FEET  
START DATE : 13-Oct-86  
START TIME : 10:25  
WATER START LEVEL: 39.72 FEET

TIME	E.T. (MIN)	LEVEL	Delta H
10:25	8725.000	39.59	0.13
10:35	8735.071	39.59	0.13
10:45	8745.070	39.59	0.13
10:55	8755.072	39.59	0.13
11:05	8765.072	39.59	0.13
11:15	8775.072	39.59	0.13
11:25	8785.072	39.59	0.13
11:35	8795.072	39.59	0.13
11:45	8805.072	39.59	0.13
11:55	8815.102	39.59	0.13
12:05	8825.090	39.59	0.13
12:15	8835.090	39.59	0.13
12:25	8845.090	39.59	0.13
12:35	8855.090	39.59	0.13
12:45	8865.090	39.59	0.13
12:55	8875.120	39.59	0.13
13:04	8884.970	39.59	0.13
13:14	8894.970	39.59	0.13
13:25	8904.970	39.59	0.13
13:34	8914.970	39.59	0.13
13:45	8924.970	39.59	0.13
13:54	8934.970	39.59	0.13
14:05	8944.970	39.59	0.13
14:14	8955.020	39.59	0.13
14:25	8965.080	39.59	0.13
14:35	8975.080	39.59	0.13
14:45	8985.080	39.59	0.13
14:55	8995.080	39.59	0.13
15:05	9005.080	39.59	0.13
15:15	9015.080	39.59	0.13
15:25	9025.080	39.59	0.13
15:35	9035.080	39.59	0.13
15:45	9045.080	39.59	0.13
15:55	9055.080	39.59	0.13
16:04	9065.020	39.59	0.13
16:15	9075.020	39.58	0.14
16:25	9084.970	39.59	0.13
16:35	9095.080	39.59	0.13
16:45	9105.080	39.58	0.14
16:55	9115.080	39.59	0.13

## ADJUSTED DATA

17:05	9125.080	39.59	0.13
17:15	9135.080	39.59	0.13
17:25	9145.080	39.59	0.13
17:35	9155.080	39.59	0.13
17:45	9165.080	39.58	0.14
17:55	9175.080	39.58	0.14
18:05	9185.080	39.58	0.14
18:15	9195.080	39.58	0.14
18:25	9205.080	39.59	0.13
18:35	9215.080	39.59	0.13
18:45	9225.080	39.58	0.14
18:55	9235.080	39.58	0.14
19:05	9245.080	39.58	0.14
19:15	9255.080	39.58	0.14
19:25	9265.080	39.58	0.14
19:35	9275.070	39.59	0.13
19:45	9285.080	39.59	0.13
19:55	9295.080	39.58	0.14
20:05	9305.080	39.58	0.14
20:15	9315.080	39.58	0.14
20:25	9325.080	39.59	0.13
20:35	9335.080	39.59	0.13
20:45	9345.080	39.58	0.14
20:55	9355.080	39.58	0.14
21:05	9365.080	39.58	0.14
21:15	9375.080	39.58	0.14
21:25	9385.080	39.58	0.14
21:35	9395.080	39.58	0.14
21:45	9405.080	39.58	0.14
21:55	9415.080	39.58	0.14
22:05	9425.080	39.58	0.14
22:15	9435.080	39.58	0.14
22:25	9445.080	39.58	0.14
22:35	9455.080	39.58	0.14
22:45	9465.080	39.58	0.14
22:54	9475.020	39.58	0.14
23:05	9485.020	39.58	0.14
23:14	9495.020	39.58	0.14
23:25	9505.020	39.58	0.14
23:34	9515.020	39.58	0.14
23:45	9525.020	39.58	0.14
23:55	9535.020	39.58	0.14
00:05	9545.020	39.58	0.14
00:15	9555.020	39.58	0.14
00:25	9565.030	39.58	0.14
00:35	9575.030	39.58	0.14
00:44	9585.030	39.58	0.14
00:55	9595.030	39.58	0.14
01:04	9605.030	39.58	0.14
01:15	9615.030	39.58	0.14
01:25	9625.030	39.58	0.14
01:35	9635.030	39.58	0.14
01:45	9645.030	39.58	0.14
01:55	9655.030	39.58	0.14
02:05	9665.030	39.58	0.14
02:14	9675.030	39.58	0.14

## ADJUSTED DATA

02:25	9685.030	39.58	0.14
02:34	9695.030	39.58	0.14
02:45	9705.030	39.58	0.14
02:55	9715.030	39.58	0.14
03:04	9725.000	39.58	0.14
03:15	9735.000	39.58	0.14
03:24	9745.000	39.58	0.14
03:35	9755.100	39.58	0.14
03:44	9765.000	39.58	0.14
03:55	9775.000	39.58	0.14
04:04	9785.000	39.58	0.14
04:15	9795.000	39.58	0.14
04:25	9805.000	39.58	0.14
04:34	9815.000	39.58	0.14
04:45	9825.000	39.58	0.14
04:54	9835.000	39.57	0.15
05:05	9845.000	39.58	0.14
05:14	9855.000	39.58	0.14
05:25	9865.000	39.58	0.14
05:34	9875.000	39.58	0.14
05:45	9885.000	39.58	0.14
05:55	9895.000	39.58	0.14
06:04	9905.000	39.58	0.14
06:15	9915.000	39.58	0.14
06:24	9925.000	39.58	0.14
06:35	9935.000	39.58	0.14
06:44	9945.000	39.58	0.14
06:55	9955.000	39.58	0.14
07:05	9965.100	39.58	0.14
07:15	9975.100	39.58	0.14
07:25	9985.100	39.57	0.15
07:35	9995.100	39.57	0.15
07:45	10005.100	39.58	0.14
07:55	10015.100	39.58	0.14
08:05	10025.100	39.58	0.14
08:15	10035.100	39.57	0.15
08:25	10045.100	39.58	0.14
08:35	10055.100	39.58	0.14
08:45	10065.100	39.58	0.14
08:55	10075.000	39.57	0.15
09:04	10085.000	39.58	0.14
09:15	10095.000	39.58	0.14
09:24	10105.000	39.58	0.14
09:28	10108.200	39.57	0.15



PROJECT NAME : FRENCH LTD.  
 PROJECT NUMBER : 275-14  
 TEST NAME: REI 10-1 RUN # 2  
 TEST TYPE: RECOVERY  
 WELL NUMBER: P 10-3 INPUT 7  
 RADIUS: 20.220 FEET  
 START DATE: 07-Oct-86  
 START TIME: 11:10  
 WATER START LEVEL: 39.72 FEET  
 WATER STOP LEVEL: 39.65 FEET  
 TOTAL PUMPING TIME: 10210.6 MIN

TIME	E.T. (MIN)	LEVEL	Delta H (REC)	Delta H (RES)
11:10	0.017	-999.99	1039.64	1039.71
11:10	0.034	-999.99	1039.64	1039.71
11:10	0.050	-999.99	1039.64	1039.71
11:10	0.067	-999.99	1039.64	1039.71
11:10	0.084	-999.99	1039.64	1039.71
11:10	0.100	-999.99	1039.64	1039.71
11:10	0.117	-999.99	1039.64	1039.71
11:10	0.134	-999.99	1039.64	1039.71
11:10	0.150	-999.99	1039.64	1039.71
11:10	0.167	-999.99	1039.64	1039.71
11:10	0.257	39.65	0.00	0.07
11:10	0.341	39.65	0.00	0.07
11:10	0.424	39.65	0.00	0.07
11:10	0.507	39.65	0.00	0.07
11:10	0.591	39.65	0.00	0.07
11:10	0.674	39.65	0.00	0.07
11:10	0.757	39.65	0.00	0.07
11:10	0.841	39.65	0.00	0.07
11:10	0.924	39.65	0.00	0.07
11:11	1.007	39.65	0.00	0.07
11:11	1.413	39.65	0.00	0.07
11:11	1.747	39.65	0.00	0.07
11:12	2.080	39.65	0.00	0.07
11:12	2.413	39.65	0.00	0.07
11:12	2.747	39.65	0.00	0.07
11:13	3.080	39.65	0.00	0.07
11:13	3.413	39.65	0.00	0.07
11:13	3.747	39.65	0.00	0.07
11:14	4.080	39.65	0.00	0.07
11:14	4.413	39.65	0.00	0.07
11:14	4.747	39.65	0.00	0.07
11:15	5.080	39.65	0.00	0.07
11:15	5.413	39.65	0.00	0.07
11:15	5.747	39.65	0.00	0.07
11:16	6.080	39.65	0.00	0.07
11:16	6.413	39.65	0.00	0.07
11:16	6.747	39.65	0.00	0.07
11:17	7.080	39.65	0.00	0.07
11:17	7.413	39.65	0.00	0.07
11:17	7.747	39.65	0.00	0.07

11:18	8.080	39.65	0.00	0.07
11:18	8.413	39.65	0.00	0.07
11:18	8.747	39.65	0.00	0.07
11:19	9.080	39.65	0.00	0.07
11:19	9.413	39.65	0.00	0.07
11:19	9.747	39.65	0.00	0.07
11:20	10.080	39.65	0.00	0.07
11:22	12.115	39.65	0.00	0.07
11:24	14.115	39.65	0.00	0.07
11:26	16.115	39.65	0.00	0.07
11:28	18.115	39.65	0.00	0.07
11:30	20.115	39.65	0.00	0.07
11:32	22.115	39.65	0.00	0.07
11:34	24.115	39.65	0.00	0.07
11:36	26.115	39.65	0.00	0.07
11:38	28.115	39.65	0.00	0.07
11:40	30.115	39.65	0.00	0.07
11:42	32.115	39.65	0.00	0.07
11:44	34.115	39.65	0.00	0.07
11:46	36.115	39.65	0.00	0.07
11:48	38.115	39.65	0.00	0.07
11:50	40.115	39.65	0.00	0.07
11:52	42.115	39.65	0.00	0.07
11:54	44.115	39.65	0.00	0.07
11:56	46.115	39.65	0.00	0.07
11:58	48.115	39.65	0.00	0.07
12:00	50.115	39.65	0.00	0.07
12:02	52.115	39.65	0.00	0.07
12:04	54.115	39.65	0.00	0.07
12:06	56.115	39.65	0.00	0.07
12:08	58.115	39.65	0.00	0.07
12:10	60.115	39.65	0.00	0.07
12:12	62.102	39.65	0.00	0.07
12:14	64.492	39.65	0.00	0.07
12:16	66.188	39.65	0.00	0.07
12:18	68.188	39.65	0.00	0.07
12:20	70.188	39.65	0.00	0.07
12:22	72.188	39.65	0.00	0.07
12:24	74.188	39.65	0.00	0.07
12:26	76.188	39.65	0.00	0.07
12:28	78.188	39.65	0.00	0.07
12:30	80.188	39.65	0.00	0.07
12:32	82.188	39.65	0.00	0.07
12:34	84.188	39.64	0.01	0.08
12:36	86.188	39.65	0.00	0.07
12:38	88.188	39.65	0.00	0.07
12:40	90.188	39.65	0.00	0.07
12:42	92.188	39.65	0.00	0.07
12:44	94.188	39.65	0.00	0.07
12:46	96.188	39.65	0.00	0.07
12:48	98.188	39.65	0.00	0.07
13:10	120.110	39.65	0.00	0.07
13:30	140.110	39.65	0.00	0.07
13:50	160.120	39.65	0.00	0.07
14:10	180.120	39.65	0.00	0.07
14:30	200.120	39.64	0.01	0.08

14:50	220.120	39.65	0.00	0.07
15:10	240.120	39.65	0.00	0.07
15:30	260.120	39.65	0.00	0.07
15:50	280.120	39.65	0.00	0.07
16:10	300.120	39.65	0.00	0.07
16:30	320.050	39.65	0.00	0.07
16:49	340.050	39.64	0.01	0.08
17:10	360.050	39.64	0.01	0.08
17:30	380.050	39.65	0.00	0.07
17:50	400.050	39.64	0.01	0.08
18:10	420.050	39.65	0.00	0.07
18:30	440.050	39.64	0.01	0.08
18:50	460.050	39.64	0.01	0.08
19:10	480.050	39.64	0.01	0.08
19:30	500.050	39.65	0.00	0.07
19:49	520.050	39.65	0.00	0.07
20:10	540.050	39.64	0.01	0.08
20:30	560.050	39.64	0.01	0.08
20:50	580.050	39.64	0.01	0.08
21:10	600.050	39.65	0.00	0.07
21:30	620.050	39.65	0.00	0.07
21:50	640.050	39.64	0.01	0.08
22:10	660.050	39.65	0.00	0.07
22:30	680.050	39.65	0.00	0.07
22:49	700.050	39.65	0.00	0.07
23:10	720.050	39.65	0.00	0.07
23:30	740.050	39.64	0.01	0.08
23:50	760.100	39.64	0.01	0.08
00:10	780.100	39.65	0.00	0.07
00:30	800.100	39.64	0.01	0.08
00:50	820.100	39.65	0.00	0.07
01:10	840.100	39.65	0.00	0.07
01:30	860.100	39.65	0.00	0.07
01:50	880.100	39.65	0.00	0.07
02:10	900.100	39.65	0.00	0.07
02:30	920.100	39.64	0.01	0.08
02:50	940.100	39.65	0.00	0.07
03:10	960.100	39.65	0.00	0.07
03:30	980.100	39.64	0.01	0.08
03:50	1000.100	39.64	0.01	0.08
04:50	1060.300	39.64	0.01	0.08
05:50	1120.300	39.64	0.01	0.08
06:50	1180.300	39.64	0.01	0.08
07:50	1240.300	39.65	0.00	0.07
08:50	1300.300	39.64	0.01	0.08
09:50	1360.300	39.64	0.01	0.08
10:50	1420.300	39.65	0.00	0.07
11:50	1480.300	39.64	0.01	0.08
12:50	1540.300	39.65	0.00	0.07
13:50	1600.300	39.64	0.01	0.08
14:50	1660.300	39.64	0.01	0.08
15:50	1720.100	39.65	0.00	0.07
16:50	1780.100	39.64	0.01	0.08
17:50	1840.100	39.64	0.01	0.08
18:50	1900.100	39.64	0.01	0.08
19:50	1960.100	39.64	0.01	0.08

20:50	2020.100	39.64	0.01	0.08
21:50	2080.100	39.64	0.01	0.08
22:50	2140.100	39.64	0.01	0.08
23:50	2200.100	39.64	0.01	0.08
00:50	2260.100	39.64	0.01	0.08
01:50	2320.100	39.64	0.01	0.08
02:50	2380.100	39.64	0.01	0.08
03:50	2440.100	39.64	0.01	0.08
04:50	2500.100	39.64	0.01	0.08
05:50	2560.100	39.64	0.01	0.08
06:50	2620.100	39.64	0.01	0.08
07:50	2680.100	39.64	0.01	0.08
08:50	2740.200	39.64	0.01	0.08
09:50	2800.200	39.64	0.01	0.08
10:50	2860.200	39.64	0.01	0.08
11:50	2920.100	39.64	0.01	0.08
12:50	2980.200	39.64	0.01	0.08
13:50	3040.200	39.64	0.01	0.08
14:50	3100.200	39.64	0.01	0.08
15:50	3160.200	39.64	0.01	0.08
16:50	3220.200	39.64	0.01	0.08
17:50	3280.200	39.64	0.01	0.08
18:50	3340.200	39.64	0.01	0.08
19:50	3400.200	39.64	0.01	0.08
20:50	3460.200	39.63	0.02	0.09
21:50	3520.200	39.64	0.01	0.08
22:50	3580.200	39.64	0.01	0.08
23:50	3640.200	39.64	0.01	0.08
00:50	3700.200	39.64	0.01	0.08
01:50	3760.200	39.63	0.02	0.09
02:50	3820.200	39.64	0.01	0.08
03:50	3880.200	39.64	0.01	0.08
04:50	3940.200	39.64	0.01	0.08
05:50	4000.200	39.63	0.02	0.09
06:50	4060.200	39.63	0.02	0.09
07:50	4120.200	39.63	0.02	0.09
08:50	4180.200	39.64	0.01	0.08
09:50	4240.200	-999.99	1039.64	1039.71
10:50	4300.200	-999.99	1039.64	1039.71
11:04	4314.800	-999.99	1039.64	1039.71

SHEET \_\_\_\_ OF \_\_\_\_

WELL NUMBER: STAFF GAUGE

**Y IN FEET.**

STARTING WATER LEVEL:

# AA

## PUMP TEST DATA SHEET FOR

SHEET 01 OF 01

PROJECT NAME: FRENCH LTD  
 PROJECT NUMBER:                       
 DATE: 10-9-86

WELL NUMBER: STAFF GAUGE  
 r IN FEET:                       
 STARTING WATER LEVEL:                     

445-0575

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
17:30		74.52	AB.		
21:30		74.52	A.B.		
23:35		74.52	A.T.		
01:26		74.52	A.T.		
03:45		74.52	A.T.		
09:02		74.51	DWD		
11:12		74.51	DRG		
13:14		74.51	DWD		
15:21		74.51	J.A.		
17:34		74.51	A.B.		
17:58		74.51	J.A.		
19:00		74.51	J.G.		
22:01		74.51	J.G.		
00:05		74.51	A.T.		
01:15		74.51	A.T.		
03:10		74.51	A.T.		
04:03		74.51	A.T.		
11:10		74.51	DRG		
13:10		74.515	DRG		
17:56		74.53	DR		
20:00		74.56	M.C.		

REI

**SHEET**        **OF**       

**JOB NO.:**

~~FLOW RATE MONITORING SHEET~~

COMPUTED BY:\_\_\_\_\_ DATE:\_\_\_\_\_

CHECKED BY : \_\_\_\_\_ DATE: \_\_\_\_\_

**WREX**

# CALCULATIONS AND COMPUTATIONS

SHEET 1 OF 1

PROJECT: \_\_\_\_\_

JOB NO.: \_\_\_\_\_

SUBJECT: FRENCH LTD WELLS

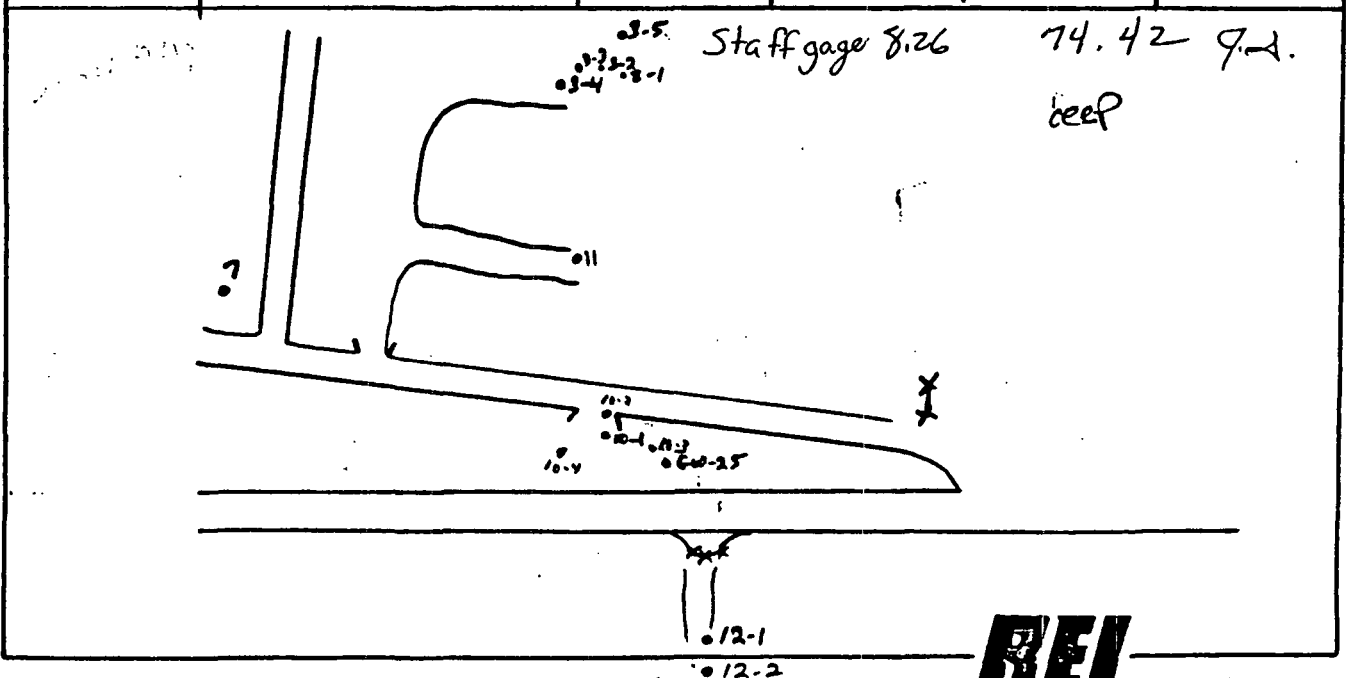
COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Initial water levels

10-7-86

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

MW#	CASING ELEVATION FEET MSL	INITIALS	TIME	WEL FROM NOTCH (FEET)	WEL FEET MSL
11	②	J.G.	8:10	78.42 ✓	
3-1					
2-2					
3-3					
3-4	④	J.G.	8:15	80.79 ✓	
3-5			8:18		
7	⑤	J.G.	8:04 A	80.33 ✓	
10-1	①	J.G.	7:52	81.34 ✓	
10-2	②	J.G.	7:56	5.78 ✓	
10-3	⑩	J.G.	7:45	7.14 ✓	
10-4	⑪	J.G.	7:58	7.66 ✓	
GW-25					
P10-2	⑥	<del>J.G.</del>	<del>7:46</del>	<del>46.06 ✓</del>	
P10-3	⑦	<del>J.G.</del>	<del>7:47</del>	<del>39.72 ✓</del>	
P10-4	⑧	<del>J.G.</del>	<del>7:50</del>	<del>38.82 ✓</del>	
12-1					
12-2					





SHEET 3 OF       

**JOB NO.:** \_\_\_\_\_

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

10-7-86

Hand-drawn sketch of a road layout. The sketch shows a road with several curves and straight sections. Key labels and measurements include:

- Top Right:** "74.42" and "deep".
- Top Center:** "7.18" and "11.58".
- Top Left:** "3-5", "3-4", "3-3", "3-2", "3-1".
- Left Side:** "7" near a vertical line.
- Bottom Center:** "10-4", "10-3", "10-2", "10-1", "60-25".
- Bottom Right:** "X" and "X" near a vertical line.
- Bottom Center:** "12-1" near a vertical line.
- Bottom Right:** "DEN" (partially visible).

**REF**

# CALCULATIONS AND COMPUTATIONS

SHEET 4 OF

PROJECT: \_\_\_\_\_

JOB NO.: \_\_\_\_\_

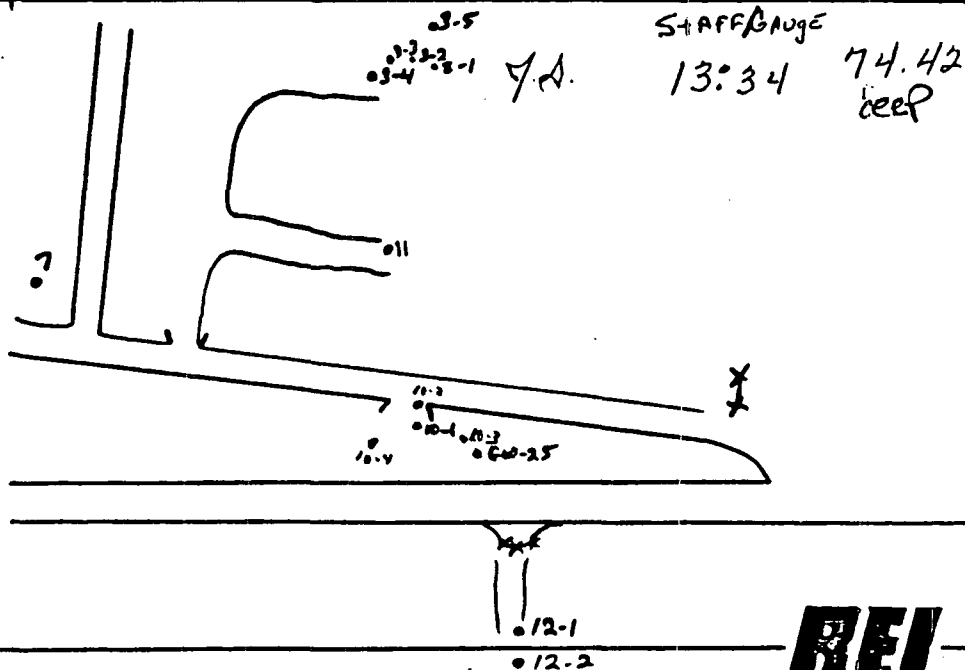
SUBJECT: FRENCH LTD WELLS

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

10-7-86

MW #	CASING ELEVATION FEET MSL	INITIALS	TIME	WEL FROM NORTH (FEET)	WEL FEET MSL
11		J.A.	13:06	80.66	
3-1					
2-2					
3-3					
3-4		J.A.	13:09	82.24	
3-5					
7		J.A.	13:03	80.35	
10-1		J.A.	13:37	111.42	
10-2		J.A.	12:55	5.77	
10-3		J.A.	12:51	7.13	
10-4		J.A.	13:00	7.64	
GW-25					
P10-2		<del>J.A.</del>	<del>12:58</del>	<del>45.97</del>	
P10-3		<del>J.A.</del>	<del>12:54</del>	<del>39.72</del>	
P10-4		<del>J.A.</del>	<del>12:57</del>	<del>38.82</del>	
12-1		J.A.	13:16	77.81	
12-2					



REI

SHEET 2 OF

JOB NO.: \_\_\_\_\_

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

10-7-86

**REF**

PROJECT NAME: FRENCH LTDWELL NUMBER: P-10-2

PROJECT NUMBER: \_\_\_\_\_

r IN FEET: \_\_\_\_\_

DATE: 10-7-86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1502		45.98			
17:13		46.01			
19:07		45.98			
21:27		45.97			
23:02		45.98			
00:45		45.96	SC		
3:04		45.96	SC		
4:56		45.96	SC		
07:04		45.96	A.T		
9:14		45.945	DRG		
11:06		45.95	DRG		
13:09		45.925	DRG		
13:10	checked	45.925	DRG		
15:10		45.91	A.B.		
17:06		45.88	AB.		
19:19		45.86	RC		
20:59		45.85	AB		
23:05		45.87	ML		
01:05		45.84	S.C.		
03:27		45.83	S.C.		
05:05		45.84	S.C.		
06:51		45.83	S.C.		
7:04		45.86	D.W.D		
11:10		45.87	D.W.D		
13:11		45.85	D.W.D		
15:25		45.87	AB.		

## PUMP TEST DATA SHEET FOR

SHEET OF

PROJECT NAME: FRENCH LTDWELL NUMBER: ~~P-10-2~~ P-10-2

PROJECT NUMBER: \_\_\_\_\_

IN FEET: \_\_\_\_\_

DATE: 10-9-86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
16:58		45.86	AB		
19:17		45.86	MC		
21:03		45.86	AB		
23:19		45.88	JB		
01:09		45.85	SB		
03:12		45.85	AT		
05:00		45.87	AT		
07:03		45.855	AT		
9:09		45.86	DRG		
11:07		45.855	DRG		
13:24		45.855	DRG		
15:15		45.86	J.A.		
17:06		45.88	AP		
19:05		45.86	J.A.		
21:03		45.89	AB		
23:10		45.88	J.G.		
01:06		45.87	J.B.		
03:08		45.88	A.T.		
05:13		45.88	J.B.		
06:59		45.87	A.T.		
9:07		45.87	AB		
11:05		45.86	DRG		
13:05		45.855	DRG		
15:24		45.95	AB		
17:05		45.94	L.A.		
19:12		45.94	MU		



## PUMP TEST DATA SHEET FOR

SHEET OF

PROJECT NAME: French Ltd  
 PROJECT NUMBER: \_\_\_\_\_  
 DATE: 10/11/86

WELL NUMBER: P-10.2  
 r IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	Δ R	t/r <sup>2</sup>
2112		45.92	DD		
2303		45.98	MC		
01128		45.92	AT		
03:19		45.93	S.B.		
05:13		45.92	A.T		
07:00		45.94	A.T		
101		45.93	J.G	← cap off in rain	
1104		45.74	J.G		
1304		45.63	J.G		
15:00		45.53	J.G		
1704		45.48	MG		
1916		45.44	MC		
21:01		45.48	AB		
23:08		45.50	MC		
1108		45.54	JB		
3:02		45.55	AC		
5:08		45.59	AB		
7:00		45.62	AC		
09:06		45.66	DRG		
13:09		45.61	DRG		
15:03		45.595	DRG		
1929		45.62	SC		
2310		45.65	SC		
03:22		45.71	S.G.		
06:52		45.73	S.C.		
07:31		45.75	J.G.		
10:02		45.78	DRG		
1122		45.855	DRG - data checked		
1158		45.91	DWD		
1320		45.875	DWD		

PHOTO OF

WELL NUMBER: P-10-2  
 & IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

**REI**

## PUMP TEST DATA SHEET FOR

SHEET OF

PROJECT NAME: FRENCH LTD

WELL NUMBER: # 7

PROJECT NUMBER:

r IN FEET:

DATE: 10-7-86

STARTING WATER LEVEL:

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1508		80.37			
17:38		80.43			
19:20		80.47			
21:53		80.51			
23:17		80.57			
00:55		80.61	SC		
3:10		80.67	SC		
5:04		80.71	SC		
7:12		80.77	A.T		
9:32		80.82	DRG		
11:21		80.875	DRG		
13:26		80.90	DRG		
15:22		80.93	A.B.		
17:16		80.95	A.B.		
19:40		80.97	MC		
21:10		81.10	AD		
23:14		81.08	ML		
01:15		81.14	SC		
03:39		81.19	SC		
05:13		81.23	SC		
06:53		81.27	SC		
9:29		81.33	DWD		
11:25		81.37	DWD		
13:23		81.41	D.W.D		
15:39		81.46	AB		

REI



## PUMP TEST DATA SHEET FOR

SHEET      OF     PROJECT NAME: FRENCH LTDWELL NUMBER: # 7PROJECT NUMBER:             I IN FEET:             DATE: 10-9-86STARTING WATER LEVEL:             

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
17:14		81.50	A.B.		
19:55		81.53	M.C.		
21:16		81.60	A.B.		
23:32		81.64	J.B.		
03:25		81.68	A.T.		
07:10		81.77	A.T.		
09:22		81.805	D.R.G.		
11:20		81.84	D.R.G.		
13:38		81.875	D.R.G.		
15:26		81.91	J.A.		
17:16		81.95	A.B.		
19:14		81.98	J.A.		
21:12		<del>81.99</del> <sup>AB</sup> 82.01	A.B.		
23:22		82.04	J.G.		
03:20		82.08	A.T.		
07:06		82.17	I.B.		
9:18		82.20	A.B.		
11:18		82.23	D.R.G.		
13:17		82.24	D.R.G.		
15:13		82.37	A.B.		
17:23		82.36	J.D.		
19:20		82.38	M.C.		

SHEET 1 OF 1

WELL NUMBER: 7

**r IN FEET:**

**STARTING WATER LEVEL:**

00/14/86

# AA

FILE #

WELL NUMBER: 7  
 & IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

# RYEN

## PUMP TEST DATA SHEET FOR

SHEET 01

PROJECT NAME: FRENCH LTD  
 PROJECT NUMBER: \_\_\_\_\_  
 DATE: 10-7-86

WELL NUMBER: P-10-4  
 r IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	A R	t/r <sup>2</sup>
1501		38.82			
17:10		38.82			
19:05		38.84			
21:23		38.84			
23:01		38.83			
00:44		38.82	SC		
3:02		38.82	SC		
4:54		38.81	SC		
07:03		38.82	A.T		
09:12		38.83	DRG		
11:04		38.82	DRG		
13:08		38.83	DRG		
15:09		38.83	I.B.		
17:04		38.83	A.B		
19:16		38.82	MC		
20:58		38.82	AB		
23:04		38.82	MC		
01:04		38.81	S.C		
03:26		38.80	SC		
05:01		38.81	S.C.		
06:50		38.82	S.C		
9:00		38.81	D.W.D		
11:08		38.81	D.W.D		
13:10		38.82.5	D.W.D		
15:23		38.82	A.B		



PROJECT NAME: FRENCH LTDWELL NUMBER: P-10-4

PROJECT NUMBER: \_\_\_\_\_

r IN FEET: \_\_\_\_\_

DATE: 10-9-86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
16:57		38.81	AB		
<del>19:22</del>		<del>39.71</del>	<del>HC</del>		
19:25		38.81	HC		
21:00		38.81	AB		
23:18		38.81	JB		
01:06		38.79	JB		
03:11		38.81	AT		
04:58		38.82	AT		
07:01		38.80	AT		
09:07		38.82	DRG		
11:06		38.805	DRG		
13:23		38.81	DRG		
15:14		38.80	J.A.		
17:03		38.81	AB		
18:04		38.80	J.A.		
21:02		38.80	AB		
23:06		38.79	JB		
01:05		38.81	JLB		
03:08		38.80 <sup>80</sup>	A.T.		
05:11		38.82	J.B.		
06:58		38.80	A.T.		
9:06		38.80	A.B.		
11:04		38.805	DRG		
13:03		38.805	DRG		
15:03		38.88	AB		
17:03		38.88	AD		
19:00		38.88	HC		



## PUMP TEST DATA SHEET FOR

SHEET

PROJECT NAME: Fiench Ltd.WELL NUMBER: P-10-4

PROJECT NUMBER: \_\_\_\_\_

r IN FEET: \_\_\_\_\_

DATE: 10/11/86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
2111		38.86	WQ		
2301		38.86	MC		
01:27		38.85	AT		
03:18		38.88	AT		
05:12		38.84	AT		
07:00		38.85	AT		
09:00		38.84	AT		
11:00		38.85	JG		
13:03		38.84	J.G		
15:08		38.82	JG		
17:01		38.84	MC		
19:13		38.83	MC		
21:00		38.82	AB		
23:07		38.80	MC		
1:07		38.83	JG		
3:00		38.80	AC		
5:07		38.80	AC		
6:59		38.80	LC		
9:04		38.805	DRG		
13:08		38.80	DRG		
15:02		38.795	DRG		
19:27		38.76	SC		
23:09		38.77	SC		
03:21		38.74	J.G		
06:51		38.75	J.G.		
07:31		38.76	J.G.		
10:00		38.76	DRG		
11:30		38.76	DRG		

REI

# UNIT 1

WELL NUMBER: P-10-4  
 IN FEET:  
 STARTING WATER LEVEL:

# ARE

PROJECT NAME: FRENCH LTD  
 PROJECT NUMBER: \_\_\_\_\_  
 DATE: 10/7/86

WELL NUMBER: P-10-3  
 T IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1457		39.72			
1702		39.74			
19:03		39.73			
2108		39.74			
23:04		39.74			
00:46		39.72	SC		
3:05		39.73	SC		
4:59		39.73	SC		
07:05		39.73	AT		
9:15		39.72	DRC		
1107		39.73	3DRC		
1212		39.725	DRC		
1511		39.74	A.B.		
17:08		39.73	A.B.		
2000		39.73	MC		
21:01		39.74	AB		
23:06		39.72	MC		
01:06		39.72	SC		
03:27		39.725	SC		
05:05		39.72	SC		
06:53		39.72	SC		
9:05		39.73	D.W.D		
1111		39.73	D.W.D		
13:12		39.725	D.W.D		
15:27		39.74	AB		



PROJECT NAME: FRENCH LTD  
 PROJECT NUMBER:                       
 DATE: 10-9-86

WELL NUMBER P-10-3  
 r IN FEET:                       
 STARTING WATER LEVEL:                     

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
17:03		39.72	AB		
19:22		39.71	HC		
21:05		39.74	AB		
23:21		39.73	JB		
01:10		39.72	FB		
03:14		39.72	AT		
05:00		39.72	AT		
07:04		39.72	AT		
09:10		39.71	DRG		
11:09		39.71	DRG		
13:26		39.72	DRG		
15:09		39.71	TA		
17:07		39.72	AB		
19:06		39.71	TA		
21:05		39.74	AB		
23:11		39.71	J.B		
01:07		39.72	J.B		
03:11		39.71	AT		
05:14		39.72	J.B		
07:00		39.71	J.B		
9:09		39.72	AB		
11:07		39.70	DRG		
13:06		39.705	DRG		
15:05		39.81	AB		
17:08		39.73	AD		
19:00		39.77	HC		

# PUMP TEST DATA SHEET FOR

SHEET      OF     

PROJECT NAME: French Lk.  
PROJECT NUMBER:             
DATE: 10/11/86

WELL NUMBER: P-10-3  
IN FEET:             
STARTING WATER LEVEL:           

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	Δ H	t/r <sup>2</sup>
2115		39.77	QW		
2257		39.77	MC		
01:29		39.76	A.F.		
03:20		39.77	S.B.		
05:15		39.75	A.F.		
07:02		39.75	A.F.		
10-12-86 904	39.68	39.68	J.G.	= 10' off in rain	
1108		39.67	J.G.		
1305		39.67	J.G.		
15:11		39.67	J.G.		
1659		39.68	MC		
1911		39.67	MC		
21:02		39.68	AB		
23:09		39.68	AME.		
10-13-86 01:10		39.67	JB		
3:03		39.66	AC		
5:09		39.67	AC		
7:02		39.67	HC		
09:08		39.675	DRG		
13:12		39.675	DRG		
15:04		39.66	DRG		
1930		39.65	SC		
2311		39.65	SC		
10/14 03:24		39.64	J.G.		
06:53		39.64	J.G.		
07:32		39.65	J.G.		
10:03		39.645	DRG		
11:23		39.64	DRG		

**REI**

**SECRET** **OF**

WELL NUMBER: P-10-3

**IN FEET:**

STARTING WATER LEVEL:

# ARE

PROJECT NAME: FRENCH LTDWELL NUMBER: 10-4

PROJECT NUMBER: \_\_\_\_\_

r IN FEET: \_\_\_\_\_

DATE: 10-7-86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1504		7.60			
17:15		7.58			
19:08		7.60			
2130		7.62			
23:06		7.63			
00:50		7.61	SC		
3:07		7.57	SC		
5:01		7.56	SC		
7:07		7.56	A.T		
920		7.58	DRG		
11:13		7.585	DRG		
1310		7.58	DRG		
1516		7.54	A.B.		
17:40		7.54	A.B.		
1921		7.52	MC		
21:04		7.55	AB		
23:09		7.54	MC		
01:08		7.50	S.C.		
03:31		7.48	S.C.		
05:06		7.49	S.C.		
06:54		7.48	S.C.		
09:47		7.54	D.W.D		
114		7.54	D.W.D		
13:17		7.52	D.W.D		
15:31		7.50	AB		

## PUMP TEST DATA SHEET FOR \_\_\_\_\_

SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NAME: \_\_\_\_\_  
 PROJECT NUMBER: \_\_\_\_\_  
 DATE: \_\_\_\_\_

WELL NUMBER: 10-4  
 IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
17:08		7.49	A.B		
19:31		7.48	MC		
21:08		7.51	A.B		
23:24		7.52	JB		
01:12		7.51	SB		
03:16		7.50	AT		
05:02		7.48	AT		
07:06		7.49	AT		
09:14		7.50	DRG		
11:13		7.50	DRG		
13:30		7.45	DRG		
15:17		7.41	J.A.		
17:10		7.41	AB		
19:10		7.40	J.A.		
21:07		7.42	AB		
23:15		7.43	SG		
01:10		7.43	J.B		
03:15		7.40	A.T		
05:16		7.39	A.T		
07:09		7.40	A.T.		
09:11		7.41	A.B		
11:12		7.465 <sup>u</sup>	DRG		
13:11		7.43	DRG		
15:08		7.38	AB		
17:12		7.37	AB		
19:10		7.41	MC		



## PUMP TEST DATA SHEET FOR

SHEET \_\_\_ OF \_\_\_

PROJECT NAME: French Ltd.WELL NUMBER: 10-4

PROJECT NUMBER: \_\_\_\_\_

IN FEET: \_\_\_\_\_

DATE: 10/11/86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
2121		7.42	DD		
2305		7.43	ML		
01:32		7.42	A.T.		
03:25		7.40	J.B.		
05:18		7.37	A.T.		
07:05		7.40	A.T.		
0907		7.47	J.B.		
1109		7.47	J.B.		
1307		7.43	J.B.		
15:14		7.33	J.B.		
1708		7.29	ML		
1919		7.23	ML		
21:06		7.23	AB		
21:12		7.18	AB		
1115		7.09	J.B.		
3:06		7.04	H.C.		
5:12		6.99	H.C.		
7:04		6.98	H.C.		
09:11		6.99	DRG		
13:15		6.945	DRG		
1508		6.905	DRG		
1932		6.82	SC		
2313		6.82	SC		
0329		6.81	J.B.		
06:56		6.81	J.B.		
09:35		6.82	J.B.		
10:06		6.88	DRG - double checked		
1116		6.825	DRG		



# PUMP TEST DATA SHEET FOR

PROJECT NAME: FRENCH LTD

PROJECT NUMBER: 1

DATE: 10-14-86

WELL NUMBER: 10-4

**IN FEET:**

STARTING WATER LEVEL:

[illegible]

# REN

## PUMP TEST DATA SHEET FOR

SHEET      OF     PROJECT NAME: FrenchWELL NUMBER: 10-3PROJECT NUMBER:           r IN FEET:           DATE: 10/7/86STARTING WATER LEVEL:           

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1455		7.07			
<del>15:00</del> 1700		7.07			
<del>18:00</del> 19:00		7.07			
2105		7.07			
23:05		7.10			
00:49		7.08	SC		
3:06		7.06	SC		
5:00		7.04	SC		
07:06		7.05	A.J.		
9:17		7.06	DRG		
11:09		7.075	DRG		
1313		7.06	DRG		
1512		7.01	A.B.		
17:09		6.98	AB		
19:04		6.98	MC		
21:02		7.00	AB		
23:02		7.00	MC		
01:07		6.98	S.C.		
03:29		6.98	S.C.		
05:05		6.97	S.C.		
06:54		6.96	S.C.		
906		7.01	D.W.D		
1113		7.03	D.W.D		
13:15		7.00	D.W.D		
15:29		6.98	A.B.		



## PUMP TEST DATA SHEET FOR

SHEET OF

PROJECT NAME: FRENCH LTD

WELL NUMBER: 10-3<sup>rd</sup>

PROJECT NUMBER: \_\_\_\_\_

T IN FEET: \_\_\_\_\_

DATE: 10-9-86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	Δ H	t/r <sup>2</sup>
17:06		6.96	A.B.		
19:29		6.98	MC		
21:06		6.99	A.B.		
23:23		7.01	JB		
01:12		6.98	JB		
03:15		6.98	AT		
05:01		6.97	AT		
07:05		6.98	AT		
09:17		6.99	DRG		
11:10		6.99	DRG		
13:28		6.94	DRG		
15:06		6.89	J.A.		
17:09		6.88	AB		
19:08		6.89	J.A.		
21:06		6.91	AB		
23:15		6.92	S.G.		
01:08		6.92	JB		
03:15		6.89	A.T.		
05:15		6.88	J.B.		
07:00		6.89	A.T.		
9:10		6.89	A.B.		
11:08		6.955	DRG		
13:08		6.92	DRG		
15:06		6.85	AB		
17:10		6.86	AB		
19:05		6.90	MC		

REI

## PUMP TEST DATA SHEET FOR

SHEET OF

PROJECT NAME: French Ltd

WELL NUMBER: 10-3

PROJECT NUMBER:

r IN FEET:

DATE: 10/11/86

STARTING WATER LEVEL:

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
10/11/86 2118		6.91	NH		
2307		6.90	MC		
01:31		6.92	A.J.		
03:22		6.90	J.B.		
05:16		6.86	A.J.		
10-12-86 07:04		6.90	A.J.		
906		6.94	J.G.		
1109		6.94	J.G.		
1306		6.89	J.G.		
15:13		6.77	J.G.		
1704		6.72	MC		
1921		6.68	MC		
21:04		6.67	APB		
23:11		6.62	MC		
10-13-86 1:13		6.56	J.B.		
3:03		6.51	AC		
5:10		6.46	AC		
7:03		6.45	AC		
09:09		6.49	DRG		
13:13		6.435	DRG		
15:06		6.385	DRG		
1931		6.30	SC		
2312		6.31	SC		
10/14 0328		6.32	J.B.		
06154		6.32	J.A.		
07134		6.33	J.G.		
10:05		6.385	D.R.G. - double checked		
1113		6.39	DRG		



FILE OF

WELL NUMBER: 10-3  
 & IN FEET:  
 STARTING WATER LEVEL:

**-APE!**

PROJECT NAME: FRENCH LTDWELL NUMBER: 10-2

PROJECT NUMBER: \_\_\_\_\_

r IN FEET: \_\_\_\_\_

DATE: 10-7-86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1500		5.73			
17:04		5.73			
19:10		5.72			
21:18		5.72			
23:07		5.76			
00:51		5.73	SC		
3:08		5.72	SC		
5:03		5.70	SC		
7:08		5.68	A.T		
9:22		5.72	DRG		
11:15		5.73	DRG		
13:19		5.72	DRG		
15:17		5.69	A.B.		
17:12		5.65	A.B.		
19:13		5.75	MC		
21:06		5.67	A.B.		
23:10		5.65	MC		
01:09		5.63	S.C.		
03:32		5.61	S.C.		
05:07		5.61	S.C.		
06:55		5.62	S.C.		
9:10		5.655	D.W.D		
11:17		5.68	D.W.D		
13:20		5.66	D.W.D		
15:33		5.62	AB.		

PROJECT NAME: FRENCH CTDWELL NUMBER: 10-2PROJECT NUMBER:             T IN FEET:             DATE: 10-9-86STARTING WATER LEVEL:             

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
17:11		5.62	A.B		
19:33		5.60	H C		
21:11		5.65	A.B		
23:26		5.64	J.B		
01:14		5.62	J.B.		
03:17		5.61	A.T		
05:04		5.61	A.T		
07:07		5.62	A.T		
09:16		5.65	DRG		
11:14		5.64	DRG		
13:32		5.595	DRG		
15:20		5.57	J.A.		
17:12		5.54	A.B		
19:11		5.54	J.A.		
21:09		5.56	AB		
23:16		5.56	SG		
01:12		5.57	J.B.		
03:17		5.51	A.T		
05:17		5.53	J.B.		
07:03		5.51	A.T.		
9:13		5.55	A.B		
11:14		5.59	DRG		
13:13		5.58	DRG		
15:10		5.55	AB.		
17:14		5.51	DD		
19:14		5.54	H C		

## PUMP TEST DATA SHEET FOR

SHEET \_\_\_ OF \_\_\_

PROJECT NAME: French Lk.

WELL NUMBER: 10-2

PROJECT NUMBER: \_\_\_\_\_

IN FEET: \_\_\_\_\_

DATE: 10/11/86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
2123		5.55	DR		
2308		5.56	MC		
01:34		5.54	A.F.		
03:26		5.54	J.B.		
05:19		5.50	A.F.		
07:06		5.52	A.F.		
908		5.61	J.G.		
1110		5.59	J.G.		
1308		5.54	J.G.		
15:16		5.43	J.G.		
1710		5.38	MC		
1924		5.32	MC		
21:07		5.30	AB		
23:14		5.26	MC.		
10-13-86 1116		5.18	JB		
3:09		5.12	AC		
5:15		5.09	AC		
7:25		5.10	AC		
9:12		5.10	DRG		
13:17		5.055	DRG		
15:09		5.015	DRG		
1733		4.93	SL		
2314		4.95	MC		
10-14 03:30		4.94	J.G.		
06:59		4.94	J.G.		
07:36		4.93	J.G.		
10:03		5.015	DRG - double checked		
11:15		5.02	DRG		

REI

**FILE NO**

WELL NUMBER: 10-2

**8 IN FEET:**

**STARTING WATER LEVEL:**

10/14/86

10/15/86

10/16/86

10/17/80

## PUMP TEST DATA SHEET FOR

SHEET \_\_\_ OF \_\_\_

PROJECT NAME: FRENCH

PROJECT NUMBER: \_\_\_\_\_

DATE: 10-7-86WELL NUMBER: 10-1

IN FEET: \_\_\_\_\_

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1459		109.92			
17:06		109.50			
19:02		116.36			
21:12		117.07			
22:57		117.61			
<del>23:40</del> 23:00	42	117.88	SC		
3:00		118.33	SC		
4:51		118.72	SC		
07:02		118.75	A-T		
9:09		118.81	DRG		
11:02		119.00	DRG		
13:04		119.33	DRG		
15:07		119.68	A.B.		
17:03		119.81	A.B.		
19:09		120.13	MC		
20:55		120.36	AB		
23:02		120.58	MC		
01:02		120.90	SC		
03:25		121.08	SC		
05:00		121.19	S.C.		
06:50		121.30	S.C.		
8:58		122.35	D.W.D.		
11:05		122.36	D.W.D.		
13:07		122.45	D.W.D.		
15:22		122.58	AB		





## PUMP TEST DATA SHEET FOR

SHEET 1 OF 1

PROJECT NAME: FRENCH LTDWELL NUMBER: 10-1

PROJECT NUMBER: \_\_\_\_\_

IN FEET: \_\_\_\_\_

DATE: 10-8-86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
16:55		122.75	A.B		
19:15		122.95	MC		
21:00		123.07	AB		
23:16		123.25	JB		
01:03		123.41	JB		
03:08		123.455	AT		
04:55		124.43	AT		
06:57		124.36	S.B.		
09:03		123.925	DRG		
11:03		123.74	DRG		
13:17		124.49	DRG		
15:11		124.47	J.A.		
17:02		124.42	A.B		
19:01		123.86	J.A.		
21:01		123.87	AB		
23:01		124.06	J.G.		
01:03		124.12	J.B.		
03:07		124.19	AT		
05:09		124.34	J.R.		
07:03		124.40	J.B.		
9:05		124.50	A.B		
11:00		124.48	DRG		
13:01		124.53	DRG		
15:01		124.70	A.B		
17:00		124.73	AB		
18:56		124.75	MC		



## PUMP TEST DATA SHEET FOR

SHEET

PROJECT NAME: French Ltd

WELL NUMBER: 10-1

PROJECT NUMBER:

I IN FEET:

DATE: 10/11/86

STARTING WATER LEVEL:

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
10/11/86 21:07		124.96	DB		
22:55		125.00	MC		
10-12-86 01:26		125.08	AG		
03:17		125.11	JB		
05:10		125.08	AG		
06:58		125.24	AG		
08:38		125.24	J.G.		
11/01 10:00	125.26		J.G.		
12:00			J.G.		
13:02		125.27	J.G.		
15:07		125.21	J.G.		
16:58		125.26	MC		
19:08		125.38	MC		
20:58		125.67	AB		
23:05		125.63	MC		
10-13-86 1:05		125.63	JB		
02:57		125.47	AC		
05:03		125.91	AC		
6:58		125.72	AC		
09:01		125.83	DRG		
10:36		126.06	DRG		
13:02		126.74	DRG		
19:25		126.80	SC		
23:07		126.85	SC		
10-14/86 03:20		127.07	J.G.		
06:50		127.18	J.G.		
07:29		127.16	J.G.		
09:58		127.32	DRG		

REI

2

WELL NUMBER: 10-1  
 IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

10-4-86

10-15-86

10-16-86

10-17-86

# REF

## PUMP TEST DATA SHEET FOR

SHEET \_\_\_ OF \_\_\_

PROJECT NAME: FRENCH LTDWELL NUMBER: 12-2

PROJECT NUMBER: \_\_\_\_\_

r IN FEET: \_\_\_\_\_

DATE: 10/10

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
23:40		4.15	S.G.		
03:39		4.13	A-T		
07:20		4.15	A.S.		
9:32		4.15	AB		
11:36		4.15	DRG		
15:28		4.20	AB		
17:48		4.13	AB		
22:01		4.11	AB		
02:07		4.13	S.B.		
03:51		4.10	A.S.		
05:50		4.12	S.B.		
07:46		4.06	J.G.		
09:49		4.01	J.G.		
11:43		3.92	J.G.		
13:35		3.83	J.G.		
15:38		3.79	AB		
17:49		3.79	AB		
23:56		3.72	H.C.		
01:29		3.73	JB		
14:55		<sup>m.s.p.</sup> <del>DRG</del> 3.675	DRG		
19:56		3.68	SC		
23:45		3.69	J.G.		
10/14/86 03:54		3.72	J.G.		
07:26		3.74	J.G.		
09:34		3.78	DRG		
12:26		3.785	DWD		
13:04		3.785	DWD		

REI

FIELD NO.

WELL NUMBER: 12-2  
 F IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

10.17-86

# ARE!

PROJECT NAME: FRENCH LTDWELL NUMBER: 3-4PROJECT NUMBER:     IN FEET:     DATE: 10-7-86STARTING WATER LEVEL:     

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1515		82.92			
17:22		83.41			
19:14		83.77			
21:48		84.28			
23:10		84.52			
104		84.81	SC		
316		85.14	SC		
510		85.37	SC		
7:16		85.605	A.T		
9:43		85.85	DRC		
11:30		86.02	DRC		
13:37		86.175	DRC		
15:24		86.32	A.B.		
17:21		86.43	AB		
19:33		86.58	MC		
21:15		86.74	AB		
23:18		86.88	MC		
01:21		87.04	SC		
03:46		87.20	SC		
05:18		87.30	SC		
6:58		87.41	SC		
9:15		87.55	D.W.D		
11:31		87.695	D.W.D	← Sounder gets rough on transducer	
13:28		87.815	D.W.D		
15:49		87.96	AB.	transducer moved back to original position after 108ers	

## PUMP TEST DATA SHEET FOR

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT NAME: FRENCA LTD  
 PROJECT NUMBER: 275-14  
 DATE: 10-9-86

WELL NUMBER: 3-4  
 T IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

## MANUAL READINGS

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
17:20		88.10	AB		
19:50		88.18	MC		
21:26		88.28	AB		
23:45		88.41	JB		
03:33		88.54	A.T		
07:15		88.74	AT		
09:34		88.84	DRG		
11:30		88.915	DRG		
13:48		89.00	DRG		
15:45		89.06	J.A.		
17:24		89.15	A.B		
19:21		89.20	J.L.		
21:21		89.27	AB		
23:30		89.31	S.G.		
03:31		89.40	A.T		
07:13		89.53	A.T.		
9:25		89.62	AB		
11:29		89.67	DRG		
13:26		89.695	DRG		
15:21		89.85	AB		
17:37		89.87	BD		
19:32		89.93	MC		

SHEET \_\_\_\_ OF \_\_\_\_

WELL NUMBER: 3-41

**r IN FEET:**

DATE: 10/1/58

**STARTING WATER LEVEL:**

$$\begin{array}{r} 80.75 \\ - 90.30 \\ \hline - 10.49 \end{array}$$



**END OF**

WELL NUMBER: 3-4  
 F IN FEET:  
 STARTING WATER LEVEL:

**REF**

PROJECT NAME: FRENCH LTDWELL NUMBER: #11

PROJECT NUMBER: \_\_\_\_\_

I IN FEET: \_\_\_\_\_

DATE: 10-7-86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1512		81.32			
17:25		81.79			
19:17		82.24			
2141		82.73			
2312		83.02			
00:58		83.29	SC		
3:12		83.64	SC		
507		83.89	SC		
7:20		84.15	A.T		
9:37		84.38	DRG		
11:26		84.56	DRG		
1331		84.72	DRG		
15:28		84.92	A.B.		
17:25		85.02	A.B.		
1927		85.18	HC		
21:19		85.39	AB		
23:16		85.50	MC		
01:18		85.66	SC		
03:42		85.83	SC		
05:15		85.94	SC		
6:56		86.06	SC		
9:25		86.23	D.W.D		
11:34		86.39	DWD		
1331		86.515	DWD		
15:44		86.66	AB		

## PUMP TEST DATA SHEET FOR \_\_\_\_\_

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT NAME: FRENCH LTD  
 PROJECT NUMBER: \_\_\_\_\_  
 DATE: 10-9-86

WELL NUMBER: #11  
 r IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
17:24		86.77	A.B.		
19:44		86.88	MC		
21:20		86.99	AB		
23:31		87.12	JB		
03:30		87.30	A-T.		
07:14		87.50	AT		
09:28		87.59	DRG		
11:25		87.68	DRG		
13:44		87.78	DRG		
15:32		87.84	J.A.		
17:20		87.92	AB.		
19:17		87.97	J.A.		
21:16		88.02	AB		
23:26		88.10	SG		
03:27		88.21	A-T.		
07:10		88.33	A.T.		
9:21		88.41	AB		
11:24		88.47	DRG		
13:23		88.525	DRG		
15:17		88.70	AB.		
17:32		88.70	DR		
19:26		88.74	MC		

SHEET \_\_\_ OF \_\_\_

WELL NUMBER: 11

**r IN FEET:**

**STARTING WATER LEVEL:**

new transfer  
level  
of 5' lower

REF ID: A66582

WELL NUMBER: ~~12~~ 11

**x IN FEET:**

**STARTING WATER LEVEL:**

# ARE

PUMP TEST DATA SHEET FOR REI 10-1 Run #2 SHEET 1 OF 1

PROJECT NAME: French Ltd  
 PROJECT NUMBER: 275-14  
 DATE: 10-7-86

WELL NUMBER: REI 12-1  
 r IN FEET: \_\_\_\_\_  
 STARTING WATER LEVEL: \_\_\_\_\_

*Manual Readings*

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	Δ H	t/r <sup>2</sup>
9:29	29	77.64	J.A.		
11:22	142	77.66	J.A.		
13:16		77.81	J.A.		
15:23		78.08			
19:26		78.71			
22:05		79.11			
23:24		79.39	SC		
108		79.59	SC		
3:25		79.95	SC		
5:15		80.23	SC		
7:26		80.54	A.J.		
9:50		80.88	DRG		
11:37		81.125	DRG		
13:45		81.34	DRG		
15:35		81.59	A.B.		
17:31		81.77	AB		
19:43		81.82	MC		
21:25		82.22	AB		
23:14		82.38	MC		
01:26		82.59	SC		
03:52		82.86	SC		
05:25		82.96	SC		
07:05		83.12	SC		
9:34		83.345	D.W.D		
11:43		83.525	D.W.D		
13:37		83.69	D.W.D		
15:58		83.89	AB		



## PUMP TEST DATA SHEET FOR

SHEET      OF     PROJECT NAME: FRENCH WDWELL NUMBER: REG 12-1PROJECT NUMBER: 275-14T IN FEET:     DATE: 10-9-86STARTING WATER LEVEL:     

## MANUAL READINGS

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
17:30		84.02	AB.		
2000		84.19	MC		
10/9/86 21:32		84.34	AB.		
23:54		84.45	JB		
03:42		84.72	A.T		
10/10/86 07:22		84.96	A.T		
09:40		85.105	DRG		
11:36		85.22	DRG		
13:56		85.35	DRG		
15:44		85.46	J.L		
17:30		85.56	AD		
18:28		85.68	J.A.		
21:29		85.73	AB		
23:33		85.88	J.L.		
03:38		<del>86.03</del> 86.03 A.T	A-T		
10-11-86 07:18		86.21	A.T		
9:31		86.33	AB		
11:35		86.35	DR		
15:27		86.67	AB		
17:46		86.69	DD		
19:39		86.78	MC		

PROJECT NAME: Finch HQWELL NUMBER: 12-1

PROJECT NUMBER: \_\_\_\_\_

r IN FEET: \_\_\_\_\_

DATE: 10/11/86

STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	A H	t/r <sup>2</sup>
10/11/86 2200		86.84	DD		
2329		86.86	MC		
02:01		87.02	J.B.		
03:51		87.02	A.T.		
05:45	"	87.13	J.B.		
07:46		87.13	J.G.		
09:48		87.13	J.G.		
11:42		87.43	J.G.		
13:34		87.13	J.G.		
15:38		87.15	AB		
17:38		87.69 AB	AB		
23:55		87.72	H.C.		
01:21		87.51	J.B.		
14:53		87.73	DRG		
19:55		87.87	SC		
23:44		87.98	J.G.		
10/12/86 03:53		88.13	J.G.		
07:25		88.22	J.G.		
09:33		88.30	DRG		
12:25		88.37	DWD		
1301		88.375	DWD		
1405		88.365	DWD		



**FILE NO.**

WELL NUMBER: 12-1

**IN FEET:**

**STARTING WATER LEVEL:**

10-14  
-----  
10-15  
-----  
10-17-86

# REM

Appendix 20

GW-25 Removal Log

~~degradation.~~

## APPENDIX —

### SUMMARY OF GW-25 WELL REMOVAL

DATE      TIME

9/20/86    09:45

#### EVENT

A Failing Holmaster 1250 was set up over GW-25 and plumbed 90 degrees from horizontal. The well's steel protective casing was removed. A 5.5 inch diameter drill bit with a one foot long guiding nose was centered over the opening of the well. Drilling fluids consisting of fire hydrant water, bentonite jel, and mica flakes were mixed.

#### COMMENTS

The steel casing and the six inch diameter PVC surface casing were loose in the ground.

DATE      TIME  
9/20/86    14:15

#### EVENT

Six inch diameter surface casing was being <sup>e</sup>removed from the ground in sections several feet long. No grout chunks were brought to the surface.

#### COMMENTS

The six inch casing showed no signs of degradation. The grout was erroded easily by jetted drilling fluids and was brought to the surface as a grey-green sediment within the drilling fluid.

DATE      TIME  
9/20/86    14:20

#### EVENT

Extremely viscous material of an almost jelly consistency was encountered at a depth of 17.5 feet. The material continued to a depth of 22 feet.

#### COMMENTS

The material was apparently a very thick bentonite jel mixture. While drilling through this material, the six inch casing was loose in the hole, and was pushed ahead of the drill bit down the hole.

DATE        TIME  
9/22/86    09:00

EVENT

Cement grout was encountered at 22 feet below the surface. The majority of six inch diameter casing was removed from the hole.

DATE        TIME  
9/22/86    14:00

EVENT

Black oily fluids started bubbling out of the boring. HNU readings were as high as eight ppm at the boring.

DATE        TIME  
9/23/86    13:55

EVENT

Drilling stopped at 55 feet below the surface because the drill bit seemed to have wandered out of the two inch diameter PVC casing.

COMMENTS

It was determined that although the bit was no longer in the two inch PVC, that it was still within the original boring, and that well destruction was continuing - as evidenced by the continued circulation to the surface of PVC cuttings, and grout material. The grout material had reverted back to being easily eroded by the drilling process, grout was only present in the cuttings as a grey-green sediment. It was decided that drilling would continue at a slow pace - guided by a study of drilling rate changes and cuttings.

DATE        TIME  
9/23/86    16:10

EVENT

The drill bit wandered into natural materials at 64 feet. The path of the well was refound using a regular 4 3/4 inch diameter drill bit.

COMMENTS

It appeared that difficulties in maintaining the <sup>diameter</sup> path of the well were due to two reasons. First, the grout was apparently not hard enough to prevent the two inch PVC casing from moving around in the hole as the drill bit rotated on it. Second, due to the flexibility of the original drilling rod used to install the well, the boring did not remain vertical with depth, but deflected in various directions.

DATE        TIME  
9/23/86    16:30

#### EVENT

Hard grout material was encountered at 65.5 feet and continued ~~down~~ to 70 feet below the surface. Below 70 feet the original boring was lost, and all cuttings suggesting well destruction stopped circulating to the surface. Drilling was terminated 75 feet below the surface in natural materials.

#### COMMENTS

It was decided that the boring would be slowly widened using a combination of increasing diameter drill bits and washing with drilling fluids to try and find the location of the original GW-25 boring which had apparently wandered to one side.

DATE            TIME  
9/25/86        12:46

#### EVENT

A 12 to 14 inch diameter boring had been drilled to a depth of 86 feet below the surface. The boring was apparently in natural materials from 70 to 86 feet. Washing of the boring with a water jet to attempt to uncover the original well boring was started.

DATE            TIME  
9/25/86        17:00

#### EVENT

A hole had been washed to a depth of 93 feet. The hole had then been widened with a 4 3/8 inch diameter drill bit. Samples of materials from 93 to 97 feet below the surface had been obtained with a split spoon sampler.

#### COMMENTS

No indications of well materials were seen between 86 and 97 feet. The samples were of natural soils. It was decided that the boring would be widened to 7 7/8 inches down to 97 feet, and that the hole would then be grouted to the surface.

DATE            TIME  
9/26/86        14:12

#### EVENT

The boring had been tremie grouted to the surface with a 96% cement , 4% bentonite jel mixture.

DATE            TIME  
9/29/86        07:00

#### EVENT

The grout seal was inspected. There was no indication of settling or cracking.

~~During the drilling-out process it was found that the~~  
~~grout material was not seen~~ 33. ~~presumably an~~  
~~effective seal around the well casing and piping.~~  
~~Based on these observations~~  
~~it appears that downward movement of~~  
~~water from the shallow to deep aquifer occurred because of an inadequate grout seal of the~~  
~~well around~~  
~~gravel.~~  
~~could have~~

#### ~~E-10.3 DISCUSSION OF GW-25 WELL REMOVAL~~

Well GW-25 was not completely removed. It is felt that the well was removed to a depth of at least 70 feet. Below that depth, the well probably remains intact. Because the shallow aquifers may continue to a depth of 76 feet below the surface, there was a six foot interval in which leakage could have possibly continued to occur. To counteract this, the boring was widened to at least 16 inches in that interval, ~~so as~~ <sup>anticipating this would</sup> ~~to hopefully~~ expose the remaining well casing so that it would be plugged during the grouting process. The results of the REI 10-1 RUN #2 Pump Test ~~showed~~ confirm ~~that~~ this approach was successful.

#### DATA GATHERING TECHNIQUES:

Water Level Monitoring: Water levels were measured with an Insitu Hydrologic Analysis System Model SE200 equipped with pressure transducers (accuracy  $\pm 0.03$  ft). Insitu measurement accuracy checked with manual readings taken with Well Wizard Series 6000 well sounders. Fluid levels in the on-site pond were measured manually with a staff gauge.

Pumping Rate Monitoring: Flow rate was measured at the pump discharge with a 5 gallon bucket and stop watch (accuracy = 0.2 gpm).

#### Meteorological Events:

Atmospheric Pressure,  
Atmospheric Temperature,  
and Relative Humidity: Weathermeasure Metrograph with a 7 day drum graph. See Section \_\_\_\_\_

Start and Stop Times  
of Rain Events, Cloud  
Cover, Wind, and Misc.  
events: Visual observation with record maintained in a log book

Appendix 21

Deep Aquifer Groundwater Analysis Reports



SEP 8, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Volatile Compounds - GC/MS Analysis Data (QR01)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4777 RESOURCE ENGINEERING

RES27514

WREI 11

860828

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound <small>Acrolein and Acrylonitrile values are screen only.</small>	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concn Added ug/l	% Recov	Unspiked Sample ug/l	Concn Added ug/l	% Recov
1V	Acrolein	ND	100	ND	ND	ND	800	113	ND	800	76
2V	Acrylonitrile	ND	100	ND	ND	ND	80.0	96	ND	80.0	77
3V	Benzene	ND	4.4	ND	ND	ND	18.0	98	ND	18.0	98
4V	bis(Chloromethyl)ether	ND	10	ND	ND	ND	0	-	ND	0	-
5V	Bromoform	ND	4.7	ND	ND	ND	18.0	99	ND	18.0	82
6V	Carbon tetrachloride	ND	2.8	ND	ND	ND	18.0	102	ND	18.0	105
7V	Chlorobenzene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	101
8V	Chlorodibromomethane	ND	3.1	ND	ND	ND	18.0	101	ND	18.0	90
9V	Chloroethane	ND	10	ND	ND	ND	18.0	104	ND	18.0	91
10V	2-Chloroethylvinyl ether	ND	10	ND	ND	ND	18.0	0 <sub>a</sub>	ND	18.0	0 <sub>a</sub>
11V	Chloroform	ND	1.6	ND	ND	ND	18.0	103	ND	18.0	102
12V	Dichlorobromomethane	ND	2.2	ND	ND	ND	18.0	103	ND	18.0	100
13V	Dichlorodifluoromethane	ND	10	ND	ND	ND	18.0	110	ND	18.0	91
14V	1,1-Dichloroethane	ND	4.7	ND	ND	ND	18.0	100	ND	18.0	104
15V	1,2-Dichloroethane	ND	2.8	ND	ND	ND	18.0	105	ND	18.0	93
16V	1,1-Dichloroethylene	ND	2.8	ND	ND	ND	18.0	100	ND	18.0	105
17V	1,2-Dichloropropane	ND	6.0	ND	ND	ND	18.0	100	ND	18.0	94
18V	cis-1,3-Dichloropropylene	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	95
19V	Ethylbenzene	ND	7.2	ND	ND	ND	18.0	101	ND	18.0	104
20V	Methyl bromide	ND	10	ND	ND	ND	18.0	109	ND	18.0	86
21V	Methyl chloride	ND	10	ND	ND	ND	18.0	106	ND	18.0	115
22V	Methylene chloride	BMDL	2.8	3.05	5.73	5.10	18.0	90	2.94	18.0	117
23V	1,1,2,2-Tetrachloroethane	ND	6.9	ND	ND	ND	18.0	103	ND	18.0	94
24V	Tetrachloroethylene	ND	4.1	ND	ND	ND	18.0	99	ND	18.0	101
25V	Toluene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	102
26V	1,2-Trans-dichloroethylene	ND	1.6	ND	ND	ND	18.0	100	ND	18.0	104
27V	1,1,1-Trichloroethane	ND	3.8	ND	ND	ND	18.0	104	ND	18.0	105
28V	1,1,2-Trichloroethane	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	88
29V	Trichloroethylene	ND	1.9	ND	ND	ND	18.0	98	ND	18.0	91
30V	Trichlorofluoromethane	ND	10	ND	ND	ND	18.0	103	ND	18.0	109
31V	Vinyl chloride	ND	10	ND	ND	ND	18.0	103	ND	18.0	94
18V	trans-1,3-Dichloropropylene	ND	10	ND	ND	ND	18.0	101	ND	18.0	95

<sup>a</sup> Recovery normally variable using established methodology.

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

SEP 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Acid Compounds - GC/MS Analysis Data (QR02)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4777 RESOURCE ENGINEERING

RES27514

WREI 11

860828

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
1A	2-Chlorophenol	ND	3.3	ND	ND	ND	100	75	ND	104	75
2A	2,4-Dichlorophenol	ND	2.7	ND	ND	ND	100	67	ND	104	74
3A	2,4-Dimethylphenol	ND	2.7	ND	ND	ND	100	68	ND	104	70
4A	4,6-Dinitro-o-cresol	ND	24	ND	ND	ND	100	67	ND	104	53
5A	2,4-Dinitrophenol	ND	42	ND	ND	ND	100	74	ND	104	62
6A	2-Nitrophenol	ND	3.6	ND	ND	ND	100	71	ND	104	75
7A	4-Nitrophenol	ND	2.4	ND	ND	ND	100	39	ND	104	36
8A	p-Chloro-m-cresol	ND	3.0	ND	ND	ND	100	60	ND	104	62
9A	Pentachlorophenol	ND	3.6	ND	ND	ND	100	56	ND	104	46
10A	Phenol	ND	1.5	4.16	2.82	ND	100	38	ND	104	44
11A	2,4,6-Trichlorophenol	ND	2.7	ND	ND	ND	100	80	ND	104	85

SEP 16, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N4777 RESOURCE ENGINEERING

RES27514

WREI 11

860828

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concn. Added ug/l	% Recov	Unspiked Sample ug/l	Concn. Added ug/l	% Recov
1B	Acenaphthene	ND	1.9	ND	ND	ND	100	77	ND	104	79
2B	Acenaphthylene	ND	3.5	ND	ND	ND	100	78	ND	104	81
3B	Anthracene	ND	1.9	ND	ND	ND	100	76	ND	104	77
4B	Benzidine	ND	44	ND	ND	ND	100	53	ND	104	74
5B	Benzo(a)anthracene	ND	7.8	ND	ND	ND	100	75	ND	104	71
6B	Benzo(a)pyrene	ND	2.5	ND	ND	ND	100	67	ND	104	44
7B	Benzo(b)fluoranthene	ND	10	ND	ND	ND	100	73	ND	104	60
8B	Benzo(ghi)perylene	ND	4.1	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	3.5	ND	ND	ND	100	66	ND	104	66
10B	bis(2-Chloroethoxy)methane	ND	5.3	ND	ND	ND	100	74	ND	104	75
11B	bis(2-Chloroethyl) ether	ND	5.7	ND	ND	ND	100	81	ND	104	77
12B	bis(2-Chloroisopropyl)ether	ND	5.7	ND	ND	ND	100	99	ND	104	87
13B	bis(2-Ethylhexyl)phthalate	ND	10	ND	ND	ND	100	79	ND	104	74
14B	4-Bromophenyl phenyl ether	ND	1.9	ND	ND	ND	100	72	ND	104	71
15B	Butyl benzyl phthalate	ND	10	ND	ND	ND	100	66	ND	104	55
16B	2-Chloronaphthalene	ND	1.9	ND	ND	ND	100	74	ND	104	75
17B	4-Chlorophenyl phenyl ether	ND	4.2	ND	ND	ND	100	82	ND	104	83
18B	Chrysene	ND	2.5	ND	ND	ND	100	77	ND	104	74
19B	Dibenzo(a,h)anthracene	ND	10	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	1.9	ND	ND	ND	100	72	ND	104	80
21B	1,3-Dichlorobenzene	ND	1.9	ND	ND	ND	100	64	ND	104	79
22B	1,4-Dichlorobenzene	ND	4.4	ND	ND	ND	100	69	ND	104	79
23B	3,3'-Dichlorobenzidine	ND	17	ND	ND	ND	100	69	ND	104	63
24B	Diethyl phthalate	ND	10	ND	ND	ND	100	36	ND	104	33
25B	Dimethyl phthalate	ND	10	ND	ND	ND	100	15	ND	104	19
26B	Di-n-butyl phthalate	ND	10	ND	ND	BMDL	100	70	ND	104	66
27B	2,4-Dinitrotoluene	ND	5.7	ND	ND	ND	100	85	ND	104	79
28B	2,6-Dinitrotoluene	ND	1.9	ND	ND	ND	100	83	ND	104	78
29B	Di-n-octyl phthalate	ND	10	ND	ND	ND	100	76	ND	104	69
30B	1,2-Diphenylhydrazine	ND	10	ND	ND	ND	100	91	ND	104	90
31B	Fluoranthene	ND	2.2	ND	ND	ND	100	81	ND	104	87
32B	Fluorene	ND	1.9	ND	ND	ND	100	82	ND	104	82

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

SEP 16, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4777 RESOURCE ENGINEERING RES27514 WREI 11 860828

ETC Sample No. Company Facility Sample Point Date Time Elapsed Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
33B	Hexachlorobenzene	ND	1.9	ND	ND	ND	100	74	ND	104	72
34B	Hexachlorobutadiene	ND	.90	ND	ND	ND	100	57	ND	104	73
35B	Hexachlorocyclopentadiene	ND	10	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	1.6	ND	ND	ND	100	52	ND	104	79
37B	Indeno(1,2,3-c,d)pyrene	ND	4.7	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	2.2	ND	ND	ND	100	77	ND	104	80
39B	Naphthalene	ND	1.6	ND	ND	ND	100	69	ND	104	66
40B	Nitrobenzene	ND	1.9	ND	ND	ND	100	75	ND	104	74
41B	N-Nitrosodimethylamine	ND	10	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	10	ND	ND	ND	100	76	ND	104	72
43B	N-Nitrosodiphenylamine	ND	1.9	ND	ND	ND	100	86	ND	104	86
44B	Phenanthrene	ND	5.4	ND	ND	ND	100	77	ND	104	75
45B	Pyrene	ND	1.9	ND	ND	ND	100	80	ND	104	85
46B	1,2,4-Trichlorobenzene	ND	1.9	ND	ND	ND	100	102	ND	104	109

A Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Aqueous Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports					
N4777	RESOURCE ENGINEERING	RES27514	WRE1-11	86082	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits..	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	.250	99	88	110
p-Bromofluorobenzene	.250	105	86	115
1,2-Dichloroethane-D4	.250	100	76	114
ACID FRACTION (GC/MS)				
Phenol-D5	100	42	10	94
2-Fluorophenol	100	56	21	100
2,4,6-Tribromophenol	100	59	10	123
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	95	35	114
2-Fluorobiphenyl	50	67	43	116
Terphenyl-D14	50	86	33	141
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	24..	154..
<small>* IFB EPA Control Limits  ** Advisory Limits Only</small>				

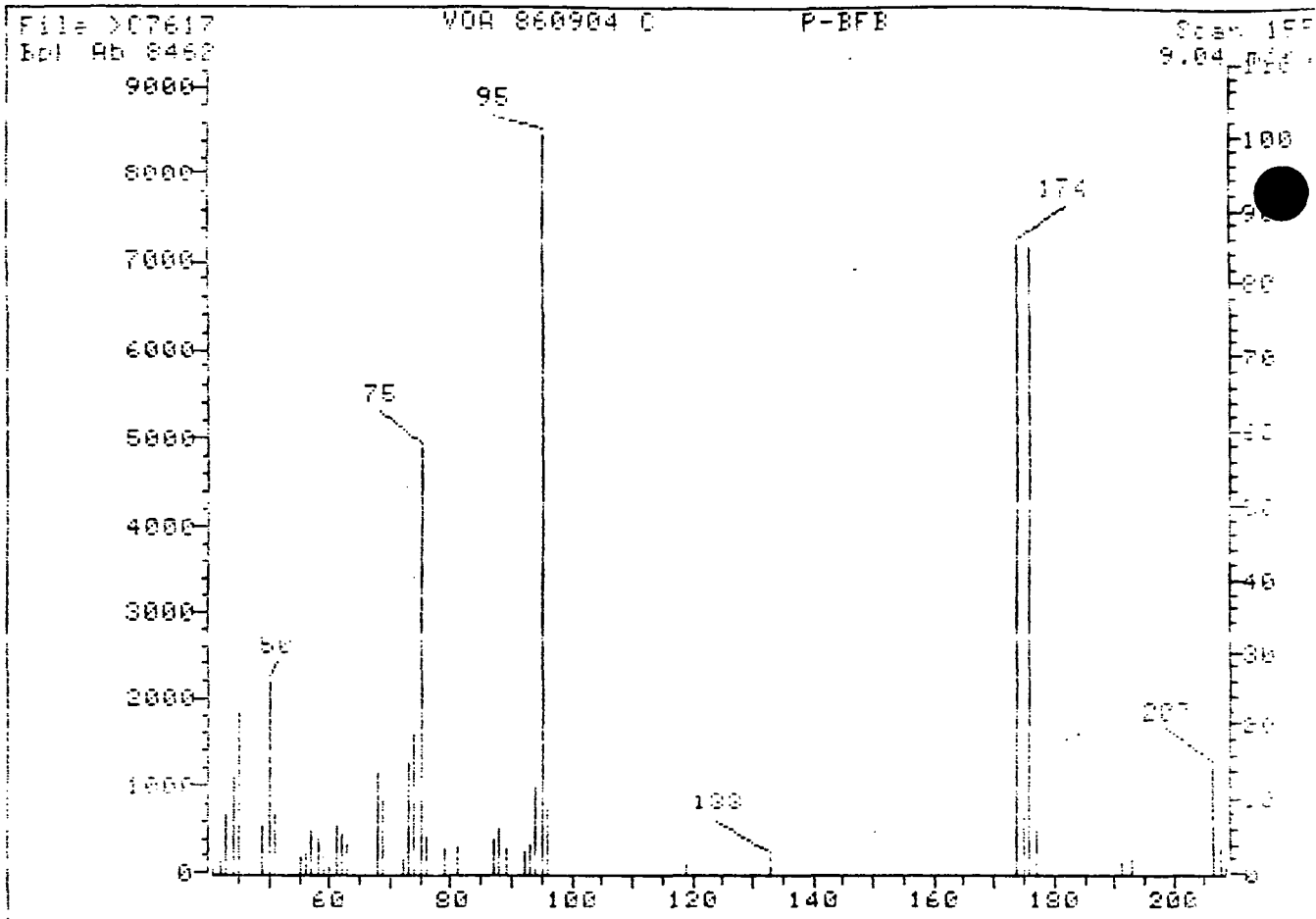


TABLE 2: METHOD PERFORMANCE DATA (QR21)

GC/ms Ionizing Data - bromofluorobenzene (BFB) for Volatiles Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
50	15-40% of mass 95	25.02	25.02	OK
75	30-60% of mass 95	57.54	57.54	OK
95	Base peak, 100% relative abundance	100.00	100.00	OK
96	5-9% of mass 95	8.33	8.33	OK
173	Less than 1% of mass 95	0.00	0.00	OK
174	Greater than 50% of mass 95	84.89	84.89	OK
175	5-9% of mass 174	7.41	8.73	OK
176	95-101% of mass 174	84.85	99.96	OK
177	5-9% of mass 176	5.72	6.74	OK

Injection Date: 09/04/86

Injection Time: 03:10

Run No: >07617

Spectrum No: 155

Analyst: *[Signature]*

Processor: *[Signature]*

GC Batch: QVS474

Samples:

N4742, N4744, N4746, N4745,  
N1590, N1591, N4343, N4344,  
N4102, N4777, N4778, N4775,  
N4779, N4780, N4776, N4180

*E.R.*  
9/6/86

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Volatile Compounds - GC/MS Analysis Data (QR01)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4775 RESOURCE ENGINEERING

RES27514

WREI 7

860829 1230

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound <small>Acrolein and Acrylonitrile values are screen only</small>	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concn Added ug/l	% Recov	Unspiked Sample ug/l	Concn Added ug/l	% Recov
1V	Acrolein	ND	100	ND	ND	ND	800	113	ND	800	76
2V	Acrylonitrile	ND	100	ND	ND	ND	80.0	96	ND	80.0	77
3V	Benzene	ND	4.4	ND	ND	ND	18.0	98	ND	18.0	98
4V	bis(Chloromethyl)ether	ND	10	ND	ND	ND	0	-	ND	0	-
5V	Bromoform	ND	4.7	ND	ND	ND	18.0	99	ND	18.0	82
6V	Carbon tetrachloride	ND	2.8	ND	ND	ND	18.0	102	ND	18.0	105
7V	Chlorobenzene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	101
8V	Chlorodibromomethane	ND	3.1	ND	ND	ND	18.0	101	ND	18.0	90
9V	Chloroethane	ND	10	ND	ND	ND	18.0	104	ND	18.0	91
10V	2-Chloroethylvinyl ether	ND	10	ND	ND	ND	18.0	0 <sub>a</sub>	ND	18.0	0 <sub>a</sub>
11V	Chloroform	ND	1.6	ND	ND	ND	18.0	103	ND	18.0	102
12V	Dichlorobromomethane	ND	2.2	ND	ND	ND	18.0	103	ND	18.0	100
13V	Dichlorodifluoromethane	ND	10	ND	ND	ND	18.0	110	ND	18.0	91
14V	1,1-Dichloroethane	ND	4.7	ND	ND	ND	18.0	100	ND	18.0	104
15V	1,2-Dichloroethane	ND	2.8	ND	ND	ND	18.0	105	ND	18.0	93
16V	1,1-Dichloroethylene	ND	2.8	ND	ND	ND	18.0	100	ND	18.0	105
17V	1,2-Dichloropropane	ND	6.0	ND	ND	ND	18.0	100	ND	18.0	94
18V	cis-1,3-Dichloropropylene	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	95
19V	Ethylbenzene	ND	7.2	ND	ND	ND	18.0	101	ND	18.0	104
20V	Methyl bromide	ND	10	ND	ND	ND	18.0	109	ND	18.0	86
21V	Methyl chloride	ND	10	ND	ND	ND	18.0	106	ND	18.0	115
22V	Methylene chloride	BM	2.8	3.05	5.73	5.10	18.0	90	2.94	18.0	117
23V	1,1,2,2-Tetrachloroethane	ND	6.9	ND	ND	ND	18.0	103	ND	18.0	94
24V	Tetrachloroethylene	ND	4.1	ND	ND	ND	18.0	99	ND	18.0	101
25V	Toluene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	102
26V	1,2-Trans-dichloroethylene	ND	1.6	ND	ND	ND	18.0	100	ND	18.0	104
27V	1,1,1-Trichloroethane	ND	3.8	ND	ND	ND	18.0	104	ND	18.0	105
28V	1,1,2-Trichloroethane	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	88
29V	Trichloroethylene	ND	1.9	ND	ND	ND	18.0	98	ND	18.0	91
30V	Trichlorofluoromethane	ND	10	ND	ND	ND	18.0	103	ND	18.0	109
31V	Vinyl chloride	ND	10	ND	ND	ND	18.0	103	ND	18.0	94
18V	trans-1,3-Dichloropropylene	ND	10	ND	ND	ND	18.0	101	ND	18.0	95

<sup>a</sup> Recovery normally variable using established methodology.

SEP 13, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Acid Compounds - GC/MS Analysis Data (QR02)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4775 RESOURCE ENGINEERING

RES27514

WRE1 7

860829 1230

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	HDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
1A	2-Chlorophenol	ND	4.1	ND	ND	ND	100	75	ND	104	75
2A	2,4-Dichlorophenol	ND	3.4	ND	ND	ND	100	67	ND	104	74
3A	2,4-Dimethylphenol	ND	3.4	ND	ND	ND	100	68	ND	104	70
4A	4,6-Dinitro-o-cresol	ND	30	ND	ND	ND	100	67	ND	104	53
5A	2,4-Dinitrophenol	ND	53	ND	ND	ND	100	74	ND	104	62
6A	2-Nitrophenol	ND	4.5	ND	ND	ND	100	71	ND	104	75
7A	4-Nitrophenol	ND	3.0	ND	ND	ND	100	39	ND	104	36
8A	p-Chloro-m-cresol	ND	3.8	ND	ND	ND	100	60	ND	104	62
9A	Pentachlorophenol	ND	4.5	ND	ND	ND	100	56	ND	104	46
10A	Phenol	ND	1.9	4.16	2.82	ND	100	38	ND	104	44
11A	2,4,6-Trichlorophenol	ND	3.4	ND	ND	ND	100	80	ND	104	85



SEP 16, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

## Chain of Custody Data Required for ETC Data Management Summary Reports

N4775 RESOURCE ENGINEERING

RES27514

WRE1 7

860829 1230

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concn. Added ug/l	% Recov	Unspiked Sample ug/l	Concn. Added ug/l	% Recov
1B	Acenaphthene	ND	2.4	ND	ND	ND	100	77	ND	104	79
2B	Acenaphthylene	ND	4.4	ND	ND	ND	100	78	ND	104	81
3B	Anthracene	ND	2.4	ND	ND	ND	100	76	ND	104	77
4B	Benzidine	ND	55	ND	ND	ND	100	53	ND	104	74
5B	Benzo(a)anthracene	ND	9.8	ND	ND	ND	100	75	ND	104	71
6B	Benzo(a)pyrene	ND	3.1	ND	ND	ND	100	67	ND	104	44
7B	Benzo(b)fluoranthene	ND	13	ND	ND	ND	100	73	ND	104	60
8B	Benzo(ghi)perylene	ND	5.1	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	4.4	ND	ND	ND	100	66	ND	104	66
10B	bis(2-Chloroethoxy)methane	ND	6.6	ND	ND	ND	100	74	ND	104	75
11B	bis(2-Chloroethyl) ether	ND	7.1	ND	ND	ND	100	81	ND	104	77
12B	bis(2-Chloroisopropyl)ether	ND	7.1	ND	ND	ND	100	99	ND	104	87
13B	bis(2-Ethylhexyl)phthalate	140	13	ND	ND	ND	100	79	ND	104	74
14B	4-Bromophenyl phenyl ether	ND	2.4	ND	ND	ND	100	72	ND	104	71
15B	Butyl benzyl phthalate	ND	13	ND	ND	ND	100	66	ND	104	55
16B	2-Chloronaphthalene	ND	2.4	ND	ND	ND	100	74	ND	104	75
17B	4-Chlorophenyl phenyl ether	ND	5.3	ND	ND	ND	100	82	ND	104	83
18B	Chrysene	ND	3.1	ND	ND	ND	100	77	ND	104	74
19B	Dibenzo(a,h)anthracene	ND	13	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	2.4	ND	ND	ND	100	72	ND	104	80
21B	1,3-Dichlorobenzene	ND	2.4	ND	ND	ND	100	64	ND	104	79
22B	1,4-Dichlorobenzene	ND	5.5	ND	ND	ND	100	69	ND	104	79
23B	3,3'-Dichlorobenzidine	ND	21	ND	ND	ND	100	69	ND	104	63
24B	Diethyl phthalate	ND	13	ND	ND	ND	100	36	ND	104	33
25B	Dimethyl phthalate	ND	13	ND	ND	ND	100	15	ND	104	19
26B	Di-n-butyl phthalate	ND	13	ND	ND	ND	100	70	ND	104	66
27B	2,4-Dinitrotoluene	ND	7.1	ND	ND	BMDL	100	85	ND	104	79
28B	2,6-Dinitrotoluene	ND	2.4	ND	ND	ND	100	83	ND	104	78
29B	Di-n-octyl phthalate	BMDL	13	ND	ND	ND	100	76	ND	104	69
30B	1,2-Diphenylhydrazine	ND	13	ND	ND	ND	100	91	ND	104	90
31B	Fluoranthene	ND	2.8	ND	ND	ND	100	81	ND	104	87
32B	Fluorene	ND	2.4	ND	ND	ND	100	82	ND	104	82

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

SEP 16, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4775 RESOURCE ENGINEERING

RES27514

WREI 7

860829 1230

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
33B	Hexachlorobenzene	ND	2.4	ND	ND	ND	100	74	ND	104	72
34B	Hexachlorobutadiene	ND	1.1	ND	ND	ND	100	57	ND	104	73
35B	Hexachlorocyclopentadiene	ND	13	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	2.0	ND	ND	ND	100	52	ND	104	79
37B	Indeno(1,2,3-c,d)pyrene	ND	5.9	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	2.8	ND	ND	ND	100	77	ND	104	80
39B	Naphthalene	ND	2.0	ND	ND	ND	100	69	ND	104	66
40B	Nitrobenzene	ND	2.4	ND	ND	ND	100	75	ND	104	74
41B	N-Nitrosodimethylamine	ND	13	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	13	ND	ND	ND	100	76	ND	104	72
43B	N-Nitrosodiphenylamine	ND	2.4	ND	ND	ND	100	86	ND	104	86
44B	Phenanthrene	ND	6.8	ND	ND	ND	100	77	ND	104	75
45B	Pyrene	ND	2.4	ND	ND	ND	100	80	ND	104	85
46B	1,2,4-Trichlorobenzene	ND	2.4	ND	ND	ND	100	102	ND	104	109

A Recovery normally varies using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Aqueous Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4775	RESOURCE ENGINEERING	RES27514	WREI 7	86082	1230	1
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	.250	99	88	110
p-Bromofluorobenzene	.250	105	86	115
1,2-Dichloroethane-D4	.250	106	76	114
ACID FRACTION (GC/MS)				
Phenol-D5	100	43	10	94
2-Fluorophenol	100	58	21	100
2,4,6-Tribromophenol	100	47	10	123
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	112	35	114
2-Fluorobiphenyl	50	68	43	116
Terphenyl-D14	50	58	33	141
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	24..	154..

\* IFB EPA Control Limits  
\*\* Advisory Limits Only

File: >07617  
Ipl. Ab 8462

VOR 860904 C

P-BFB

Scan 1  
9.04 m/z

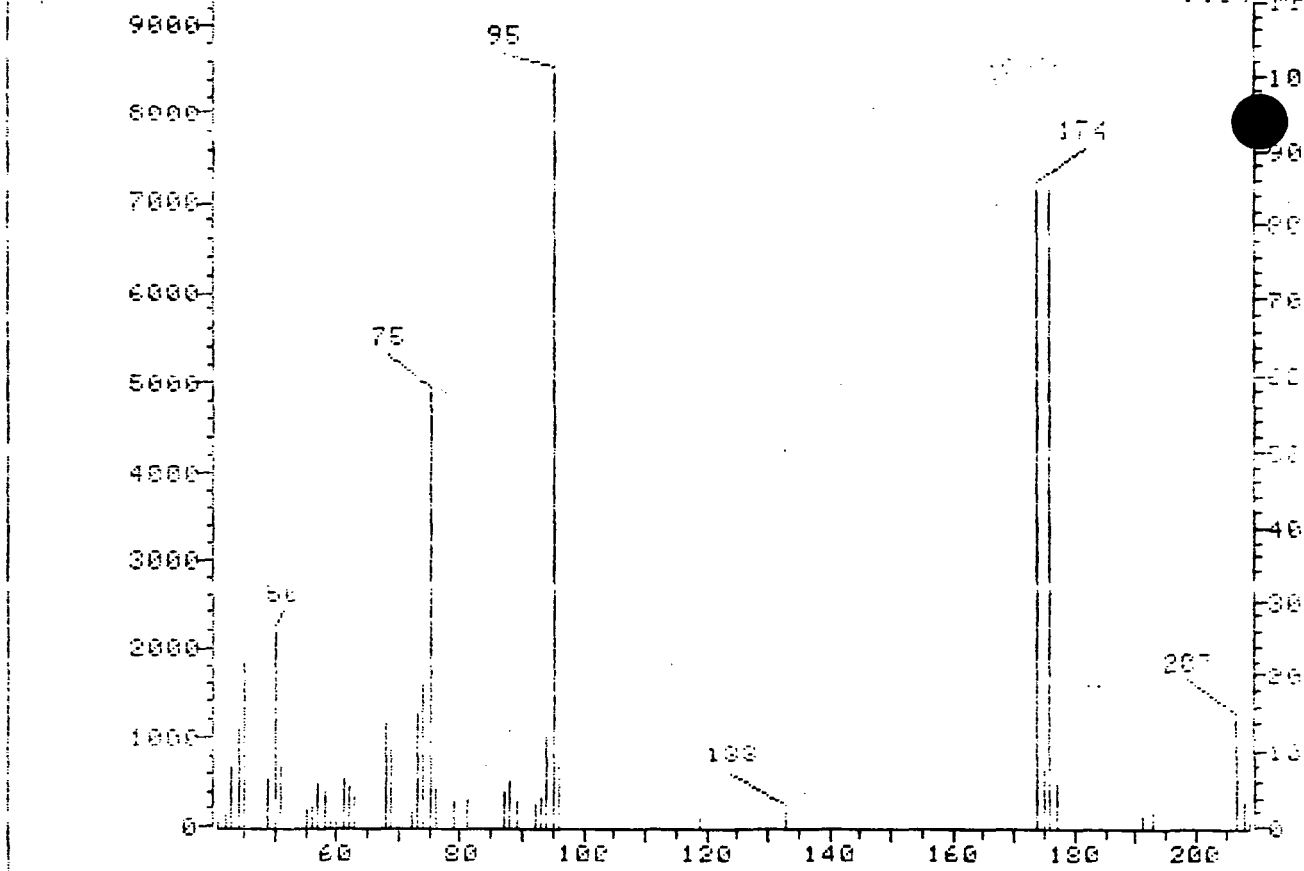


TABLE 2: METHOD PERFORMANCE DATA (QR21)

GC/MS Tuning Data - Bromofluorobenzene (BFB) for Volatiles Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
50	15-40% of mass 95	25.02	25.02	OK
75	30-60% of mass 95	57.54	57.54	OK
95	Base peak, 100% relative abundance	100.00	100.00	OK
96	5-9% of mass 95	8.33	8.33	OK
173	Less than 1% of mass 95	0.00	0.00	OK
174	Greater than 50% of mass 95	84.89	84.89	OK
175	5-9% of mass 174	7.41	8.73	OK
176	95-101% of mass 174	84.85	99.96	OK
177	5-9% of mass 175	5.72	6.74	OK

Injection Date: 09/04/86

Injection Time: 03:10

Run No: >07617

Spectrum No: 155

Analyst:

Processor:

QC Batch:

Samples:

*[Signature]*  
N4742, N4744, N4746, N4748  
N1590, N1591, N4343, N4344  
N4102, N4777, N4778, N4779  
N4779, N4780, N4776, N4780

*[Signature]*  
9/6/86

SEP 8, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Volatile Compounds - GC/MS Analysis Data (QR01)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4776 RESOURCE ENGINEERING

RES27514

WREI 12-1

860829 1430

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound <small>Acrolein and Acrylonitrile values are screen only.</small>	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov.	Unspiked Sample ug/l	Concen. Added ug/l	% Recov.
1V	Acrolein	ND	100	ND	ND	ND	800	113	ND	800	76
2V	Acrylonitrile	ND	100	ND	ND	ND	80.0	96	ND	80.0	77
3V	Benzene	ND	4.4	ND	ND	ND	18.0	98	ND	18.0	98
4V	bis(Chloromethyl)ether	ND	10	ND	ND	ND	0	-	ND	0	-
5V	Bromoform	ND	4.7	ND	ND	ND	18.0	99	ND	18.0	82
6V	Carbon tetrachloride	ND	2.8	ND	ND	ND	18.0	102	ND	18.0	105
7V	Chlorobenzene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	101
8V	Chlorodibromomethane	ND	3.1	ND	ND	ND	18.0	101	ND	18.0	90
9V	Chloroethane	ND	10	ND	ND	ND	18.0	104	ND	18.0	91
10V	2-Chloroethylvinyl ether	ND	10	ND	ND	ND	18.0	0 <sup>a</sup>	ND	18.0	0 <sup>a</sup>
11V	Chloroform	ND	1.6	ND	ND	ND	18.0	103	ND	18.0	102
12V	Dichlorobromomethane	ND	2.2	ND	ND	ND	18.0	103	ND	18.0	100
13V	Dichlorodifluoromethane	ND	10	ND	ND	ND	18.0	110	ND	18.0	91
14V	1,1-Dichloroethane	ND	4.7	ND	ND	ND	18.0	100	ND	18.0	104
15V	1,2-Dichloroethane	ND	2.8	ND	ND	ND	18.0	105	ND	18.0	93
16V	1,1-Dichloroethylene	ND	2.8	ND	ND	ND	18.0	100	ND	18.0	105
17V	1,2-Dichloropropane	ND	6.0	ND	ND	ND	18.0	100	ND	18.0	94
18V	cis-1,3-Dichloropropylene	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	95
19V	Ethylbenzene	ND	7.2	ND	ND	ND	18.0	101	ND	18.0	104
20V	Methyl bromide	ND	10	ND	ND	ND	18.0	109	ND	18.0	86
21V	Methyl chloride	ND	10	ND	ND	ND	18.0	106	ND	18.0	115
22V	Methylene chloride	4.95	2.8	3.05	5.73	5.10	18.0	90	2.94	18.0	117
23V	1,1,2,2-Tetrachloroethane	ND	6.9	ND	ND	ND	18.0	103	ND	18.0	94
24V	Tetrachloroethylene	ND	4.1	ND	ND	ND	18.0	99	ND	18.0	101
25V	Toluene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	102
26V	1,2-Trans-dichloroethylene	ND	1.6	ND	ND	ND	18.0	100	ND	18.0	104
27V	1,1,1-Trichloroethane	ND	3.8	ND	ND	ND	18.0	104	ND	18.0	105
28V	1,1,2-Trichloroethane	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	88
29V	Trichloroethylene	ND	1.9	ND	ND	ND	18.0	98	ND	18.0	91
30V	Trichlorofluoromethane	ND	10	ND	ND	ND	18.0	103	ND	18.0	109
31V	Vinyl chloride	ND	10	ND	ND	ND	18.0	103	ND	18.0	94
18V	trans-1,3-Dichloropropylene	ND	10	ND	ND	ND	18.0	101	ND	18.0	95

<sup>a</sup> Recovery normally variable using established methodology.

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

SEP 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Acid Compounds - GC/MS Analysis Data (QR02)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4776 RESOURCE ENGINEERING

RES27514 WREI 12-1 860829 1430

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
1A	2-Chlorophenol	ND	3.8	ND	ND	ND	100	75	ND	104	75
2A	2,4-Dichlorophenol	ND	3.1	ND	ND	ND	100	67	ND	104	74
3A	2,4-Dimethylphenol	ND	3.1	ND	ND	ND	100	68	ND	104	70
4A	4,6-Dinitro-o-cresol	ND	28	ND	ND	ND	100	67	ND	104	53
5A	2,4-Dinitrophenol	ND	48	ND	ND	ND	100	74	ND	104	62
6A	2-Nitrophenol	ND	4.1	ND	ND	ND	100	71	ND	104	75
7A	4-Nitrophenol	ND	2.8	ND	ND	ND	100	39	ND	104	36
8A	p-Chloro-m-cresol	ND	3.4	ND	ND	ND	100	60	ND	104	62
9A	Pentachlorophenol	ND	4.1	ND	ND	ND	100	56	ND	104	46
10A	Phenol	ND	1.7	4.16	2.82	ND	100	38	ND	104	44
11A	2,4,6-Trichlorophenol	ND	3.1	ND	ND	ND	100	80	ND	104	85

SEP 16, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4776 RESOURCE ENGINEERING

RES27514

WREI 12-1

860829 1430

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
1B	Acenaphthene	ND	2.2	ND	ND	ND	100	77	ND	104	79
2B	Acenaphthylene	ND	4.0	ND	ND	ND	100	78	ND	104	81
3B	Anthracene	ND	2.2	ND	ND	ND	100	76	ND	104	77
4B	Benzidine	ND	51	ND	ND	ND	100	53	ND	104	74
5B	Benzo(a)anthracene	ND	9.0	ND	ND	ND	100	75	ND	104	71
6B	Benzo(a)pyrene	ND	2.9	ND	ND	ND	100	67	ND	104	44
7B	Benzo(b)fluoranthene	ND	11	ND	ND	ND	100	73	ND	104	60
8B	Benzo(ghi)perylene	ND	4.7	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	4.0	ND	ND	ND	100	66	ND	104	66
10B	bis(2-Chloroethoxy)methane	ND	6.1	ND	ND	ND	100	74	ND	104	75
11B	bis(2-Chloroethyl) ether	ND	6.6	ND	ND	ND	100	81	ND	104	77
12B	bis(2-Chloroisopropyl)ether	ND	6.6	ND	ND	ND	100	99	ND	104	87
13B	bis(2-Ethylhexyl)phthalate	BMDL	11	ND	ND	ND	100	79	ND	104	74
14B	4-Bromophenyl phenyl ether	ND	2.2	ND	ND	ND	100	72	ND	104	71
15B	Butyl benzyl phthalate	ND	11	ND	ND	ND	100	66	ND	104	55
16B	2-Chloronaphthalene	ND	2.2	ND	ND	ND	100	74	ND	104	75
17B	4-Chlorophenyl phenyl ether	ND	4.8	ND	ND	ND	100	82	ND	104	83
18B	Chrysene	ND	2.9	ND	ND	ND	100	77	ND	104	74
19B	Dibenzo(a,h)anthracene	ND	11	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	2.2	ND	ND	ND	100	72	ND	104	80
21B	1,3-Dichlorobenzene	ND	2.2	ND	ND	ND	100	64	ND	104	79
22B	1,4-Dichlorobenzene	ND	5.1	ND	ND	ND	100	69	ND	104	79
23B	3,3'-Dichlorobenzidine	ND	19	ND	ND	ND	100	69	ND	104	63
24B	Diethyl phthalate	ND	11	ND	ND	ND	100	36	ND	104	33
25B	Dimethyl phthalate	ND	11	ND	ND	ND	100	15	ND	104	19
26B	Di-n-butyl phthalate	ND	11	ND	ND	BMDL	100	70	ND	104	66
27B	2,4-Dinitrotoluene	ND	6.6	ND	ND	ND	100	85	ND	104	79
28B	2,6-Dinitrotoluene	ND	2.2	ND	ND	ND	100	83	ND	104	78
29B	Di-n-octyl phthalate	ND	11	ND	ND	ND	100	76	ND	104	69
30B	1,2-Diphenylhydrazine	ND	11	ND	ND	ND	100	91	ND	104	90
31B	Fluoranthene	ND	2.5	ND	ND	ND	100	81	ND	104	87
32B	Fluorene	ND	2.2	ND	ND	ND	100	82	ND	104	82

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

SEP 16, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4776 RESOURCE ENGINEERING

RES27514

WREI 12-1

860829 1430

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
33B	Hexachlorobenzene	ND	2.2	ND	ND	ND	100	74	ND	104	72
34B	Hexachlorobutadiene	ND	1.0	ND	ND	ND	100	57	ND	104	73
35B	Hexachlorocyclopentadiene	ND	11	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	1.8	ND	ND	ND	100	52	ND	104	79
37B	Indeno(1,2,3-c,d)pyrene	ND	5.4	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	2.5	ND	ND	ND	100	77	ND	104	80
39B	Naphthalene	ND	1.8	ND	ND	ND	100	69	ND	104	66
40B	Nitrobenzene	ND	2.2	ND	ND	ND	100	75	ND	104	74
41B	N-Nitrosodimethylamine	ND	11	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	11	ND	ND	ND	100	76	ND	104	72
43B	N-Nitrosodiphenylamine	ND	2.2	ND	ND	ND	100	86	ND	104	86
44B	Phenanthrene	ND	6.2	ND	ND	ND	100	77	ND	104	75
45B	Pyrene	ND	2.2	ND	ND	ND	100	80	ND	104	85
46B	1,2,4-Trichlorobenzene	ND	2.2	ND	ND	ND	100	102	ND	104	109

A Recovery normally variable using established methodology.



**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Aqueous Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4776	RESOURCE ENGINEERING	RES27514	WRE1 12-1	86082	1430	1
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	.250	97	88	110
p-Bromofluorobenzene	.250	101	86	115
1,2-Dichloroethane-D4	.250	98	76	114
ACID FRACTION (GC/MS)				
Phenol-D5	100	37	10	94
2-Fluorophenol	100	50	21	100
2,4,6-Tribromophenol	100	47	10	123
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	90	35	114
2-Fluorobiphenyl	50	56	43	116
Terphenyl-D14	50	125	33	141
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	24..	154..
* IPB EPA Control Limits				
** Advisory Limits Only				

\* IFB EPA Control Limits

\*\* Advisory Limits Only

File >C7617  
Bpk Ab 8462

VOR 860904 C

P-BFB

Scan 155  
9.04 min

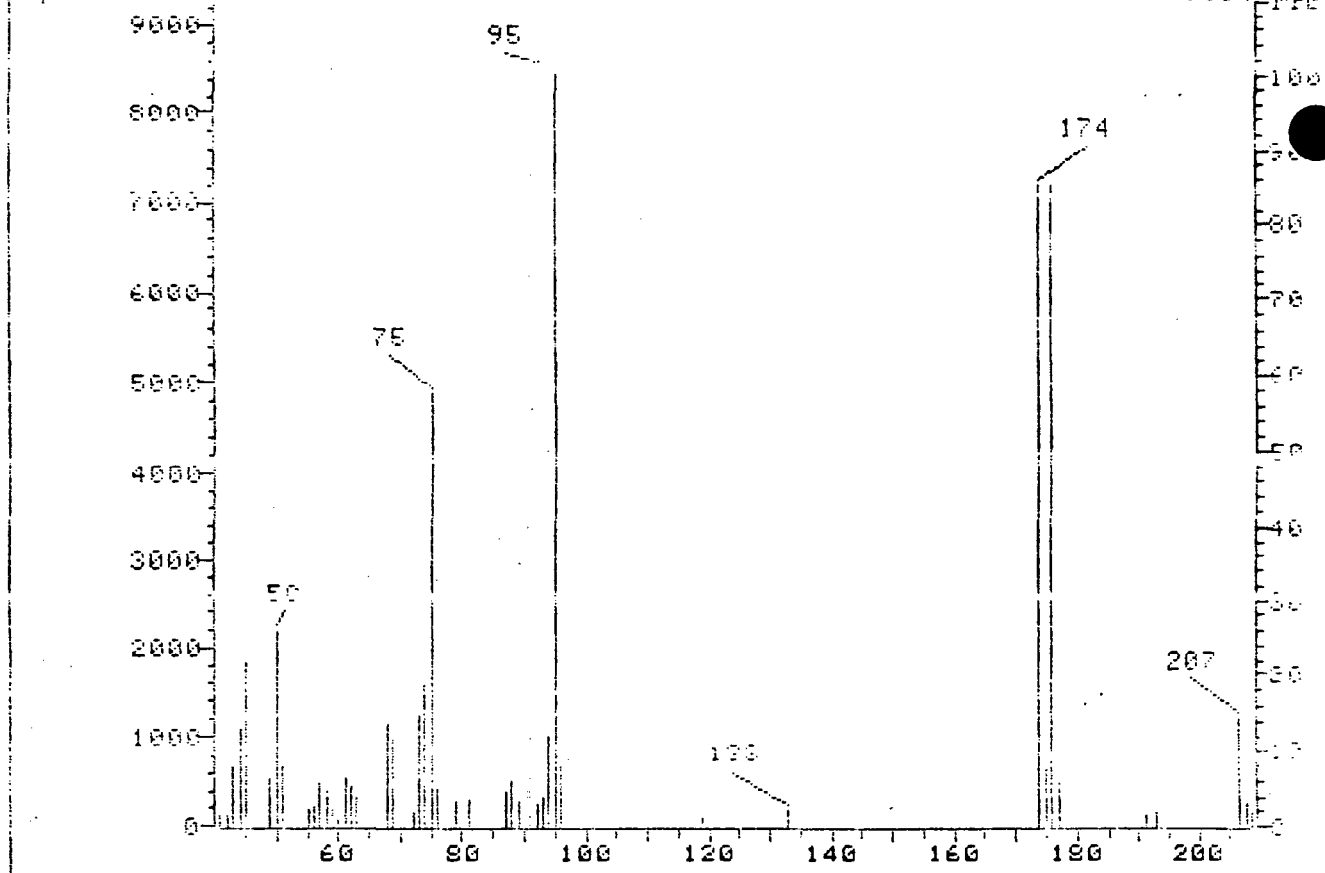


TABLE 2: METHOD PERFORMANCE DATA (QR21)

GC/KC Tuning Data - Bromofluorobenzene (BFB) for Volatiles Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
50	15-40% of mass 95	25.82	25.82	OK
75	30-60% of mass 95	57.54	57.54	OK
95	Base peak, 100% relative abundance	100.00	100.00	OK
96	5-9% of mass 95	8.33	8.33	OK
173	Less than 1% of mass 95	0.00	0.00	OK
174	Greater than 50% of mass 95	84.89	84.89	OK
175	5-9% of mass 174	7.41	8.73	OK
176	95-101% of mass 174	84.85	99.96	OK
177	5-9% of mass 176	5.73	6.74	OK

Injection Date: 09/04/86  
Injection Time: 05:16  
Run No: >C7617  
Spectrum No: 155

Analyst: *[Signature]*  
Processor: *[Signature]*  
GC Batch: QV5474  
Samples: N4742, N4744, N4746, N4745,  
N1590, N1591, N4343, N4344,  
N4102, N4777, N4778, N4775,  
N4779, N4780, N4776, N4132

*[Signature]*  
9/6/86

SEP 8, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Volatile Compounds - GC/MS Analysis Data (QR01)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4778 RESOURCE ENGINEERING

RES27514

WREI 3-4

860828 1910

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound <small>Acrolein and Acrylonitrile values are screen only.</small>	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
1V	Acrolein	ND	100	ND	ND	ND	800	113	ND	800	76
2V	Acrylonitrile	ND	100	ND	ND	ND	80.0	96	ND	80.0	77
3V	Benzene	ND	4.4	ND	ND	ND	18.0	98	ND	18.0	98
4V	bis(Chloromethyl)ether	ND	10	ND	ND	ND	0	-	ND	0	-
5V	Bromoform	ND	4.7	ND	ND	ND	18.0	99	ND	18.0	82
6V	Carbon tetrachloride	ND	2.8	ND	ND	ND	18.0	102	ND	18.0	105
7V	Chlorobenzene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	101
8V	Chlorodibromomethane	ND	3.1	ND	ND	ND	18.0	101	ND	18.0	90
9V	Chloroethane	ND	10	ND	ND	ND	18.0	104	ND	18.0	91
10V	2-Chloroethylvinyl ether	ND	10	ND	ND	ND	18.0	0 <sup>a</sup>	ND	18.0	0 <sup>a</sup>
11V	Chloroform	ND	1.6	ND	ND	ND	18.0	103	ND	18.0	102
12V	Dichlorobromomethane	ND	2.2	ND	ND	ND	18.0	103	ND	18.0	100
13V	Dichlorodifluoromethane	ND	10	ND	ND	ND	18.0	110	ND	18.0	91
14V	1,1-Dichloroethane	ND	4.7	ND	ND	ND	18.0	100	ND	18.0	104
15V	1,2-Dichloroethane	ND	2.8	ND	ND	ND	18.0	105	ND	18.0	93
16V	1,1-Dichloroethylene	ND	2.8	ND	ND	ND	18.0	100	ND	18.0	105
17V	1,2-Dichloropropane	ND	6.0	ND	ND	ND	18.0	100	ND	18.0	94
18V	cis-1,3-Dichloropropylene	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	95
19V	Ethylbenzene	ND	7.2	ND	ND	ND	18.0	101	ND	18.0	104
20V	Methyl bromide	ND	10	ND	ND	ND	18.0	109	ND	18.0	86
21V	Methyl chloride	ND	10	ND	ND	ND	18.0	106	ND	18.0	115
22V	Methylene chloride	ND	2.8	3.05	5.73	5.10	18.0	90	2.94	18.0	117
23V	1,1,2,2-Tetrachloroethane	ND	6.9	ND	ND	ND	18.0	103	ND	18.0	94
24V	Tetrachloroethylene	ND	4.1	ND	ND	ND	18.0	99	ND	18.0	101
25V	Toluene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	102
26V	1,2-Trans-dichloroethylene	ND	1.6	ND	ND	ND	18.0	100	ND	18.0	104
27V	1,1,1-Trichloroethane	ND	3.8	ND	ND	ND	18.0	104	ND	18.0	105
28V	1,1,2-Trichloroethane	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	88
29V	Trichloroethylene	ND	1.9	ND	ND	ND	18.0	98	ND	18.0	91
30V	Trichlorofluoromethane	ND	10	ND	ND	ND	18.0	103	ND	18.0	109
31V	Vinyl chloride	ND	10	ND	ND	ND	18.0	103	ND	18.0	94
18V	trans-1,3-Dichloropropylene	ND	10	ND	ND	ND	18.0	101	ND	18.0	95

<sup>a</sup> Recovery normally variable using established methodology.

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

SEP 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Acid Compounds - GC/MS Analysis Data (QR02)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4778 RESOURCE ENGINEERING

RES27514

WREI 3-4

860828 1910

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
1A	2-Chlorophenol	ND	3.9	ND	ND	ND	100	75	ND	104	75
2A	2,4-Dichlorophenol	ND	3.2	ND	ND	ND	100	67	ND	104	74
3A	2,4-Dimethylphenol	ND	3.2	ND	ND	ND	100	68	ND	104	70
4A	4,6-Dinitro-o-cresol	ND	29	ND	ND	ND	100	67	ND	104	53
5A	2,4-Dinitrophenol	ND	50	ND	ND	ND	100	74	ND	104	62
6A	2-Nitrophenol	ND	4.3	ND	ND	ND	100	71	ND	104	75
7A	4-Nitrophenol	ND	2.9	ND	ND	ND	100	39	ND	104	36
8A	p-Chloro-m-cresol	ND	3.6	ND	ND	ND	100	60	ND	104	62
9A	Pentachlorophenol	ND	4.3	ND	ND	ND	100	56	ND	104	46
10A	Phenol	ND	1.8	4.16	2.82	ND	100	38	ND	104	44
11A	2,4,6-Trichlorophenol	ND	3.2	ND	ND	ND	100	80	ND	104	85

SEP 16, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4778 RESOURCE ENGINEERING

RES27514

WREI 3-4

860828 1910

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
1B	Acenaphthene	ND	2.3	ND	ND	ND	100	77	ND	104	79
2B	Acenaphthylene	ND	4.2	ND	ND	ND	100	78	ND	104	81
3B	Anthracene	ND	2.3	ND	ND	ND	100	76	ND	104	77
4B	Benidine	ND	52	ND	ND	ND	100	53	ND	104	74
5B	Benzo(a)anthracene	ND	9.3	ND	ND	ND	100	75	ND	104	71
6B	Benzo(a)pyrene	ND	3.0	ND	ND	ND	100	67	ND	104	44
7B	Benzo(b)fluoranthene	ND	12	ND	ND	ND	100	73	ND	104	60
8B	Benzo(ghi)perylene	ND	4.9	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	4.2	ND	ND	ND	100	66	ND	104	66
10B	bis(2-Chloroethoxy)methane	ND	6.3	ND	ND	ND	100	74	ND	104	75
11B	bis(2-Chloroethyl) ether	ND	6.8	ND	ND	ND	100	81	ND	104	77
12B	bis(2-Chloroisopropyl) ether	ND	6.8	ND	ND	ND	100	99	ND	104	87
13B	bis(2-Ethylhexyl)phthalate	ND	12	ND	ND	ND	100	79	ND	104	74
14B	4-Bromophenyl phenyl ether	ND	2.3	ND	ND	ND	100	72	ND	104	71
15B	Butyl benzyl phthalate	ND	12	ND	ND	ND	100	66	ND	104	55
16B	2-Chloronaphthalene	ND	2.3	ND	ND	ND	100	74	ND	104	75
17B	4-Chlorophenyl phenyl ether	ND	5.0	ND	ND	ND	100	82	ND	104	83
18B	Chrysene	ND	3.0	ND	ND	ND	100	77	ND	104	74
19B	Dibenzo(a,h)anthracene	ND	12	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	2.3	ND	ND	ND	100	72	ND	104	80
21B	1,3-Dichlorobenzene	ND	2.3	ND	ND	ND	100	64	ND	104	79
22B	1,4-Dichlorobenzene	ND	5.2	ND	ND	ND	100	69	ND	104	79
23B	3,3'-Dichlorobenzidine	ND	20	ND	ND	ND	100	69	ND	104	63
24B	Diethyl phthalate	ND	12	ND	ND	ND	100	36	ND	104	33
25B	Dimethyl phthalate	ND	12	ND	ND	ND	100	15	ND	104	19
26B	Di-n-butyl phthalate	ND	12	ND	ND	BMDL	100	70	ND	104	66
27B	2,4-Dinitrotoluene	ND	6.8	ND	ND	ND	100	85	ND	104	79
28B	2,6-Dinitrotoluene	ND	2.3	ND	ND	ND	100	83	ND	104	78
29B	Di-n-octyl phthalate	ND	12	ND	ND	ND	100	76	ND	104	69
30B	1,2-Diphenylhydrazine	ND	12	ND	ND	ND	100	91	ND	104	90
31B	Fluoranthene	ND	2.6	ND	ND	ND	100	81	ND	104	87
32B	Fluorene	ND	2.3	ND	ND	ND	100	82	ND	104	82

SEP 16, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**  
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4778 RESOURCE ENGINEERING

RES27514

WREI 3-4

860828 1910

1

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
33B	Hexachlorobenzene	ND	2.3	ND	ND	ND	100	74	ND	104	72
34B	Hexachlorobutadiene	ND	1.1	ND	ND	ND	100	57	ND	104	73
35B	Hexachlorocyclopentadiene	ND	12	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	1.9	ND	ND	ND	100	52	ND	104	79
37B	Indeno(1,2,3-c,d)pyrene	ND	5.6	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	2.6	ND	ND	ND	100	77	ND	104	80
39B	Naphthalene	ND	1.9	ND	ND	ND	100	69	ND	104	66
40B	Nitrobenzene	ND	2.3	ND	ND	ND	100	75	ND	104	74
41B	N-Nitrosodimethylamine	ND	12	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	12	ND	ND	ND	100	76	ND	104	72
43B	N-Nitrosodiphenylamine	ND	2.3	ND	ND	ND	100	86	ND	104	86
44B	Phenanthrene	ND	6.4	ND	ND	ND	100	77	ND	104	75
45B	Pyrene	ND	2.3	ND	ND	ND	100	80	ND	104	85
46B	1,2,4-Trichlorobenzene	ND	2.3	ND	ND	ND	100	102	ND	104	109

A Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Aqueous Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4778	RESOURCE ENGINEERING	RES27514	WREI 3-4	86082	1910	1
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	.250	97	88	110
p-Bromofluorobenzene	.250	104	86	115
1,2-Dichloroethane-D4	.250	104	76	114
ACID FRACTION (GC/MS)				
Phenol-D5	100	41	10	94
2-Fluorophenol	100	58	21	100
2,4,6-Tribromophenol	100	57	10	123
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	88	35	114
2-Fluorobiphenyl	50	69	43	116
Terphenyl-D14	50	80	33	141
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	24..	154..
* IFB EPA Control Limits				
** Advisory Limits Only				

\* IFB EPA Control Limits

\*\* Advisory Limits Only

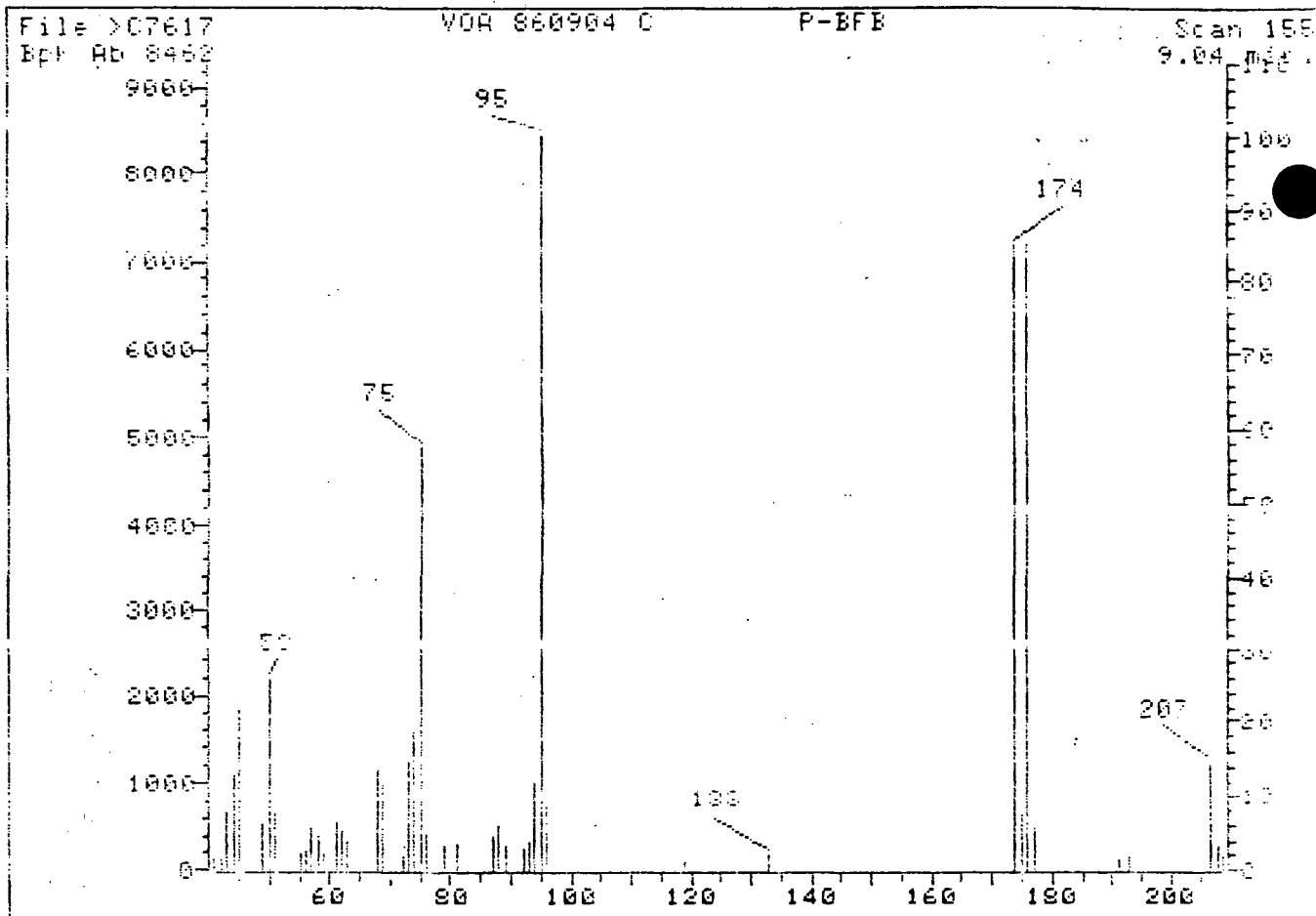


TABLE 2: METHOD PERFORMANCE DATA (QR21)

GC/MS Tuning Data - Bromofluorobenzene (BFB) for Volatiles Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
50	15-40% of mass 95	25.82	25.82	OK
75	30-60% of mass 95	57.54	57.54	OK
95	Base peak, 100% relative abundance	100.00	100.00	OK
96	5-9% of mass 95	8.32	8.32	OK
173	Less than 1% of mass 95	0.00	0.00	OK
174	Greater than 50% of mass 95	84.89	84.89	OK
175	5-9% of mass 174	7.41	8.73	OK
176	95-101% of mass 174	84.85	99.96	OK
177	5-9% of mass 176	5.72	6.74	OK

Injection Date: 09/04/86

Injection Time: 05:46

Run No: >C7617

Spectrum No: 155

Analyst: *[Signature]*

Processor: *[Signature]*

QC Batch: *[Signature]*

Samples:

*[Signature]*  
N4742, N4744, N4746, N4745,  
N1590, N1591, N4343, N4344,  
N4102, N4777, N4778, N4775,  
N4779, N4780, N4776, N4180

*[Signature]*  
9/6/86



SEP 8, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Volatile Compounds - GC/MS Analysis Data (QR01)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4779 RESOURCE ENGINEERING

RES27514

WREI 10-1

860828 1400

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound <small>Acrolein and Acrylonitrile values are screen only.</small>	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
1V	Acrolein	ND	100	ND	ND	ND	800	113	ND	800	76
2V	Acrylonitrile	ND	100	ND	ND	ND	80.0	96	ND	80.0	77
3V	Benzene	ND	4.4	ND	ND	ND	18.0	98	ND	18.0	98
4V	bis(Chloromethyl)ether	ND	10	ND	ND	ND	0	-	ND	0	-
5V	Bromoform	ND	4.7	ND	ND	ND	18.0	99	ND	18.0	82
6V	Carbon tetrachloride	ND	2.8	ND	ND	ND	18.0	102	ND	18.0	105
7V	Chlorobenzene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	101
8V	Chlorodibromomethane	ND	3.1	ND	ND	ND	18.0	101	ND	18.0	90
9V	Chloroethane	ND	10	ND	ND	ND	18.0	104	ND	18.0	91
10V	2-Chloroethylvinyl ether	ND	10	ND	ND	ND	18.0	0 <sub>a</sub>	ND	18.0	0 <sub>a</sub>
11V	Chloroform	ND	1.6	ND	ND	ND	18.0	103	ND	18.0	102
12V	Dichlorobromomethane	ND	2.2	ND	ND	ND	18.0	103	ND	18.0	100
13V	Dichlorodifluoromethane	ND	10	ND	ND	ND	18.0	110	ND	18.0	91
14V	1,1-Dichloroethane	ND	4.7	ND	ND	ND	18.0	100	ND	18.0	104
15V	1,2-Dichloroethane	ND	2.8	ND	ND	ND	18.0	105	ND	18.0	93
16V	1,1-Dichloroethylene	ND	2.8	ND	ND	ND	18.0	100	ND	18.0	105
17V	1,2-Dichloropropane	ND	6.0	ND	ND	ND	18.0	100	ND	18.0	94
18V	cis-1,3-Dichloropropylene	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	95
19V	Ethylbenzene	ND	7.2	ND	ND	ND	18.0	101	ND	18.0	104
20V	Methyl bromide	ND	10	ND	ND	ND	18.0	109	ND	18.0	86
21V	Methyl chloride	ND	10	ND	ND	ND	18.0	106	ND	18.0	115
22V	Methylene chloride	ND	2.8	3.05	5.73	5.10	18.0	90	2.94	18.0	117
23V	1,1,2,2-Tetrachloroethane	ND	6.9	ND	ND	ND	18.0	103	ND	18.0	94
24V	Tetrachloroethylene	ND	4.1	ND	ND	ND	18.0	99	ND	18.0	101
25V	Toluene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	102
26V	1,2-Trans-dichloroethylene	ND	1.6	ND	ND	ND	18.0	100	ND	18.0	104
27V	1,1,1-Trichloroethane	ND	3.8	ND	ND	ND	18.0	104	ND	18.0	105
28V	1,1,2-Trichloroethane	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	88
29V	Trichloroethylene	ND	1.9	ND	ND	ND	18.0	98	ND	18.0	91
30V	Trichlorofluoromethane	ND	10	ND	ND	ND	18.0	103	ND	18.0	109
31V	Vinyl chloride	ND	10	ND	ND	ND	18.0	103	ND	18.0	94
18V	trans-1,3-Dichloropropylene	ND	10	ND	ND	ND	18.0	101	ND	18.0	95

<sup>a</sup> Recovery normally variable using established methodology.

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Acid Compounds - GC/MS Analysis Data (QR02)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4779 RESOURCE ENGINEERING

RES27514

WREI 10-1

860828 1400

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
1A	2-Chlorophenol	ND	3.6	ND	ND	ND	100	75	ND	104	75
2A	2,4-Dichlorophenol	ND	2.9	ND	ND	ND	100	67	ND	104	74
3A	2,4-Dimethylphenol	ND	2.9	ND	ND	ND	100	68	ND	104	70
4A	4,6-Dinitro-o-cresol	ND	26	ND	ND	ND	100	67	ND	104	53
5A	2,4-Dinitrophenol	ND	46	ND	ND	ND	100	74	ND	104	62
6A	2-Nitrophenol	ND	3.9	ND	ND	ND	100	71	ND	104	75
7A	4-Nitrophenol	ND	2.6	ND	ND	ND	100	39	ND	104	36
8A	p-Chloro-m-cresol	ND	3.3	ND	ND	ND	100	60	ND	104	62
9A	Pentachlorophenol	ND	3.9	ND	ND	ND	100	56	ND	104	46
10A	Phenol	4.16	1.6	4.16	2.82	ND	100	38	ND	104	44
11A	2,4,6-Trichlorophenol	ND	2.9	ND	ND	ND	100	80	ND	104	85

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4779 RESOURCE ENGINEERING

RES27514

WREI 10-1

860828 1400

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen Added ug/l	% Recov	Unspiked Sample ug/l	Concen Added ug/l	% Recov
1B	Acenaphthene	ND	2.1	ND	ND	ND	100	77	ND	104	79
2B	Acenaphthylene	ND	3.8	ND	ND	ND	100	78	ND	104	81
3B	Anthracene	ND	2.1	ND	ND	ND	100	76	ND	104	77
4B	Benzidine	ND	48	ND	ND	ND	100	53	ND	104	74
5B	Benzo(a)anthracene	ND	8.5	ND	ND	ND	100	75	ND	104	71
6B	Benzo(a)pyrene	ND	2.7	ND	ND	ND	100	67	ND	104	44
7B	Benzo(b)fluoranthene	ND	11	ND	ND	ND	100	73	ND	104	60
8B	Benzo(ghi)perylene	ND	4.5	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	3.8	ND	ND	ND	100	66	ND	104	66
10B	bis(2-Chloroethoxy)methane	ND	5.8	ND	ND	ND	100	74	ND	104	75
11B	bis(2-Chloroethyl) ether	ND	6.2	ND	ND	ND	100	81	ND	104	77
12B	bis(2-Chloroisopropyl)ether	ND	6.2	ND	ND	ND	100	99	ND	104	87
13B	bis(2-Ethylhexyl)phthalate	ND	11	ND	ND	ND	100	79	ND	104	74
14B	4-Bromophenyl phenyl ether	ND	2.1	ND	ND	ND	100	72	ND	104	71
15B	Butyl benzyl phthalate	ND	11	ND	ND	ND	100	66	ND	104	55
16B	2-Chloronaphthalene	ND	2.1	ND	ND	ND	100	74	ND	104	75
17B	4-Chlorophenyl phenyl ether	ND	4.6	ND	ND	ND	100	82	ND	104	83
18B	Chrysene	ND	2.7	ND	ND	ND	100	77	ND	104	74
19B	Dibenzo(a,h)anthracene	ND	11	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	2.1	ND	ND	ND	100	72	ND	104	80
21B	1,3-Dichlorobenzene	ND	2.1	ND	ND	ND	100	64	ND	104	79
22B	1,4-Dichlorobenzene	ND	4.8	ND	ND	ND	100	69	ND	104	79
23B	3,3'-Dichlorobenzidine	ND	18	ND	ND	ND	100	69	ND	104	63
24B	Diethyl phthalate	ND	11	ND	ND	ND	100	36	ND	104	33
25B	Dimethyl phthalate	ND	11	ND	ND	ND	100	15	ND	104	19
26B	Di-n-butyl phthalate	ND	11	ND	ND	BMDL	100	70	ND	104	66
27B	2,4-Dinitrotoluene	ND	6.2	ND	ND	ND	100	85	ND	104	79
28B	2,6-Dinitrotoluene	ND	2.1	ND	ND	ND	100	83	ND	104	78
29B	Di-n-octyl phthalate	ND	11	ND	ND	ND	100	76	ND	104	69
30B	1,2-Diphenylhydrazine	ND	11	ND	ND	ND	100	91	ND	104	90
31B	Fluoranthene	ND	2.4	ND	ND	ND	100	81	ND	104	87
32B	Fluorene	ND	2.1	ND	ND	ND	100	82	ND	104	82

ETC

ENVIRONMENTAL  
TESTING and CERTIFICATION

SEP 16, 1986

## TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4779 RESOURCE ENGINEERING

RES27514 WREI 10-1 860828 1400

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

PDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen: ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
33B	Hexachlorobenzene	ND	2.1	ND	ND	ND	100	74	ND	104	72
34B	Hexachlorobutadiene	ND	.98	ND	ND	ND	100	57	ND	104	73
35B	Hexachlorocyclopentadiene	ND	11	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	1.7	ND	ND	ND	100	52	ND	104	79
37B	Indeno(1,2,3-c,d)pyrene	ND	5.1	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	2.4	ND	ND	ND	100	77	ND	104	80
39B	Naphthalene	ND	1.7	ND	ND	ND	100	69	ND	104	66
40B	Nitrobenzene	ND	2.1	ND	ND	ND	100	75	ND	104	74
41B	N-Nitrosodimethylamine	ND	11	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	11	ND	ND	ND	100	76	ND	104	72
43B	N-Nitrosodiphenylamine	ND	2.1	ND	ND	ND	100	86	ND	104	86
44B	Phenanthrene	ND	5.9	ND	ND	ND	100	77	ND	104	75
45B	Pyrene	ND	2.1	ND	ND	ND	100	80	ND	104	85
46B	1,2,4-Trichlorobenzene	ND	2.1	ND	ND	ND	100	102	ND	104	109

A Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Aqueous Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4779	RESOURCE ENGINEERING	RES27514	WRE1 10-1	86082	1400	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits.	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	.250	97	88	110
p-Bromofluorobenzene	.250	104	86	115
1,2-Dichloroethane-D4	.250	101	76	114
ACID FRACTION (GC/MS)				
Phenol-D5	100	43	10	94
2-Fluorophenol	100	54	21	100
2,4,6-Tribromophenol	100	59	10	123
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	86	35	114
2-Fluorobiphenyl	50	62	43	116
Terphenyl-D14	50	62	33	141
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloredate	-	-	24..	154..
* IFB EPA Control Limits ** Advisory Limits Only				

File >07617  
Bpk Ab 8462

V09 860904 C

P-BFB

Scan 155  
9.04 min

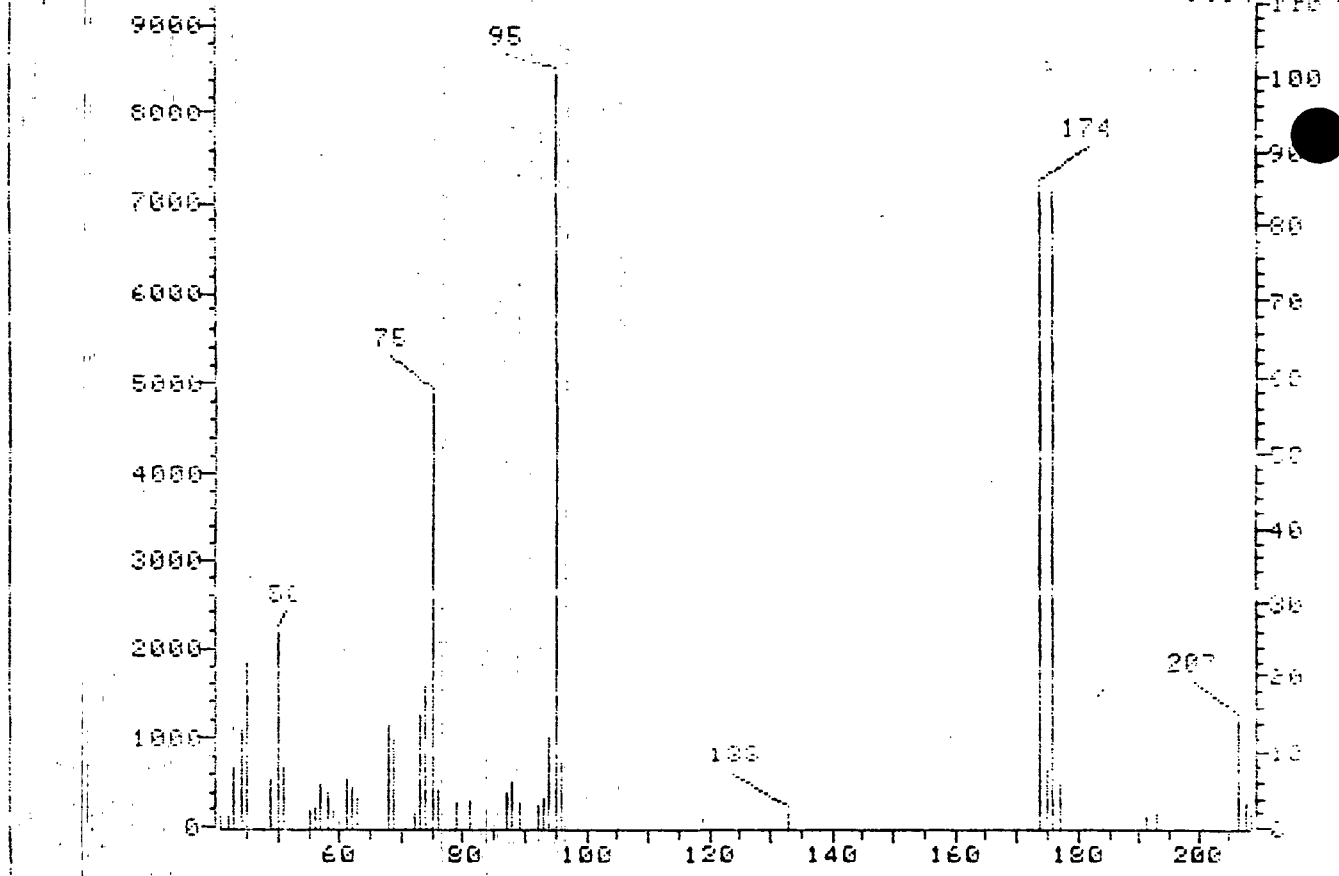


TABLE 2: METHOD PERFORMANCE DATA (QR21)

GC/MS Tuning Data - Bromofluorobenzene (BFB) for Volatiles Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		base Peak	Appropriate Peak	
50	15-40% of mass 95	25.82	25.82	OK
75	30-60% of mass 95	57.54	57.54	OK
95	Base peak, 100% relative abundance	100.00	100.00	OK
96	5-9% of mass 95	8.33	8.33	OK
173	Less than 1% of mass 95	0.00	0.00	OK
174	Greater than 50% of mass 95	84.89	84.89	OK
175	5-9% of mass 174	7.41	8.73	OK
176	95-101% of mass 174	84.85	99.96	OK
177	5-9% of mass 176	5.72	6.74	OK

Injection Date: 09/04/86  
Injection Time: 05:16  
Run No: >07617  
Spectrum No: 155

Analyst: *[Signature]*  
Processor: *[Signature]*  
QC Batch: *[Signature]*  
Samples: N4742, N4744, N4746, N4745,  
N1590, N1591, N4343, N4344,  
N4102, N4777, N4778, N4775,  
N4779, N4780, N4776, N4180

*u.f.*  
*9/6/86*

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## Volatile Compounds - GC/MS Analysis Data (QR01)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4780 RESOURCE ENGINEERING

RES27514

WGW-25

860828 1130

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound <small>Acrolein and Acrylonitrile values are screen only.</small>	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concn ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concn Added ug/l	% Recov	Unspiked Sample ug/l	Concn Added ug/l	% Recov
1V	Acrolein	ND	100	ND	ND	ND	800	113	ND	800	76
2V	Acrylonitrile	ND	100	ND	ND	ND	80.0	96	ND	80.0	77
3V	Benzene	101	4.4	ND	ND	ND	18.0	98	ND	18.0	98
4V	bis(Chloromethyl)ether	ND	10	ND	ND	ND	0	-	ND	0	-
5V	Bromoform	ND	4.7	ND	ND	ND	18.0	99	ND	18.0	82
6V	Carbon tetrachloride	ND	2.8	ND	ND	ND	18.0	102	ND	18.0	105
7V	Chlorobenzene	ND	6.0	ND	ND	ND	18.0	101	ND	18.0	101
8V	Chlorodibromomethane	ND	3.1	ND	ND	ND	18.0	101	ND	18.0	90
9V	Chloroethane	56.1	10	ND	ND	ND	18.0	104	ND	18.0	91
10V	2-Chloroethylvinyl ether	ND	10	ND	ND	ND	18.0	0 <sup>a</sup>	ND	18.0	0 <sup>a</sup>
11V	Chloroform	ND	1.6	ND	ND	ND	18.0	103	ND	18.0	102
12V	Dichlorobromomethane	ND	2.2	ND	ND	ND	18.0	103	ND	18.0	100
13V	Dichlorodifluoromethane	ND	10	ND	ND	ND	18.0	110	ND	18.0	91
14V	1,1-Dichloroethane	87.1	4.7	ND	ND	ND	18.0	100	ND	18.0	104
15V	1,2-Dichloroethane	ND	2.8	ND	ND	ND	18.0	105	ND	18.0	93
16V	1,1-Dichloroethylene	ND	2.8	ND	ND	ND	18.0	100	ND	18.0	105
17V	1,2-Dichloropropane	ND	6.0	ND	ND	ND	18.0	100	ND	18.0	94
18V	cis-1,3-Dichloropropylene	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	95
19V	Ethylbenzene	16.1	7.2	ND	ND	ND	18.0	101	ND	18.0	104
20V	Methyl bromide	ND	10	ND	ND	ND	18.0	109	ND	18.0	86
21V	Methyl chloride	ND	10	ND	ND	ND	18.0	106	ND	18.0	115
22V	Methylene chloride	5.33	2.8	3.05	5.73	5.10	18.0	90	2.94	18.0	117
23V	1,1,2,2-Tetrachloroethane	ND	6.9	ND	ND	ND	18.0	103	ND	18.0	94
24V	Tetrachloroethylene	ND	4.1	ND	ND	ND	18.0	99	ND	18.0	101
25V	Toluene	42.0	6.0	ND	ND	ND	18.0	101	ND	18.0	102
26V	1,2-Trans-dichloroethylene	17.8	1.6	ND	ND	ND	18.0	100	ND	18.0	104
27V	1,1,1-Trichloroethane	ND	3.8	ND	ND	ND	18.0	104	ND	18.0	105
28V	1,1,2-Trichloroethane	ND	5.0	ND	ND	ND	18.0	102	ND	18.0	88
29V	Trichloroethylene	ND	1.9	ND	ND	ND	18.0	98	ND	18.0	91
30V	Trichlorofluoromethane	ND	10	ND	ND	ND	18.0	103	ND	18.0	109
31V	Vinyl chloride	226	10	ND	ND	ND	18.0	103	ND	18.0	94
18V	trans-1,3-Dichloropropylene	ND	10	ND	ND	ND	18.0	101	ND	18.0	95

<sup>a</sup> Recovery normally variable using established methodology.

**ETC**ENVIRONMENTAL  
TESTING and CERTIFICATION

SEP 13, 1986

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA****Acid Compounds - GC/MS Analysis Data (QR02)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4780

RESOURCE ENGINEERING

RES27514

WGW-25

860828 1130

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen Added ug/l	% Recov	Unspiked Sample ug/l	Concen Added ug/l	% Recov
1A	2-Chlorophenol	ND	3.3	ND	ND	ND	100	75	ND	104	75
2A	2,4-Dichlorophenol	ND	2.7	ND	ND	ND	100	67	ND	104	74
3A	2,4-Dimethylphenol	3.15	2.7	ND	ND	ND	100	68	ND	104	70
4A	4,6-Dinitro-o-cresol	ND	24	ND	ND	ND	100	67	ND	104	53
5A	2,4-Dinitrophenol	ND	42	ND	ND	ND	100	74	ND	104	62
6A	2-Nitrophenol	ND	3.6	ND	ND	ND	100	71	ND	104	75
7A	4-Nitrophenol	ND	2.4	ND	ND	ND	100	39	ND	104	36
8A	p-Chloro-m-cresol	ND	3.0	ND	ND	ND	100	60	ND	104	62
9A	Pentachlorophenol	ND	3.6	ND	ND	ND	100	56	ND	104	46
10A	Phenol	89.2	1.5	4.16	2.82	ND	100	38	ND	104	44
11A	2,4,6-Trichlorophenol	ND	2.7	ND	ND	ND	100	80	ND	104	85



SEP 16, 1986

TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA

## BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)

Chain of Custody Data Required for ETC Data Management Summary Reports

N4780 RESOURCE ENGINEERING

RES27514

WGW-25

860828 1130

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
1B	Acenaphthene	ND	1.9	ND	ND	ND	100	77	ND	104	79
2B	Acenaphthylene	ND	3.5	ND	ND	ND	100	78	ND	104	81
3B	Anthracene	ND	1.9	ND	ND	ND	100	76	ND	104	77
4B	Benzidine	ND	44	ND	ND	ND	100	53	ND	104	74
5B	Benzo(a)anthracene	ND	7.8	ND	ND	ND	100	75	ND	104	71
6B	Benzo(a)pyrene	ND	2.5	ND	ND	ND	100	67	ND	104	44
7B	Benzo(b)fluoranthene	ND	10	ND	ND	ND	100	73	ND	104	60
8B	Benzo(ghi)perylene	ND	4.1	ND	ND	ND	0	-	ND	0	-
9B	Benzo(k)fluoranthene	ND	3.5	ND	ND	ND	100	66	ND	104	66
10B	bis(2-Chloroethoxy)methane	ND	5.3	ND	ND	ND	100	74	ND	104	75
11B	bis(2-Chloroethyl) ether	ND	5.7	ND	ND	ND	100	81	ND	104	77
12B	bis(2-Chloroisopropyl)ether	ND	5.7	ND	ND	ND	100	99	ND	104	87
13B	bis(2-Ethylhexyl)phthalate	11.7	10	ND	ND	ND	100	79	ND	104	74
14B	4-Bromophenyl phenyl ether	ND	1.9	ND	ND	ND	100	72	ND	104	71
15B	Butyl benzyl phthalate	ND	10	ND	ND	ND	100	66	ND	104	55
16B	2-Chloronaphthalene	ND	1.9	ND	ND	ND	100	74	ND	104	75
17B	4-Chlorophenyl phenyl ether	ND	4.2	ND	ND	ND	100	82	ND	104	83
18B	Chrysene	ND	2.5	ND	ND	ND	100	77	ND	104	74
19B	Dibenzo(a,h)anthracene	ND	10	ND	ND	ND	0	-	ND	0	-
20B	1,2-Dichlorobenzene	ND	1.9	ND	ND	ND	100	72	ND	104	80
21B	1,3-Dichlorobenzene	ND	1.9	ND	ND	ND	100	64	ND	104	79
22B	1,4-Dichlorobenzene	ND	4.4	ND	ND	ND	100	69	ND	104	79
23B	3,3'-Dichlorobenzidine	ND	17	ND	ND	ND	100	69	ND	104	63
24B	Diethyl phthalate	ND	10	ND	ND	ND	100	36	ND	104	33
25B	Dimethyl phthalate	ND	10	ND	ND	ND	100	15 <sup>a</sup>	ND	104	19 <sup>a</sup>
26B	Di-n-butyl phthalate	ND	10	ND	ND	BMDL	100	70	ND	104	66
27B	2,4-Dinitrotoluene	ND	5.7	ND	ND	ND	100	85	ND	104	79
28B	2,6-Dinitrotoluene	ND	1.9	ND	ND	ND	100	83	ND	104	78
29B	Di-n-octyl phthalate	ND	10	ND	ND	ND	100	76	ND	104	69
30B	1,2-Diphenylhydrazine	ND	10	ND	ND	ND	100	91	ND	104	90
31B	Fluoranthene	ND	2.2	ND	ND	ND	100	81	ND	104	87
32B	Fluorene	ND	1.9	ND	ND	ND	100	82	ND	104	82

**TABLE 1: QUANTITATIVE RESULTS and QUALITY ASSURANCE DATA**
**BASE/NEUTRAL COMPOUNDS - GC/MS ANALYSIS DATA (QR03)**

Chain of Custody Data Required for ETC Data Management Summary Reports

N4780 RESOURCE ENGINEERING

RES27514

WGW-25

860828 1130

ETC Sample No.

Company

Facility

Sample Point

Date

Time

Elapsed  
Hours

NPDES Number	Compound	Results		QC Replicate		QC Blank and Spiked Blank			QC Matrix Spike		
		Sample Concen. ug/l	MDL ug/l	First ug/l	Second ug/l	Blank Data ug/l	Concen. Added ug/l	% Recov	Unspiked Sample ug/l	Concen. Added ug/l	% Recov
33B	Hexachlorobenzene	ND	1.9	ND	ND	ND	100	74	ND	104	72
34B	Hexachlorobutadiene	ND	.90	ND	ND	ND	100	57	ND	104	73
35B	Hexachlorocyclopentadiene	ND	10	ND	ND	ND	0	-	ND	0	-
36B	Hexachloroethane	ND	1.6	ND	ND	ND	100	52	ND	104	79
37B	Indeno(1,2,3-c,d)pyrene	ND	4.7	ND	ND	ND	0	-	ND	0	-
38B	Isophorone	ND	2.2	ND	ND	ND	100	77	ND	104	80
39B	Naphthalene	7.83	1.6	ND	ND	ND	100	69	ND	104	66
40B	Nitrobenzene	ND	1.9	ND	ND	ND	100	75	ND	104	74
41B	N-Nitrosodimethylamine	ND	10	ND	ND	ND	0	-	ND	0	-
42B	N-Nitrosodi-n-propylamine	ND	10	ND	ND	ND	100	76	ND	104	72
43B	N-Nitrosodiphenylamine	ND	1.9	ND	ND	ND	100	86	ND	104	86
44B	Phenanthrene	ND	5.4	ND	ND	ND	100	77	ND	104	75
45B	Pyrene	ND	1.9	ND	ND	ND	100	80	ND	104	85
46B	1,2,4-Trichlorobenzene	ND	1.9	ND	ND	ND	100	102	ND	104	109

A Recovery normally variable using established methodology.

**TABLE 2: METHOD PERFORMANCE DATA**  
**Surrogate Recovery - Aqueous Matrices (QR20)**

Chain of Custody Data Required for ETC Data Management Summary Reports						
N4780	RESOURCE ENGINEERING	RES27514	WGW-25	86082	1130	0
ETC Sample No.	Company	Facility	Sample Point	Date	Time	Elapsed Hours

Compound	Amount added ug	% Recovery	Control Limits	
			Lower	Upper
VOLATILE FRACTION (GC/MS)				
Toluene-D8	.250	100	88	110
p-Bromofluorobenzene	.250	102	86	115
1,2-Dichloroethane-D4	.250	98	76	114
ACID FRACTION (GC/MS)				
Phenol-D5	100	85	10	94
2-Fluorophenol	100	56	21	100
2,4,6-Tribromophenol	100	63	10	123
BASE/NEUTRAL FRACTION (GC/MS)				
Nitrobenzene-D5	50	111	35	114
2-Fluorobiphenyl	50	83	43	116
Terphenyl-D14	50	85	33	141
PESTICIDE/PCB FRACTION (GC)				
Dibutylchloroendate	-	-	24..	154..
* IFB EPA Control Limits ** Advisory Limits Only				

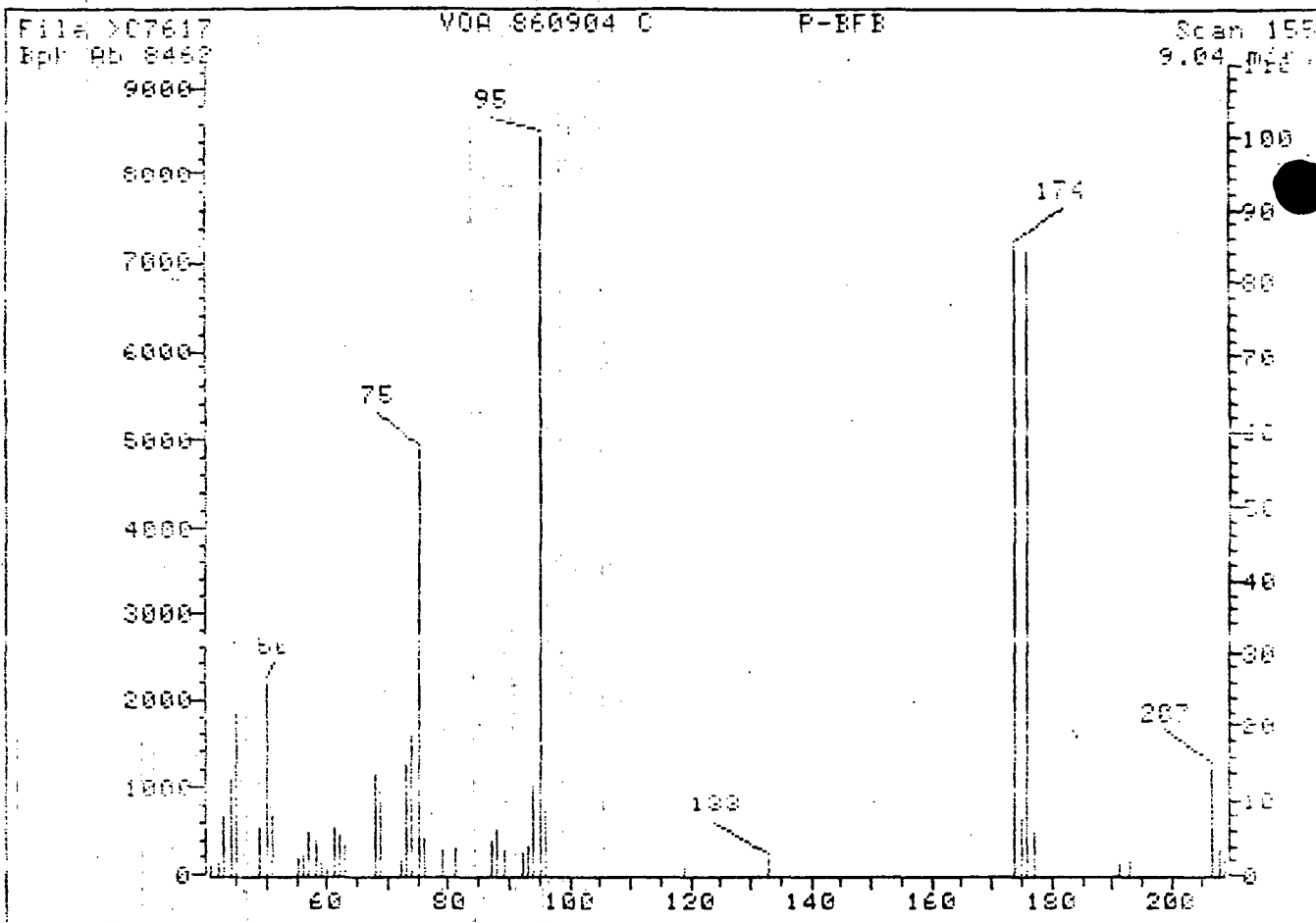


TABLE 2: METHOD PERFORMANCE DATA (QR21)

GC/MS Tuning Data - Bromofluorobenzene (BFB) for Volatiles Analysis

m/z	Ion Abundance Criteria	% Relative Abundance		Status
		Base Peak	Appropriate Peak	
56	15-60% of mass 95	25.02	25.02	OK
75	30-60% of mass 95	57.54	57.54	OK
95	Base peak, 100% relative abundance	100.00	100.00	OK
96	5-9% of mass 95	8.33	8.33	OK
173	Less than 1% of mass 95	0.00	0.00	OK
174	Greater than 50% of mass 95	84.89	84.89	OK
175	5-9% of mass 174	7.41	8.73	OK
176	95-101% of mass 174	84.85	99.96	OK
177	5-9% of mass 176	5.72	6.74	OK

Injection Date: 09/04/86

Injection Time: 05:16

Run No: >07617

Spectrum No: 155

Analyst: *[Signature]*

Processor: *[Signature]*

QC Batch: *[Signature]*

Samples:

*[Signature]*  
 N4742, N4744, N4746, N4745,  
 N1590, N1591, N4343, N4344,  
 N4702, N4777, N4778, N4775,  
 N4779, N4780, N4776, N4780

*E.R.*  
 9/6/86

Appendix 22

REI 3-3 Pumping Test Data Sheets

FRENCH LT2 REI 3-4  
Run 2  
08/21/87

SE2000 DATA  
constant rate test

TRANSDUCER TABLE

Input 1: REI 7-1	
Transducer s/n:	139
Scale factor:	49.59
Initial level:	81.69 feet
Input 2: REI 11	
Transducer s/n:	1857858
Scale factor:	50.4
Initial level:	79.28 feet
Input 3: REI 7	
Transducer s/n:	1994850
Scale factor:	10.08
Initial level:	81.17 feet
Input 4: REI 10-1	
Transducer s/n:	1937859
Scale factor:	10.09
Initial level:	81.18 feet
Input 5: REI 7-1	
Transducer s/n:	1362851
Scale factor:	10.03
Initial level:	6.29 feet
Input 6: REI 3-2	
Transducer s/n:	774844
Scale factor:	10.05
Initial level:	5.87 feet
Input 7: REI 3-3	
Transducer s/n:	1518854
Scale factor:	10.08
Initial level:	7.32 feet

# CALCULATIONS AND COMPUTATIONS

SHEET 1 OF 1

PROJECT: French Ltd.

JOB NO.: 225-19

SUBJECT: FLOW RATE MONITORING SHEET  
RET 3-3C pumping

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

FLOW RATE	TIME (2400)	MONITORS INITIALS		FLOW RATE	TIME (2400)	MONITORS INITIALS
Variable				3.0	00:27	DRG
3	18.31	RK		3.0	00:32	RK
2.9	18.35	RK		3.0	00:51	DRG
3	18.42	RK	D.D. now Av. Taylor take shift	3.0	01:11	D.D.
3	18.55	RK		3.0	02:04	D.D.
3	19.05	RK		3.0	03:10	A.T.
3	19.11	RK		3.0	03:50	A.T.
3.2	19.24	RK		3.0	04:00	D.D.
3.0	19.27	PCM		3.0	05:00	A.T.
3.0	19.30	RK		3.0	06:00	A.T.
3.0	19.42	DRG		3.0	06:51	A.T.
3.0	19.47	RK		3.0	07:00	D.D.
3.0	19.57	RK		3.0	08:15	A.T.
3.0	20.23	RK		3.0	09:01	PCM
3.0	20.29	RK				
3.0	20.41	RK				
3.0	20.51	RK				
3.0	20.59	RK				
3.0	21.11	DRG				
3.0	21.25	DRG				
3.0	21.32	RK				
3.0	21.54	DRG				
3.0	22:32	DRG				
3.0	23:02	RK				
3.0	23.15	RK				
3.0	23:36	DRG				
3.0	23:45	RK				
3.0	23:58	RK				

may be for  
much  
ca 3.4

**AFEN**

PUMP TEST DATA SHEET FOR REI 3-3 shallow SHEET 1 OF 4

PROJECT NAME: French Ltd  
PROJECT NUMBER: 275-14  
DATE: 8-11-86

WELL NUMBER: REI 3-3 (pumping)  
r IN FEET: 1.66  
STARTING WATER LEVEL: 2.22

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	Δ H	t/r <sup>2</sup>
18:30	0	7.22	PCM		
	.5	8.27	PCM ✓	1.05	$1.26 \times 10^{-2}$
18:31	1	9.15	PCM ✓	1.93	$2.52 \times 10^{-2}$
	1.5	9.19	PCM ✓	1.97	$3.77 \times 10^{-2}$
18:32:00	2	9.28	PCM ✓	2.06	$5.05 \times 10^{-2}$
	2.5	9.39	PCM ✓	2.17	$6.29 \times 10^{-2}$
18:33:00	3	9.48	PCM ✓	2.26	$7.58 \times 10^{-2}$
	3.5	9.58	PCM	2.36	$8.85 \times 10^{-2}$
18:34	4	9.68	PCM ✓	2.46	$1.01 \times 10^{-1}$
	4.5	9.72	PCM	2.50	$1.13 \times 10^{-1}$
18:35	5	9.77	PCM ✓	2.55	$1.26 \times 10^{-1}$
18:36	6	9.92	PCM	2.70	$1.51 \times 10^{-1}$
18:37	7	10.02	PCM ✓	2.80	$1.76 \times 10^{-1}$
18:38	8	10.13	PCM	2.91	$2.02 \times 10^{-1}$
18:39	9	10.21	PCM ✓	2.99	$2.27 \times 10^{-1}$
18:40	10	10.28	PCM	3.06	$2.52 \times 10^{-1}$
18:42	12	10.41	PCM	3.19	$3.02 \times 10^{-1}$
18:44	14	10.51	PCM ✓	3.29	$3.53 \times 10^{-1}$
18:46	16	10.60	PCM	3.38	$4.03 \times 10^{-1}$
18:48	18	10.68	PCM ✓	3.46	$4.55 \times 10^{-1}$
18:50	20	10.74	PCM	3.52	$5.05 \times 10^{-1}$
18:52	22	10.78	PCM	3.56	$5.56 \times 10^{-1}$

Calculated By R Krishna

Checked by D. Kumar





PUMP TEST DATA SHEET FOR REI 3-3 (shallow) SHEET 2 OF 4

PROJECT NAME: French Ltd.  
PROJECT NUMBER: 275-14  
DATE: 8-11-86

WELL NUMBER: REI-3-3 (pumping)  
r IN FEET: .166  
STARTING WATER LEVEL: 7.22

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	Δ H	t/r <sup>2</sup>
18:54	24	10.86	PCM ✓	3.64	$6.06 \times 10^{-1}$
18:56	26	10.91	PCM	3.69	$6.54 \times 10^{-1}$
18:58	28	10.98	PCM	3.76	$7.04 \times 10^{-1}$
19:00	30	11.02	PCM	3.80	$7.58 \times 10^{-1}$
19:02	32	11.06	PCM ✓	3.84	$8.06 \times 10^{-1}$
19:04	34	11.12	PCM	3.90	$8.55 \times 10^{-1}$
19:06	36	11.15	PCM	3.93	$9.09 \times 10^{-1}$
19:08	38	11.17	PCM	3.95	$9.62 \times 10^{-1}$
19:10	40	11.20	PCM ✓	3.98	$1.01 \times 10^0$
19:12	42	11.24	PCM	4.02	$1.06 \times 10^0$
19:14	44	11.26	PCM ✓	4.04	$1.11 \times 10^0$
19:16	46	11.29	PCM	4.07	$1.16 \times 10^0$
19:18	48	11.34	PCM	4.12	$1.21 \times 10^0$
19:20	50	11.35	DRG	4.13	$1.26 \times 10^0$
19:22	52	11.37	DRG	4.15	$1.31 \times 10^0$
19:24	54	11.39	PCM ✓	(4.17)	$1.36 \times 10^0$
19:26	56	10.87	PMC ✓	3.65	$1.41 \times 10^0$
19:28	58	10.72	PMC	3.50	$1.54 \times 10^0$
19:30	60	10.65	PCM	3.43	$1.51 \times 10^0$
19:35	65	10.50	LD ✓	3.28	$1.64 \times 10^0$
19:40	70	10.44	RR	3.22	$1.76 \times 10^0$
19:45	75	10.41	PR	3.19	$1.89 \times 10^0$
19:50	80	10.37	PR	3.17	$2.02 \times 10^0$
19:55	85	10.37	PR ✓	3.15	$2.14 \times 10^0$
20:00	90	10.37	PR	3.15	$2.27 \times 10^0$
20:05	95	PR			

Calculated by R Krosch Checked by D. Poma

**REI**

SHEET 3 OF 4

WELL NUMBER: REI 3-3 (pumpine)

**r IN FEET:**

STARTING WATER LEVEL: 7.22

Adjustment  
made to  
flow meter -

calculated by Ali Jaffer. checked by J. Duman



## PUMP TEST DATA SHEET FOR REI 3-3 SHALLOW

SHEET 4 OF 4

PROJECT NAME: FRENCH  
 PROJECT NUMBER: 275-14  
 DATE: 8/12/86

WELL NUMBER: REI 3-3 (PUMPING)  
 & IN FEET: 0.166  
 STARTING WATER LEVEL: 7.22  
 STOPPING WATER LEVEL: 10.54

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVER INITIALS	H RECOVERY	t/r <sup>2</sup>	ΔH (RESIDUAL DRAWDOWN)	t/t'
0915	885 (0)	10.54					
	0.5	10.015		0.52	1.26 E-2	-2.80	1.77 E+3
	1	9.79		0.75	2.52 E-2	2.57	8.86 E+2
	1.5	9.56		0.98	3.78 E-2	2.34	5.91 E+2
	2	9.45		1.09	5.04 E-2	2.23	4.44 E+2
	2.5	9.345		1.19	6.30 E-2	2.13	3.55 E+2
	3	9.24		1.30	7.56 E-2	2.02	2.96 E+2
	3.5	9.17		1.37	8.82 E-2	1.95	2.54 E+2
	4	9.10		1.44	1.01 E-1	1.88	2.22 E+2
	4.5	9.045		1.49	1.13 E-1	1.83	1.98 E+2
	5	8.995		1.54	1.26 E-1	1.78	1.78 E+2
	5.5	8.94		1.60	1.39 E-1	1.72	1.62 E+2
	6	8.885		1.65	1.51 E-1	1.67	1.49 E+2
	7	8.825		1.71	1.76 E-1	1.61	1.27 E+2
	8	8.74		1.80	2.02 E-1	1.52	1.12 E+2
	9	8.68		1.86	2.27 E-1	1.46	9.93 E+1
	10	8.625		1.91	2.52 E-1	1.41	8.95 E+1
	12	8.54		2.00	3.02 E-1	1.32	7.48 E+1
	14	8.46		2.08	3.53 E-1	1.24	6.42 E+1
0930	15	8.425		2.11	3.78 E-1	1.21	6.00 E+1
	17	8.38		2.16	4.28 E-1	1.16	5.31 E+1
	19	8.32		2.22	4.79 E-1	1.10	4.76 E+1
	20	8.305		2.23	5.04 E-1	1.09	4.53 E+1
	25	8.20		2.34	6.30 E-1	0.98	3.64 E+1
0945	30	8.14		2.40	7.56 E-1	0.92	3.05 E+1

REI

## PUMP TEST DATA SHEET FOR REI 3-3 SHALLOW

SHEET 1 OF 5

PROJECT NAME: French Ltd  
 PROJECT NUMBER: 275-19  
 DATE: 8-11-86

WELL NUMBER: REI-566s  
 r IN FEET: 39.33'  
 STARTING WATER LEVEL: 5.18'

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1740		5.17	BMB		
1830	0	5.18			
1831	1	5.18		0.00	<sup>4.48</sup> $4.48 \times 10^{-7}$
1832	2	5.18		0.00	<sup>9.98</sup> $9.01 \times 10^{-7}$
1833	3	5.18		0.00	$1.35 \times 10^{-6}$
1834	4	5.20		0.02	$1.80 \times 10^{-6}$
1835	5	5.22		0.04	$2.25 \times 10^{-6}$
1836	6	5.24		0.06	$2.70 \times 10^{-6}$
1837	7	5.26		0.08	$3.14 \times 10^{-6}$
1838	8	5.28		0.10	$3.60 \times 10^{-6}$
1839	9	5.31		0.13	$4.05 \times 10^{-6}$
1840	10	5.33		0.15	$4.48 \times 10^{-6}$
1841	11	5.36		0.18	$4.95 \times 10^{-6}$
1842	12	5.38		0.20	$5.38 \times 10^{-6}$
1843	13	5.40		0.22	$5.85 \times 10^{-6}$
1844	14	5.42		0.24	$6.29 \times 10^{-6}$
1845	15	5.44		0.26	$6.76 \times 10^{-6}$
1846	16	5.46		0.28	$7.19 \times 10^{-6}$
1848	18	5.50		0.32	$8.06 \times 10^{-6}$
1850	20	<sup>5.54</sup> <del>5.54</del>		0.36	<sup>8.98</sup> $9.01 \times 10^{-6}$
1852	22	5.58		0.40	$9.90 \times 10^{-6}$
1854	24	5.61		0.43	$1.08 \times 10^{-5}$
1856	26	5.65		0.47	$1.17 \times 10^{-5}$

Calculated by D. RomanChecked by R. Krasinski**REI**

PUMP TEST DATA SHEET FOR REI 3-2 SHALLOWSHEET 2 OF 5

PROJECT NAME: French  
 PROJECT NUMBER: 275-14  
 DATE: 8-11-86

WELL NUMBER: REI #3-5  
 r IN FEET: 39'.33  
 STARTING WATER LEVEL: 5.18'

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
1858	28	5.69	BMB	0.51	$1.26 \times 10^{-5}$
1900	30	5.71		0.53	$1.35 \times 10^{-5}$
1905	35	5.78		0.60	$1.57 \times 10^{-5}$
1910	40	5.85		0.67	$1.80 \times 10^{-5}$
1915	45	5.90		0.72	$2.02 \times 10^{-5}$
1920	50	5.95		0.77	$2.25 \times 10^{-5}$
1925	55	5.99		0.81	$2.47 \times 10^{-5}$
1930	60	6.02		0.84	$2.70 \times 10^{-5}$
1936	66	6.02	RL	0.84	$2.97 \times 10^{-5}$
1941	71	6.015	RL	0.84	$3.18 \times 10^{-5}$
1946	76	6.01	RL	0.83	$3.41 \times 10^{-5}$
1951	81	6.01	RL	0.83	$3.64 \times 10^{-5}$
1956	86	6.015	RL	0.84	$3.86 \times 10^{-5}$
2001	91	6.015	RL	0.84	$4.08 \times 10^{-5}$
<del>2006</del>	<del>96</del> R		<del>RL</del>		
2011	101	6.02	RL	0.84	$4.52 \times 10^{-5}$
<del>2016</del>	<del>106</del> R				
2021	111	6.03	RL	0.85	$4.98 \times 10^{-5}$
<del>2026</del>	<del>116</del> R				
2031	121	6.04	RL	0.86	$5.43 \times 10^{-5}$
2041	131	6.05	RL	0.87	$5.88 \times 10^{-5}$
2051	141	6.06	RL	0.88	$6.33 \times 10^{-5}$
2101	151	6.07	RL	0.89	$6.76 \times 10^{-5}$
2111	161	6.08	RL	0.90	$7.25 \times 10^{-5}$
2121	171	6.085	RL	0.91	$7.69 \times 10^{-5}$
2131	181	6.095	RL	0.92	$8.13 \times 10^{-5}$

Calculated by D. Benson Checked by R. French

**REI**

WELL NUMBER: REI 03-5  
r IN FEET: 39.33  
STARTING WATER LEVEL: 5.18

adjustment  $\Rightarrow$   
made to the  
meter.

calculated by Mr Taylor. checked by J. Darnum



PUMP TEST DATA SHEET FOR REI 3-3 SHALLOWSHEET 4 OF 5

PROJECT NAME: FRENCH  
 PROJECT NUMBER: 275-14  
 DATE: 8/12/86

WELL NUMBER: REI 3-5 OBSERV  
 & IN FEET: 39.33'  
 STARTING WATER LEVEL: 5.18'  
 STOPPING WATER LEVEL: 6.25'

\* RECOVERY BEGUN

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVER INITIALS	H RECOVERY	$t/t^2$	$\Delta H$ (RESIDUAL DRAWDOWN)	$t/t'$
9:14	884	6.25					
* 9:15	885 (0)	6.25					
9:16	1	6.25		0.00	4.49 E-7	-1.07	8.86 E+2
9:17	2	6.24		0.00	8.98 E-7	1.07	4.44 E+2
9:18	3	6.24		+ 0.01	1.35 E-6	1.06	2.96 E+2
9:19	4	6.24		0.01	1.80 E-6	1.06	2.22 E+2
9:20	5	6.23		0.02	2.24 E-6	1.05	1.78 E+2
9:21	6	6.22		0.03	2.70 E-6	1.04	1.49 E+2
9:22	7	6.21		0.04	3.14 E-6	1.03	1.27 E+2
9:23	8	6.20		0.05	3.59 E-6	1.02	1.12 E+2
9:24	9	6.19		0.06	4.04 E-6	1.01	9.93 E+1
9:25	10	6.18		0.07	4.49 E-6	1.00	8.95 E+1
9:26	11	6.17		0.08	4.94 E-6	0.99	8.15 E+1
9:27	12	6.16		0.09	5.39 E-6	0.98	7.48 E+1
9:28	13	6.14		0.11 <del>0.04</del>	5.84 E-6	0.96	6.91 E+1
9:29	14	6.13		0.12	6.29 E-6	0.95	6.42 E+1
9:30	15	6.12		0.13	6.73 E-6	0.94	6.00 E+1
9:31	16	6.11		0.14	7.18 E-6	0.93	5.63 E+1
9:32	17	6.09		0.16	7.63 E-6	0.91	5.31 E+1
9:33	18	6.08		0.17	8.08 E-6	0.90	5.02 E+1
9:34	19	6.07		0.18	8.53 E-6	0.89	4.76 E+1
9:35	20	6.06		0.19	8.98 E-6	0.88	4.53 E+1
9:36	21	6.05		0.20	9.43 E-6	0.87	4.31 E+1
9:37	22	6.04		0.21	9.88 E-6	0.86	4.12 E+1
9:38	23	6.03		0.22	1.03 E-5	0.85	3.95 E+1
9:39	24	6.02		0.23	1.08 E-5	0.84	3.79 E+1

**REI**

## PUMP TEST DATA SHEET FOR REI 3-3 SHALLOW

SHEET 5 OF 5

PROJECT NAME: FRENCH  
 PROJECT NUMBER: 275-14  
 DATE: 8/12/86

WELL NUMBER: REI 3-5  
 Z IN FEET: 39.33  
 STARTING WATER LEVEL: 5.18

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVER INITIALS	H RECOVERY	$t/t^2$	$\Delta H$ (RESIDUAL DRAWDOWN)	$t/t'$
9:41	26	6.00		0.25	1.17 E-5	-0.82	3.50 E+1
9:43	28	5.99		0.26	1.26 E-5	0.81	3.26 E+1
9:45	30	5.97		0.28	1.35 E-5	0.79	3.05 E+1
9:47	32	5.95		0.30	1.44 E-5	0.77	2.87 E+1
9:49	34	5.94		<del>0.31</del> 0.30	1.53 E-5	0.76	2.70 E+1
9:51	36	5.93		0.32	1.62 E-5	0.75	2.56 E+1
9:53	38	5.92		0.33	1.71 E-5	0.74	2.43 E+1
9:55	40	5.90		0.35	1.80 E-5	0.72	2.31 E+1
9:57	42	5.88		0.37	1.89 E-5	0.70	2.21 E+1
9:59	44	5.86		0.39	1.98 E-5	0.68	2.11 E+1
10:00	45	5.85		0.40	2.02 E-5	0.67	2.07 E+1
10:05	50	5.82		0.43	2.24 E-5	0.64	1.87 E+1
10:10	55	5.78		0.47	2.47 E-5	0.60	1.71 E+1
10:15	60	5.76		0.49	2.69 E-5	0.58	1.58 E+1
10:25	70	5.71		0.54	3.14 E-5	0.53	1.36 E+1
10:35	80	5.67		0.58	3.59 E-5	0.49	1.21 E+1
10:50	95	5.62		0.63	4.26 E-5	0.44	1.03 E+1
11:00	105	5.59		0.66	4.71 E-5	0.41	9.43 E+0
11:30	135	5.53		0.72	6.06 E-5	0.35	7.56 E+0

REI



PUMP TEST DATA SHEET FOR REI 3-3 SHALLOWSHEET 1 OF 5

PROJECT NAME: French  
 PROJECT NUMBER: 275-14  
 DATE: 8-11-86

WELL NUMBER: P3-3 shallow obs  
 r IN FEET: 12.5' 12.42' DES  
 STARTING WATER LEVEL: 5.27'

~~ELAPSED~~ CLOCK

<del>CLOCK</del> TIME (2400)	<del>ELAPSED</del> TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	Δ H	t/r <sup>2</sup>
1829					
18:30:00		5.27	RSA		
0.5		5.27	RSA	0.00	$2.25 \times 10^{-6}$
1.0		5.27	RSA	0.00	$4.50 \times 10^{-6}$
1.5		5.275	RSA ✓	0.01	$6.75 \times 10^{-6}$
2.0		5.28	RSA ✓	0.01	$9.00 \times 10^{-6}$
2.5		5.29	RSA ✓	0.02	$1.12 \times 10^{-5}$
3.0		5.30	RSA ✓	0.03	$1.35 \times 10^{-5}$
3.5		5.32	RSA ✓	0.05	$1.57 \times 10^{-5}$
4.0		5.335	RSA ✓	0.07	$1.80 \times 10^{-5}$
4.5		5.35	RSA ✓	0.08	$2.02 \times 10^{-5}$
5.0		5.37	RSA ✓	0.10	$2.25 \times 10^{-5}$
<del>5.5</del>		<del>5.37</del>	RSA		
6.0		5.42	RSA ✓	0.15	$2.70 \times 10^{-5}$
7.0		5.46	RSA ✓	0.19	$3.15 \times 10^{-5}$
8.0		5.505	RSA ✓	0.24	$3.60 \times 10^{-5}$
9.0		5.56	RSA ✓	0.29	$4.05 \times 10^{-5}$
10.0		5.605	RSA ✓	0.34	$4.50 \times 10^{-5}$
12.0		5.71	RSA ✓	0.44	$5.40 \times 10^{-5}$
14.0		5.815	RSA ✓	0.55	$6.29 \times 10^{-5}$
16.0		5.92	RSA ✓	0.65	$7.19 \times 10^{-5}$
18.0		6.025	RSA ✓	0.76	$8.13 \times 10^{-5}$
20.0		6.12	RSA ✓	0.85	$9.00 \times 10^{-5}$
22.0		6.215	RSA	0.95	$9.90 \times 10^{-5}$
24.0		6.305	RSA ✓	1.04	$1.08 \times 10^{-4}$

Calculated by D. Roman Checked by R. Kersh



PUMP TEST DATA SHEET FOR REI 3-3 SHALLOWSHEET 2 OF 5

PROJECT NAME: French Ltd  
 PROJECT NUMBER: 275-14  
 DATE: 8-11-86

WELL NUMBER: P3-3 shallow observ.  
 r IN FEET: 12.5  
 STARTING WATER LEVEL: 5.27'

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$t/r^2$
18:56	26.0	6.395	RSA ✓	1.73	$1.17 \times 10^{-4}$
18:58	28.0	6.47	RSA ✓	1.20	$1.26 \times 10^{-4}$
19:00	30.0	6.55	RSA	1.28	$1.35 \times 10^{-4}$
19:02	32.0	6.62	RSA ✓	1.35	$1.44 \times 10^{-4}$
19:04	34.0	6.69	RSA	1.42	$1.53 \times 10^{-4}$
19:06	36.0	6.75	RSA ✓	1.48	$1.62 \times 10^{-4}$
19:08	38.0	6.805	RSA	1.54	$1.71 \times 10^{-4}$
19:10	40.0	6.86	RSA ✓	1.59	$1.80 \times 10^{-4}$
19:12	42.0	6.91	RSA	1.64	$1.89 \times 10^{-4}$
19:14	44.0	6.95	RSA ✓	1.68	$1.98 \times 10^{-4}$
19:16	46.0	7.00	RSA	1.73	$2.07 \times 10^{-4}$
19:18	48.0	7.03	RSA ✓	1.76	$2.16 \times 10^{-4}$
19:20	50.0	7.07	RSA	1.80	$2.25 \times 10^{-4}$
19:22	52.0	7.10	RSA ✓	1.83	$2.34 \times 10^{-4}$
19:24	54.0	7.13	RSA	1.86	$2.43 \times 10^{-4}$
19:26	56.0	7.16	RSA	1.89	$2.52 \times 10^{-4}$
19:28	58.0	7.17	RSA	1.90	$2.61 \times 10^{-4}$
19:30	60.0	7.17	RK ✓	1.90	$2.70 \times 10^{-4}$
19:35	65.0	7.16	DRG	1.89	$2.92 \times 10^{-4}$
19:40	70.0	7.135	DRG	1.87	$3.15 \times 10^{-4}$
19:45	75.0	7.10	DRG	1.83	$3.38 \times 10^{-4}$
19:50	80.0	7.08	DRG ✓	1.81	$3.60 \times 10^{-4}$
19:55	85.0	7.055	DRG	1.79	$3.83 \times 10^{-4}$
20:00	90.0	7.045	DRG	1.78	$4.05 \times 10^{-4}$
20:10	100.0	7.025	DRG	1.76	$4.50 \times 10^{-4}$
20:20	110.0	7.02	DRG ✓	1.75	$4.95 \times 10^{-4}$

Calculated by D. Roman checked by R. Knecht



## PUMP TEST DATA SHEET FOR REI 3-3 SHALLOW

SHEET 3 OF 5

PROJECT NAME: French Ltd  
 PROJECT NUMBER: 275-14  
 DATE: 8-11-86/8-12-86

WELL NUMBER: P3-3 shallow ds.  
 r IN FEET: 12' 5" 12.42 dec  
 STARTING WATER LEVEL: 5.27

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	Δ H	t/r <sup>2</sup>
20:30	120.0	7.015	DRG	1.75	5.41x10 <sup>-4</sup>
20:40	130.0	7.035	DRG ✓	1.77	5.85x10 <sup>-4</sup>
20:50	140.0	7.05	DRG	1.78	6.29x10 <sup>-4</sup>
21:00	150.0	7.07	DRG ✓	1.80	6.76x10 <sup>-4</sup>
21:10	160.0	7.08	DRG	1.81	7.19x10 <sup>-4</sup>
21:20	170.0	7.09	DRG	1.82	7.63x10 <sup>-4</sup>
21:30	180.0	7.105	DRG	1.84	8.13x10 <sup>-4</sup>
21:50	200.0	7.11	DRG ✓	1.84	9.01x10 <sup>-4</sup>
22:10	220.0	7.09	DRG	1.82	9.90x10 <sup>-4</sup>
22:30	240.0	7.08	DRG ✓	1.81	1.08x10 <sup>-3</sup>
23:00	270.0	7.07	DRG ✓	1.80	1.22x10 <sup>-3</sup>
23:30	300.0	7.085	DRG	1.82	1.35x10 <sup>-3</sup>
24:00	330.0	7.11	DRG ✓	1.84	1.49x10 <sup>-3</sup>
01:00	390.0	7.19	DRG ✓	1.92	1.75x10 <sup>-3</sup>
02:00	450.0	7.215	A.T. ✓	1.95	2.02x10 <sup>-3</sup>
03:00	510.0	7.210	A.T.	1.94	2.29x10 <sup>-3</sup>
04:00	570.0	7.235	A.T. ✓	1.97	2.56x10 <sup>-3</sup>
05:00	630	7.230	A.T.	1.96	2.83x10 <sup>-3</sup>
06:00	690	7.230	A.T.	1.96	3.11x10 <sup>-3</sup>
07:00	<sup>DD 11-24-86</sup> <del>760</del> 750	7.150	A.T. ✓	1.88	3.37x10 <sup>-3</sup> <sup>DD 11-24-86</sup> <del>3.42x10<sup>-3</sup></del>
08:00	<sup>DD 11-24-86</sup> <del>820</del> 810	7.25	A.T.	1.98	3.65x10 <sup>-3</sup> <sup>DD 11-24-86</sup> <del>3.69x10<sup>-3</sup></del>
09:00	<sup>DD 11-24-86</sup> <del>880</del> 870	7.25	A.T. ✓	1.98	3.92x10 <sup>-3</sup> <sup>DD 11-24-86</sup> <del>3.97x10<sup>-3</sup></del>

D. Dorman +  
A. Tayer take  
shift.

Adjustment →  
made to  
flow meter

calculated by Pris Taylor checked by D. Dorman



## PUMP TEST DATA SHEET FOR REI 3-3 SHALLOW

SHEET 4 OF 5

PROJECT NAME: FRENCH  
 PROJECT NUMBER: 275-14  
 DATE: 8/12/86

WELL NUMBER: 03-3  
 SHALLOW OBSERV  
 IN FEET: 12.42  
 STARTING WATER LEVEL: 5.27  
 STOPPING WATER LEVEL: 7.25

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVER INITIALS	H RECOVERY	$t/t^2$	$\Delta H$ (RESIDUAL DRAWDOWN)	$t/t'$
0914	894	7.25					
0915	895 0	7.25					
	3.5	7.25	0.	0.00	1.58 E-5	-1.98	$2.54 \times 10^2$
	4.5	7.235		0.02	2.03 E-5	1.97	$1.98 \times 10^2$
	5.5	7.21		0.04	2.48 E-5	1.94	$1.62 \times 10^2$
	6	7.20		0.05	2.70 E-5	1.93	$1.48 \times 10^2$
	7	7.17		0.08	3.15 E-5	1.90	$1.27 \times 10^2$
	8	7.14		0.11	3.60 E-5	1.87	$1.12 \times 10^2$
	10	7.075		0.17	4.50 E-5	1.81	$8.95 \times 10^1$
	12	7.025		0.22	5.40 E-5	1.76	$7.48 \times 10^1$
	14	6.95		0.30	6.30 E-5	1.68	$6.42 \times 10^1$
	15	6.92		0.33	6.75 E-5	1.65	$6.00 \times 10^1$
	17	6.865		0.38	7.65 E-5	1.60	$5.31 \times 10^1$
	19	6.81		0.44	8.55 E-5	1.54	$4.76 \times 10^1$
	20	6.775		0.47	9.00 E-5	1.51	$4.53 \times 10^1$
	25	6.64		0.61	1.13 E-4	1.37	$3.64 \times 10^1$
	30	6.525		0.72	1.35 E-4	1.26	$3.05 \times 10^1$
	35	6.415		0.83	1.58 E-4	1.15	$2.63 \times 10^1$
	40	6.33		0.92	1.80 E-4	1.06	$2.31 \times 10^1$
	45	6.25		1.00	2.03 E-4	0.98	$2.07 \times 10^1$
	50	6.185		1.06	2.25 E-4	0.92	$1.87 \times 10^1$
	55	6.125		1.12	2.48 E-4	0.86	$1.71 \times 10^1$
	60	6.070		1.18	2.70 E-4	0.80	$1.58 \times 10^1$
	65	6.020		1.23	2.93 E-4	0.75	$1.46 \times 10^1$
	71	5.97		1.28	3.20 E-4	0.70	$1.35 \times 10^1$

AER

REI 3-3 SHALLOW

**PHIL S O S**

**PROJECT NAME:** FRENCH

**PROJECT NUMBER:** 275-14

**DATE:** 8/12/86

WELL NUMBER: SHALLOW OBSERV

**IN FEET:** 12.42

**STARTING WATER LEVEL:** 5.27

# REN

Appendix 23

REI 10-1 and REI 12-1 Well  
Drawdown Test Data

## PUMP TEST DATA SHEET FOR

RecoverySHEET 1 OF     PROJECT NAME: FRENCH LIMITEDWELL NUMBER: GW-25PROJECT NUMBER:     r IN FEET: 67.7'DATE: 8-16-86STARTING WATER LEVEL: 82.52

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$r^2/T$
0920	—	82.52	MD	0	
1030	Pump On				
1054	24	83.71	"	1.19	
1055	25	83.73		1.21	
1101	31	83.83		1.31	
1107	37	83.91		1.39	
1110	40	83.94		1.42	
1120	50	84.04		1.52	
1126	56	84.10		1.58	
1137	67	84.16		1.64	
1140	70	84.21		1.69	
12:00					
12:01		84.31			
12:02		84.27			
12:02:30		84.22			
12:03		84.15			
12:03:30		84.09			
12:04:00		84.04			
12:04:30		83.98			
12:05:04		83.95			
12:06		83.85			
12:07		83.79			
12:08		83.72			
12:09		83.68			
12:10 <i>pc</i>					

**SHEET\_\_\_ OF\_\_**

WELL NUMBER: \_\_\_\_\_  
r IN FEET: \_\_\_\_\_  
STARTING WATER LEVEL: \_\_\_\_\_

# NEW



Preliminary PUMP TEST DATA SHEET FOR REI 10-1

SHEET      OF     

PROJECT NAME: French  
PROJECT NUMBER: 275-14  
DATE: 8-16-86

WELL NUMBER: REI-10-1  
IN FEET: 166  
STARTING WATER LEVEL:     

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVERS INITIALS	$\Delta H$	$r^2/T$
8:40	—	81.03	RK		
9:59	—	81.05	A.B.		
10:28		81.03	P.M.		
10:30	0.	81.03			
	0:45	88.50		7.47	$5.29 \times 10^1$
	1:30	89.70		8.67	$2.65 \times 10^1$
	2:00	90.44		9.41	$1.98 \times 10^1$
	2:30	91.02		9.99	$1.59 \times 10^1$
	3:00	missed			
	3:30	91.67		10.64	$1.13 \times 10^1$
	4:00	91.89		10.86	$9.92 \times 10^0$
	4:30	92.55		11.02	$8.82 \times 10^0$
	5:00	92.20		11.17	$7.94 \times 10^0$
	5:30	92.33		11.30	$7.21 \times 10^0$
1 min. interval	6:00	92.51		11.48	$6.61 \times 10^0$
	7:00	92.83		11.80	$5.67 \times 10^0$
	8:00	92.98		11.95	$4.96 \times 10^0$
	9:00	93.11		12.08	$4.41 \times 10^0$
	10:00	93.20		12.17	$3.97 \times 10^0$
	11:00	93.27		12.24	$3.61 \times 10^0$
	12:00	93.35		12.32	$3.31 \times 10^0$
	13:00	93.41		12.38	$3.05 \times 10^0$
	14:00	93.45		12.42	$2.83 \times 10^0$
2 min. interval	16:00	93.53		12.50	$2.48 \times 10^0$
	18:00	93.61		12.58	$2.20 \times 10^0$
	20:00	93.69		12.66	$1.98 \times 10^0$

8 gpm

**SHEET**      **OF**     

WELL NUMBER: \_\_\_\_\_  
r IN FEET: \_\_\_\_\_  
STARTING WATER LEVEL: \_\_\_\_\_

# REI

*preliminary* PUMP TEST DATA SHEET FOR RE-10-1 recovery SHEET OF

PROJECT NAME: \_\_\_\_\_  
PROJECT NUMBER: \_\_\_\_\_  
DATE: \_\_\_\_\_

WELL NUMBER: RE-10-1  
P IN FEET: \_\_\_\_\_  
STARTING WATER LEVEL: \_\_\_\_\_

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVER INITIALS	H RECOVERY	R <sup>2</sup> /T	ΔH (RESIDUAL DRAWDOWN)	T/T'
	.36	89.71		4.87	7.94X10 <sup>1</sup>	8.68	1.81X10 <sup>2</sup>
	1.00	86.95		7.63	3.97X10 <sup>1</sup>	5.92	9.10X10 <sup>1</sup>
	1.30	85.10		9.48	2.65X10 <sup>1</sup>	4.07	6.10X10 <sup>1</sup>
	2.00	84.16		10.42	1.98X10 <sup>1</sup>	3.13	4.60X10 <sup>1</sup>
	2.30	83.50		11.08	1.59X10 <sup>1</sup>	2.47	3.70X10 <sup>1</sup>
	3.00	83.15		11.43	1.32X10 <sup>1</sup>	2.12	3.10X10 <sup>1</sup>
	3.30	82.89		11.69	1.13X10 <sup>1</sup>	1.86	2.67X10 <sup>1</sup>
	4.00	82.72		11.86	9.92X10 <sup>0</sup>	1.69	2.35X10 <sup>1</sup>
	4.30	82.53		12.05	8.82X10 <sup>0</sup>	1.50	2.10X10 <sup>1</sup>
	5.00	82.44		12.14	7.94X10 <sup>0</sup>	1.41	1.90X10 <sup>1</sup>
	6.00	82.39		12.19	6.61X10 <sup>0</sup>	1.36	1.60X10 <sup>1</sup>
	7.00	82.32		12.26	5.67X10 <sup>0</sup>	1.29	1.39X10 <sup>1</sup>
	8.00	82.25		12.33	4.96X10 <sup>0</sup>	1.22	1.23X10 <sup>1</sup>
	9.00	82.19		12.39	4.41X10 <sup>0</sup>	1.16	1.10X10 <sup>1</sup>
	10.00	82.14		12.44	3.97X10 <sup>0</sup>	1.11	1.00X10 <sup>1</sup>
	12.00	82.07		12.51	3.31X10 <sup>0</sup>	1.04	8.50X10 <sup>0</sup>
	15	81.98		12.60	2.65X10 <sup>0</sup>	.95	7.60X10 <sup>0</sup>
	20	81.89		12.69	1.98X10 <sup>0</sup>	.86	5.50X10 <sup>0</sup>
	25	81.82		12.76	1.59X10 <sup>0</sup>	.79	4.60X10 <sup>0</sup>
	30	81.77		12.81	1.32X10 <sup>0</sup>	.74	4.00X10 <sup>0</sup>
	35	81.73		12.85	1.13X10 <sup>0</sup>	.70	3.57X10 <sup>0</sup>
	45	81.67		12.91	8.82X10 <sup>-1</sup>	.64	3.60X10 <sup>0</sup>

Drawdown Test @ BET 10-1

START 6:19:00

C. Itin  
T. Beck

81.57'

102.8      6:22:40      Flow RATE  $\approx$  14-15 gpm  
(fluctuating)

103.55      6:24:00

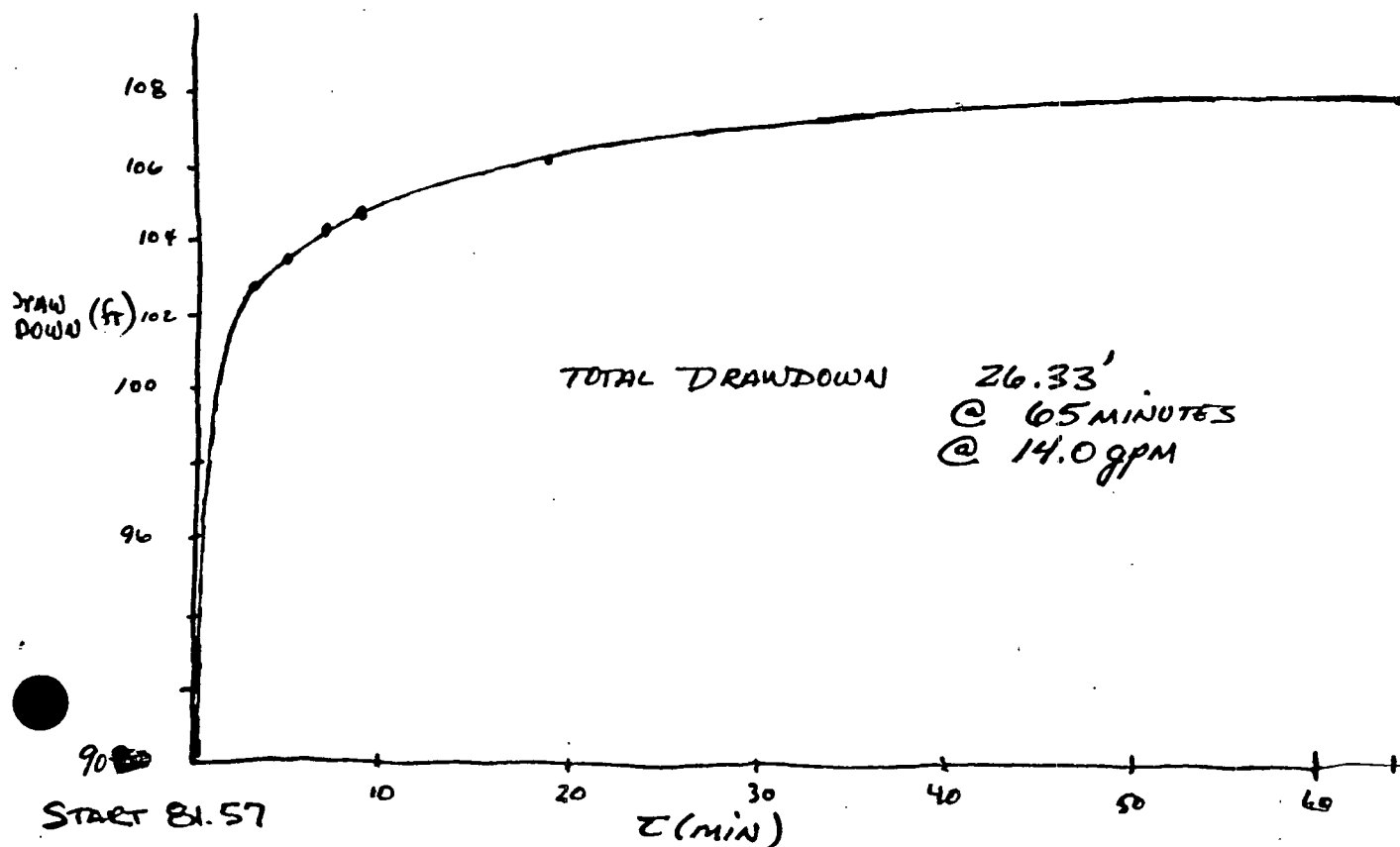
104.2      6:26:05

104.6      6:28:09      Flow RATE = 14.0 gpm

106.1      6:38:20

107.9      7:24:00      Flowrate 14.0 gpm  
 $\pm$ 

Pump Set @ 139' from Gr Surface



PUMP TEST DATA SHEET FOR REI-11SHEET      OF     

PROJECT NAME:                       
 PROJECT NUMBER:                       
 DATE:                     

WELL NUMBER: REI-11  
 r IN FEET: 1.66  
 STARTING WATER LEVEL: 64.55

pumping rate 55 gpm

92.16

CLOCK TIME (2400)	ELAPSED TIME (Min)	DEPTH TO WATER (Feet)	OBSERVER INITIALS	$\Delta H$ (RESIDUAL DRAWDOWN)	H RECOVERY	$R^2/T$	T/T'
	0						
	1	86.19		21.64		3.97x10 <sup>6</sup>	
	1.5	84.57		20.02		2.65x10 <sup>6</sup>	
	2	83.55		19.00		1.98x10 <sup>6</sup>	
	2.5	82.89		18.34		1.59x10 <sup>6</sup>	
	3	82.29		17.74		1.32x10 <sup>6</sup>	
	3.5	81.95		17.40		1.13x10 <sup>6</sup>	
	4	81.66		17.11		9.92x10 <sup>5</sup>	
	4.5	81.42		16.87		8.82x10 <sup>5</sup>	
	5	81.28		16.73		7.94x10 <sup>5</sup>	
	6	81.05		16.50		6.61x10 <sup>5</sup>	
	7	80.90		16.35		5.67x10 <sup>5</sup>	
	8	80.78		16.23		4.96x10 <sup>5</sup>	
	9	80.68		16.13		4.41x10 <sup>5</sup>	
	10	80.61		16.06		3.97x10 <sup>5</sup>	
	12	80.52		15.97		3.31x10 <sup>5</sup>	
	14	80.46		15.91		2.83x10 <sup>5</sup>	
	16	80.40		15.85		2.48x10 <sup>5</sup>	
	20	80.23		15.68		1.98x10 <sup>5</sup>	
	25	80.18		15.63		1.59x10 <sup>5</sup>	
	30	80.11		15.56		1.32x10 <sup>5</sup>	
	40	79.98		15.43		9.92x10 <sup>4</sup>	
	57.5	78.80		14.25		6.9x10 <sup>4</sup>	

**REI**

French LTD

11-1-85

REI. T. Beck, M. Beck, J. Brothers, D. Siegle (ERT)

Purpose: To sample GW-12, GW-25,  
REI-7, REI 3-4GW-12

Depth to Water 82.17'

START pumping @ 10:55 AM FlowRate  $\approx$  5gpm

Water Clear then dirty / to Clear at end of test

<u>Time</u>	<u>pH</u>	<u>Conductivity</u>
11:00	10.2	800
11:05	9.55	475
11:08	9.22	420
11:12	8.42	420
11:16	8.65	410
11:20	8.84	410
11:22	8.84	410
11:23	8.84	410

Pumping STOPPED

ETC Shuttle K4142 USED

Time

12:55

12:5

12:5

13:0

13:0

13:0

13:0

13:0

13:1

13:1

13:1

13:1

13:1

13:2

13:2

13:2

13:2

13:2

GW-2

Depth to Water — 83.77'

ETC# K4140

PRIORITY  
POLLUTANTS

START - 12:52

Flow Rate  $\approx$  4.5 gpm  
YSI  $\rightarrow$  Conductivity

ORION Research 210 pH,

Time	pH	Conduct $\mu\text{mho}$	TOC #1	TEMP	Vol
12:55	8.55	200			
12:56	8.51	190			
			#2		
12:58	8.44	400		72°F	
13:00	8.43	400			
13:02	8.43	400		72°F	
13:04	8.32	400		73°F	
13:05	8.37	350		72°F	
13:08	8.40	350			
			#3		
13:11	8.40	375		73°F	
13:13	8.40	390			
13:16	8.39	390		72°F	
13:19	8.41	375		72°F	
13:21	8.41	380		72°F	
13:26	8.39	390		71°F	
			#4		
13:29	8.38	390		71	150 gal
13:30	8.40	390		72	
			#5		
13:42	8.41	390		72	200 gal
13:46	8.41	395			

REI 3-4

Depth to Water 85.06'

Flow Rate 5-6 gpm

ETC Shuttle # K4143

3-3

3-2

3-1

<u>Time</u>	<u>pH</u>	<u>Conductivity</u>	<u>Temp</u>
17:48	11.72	2180	21°C
17:52	11.75	2000	21°C
17:57	11:36	800	21°C
18:04	10:87	500	21°C
18:11	10.42	490	21°C
18:22	9.91	417	

MW-07

Depth to Water 83.55'

ETC Shuttle K4144

Pumping @ 16:12

<u>Time</u>	<u>pH</u>	<u>Cond</u>	<u>Temp</u>
	11.25	810	
16:24	11.26	900	22°C
16:28	11.21	900	22°C
16:33	11.15	800	22°C
16:38	11.19	800	22°C
16:45	11.11	750	21°C
16:52	10.91	600	21°C
16:56	11.02	650	21°C
16:60	10:10	450	21°C
17:07	9.47	400	21°C
17:10	9.82	400	21°C
17:13	9.58	380	21°C



Barta Electric (Sunny Barta)  
Century RENTAL (Dennis Wagner)

424-7435  
449-0575

4.30  
76.81

FRENCH LTD 10-2-86

A. TAYAR, T. Beck

CONDUCT "MINI" PUMPTEST AT 12-1 CLUSTER  
PUMP INSTALLED IN WELL TO ~~135~~ 135

INITIAL WATER LEVELS W/PUMP INSTALLED

TIME	12-1 (TDC)	12-2 (TDC)	
8:55	76.81	4.30	
8:58	77.10	4.30	
9:01	77.20	4.30	(AVG) START TEST
9:03	81.25	4.29	(ART)
9:05	96.60	4.29	<del>8.69</del> pH 8.69
9:07	102.81	4.29	9.32 pH
9:09	108.72	4.29	9.62
9:12	112.82	4.28	
9:15	116.40	4.29	9.68
9:18	119.8	4.29	WATER STILL EXTREMELY SILTY 9.42 pH
9:21		4.28	
9:25	127.25	4.29	

TOP FLOW RATE COULD  
NOT HOLD ON 40 GPM  
REDUCED TO 30 GPM

Time  
9:3  
9:5  
9:40  
9:48  
9:57  
9:58  
10:0  
10:1  
10:1  
10:2  
10:3  
10:3  
10:40  
10:5  
10:5  
11:01  
11:0  
11:0  
11:11

TIME	12-1	12-2	pH
			PH 9.03 / 8.91 Flow ADJUSTED TO 3.50 gpm
9:30	117.70	4.28	
9:36	119.30	4.28	
9:40	120.02	4.28	8.91
9:45	121.25	4.28	→ top of pump 8.73
9:48	120.50		42 Adjust pump to 3.25
9:50	120.09	4.27	8.82
9:55	118.68	4.27	8.80
10:00	118.19	4.275	<del>8.80</del> 8.80
10:05	117.97	4.27	8.81
10:15	118.22	4.27	8.81
10:20	118.26	4.27	8.83
10:25	118.18	4.275	8.81 Rate 3.25
10:30	118.11	4.27	8.77 water is completely clear &
10:35	117.95	4.27	8.77
10:40	Shut down pump to lower pump to 135'		
10:50	110.5'	4.27	8.78
10:55	116.25'	4.27	8.79
11:00	119.15	4.275	8.75 3.5 gpm
11:05	121.05	4.275	8.76
11:07	Pumping Rate upped to 4.0 gpm		
11:10	123.75	4.275	8.76 4.0 gpm

<u>Time</u>	<u>RET 12-1</u>	<u>RET 12-2</u>	<u>Comments</u>
11:15	124.87	4.275	#8.75
11:20	<del>22</del> NR Generator out of Gas	4.27	
11:30	Generator pack up Flow Rate 5.5gpm to establish Drawdown		
11:35	114.20'	4.275	4.5gpm 8.77
11:40	124.70'	4.27'	4.5gpm 8.73
11:45	128.42	4.27	4.5gpm 8.68
11:50	130.70	4.27	4.25gpm 8.70
11:55	130.85	4.265	4.25 8.70
12:05	130.93	4.265	4.25gpm
12:10	130.23	4.265	4.25gpm 8.70
12:15	130.45	4.265	4.25gpm 8.66
12:20	130.50	4.265	4.25gpm 8.63
12:25	130.63	4.265	4.25gpm
12:30	131.78	4.265	@ 4.25gpm
12:32	132.0		
12:33	132.15		4.25gpm
12:34	132.15	4.265	
12:35	132.20		

# CALCULATIONS AND COMPUTATIONS

SHEET 1 OF 2

PROJECT: FIRE UNIT

JOB NO.: \_\_\_\_\_

SUBJECT: Stop down test

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Rate  
2 GPM

(12-1)			14:48:00	109.15	SC
14:18	75.34'	DEG	14:49	110.00	SC
14:32	85.40	SC	14:50	110.80	SC
14:33	86.80	SC	14:51	111.52	SC
14:33:30	88.2	SC	14:52	112.25	SC
14:34	88.9	SC	14:53	112.95	SC
14:34:30	<del>88</del> 89.9	SC	14:54	113.67	STAT
14:35	90.98	SC	14:55	114.37	AT
14:35:30	91.85	SC	14:57	115.70	DR
14:36	93.1	SC	14:59	116.65	DR
14:36:30	—	—	15:01	117.63	DR
14:37	95.0	SC	15:03	118.10	SC
14:38	96.3	SC	15:05	118.64	SC
14:38:30	—	—	15:07	118.34	SC
14:40:00	99.85	SC	15:08	119.35	SC
14:40:30	100.45	SC	15:10	—	—
14:41:00	101.05	SC	15:15	120.29	A.T.
14:41:30	101.80	SC	15:20	120.80	A.T.
14:42:00	102.55	SC	15:30	121.77	A.T.
14:42:30	103.20	SC	15:35	129.00	A.T.
14:43:00	103.85	SC	15:40	133.25	A.T.
14:44:00	105.10	SC	15:45	Below 136, can't be reaching.	
14:45:00	106.18	SC	16:15		
14:46:00	107.25	SC			
14:47:00	108.15	SC			

trouble with flow

36 GPM

259

**REI**

# CALCULATIONS AND COMPUTATIONS

SHEET 2 OF 2

PROJECT: \_\_\_\_\_

JOB NO.: \_\_\_\_\_

SUBJECT: \_\_\_\_\_

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

16:15 ~~changed~~ flow rate changed to 2.25 GPM

16:27 135.78' A.T.

16:35 134.25' A.T.

16:45 134.36' A.T.

17:00 134.81 A.T.

17:15 Below 136. A.T.

17:30 " " A.T.

18:45 " " A.T.

## CALCULATIONS AND COMPUTATIONS

SHEET 1 OF 3PROJECT: FRENCHJOB NO.: 275-14SUBJECT: Step draw-down MW-12-1COMPUTED BY: \_\_\_\_\_ DATE: 9/11

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Time	$\Delta t$ min	VOL	Depth ft	$\Delta H$ ft	OBS.	Rate GPM	pH
14:30	0	-	75.34	<del>0</del> 0	DRC	2	-
14:32	2	-	85.40	10.06	SC	2	-
14:33	3	-	86.80	11.46	SC	2	-
14:33:30	3.5	-	88.20	12.86	SC	2	-
14:34	4	-	88.90	13.56	SC	2	-
14:34:30	4.5	-	89.9	14.56	SC	2	-
14:35	5	-	90.98	15.64	SC	2	-
14:35:30	5.5	-	91.85	16.51	SC	2	-
14:36	6	-	93.10	17.76	SC	2	-
14:37:30	7	-	95.00	19.66	SC	2	-
14:38	8	-	96.30	20.96	SC	2	-
14:40	10	-	99.85	24.51	SC	2	-
14:40:30	10.5	-	100.45	25.11	SC	2	-
14:41:00	11	-	101.05	25.71	SC	2	-
14:41:30	11.5	-	101.80	26.46	SC	2	-
14:42:00	12	-	102.55	27.21	SC	2	-
14:43:00	13	-	103.20	27.86	SC	2	-
14:44:00	14	-	105.10	29.76	SC	2	-
14:45:00	15	-	106.18	30.84	SC	2	-
14:46:00	16	-	107.25	31.91	SC	2	-

**ARE**

## CALCULATIONS AND COMPUTATIONS

SHEET 2 OF 3

PROJECT: \_\_\_\_\_

JOB NO.: \_\_\_\_\_

SUBJECT: \_\_\_\_\_

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Time	$\Delta t$	VOL	Depth	$\Delta H$	OBS.	Rate	pH
14:47	17	—	108.15	32.81	SC	2	—
14:48	18	—	109.15	33.81	SC	2	—
14:49	19	—	110.00	34.66	SC	2	—
14:50	20	—	110.80	35.46	SC	2	—
14:51	21	—	111.52	36.18	SC	2	—
14:52	22	—	112.25	36.91	SC	2	—
14:53	23	—	112.95	37.61	SC	2	—
14:54	24	—	113.67	38.33	AT	2	—
14:55	25	1	114.37	39.03	AT	2	10.4
14:57	27	—	115.70	40.36	DR	2	—
14:59	29	—	116.65	41.31	DR	2	—
15:01	31	—	117.63	42.29	DR	2	—
15:03	33	1 1/3	118.10	42.76	SC	2	9.4
15:05	35	—	118.64	43.30	SC	<sup>trouble</sup> 2 1/2 flow	—
15:07	37	—	118.34	43.00	SC	2	—
15:10	40	1 2/3	119.35	44.01	SC	2	9.0
15:15	45	—	120.29	44.95	AT	2	—
15:20	50	2	120.80	45.46	AT	2	9.0
15:30	60	2 1/3	121.77	46.43	AT	3	8.9
15:36	66	2 2/3	122.00	53.66	AT	3	8.8

REI

## CALCULATIONS AND COMPUTATIONS

SHEET 3 OF 3

PROJECT: \_\_\_\_\_

JOB NO.: \_\_\_\_\_

SUBJECT: \_\_\_\_\_

COMPUTED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Time	$\Delta t$	VOL	Depth	$\Delta H$	OBS.	Rate	pH
15:40	70	3	133.35	58.01	AT	3	8.6
15:45	75	3 1/3	Below 136.	-	AT	3	8.6
15:51	81	3 2/3	"	-	AT	3	8.6
16:00	90	4 1/3	"	-	AT	3.2	8.6
16:13	103	5 1/4	"	-	AT	3.2	8.4
16:15	105	-	"	-	AT	2.25	-
16:27	117	-	135.78	60.44	AT	2.25	-
16:30	120	6	-	-	AT	2.25	8.6
16:35	125	-	134.25	58.91	AT	2.25	-
16:41	131	6 1/2	-	-	AT	2.25	8.5
16:45	135	-	134.36	59.02	AT	2.25	-
16:52	142	7	-	-	AT	2.25	8.5
17:00	150	-	134.81	59.47	AT	2.25	-
17:03	153	7 1/2	-	-	AT	2.25	8.5
17:15	165	8	Below 136.	-	AT	2.25	8.5
17:30	180	-	"	-	AT	2.25	-
17:40	190	9	"	-	AT	2.25	8.5
17:45	195	9 1/2	"	-	AT	2.25	8.5

**REN**



## CALCULATIONS AND COMPUTATIONS

SHEET 1 OF 3PROJECT: FRENCHJOB NO.: 275-141SUBJECT: Recovery of 12-1COMPUTED BY: \_\_\_\_\_ DATE: 9/11

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Time	$\Delta t$	VOL	Depth	$\Delta H$	OBS.	Rate	pH
17:46	0		Below 136	0	DRG		
17:46:30	.5		134.38	1.62			
17:47	1.0		132.75	3.25			
17:47:30	1.5		131.10	4.9			
17:48	2		129.43	6.57			
17:48:30	2.5		127.77	8.23			
17:49	3		126.22	9.78			
17:49:30	3.5		124.69	11.31			
17:50	4		123.25	12.75			
17:51	5		120.94	15.06			
17:52	6		118.23	17.17			
17:52:30	6.5		117.625	18.375			
17:53	7		116.505	19.495			
17:53:30	7.5		115.38	20.62			
17:54	8		114.265	21.735			
17:54:30	8.5		113.25	22.75			
17:55	9		112.26	23.74			
17:55:30	9.5		111.22	24.78			
17:56	10		110.26	25.74			
17:56:30	10.5		109.34	26.66	✓		

**REI**

# CALCULATIONS AND COMPUTATIONS

SHEET 2 OF 3

PROJECT: FRENCH

JOB NO.: 275-14

SUBJECT: Recovery 12-1

COMPUTED BY: \_\_\_\_\_ DATE: 9/11

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Time	$\Delta t$	VOL	Depth	$\Delta H$	OBS.	Rate	pH
17:57	11		108.45	27.55	DRG		
17:57:30	11.5		107.51	28.49			
17:58	12		106.69	29.49			
17:58:30	12.5		105.86	30.14			
17:59	13		105.08	30.92			
17:59:30	13.5		104.29	31.71			
18:00	14		103.58	32.42			
18:01	14.5		102.84	33.16			
18:01	15		102.15	33.85			
18:02	16		100.80	35.20			
18:03	17		99.57	36.43			
18:04	18		98.41	37.59			
18:05	19		97.30	38.70			
18:06	20		96.28	39.72			
18:07	21		95.32	40.68			
18:08	22		94.39	41.61			
18:09	23		93.55	42.45			
18:10	24		92.75	43.25			
18:11	25		91.98	44.02			
18:13	27		90.58	45.42	✓		

**REI**

SHEET 2 OF 3

JOB NO.: 275-14

COMPUTED BY: \_\_\_\_\_ DATE: 9/11

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

# AREA

Appendix 24

Test Data for Artifical  
Penetration Anomaly

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: French, GW-25 Correlation Test

JOB NO.: \_\_\_\_\_

SUBJECT: FLOW RATE MONITORING SHEET

COMPUTED BY: \_\_\_\_\_ DATE: 7/17/86

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

FLOW RATE	TIME (2400)	MONITORS INITIALS	FLOW RATE	TIME (2400)	MONITORS INITIALS
Start	1220	DD			
30	1220:23	DD			
29	1220:46	DD			
27.9	1221	DD			
27.4	1221:14	DD			
2 schedules with 11					
14	1222:28	DD			
15	1223:30	DD			
14.9	1225	DD			
14.8	1230	DD			
14.5	1235	DD			
14.4	1240	DD			
14.7	1300	DD			
14.6	1315	DD			
14.9	1320	DD			
14.8	1345	DD			
14.6	1400	DD			
set to 14.1	1407	DD			
14.0	1415	DD			
14.0	1430	DD			
14.0	1449	DD			
14.0	1500	DD			
14.0	1510	DD			
14.2	1530	DD			
18	1557:30	DD			
Stop	1600	DD			

**REI**

FRENCH LTD. GW-25 TEST

Run 1  
09/19/86

SE200B DATA  
constant rate test

test is to be compared with  
REI 10-1 pump test data

TRANSDUCER TABLE

Input 1: REI 10-1  
Transducer s/n: 139  
Scale factor: 49.59  
Initial level: 81 feet

Input 2: GW-25  
Transducer s/n: 1857/858  
Scale factor: 50.4  
Initial level: 84.64 feet

Input 3: NONE  
Transducer s/n: NONE  
Scale factor: 1

Input 4: REI 3-4  
Transducer s/n: 1504/854  
Scale factor: 10.09  
Initial level: 82.31 feet

Input 5: REI 11  
Transducer s/n: 1076/849  
Scale factor: 10.07  
Initial level: 79.97 feet

Input 6: P-10-2  
Transducer s/n: 1634/857  
Scale factor: 10.08  
Initial level: 46.07 feet

Input 7: P-10-3  
Transducer s/n: 1518/854  
Scale factor: 10.08  
Initial level: 40.09 feet

Input 8: P-10-4  
Transducer s/n: 2344/85N  
Scale factor: 10.13  
Initial level: 38.82 feet

Input 9: REI 10-2  
Transducer s/n: 516/830  
Scale factor: 10.04  
Initial level: 5.67 feet

Input 10: REI 10-3A  
Transducer s/n: 596/841  
Scale factor: 10.03  
Initial level: 7.05 feet

#### FAST DATA

Input 11: REI 10-3B  
Transducer s/n: 383/839  
Scale factor: 10.05  
Initial level: 7.05 feet

Input 12: REI 10-4  
Transducer s/n: 1631/857  
Scale factor: 10.05  
Initial level: 7.56 feet

#### PUMP SCHEDULE

Drawdown for 1000 min  
Pump at 30 GPM  
Pump set at 140 feet

Recovery for 500 min

#### SAMPLING SCHEDULE

0-10	sec	@	1 sec
10-60	sec	@	5 sec
1-10	min	@	20 sec
10-100	min	@	2 min
100-1000	min	@	20 min
1000-10000	min	@	60 min
10000-99999	min	@	200 min

-----DRAWDOWN REPORT-----

Started at 1220  
Lasted 219.98 min

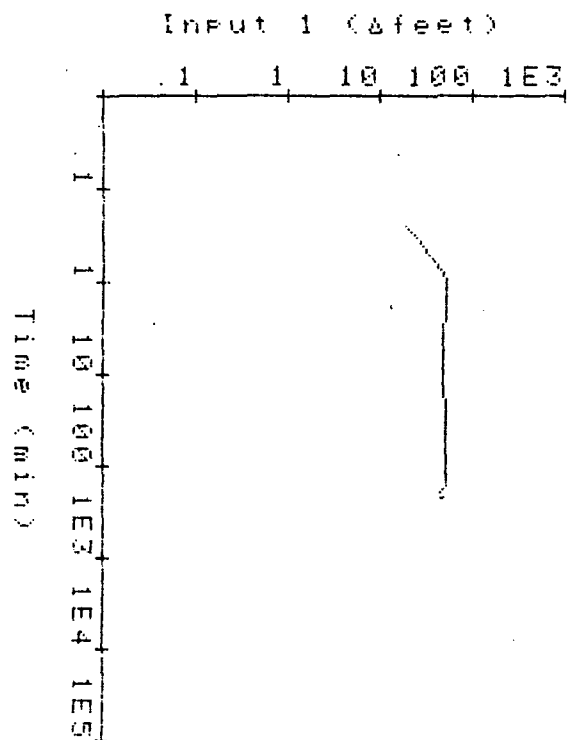
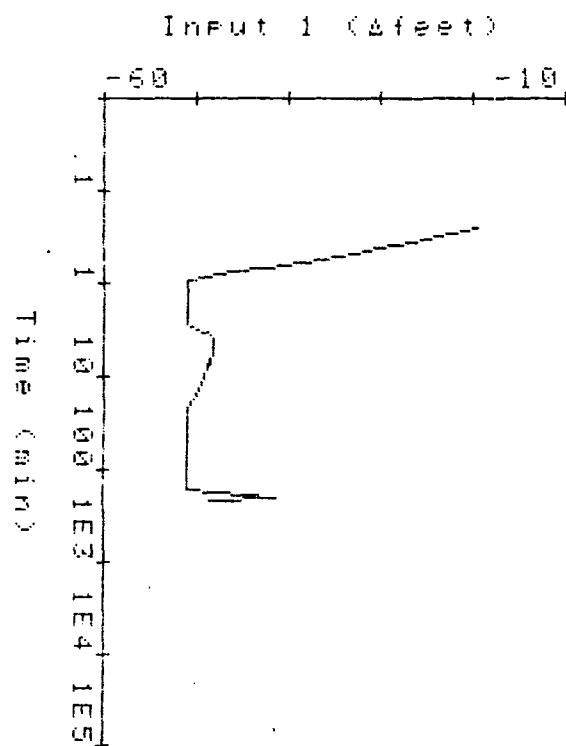
Input 1 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	81.00	0.00
1220	0.257	100.42	-19.42
1220	0.341	105.94	-24.94
1220	0.424	110.93	-29.93
1220	0.507	115.39	-34.39
1220	0.591	119.54	-38.54
1220	0.674	123.35	-42.35
1220	0.757	126.85	-45.85
1220	0.841	130.17	-49.17
1220	0.924	131.87	-50.87
1221	1.007	131.87	-50.87
1221	1.417	131.89	-50.89
1221	1.750	131.90	-50.90
1222	2.084	131.90	-50.90
1222	2.417	131.92	-50.92
1222	2.750	131.92	-50.92
1223	3.084	130.92	-49.92
1223	3.417	129.76	-48.76
1223	3.750	129.34	-48.34
1224	4.084	129.19	-48.19
1224	4.417	129.10	-48.10
1224	4.750	129.04	-48.04
1225	5.084	129.04	-48.04
1225	5.417	129.03	-48.03
1225	5.750	129.11	-48.12
1226	6.084	129.20	-48.20
1226	6.417	129.30	-48.30
1226	6.750	129.36	-48.36
1227	7.084	129.47	-48.47
1227	7.417	129.54	-48.55
1227	7.750	129.64	-48.64
1228	8.084	129.71	-48.72
1228	8.417	129.80	-48.80
1228	8.750	129.89	-48.89
1229	9.084	129.94	-48.94
1229	9.417	130.01	-49.02
1229	9.750	130.07	-49.07
1230	10.084	130.14	-49.14
1232	12.111	130.50	-49.50
1234	14.111	130.79	-49.79
1236	16.099	131.07	-50.07
1238	18.098	131.32	-50.32
1240	20.098	131.53	-50.53



1242	22.098	131.92	-50.92
1244	24.098	131.92	-50.92
1246	26.098	131.92	-50.92
1248	28.098	131.92	-50.92
1250	30.098	131.92	-50.92
1252	32.098	131.92	-50.92
1254	34.098	131.92	-50.92
1256	36.123	131.92	-50.92
1258	38.265	131.92	-50.92
1300	40.108	131.92	-50.92
1302	42.202	131.92	-50.92
1304	44.160	131.92	-50.92
1306	46.160	131.92	-50.92
1308	48.160	131.92	-50.92
1310	50.188	131.90	-50.90
1312	52.113	131.92	-50.92
1314	54.113	131.92	-50.92
1316	56.113	131.90	-50.90
1318	58.113	131.92	-50.92
1320	60.113	131.90	-50.90
1322	62.238	131.92	-50.92
1324	64.113	131.90	-50.90
1326	66.113	131.92	-50.92
1328	68.113	131.92	-50.92
1330	70.113	131.92	-50.92
1332	72.113	131.92	-50.92
1334	74.113	131.92	-50.92
1336	76.133	131.90	-50.90
1338	78.113	131.92	-50.92
1340	80.113	131.92	-50.92
1342	82.212	131.92	-50.92
1344	84.113	131.92	-50.92
1346	86.105	131.92	-50.92
1348	88.113	131.92	-50.92
1350	90.113	131.92	-50.92
1352	92.245	131.92	-50.92
1354	94.113	131.92	-50.92
1356	96.113	131.92	-50.92
1358	98.113	131.92	-50.92
1420	120.110	131.92	-50.92
1440	140.250	131.92	-50.92
1500	160.110	131.92	-50.92
1520	180.030	128.41	-47.41
1540	200.120	122.28	-41.28
1559	219.980	129.30	-48.30

Average level: 130.30

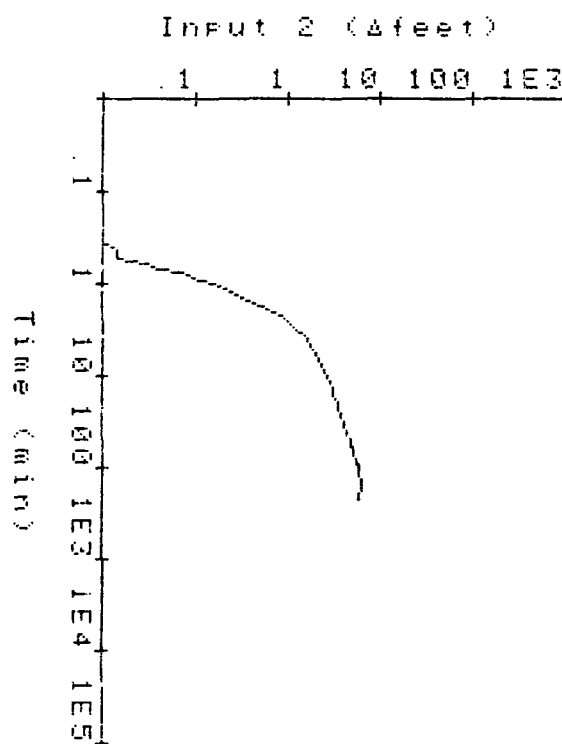
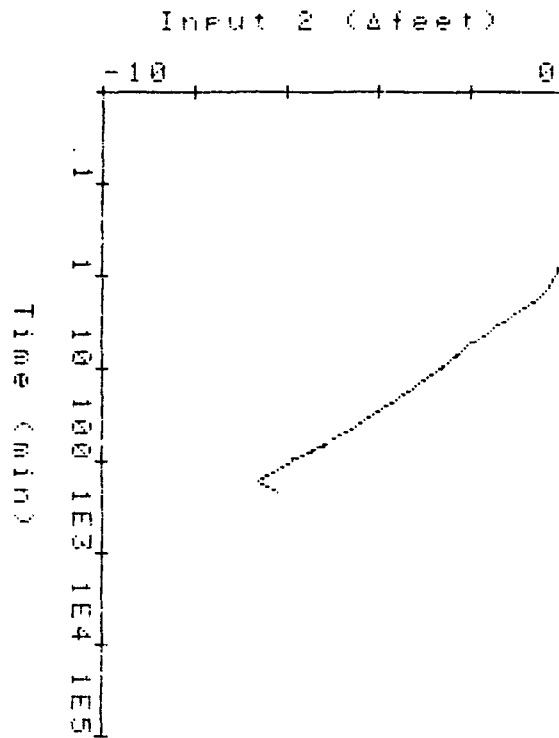


Input 2 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	84.64	0.00
1220	0.257	84.64	0.00
1220	0.341	84.64	0.00
1220	0.424	84.65	-0.01
1220	0.507	84.65	-0.01
1220	0.591	84.67	-0.03
1220	0.674	84.68	-0.04
1220	0.757	84.71	-0.07
1220	0.841	84.74	-0.10
1220	0.924	84.76	-0.12
1221	1.007	84.80	-0.16
1221	1.417	84.99	-0.35
1221	1.750	85.18	-0.54
1222	2.084	85.38	-0.74
1222	2.417	85.57	-0.93
1222	2.750	85.74	-1.10
1223	3.084	85.90	-1.26
1223	3.417	86.05	-1.41
1223	3.750	86.17	-1.53
1224	4.084	86.28	-1.64
1224	4.417	86.38	-1.74
1224	4.750	86.46	-1.82
1225	5.084	86.54	-1.90
1225	5.417	86.62	-1.98
1225	5.750	86.67	-2.03
1226	6.084	86.75	-2.11
1226	6.417	86.81	-2.17
1226	6.750	86.86	-2.22
1227	7.084	86.92	-2.28
1227	7.417	86.97	-2.33
1227	7.750	87.02	-2.38
1228	8.084	87.07	-2.43
1228	8.417	87.11	-2.47
1228	8.750	87.17	-2.53
1229	9.084	87.20	-2.56
1229	9.417	87.24	-2.60
1229	9.750	87.29	-2.64
1230	10.084	87.33	-2.69
1232	12.111	87.55	-2.91
1234	14.111	87.74	-3.10
1236	16.099	87.88	-3.24
1238	18.098	88.03	-3.39
1240	20.098	88.17	-3.53
1242	22.098	88.27	-3.63
1244	24.098	88.39	-3.75
1246	26.098	88.51	-3.87
1248	28.098	88.61	-3.97
1250	30.098	88.69	-4.05
1252	32.098	88.78	-4.14

1254	34.098	88.87	-4.23
1256	36.123	88.94	-4.30
1258	38.265	89.03	-4.39
1300	40.108	89.09	-4.45
1302	42.202	89.16	-4.52
1304	44.160	89.23	-4.59
1306	46.160	89.29	-4.65
1308	48.160	89.35	-4.71
1310	50.188	89.41	-4.77
1312	52.113	89.46	-4.82
1314	54.113	89.52	-4.88
1316	56.113	89.58	-4.94
1318	58.113	89.62	-4.98
1320	60.113	89.68	-5.04
1322	62.238	89.73	-5.09
1324	64.113	89.77	-5.13
1326	66.113	89.81	-5.17
1328	68.113	89.86	-5.22
1330	70.113	89.90	-5.26
1332	72.113	89.96	-5.32
1334	74.113	90.00	-5.36
1336	76.133	90.05	-5.41
1338	78.113	90.10	-5.46
1340	80.113	90.15	-5.51
1342	82.212	90.19	-5.55
1344	84.113	90.24	-5.59
1346	86.105	90.28	-5.64
1348	88.113	90.32	-5.68
1350	90.113	90.37	-5.73
1352	92.245	90.41	-5.77
1354	94.113	90.45	-5.81
1356	96.113	90.50	-5.86
1358	98.113	90.54	-5.90
1420	120.110	90.82	-6.18
1440	140.250	91.08	-6.44
1500	160.110	91.30	-6.66
1520	180.030	91.21	-6.57
1540	200.120	90.89	-6.25
1559	219.980	90.82	-6.18

Average level: 90.15

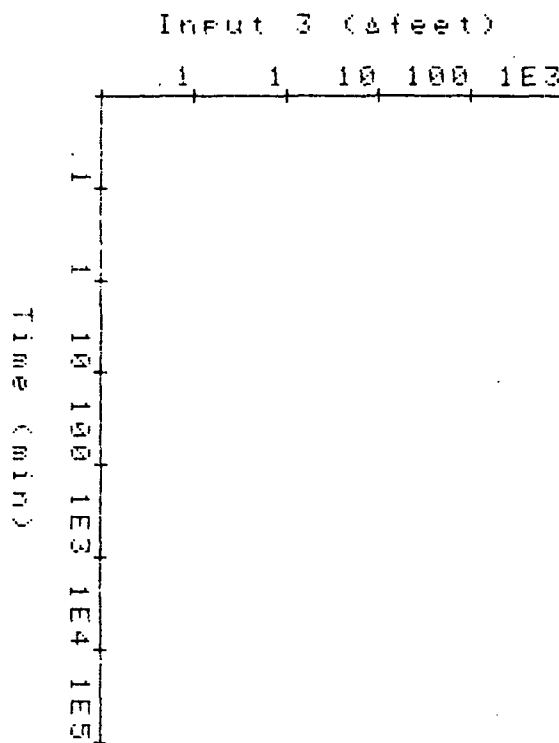
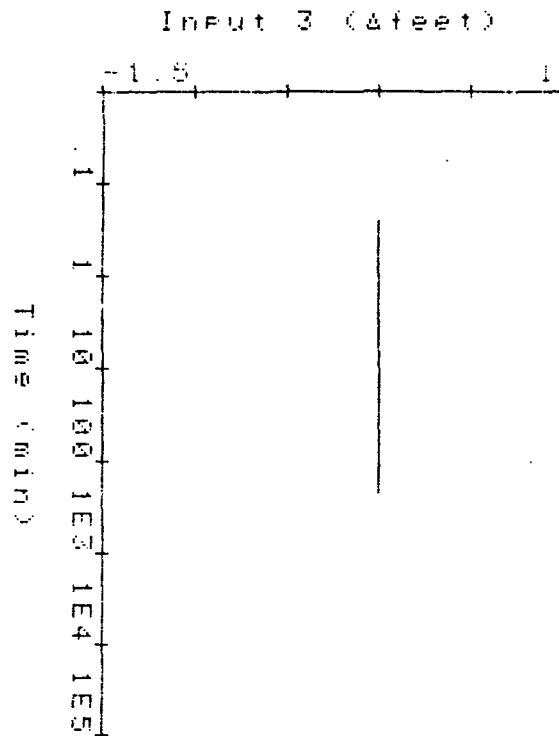


## Input 3 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	0.00	0.00
1220	0.257	0.00	-0.00
1220	0.341	0.00	0.00
1220	0.424	-0.00	0.00
1220	0.507	-0.00	0.00
1220	0.591	-0.00	0.00
1220	0.674	-0.00	0.00
1220	0.757	-0.00	0.00
1220	0.841	-0.00	0.00
1220	0.924	-0.00	0.00
1221	1.007	-0.00	0.00
1221	1.417	-0.00	0.00
1221	1.750	-0.00	0.00
1222	2.084	-0.00	0.00
1222	2.417	0.00	0.00
1222	2.750	0.00	-0.00
1223	3.084	-0.00	0.00
1223	3.417	0.00	0.00
1223	3.750	-0.00	0.00
1224	4.084	-0.00	0.00
1224	4.417	0.00	0.00
1224	4.750	-0.00	0.00
1225	5.084	0.00	0.00
1225	5.417	-0.00	0.00
1225	5.750	0.00	0.00
1226	6.084	0.00	-0.00
1226	6.417	-0.00	0.00
1226	6.750	0.00	0.00
1227	7.084	-0.00	0.00
1227	7.417	-0.00	0.00
1227	7.750	-0.00	0.00
1228	8.084	-0.00	0.00
1228	8.417	0.00	-0.00
1228	8.750	0.00	0.00
1229	9.084	-0.00	0.00
1229	9.417	-0.00	0.00
1229	9.750	0.00	-0.00
1230	10.084	0.00	-0.00
1232	12.111	0.00	0.00
1234	14.111	-0.00	0.00
1236	16.098	-0.00	0.00
1238	18.098	-0.00	0.00
1240	20.098	-0.00	0.00
1242	22.098	-0.00	0.00
1244	24.098	-0.00	0.00
1246	26.098	-0.00	0.00
1248	28.098	-0.00	0.00

1250	30.098	-0.00	0.00
1252	32.098	-0.00	0.00
1254	34.098	-0.00	0.00
1256	36.123	-0.00	0.00
1258	38.265	-0.00	0.00
1300	40.108	-0.00	0.00
1302	42.202	-0.00	0.00
1304	44.160	-0.00	0.00
1306	46.160	-0.00	0.00
1308	48.160	-0.00	0.00
1310	50.188	-0.00	0.00
1312	52.113	-0.00	0.00
1314	54.113	-0.00	0.00
1316	56.113	0.00	0.00
1318	58.113	-0.00	0.00
1320	60.113	-0.00	0.00
1322	62.238	0.00	0.00
1324	64.113	-0.00	0.00
1326	66.113	-0.00	0.00
1328	68.113	-0.00	0.00
1330	70.113	-0.00	0.00
1332	72.113	0.00	0.00
1334	74.113	-0.00	0.00
1336	76.133	-0.00	0.00
1338	78.113	-0.00	0.00
1340	80.113	-0.00	0.00
1342	82.212	-0.00	0.00
1344	84.113	-0.00	0.00
1346	86.105	-0.00	0.00
1348	88.113	-0.00	0.00
1350	90.113	-0.00	0.00
1352	92.245	-0.00	0.00
1354	94.113	-0.00	0.00
1356	96.113	-0.00	0.00
1358	98.113	0.00	0.00
1420	120.110	0.00	-0.00
1440	140.250	0.00	0.00
1500	160.110	0.00	-0.00
1520	180.030	0.00	-0.00
1540	200.120	0.00	0.00
1559	219.980	-0.00	0.00

Average level: -0.00



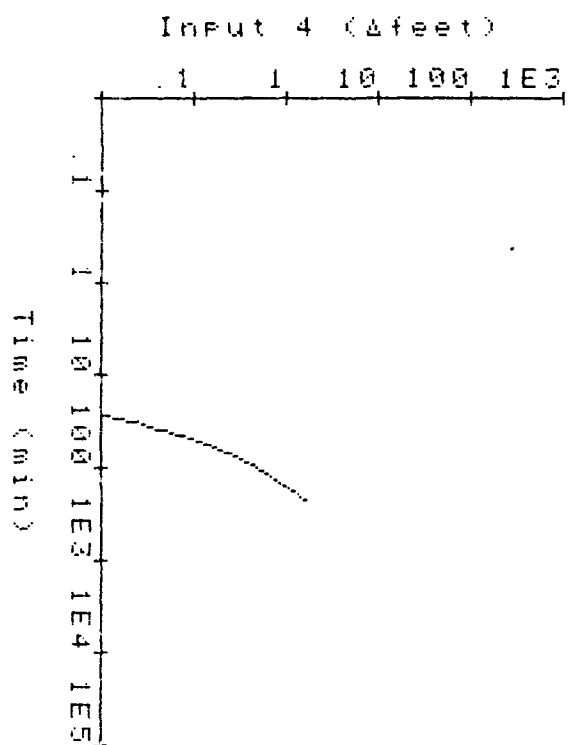
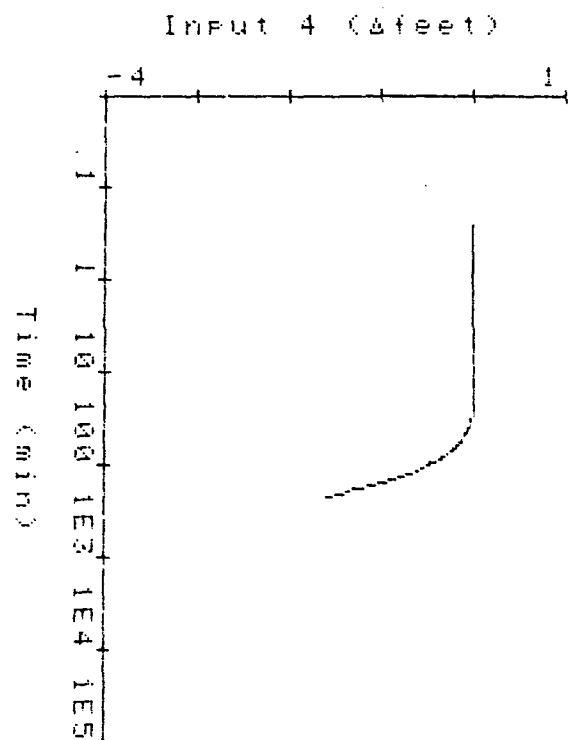


Input 4 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	82.31	0.00
1220	0.257	82.31	0.00
1220	0.341	82.31	0.00
1220	0.424	82.31	0.00
1220	0.507	82.31	0.00
1220	0.591	82.31	0.00
1220	0.674	82.31	0.00
1220	0.757	82.31	0.00
1220	0.841	82.31	0.00
1220	0.924	82.31	0.00
1221	1.007	82.31	0.00
1221	1.417	82.31	0.00
1221	1.750	82.31	0.00
1222	2.084	82.31	0.00
1222	2.417	82.31	0.00
1222	2.750	82.31	0.00
1223	3.084	82.31	0.00
1223	3.417	82.31	0.00
1223	3.750	82.31	0.00
1224	4.084	82.31	0.00
1224	4.417	82.31	0.00
1224	4.750	82.31	0.00
1225	5.084	82.31	0.00
1225	5.417	82.31	0.00
1225	5.750	82.31	0.00
1226	6.084	82.31	0.00
1226	6.417	82.31	0.00
1226	6.750	82.31	0.00
1227	7.084	82.31	0.00
1227	7.417	82.31	0.00
1227	7.750	82.31	0.00
1228	8.084	82.31	0.00
1228	8.417	82.31	0.00
1228	8.750	82.31	0.00
1229	9.084	82.31	0.00
1229	9.417	82.31	0.00
1229	9.750	82.31	0.00
1230	10.084	82.31	0.00
1232	12.111	82.31	0.00
1234	14.111	82.31	0.00
1236	16.099	82.31	0.00
1238	18.098	82.31	0.00
1240	20.098	82.31	0.00
1242	22.098	82.31	-0.00
1244	24.098	82.31	-0.00
1246	26.098	82.32	-0.01
1248	28.098	82.32	-0.01
1250	30.098	82.33	-0.01
1252	32.098	82.33	-0.02
1254	34.098	82.34	-0.03
1256	36.123	82.35	-0.03

1258	38.265	82.35	-0.04
1300	40.108	82.36	-0.05
1302	42.202	82.37	-0.06
1304	44.160	82.38	-0.07
1306	46.160	82.39	-0.08
1308	48.160	82.40	-0.09
1310	50.188	82.41	-0.10
1312	52.113	82.42	-0.11
1314	54.113	82.44	-0.13
1316	56.113	82.45	-0.14
1318	58.113	82.46	-0.15
1320	60.113	82.47	-0.16
1322	62.238	82.49	-0.18
1324	64.113	82.51	-0.19
1326	66.113	82.52	-0.21
1328	68.113	82.53	-0.22
1330	70.113	82.55	-0.24
1332	72.113	82.57	-0.26
1334	74.113	82.58	-0.27
1336	76.133	82.60	-0.29
1338	78.113	82.62	-0.31
1340	80.113	82.63	-0.32
1342	82.212	82.65	-0.34
1344	84.113	82.67	-0.35
1346	86.105	82.68	-0.37
1348	88.113	82.70	-0.39
1350	90.113	82.72	-0.41
1352	92.245	82.74	-0.43
1354	94.113	82.76	-0.45
1356	96.113	82.78	-0.47
1358	98.113	82.79	-0.48
1420	120.110	83.00	-0.69
1440	140.250	83.20	-0.89
1500	160.110	83.39	-1.08
1520	180.030	83.58	-1.27
1540	200.120	83.76	-1.45
1559	219.980	83.91	-1.60

Average level: 83.02

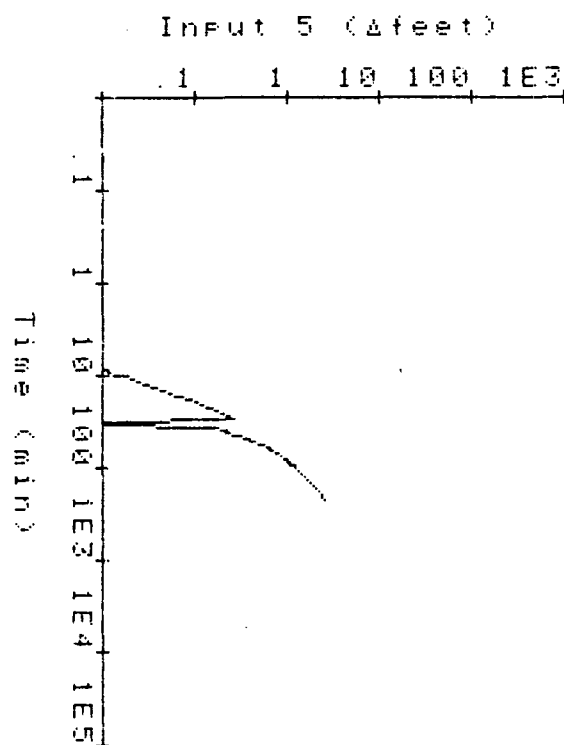
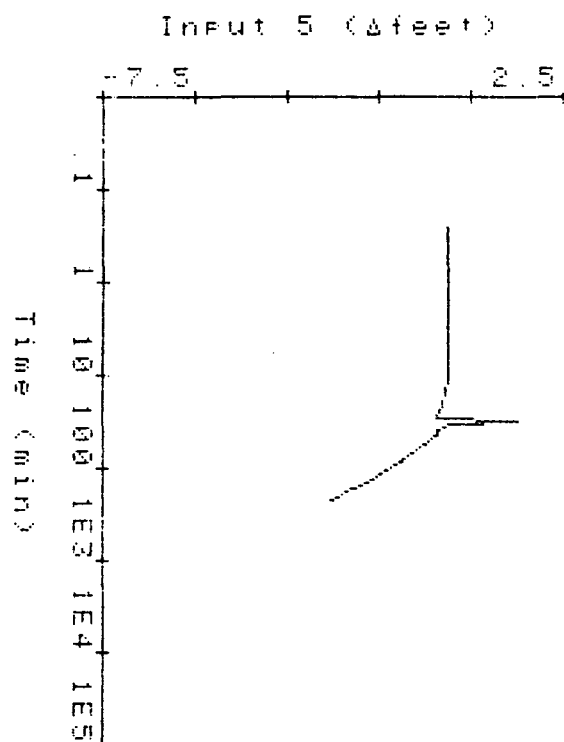


Input 5 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	79.97	0.00
1220	0.257	79.97	0.00
1220	0.341	79.97	0.00
1220	0.424	79.97	0.00
1220	0.507	79.97	0.00
1220	0.591	79.97	0.00
1220	0.674	79.97	0.00
1220	0.757	79.97	0.00
1220	0.841	79.97	0.00
1220	0.924	79.97	0.00
1221	1.007	79.97	0.00
1221	1.417	79.97	0.00
1221	1.750	79.97	0.00
1222	2.084	79.97	0.00
1222	2.417	79.97	0.00
1222	2.750	79.97	0.00
1223	3.084	79.97	-0.00
1223	3.417	79.97	0.00
1223	3.750	79.97	0.00
1224	4.084	79.97	0.00
1224	4.417	79.97	0.00
1224	4.750	79.97	0.00
1225	5.084	79.97	0.00
1225	5.417	79.97	-0.00
1225	5.750	79.97	-0.00
1226	6.084	79.97	-0.00
1226	6.417	79.97	-0.00
1226	6.750	79.97	-0.00
1227	7.084	79.98	-0.01
1227	7.417	79.98	-0.01
1227	7.750	79.98	-0.01
1228	8.084	79.98	-0.01
1228	8.417	79.98	-0.01
1228	8.750	79.98	-0.01
1229	9.084	79.98	-0.01
1229	9.417	79.98	-0.01
1229	9.750	79.99	-0.01
1230	10.084	79.99	-0.02
1232	12.111	80.00	-0.03
1234	14.111	80.02	-0.05
1236	16.099	80.04	-0.07
1238	18.098	80.06	-0.09
1240	20.098	80.09	-0.12
1242	22.098	80.12	-0.15
1244	24.098	80.15	-0.17

1246	26.098	80.17	-0.20
1248	28.098	80.21	-0.24
1250	30.098	80.24	-0.26
1252	32.098	78.50	1.47
1254	34.098	79.97	-0.00
1256	36.123	80.12	-0.15
1258	38.265	80.20	-0.23
1300	40.108	80.19	-0.22
1302	42.202	80.20	-0.23
1304	44.160	80.24	-0.26
1306	46.160	80.27	-0.30
1308	48.160	80.33	-0.36
1310	50.188	80.37	-0.40
1312	52.113	80.38	-0.41
1314	54.113	80.43	-0.46
1316	56.113	80.49	-0.52
1318	58.113	80.54	-0.57
1320	60.113	80.58	-0.60
1322	62.238	80.61	-0.64
1324	64.113	80.64	-0.66
1326	66.113	80.69	-0.72
1328	68.113	80.73	-0.76
1330	70.113	80.77	-0.80
1332	72.113	80.80	-0.83
1334	74.113	80.83	-0.86
1336	76.133	80.85	-0.88
1338	78.113	80.89	-0.91
1340	80.113	80.92	-0.95
1342	82.212	80.95	-0.98
1344	84.113	81.00	-1.03
1346	86.105	81.02	-1.05
1348	88.113	81.04	-1.07
1350	90.113	81.07	-1.10
1352	92.245	81.12	-1.15
1354	94.113	81.14	-1.17
1356	96.113	81.17	-1.20
1358	98.113	81.20	-1.23
1420	120.110	81.52	-1.55
1440	140.250	81.79	-1.82
1500	160.110	82.02	-2.05
1520	180.030	82.20	-2.23
1540	200.120	82.37	-2.40
1559	219.980	82.51	-2.53

Average level: 81.33



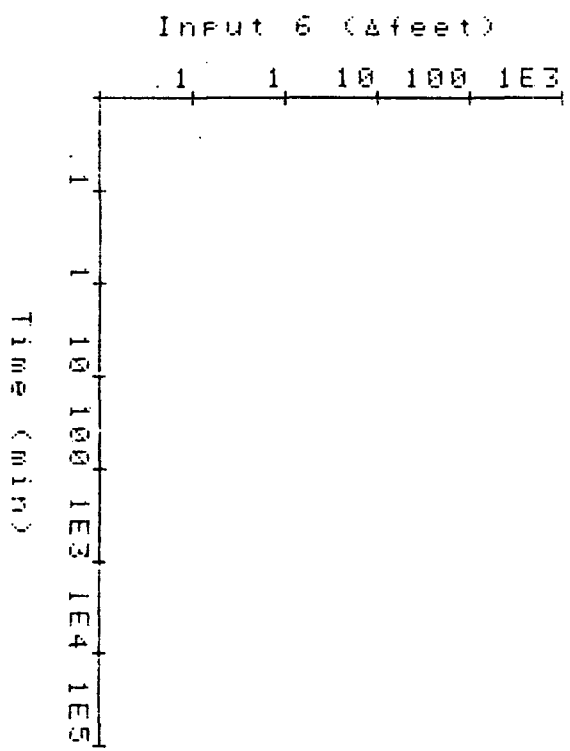
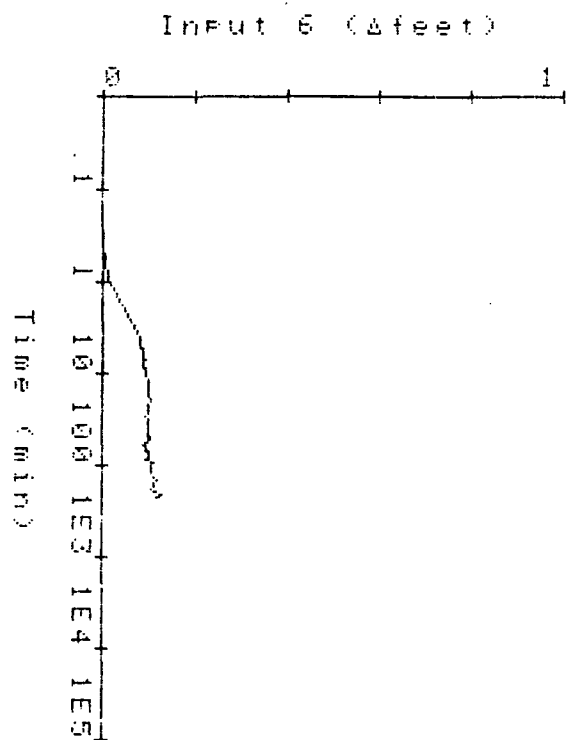
Input 6 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	46.07	0.00
1220	0.257	46.07	0.00
1220	0.341	46.07	0.00
1220	0.424	46.07	0.00
1220	0.507	46.07	0.01
1220	0.591	46.07	0.01
1220	0.674	46.07	0.01
1220	0.757	46.06	0.01
1220	0.841	46.06	0.01
1220	0.924	46.06	0.01
1221	1.007	46.06	0.02
1221	1.417	46.04	0.03
1221	1.750	46.03	0.04
1222	2.084	46.03	0.05
1222	2.417	46.02	0.06
1222	2.750	46.01	0.06
1223	3.084	46.01	0.07
1223	3.417	46.00	0.07
1223	3.750	46.00	0.08
1224	4.084	45.99	0.08
1224	4.417	45.99	0.08
1224	4.750	45.99	0.08
1225	5.084	45.99	0.08
1225	5.417	45.99	0.09
1225	5.750	45.99	0.09
1226	6.084	45.98	0.09
1226	6.417	45.98	0.09
1226	6.750	45.98	0.09
1227	7.084	45.98	0.09
1227	7.417	45.99	0.09
1227	7.750	45.99	0.09
1228	8.084	45.98	0.09
1228	8.417	45.98	0.09
1228	8.750	45.98	0.09
1229	9.084	45.98	0.09
1229	9.417	45.98	0.09
1229	9.750	45.98	0.10
1230	10.084	45.98	0.10
1232	12.111	45.98	0.10
1234	14.111	45.98	0.10
1236	16.099	45.97	0.10
1238	18.098	45.98	0.10
1240	20.098	45.97	0.10
1242	22.098	45.98	0.10
1244	24.098	45.97	0.10
1246	26.098	45.97	0.10
1248	28.098	45.97	0.10
1250	30.098	45.98	0.10

1252	32.098	45.98	0.10
1254	34.098	45.97	0.10
1256	36.123	45.97	0.10
1258	38.265	45.97	0.10
1300	40.108	45.97	0.10
1302	42.202	45.97	0.10
1304	44.160	45.97	0.10
1306	46.160	45.97	0.10
1308	48.160	45.97	0.10
1310	50.188	45.97	0.10
1312	52.113	45.97	0.10
1314	54.113	45.98	0.10
1316	56.113	45.98	0.10
1318	58.113	45.98	0.09
1320	60.113	45.98	0.09
1322	62.238	45.98	0.10
1324	64.113	45.98	0.10
1326	66.113	45.98	0.10
1328	68.113	45.98	0.09
1330	70.113	45.98	0.10
1332	72.113	45.98	0.10
1334	74.113	45.98	0.10
1336	76.133	45.98	0.10
1338	78.113	45.98	0.10
1340	80.113	45.97	0.10
1342	82.212	45.98	0.10
1344	84.113	45.98	0.10
1346	86.105	45.98	0.10
1348	88.113	45.98	0.10
1350	90.113	45.97	0.10
1352	92.245	45.97	0.11
1354	94.113	45.96	0.11
1356	96.113	45.96	0.11
1358	98.113	45.97	0.11
1420	120.110	45.97	0.11
1440	140.250	45.96	0.12
1500	160.110	45.96	0.11
1520	180.030	45.97	0.11
1540	200.120	45.94	0.13
1559	219.980	45.96	0.12

Average level: 45.97



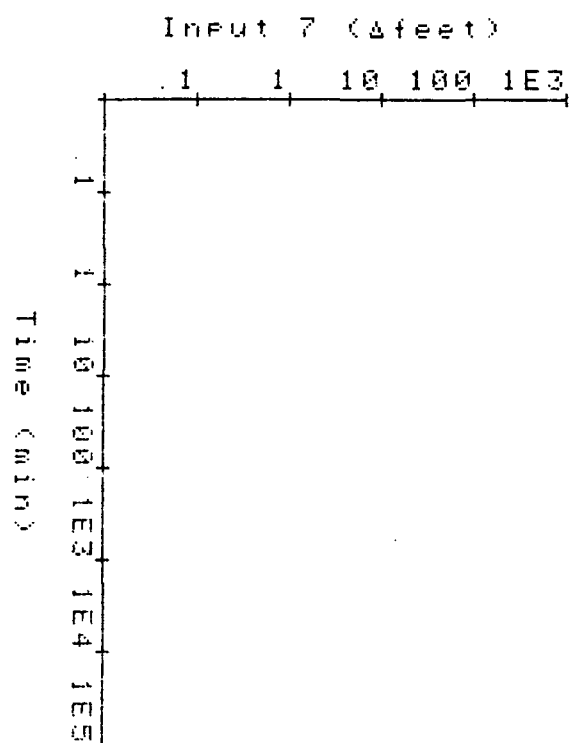
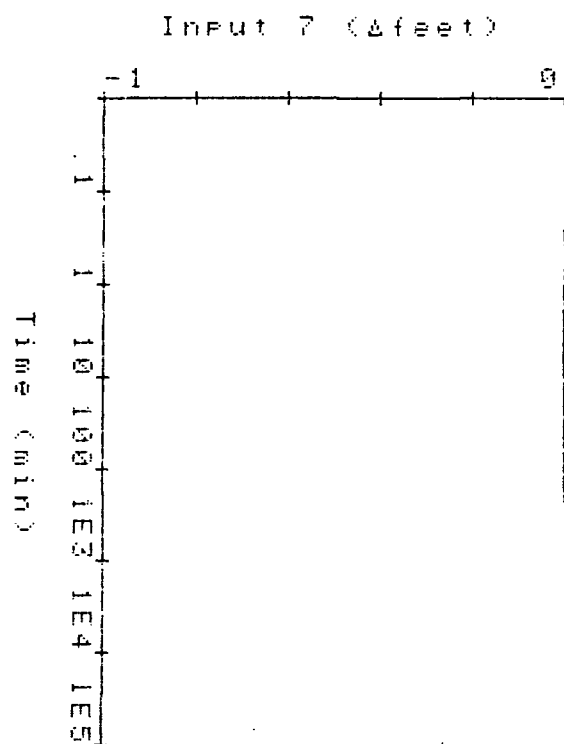


Input 7 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	40.09	0.00
1220	0.257	40.09	-0.00
1220	0.341	40.09	-0.00
1220	0.424	40.09	-0.00
1220	0.507	40.09	-0.00
1220	0.591	40.09	-0.00
1220	0.674	40.09	-0.00
1220	0.757	40.09	-0.00
1220	0.841	40.09	-0.00
1220	0.924	40.09	0.00
1221	1.007	40.09	0.00
1221	1.417	40.09	0.00
1221	1.750	40.09	0.00
1222	2.084	40.09	0.00
1222	2.417	40.09	0.00
1222	2.750	40.09	0.00
1223	3.084	40.09	-0.00
1223	3.417	40.09	-0.00
1223	3.750	40.09	0.00
1224	4.084	40.09	-0.00
1224	4.417	40.09	0.00
1224	4.750	40.09	0.00
1225	5.084	40.09	0.00
1225	5.417	40.09	-0.00
1225	5.750	40.09	-0.00
1226	6.084	40.09	0.00
1226	6.417	40.09	0.00
1226	6.750	40.09	-0.00
1227	7.084	40.09	-0.00
1227	7.417	40.09	-0.00
1227	7.750	40.09	-0.00
1228	8.084	40.09	0.00
1228	8.417	40.09	0.00
1228	8.750	40.09	-0.00
1229	9.084	40.09	-0.00
1229	9.417	40.09	-0.00
1229	9.750	40.09	-0.00
1230	10.084	40.09	-0.00
1232	12.111	40.09	-0.00
1234	14.111	40.09	-0.00
1236	16.099	40.09	-0.00
1238	18.098	40.09	-0.00
1240	20.098	40.09	0.00
1242	22.098	40.09	-0.00

1244	24.098	40.09	-0.00
1246	26.098	40.09	0.00
1248	28.098	40.09	0.00
1250	30.098	40.09	0.00
1252	32.098	40.09	0.00
1254	34.098	40.09	-0.00
1256	36.123	40.09	0.00
1258	38.265	40.09	0.00
1300	40.108	40.09	-0.00
1302	42.202	40.09	0.00
1304	44.160	40.09	-0.00
1306	46.160	40.09	-0.00
1308	48.160	40.09	0.00
1310	50.188	40.09	-0.00
1312	52.113	40.09	0.00
1314	54.113	40.09	-0.00
1316	56.113	40.09	0.00
1318	58.113	40.09	0.00
1320	60.113	40.09	0.00
1322	62.238	40.09	-0.00
1324	64.113	40.09	0.00
1326	66.113	40.09	-0.00
1328	68.113	40.09	0.00
1330	70.113	40.09	-0.00
1332	72.113	40.09	0.00
1334	74.113	40.09	-0.00
1336	76.133	40.09	0.00
1338	78.113	40.09	-0.00
1340	80.113	40.09	0.00
1342	82.212	40.09	0.00
1344	84.113	40.09	0.00
1346	86.105	40.09	0.00
1348	88.113	40.09	-0.00
1350	90.113	40.09	-0.00
1352	92.245	40.09	0.00
1354	94.113	40.09	0.00
1356	96.113	40.09	0.00
1358	98.113	40.09	0.00
1420	120.110	40.09	0.00
1440	140.250	40.09	0.00
1500	160.110	40.09	0.00
1520	180.030	40.09	0.00
1540	200.120	40.09	0.00
1559	219.980	40.09	0.00

Average level: 40.09

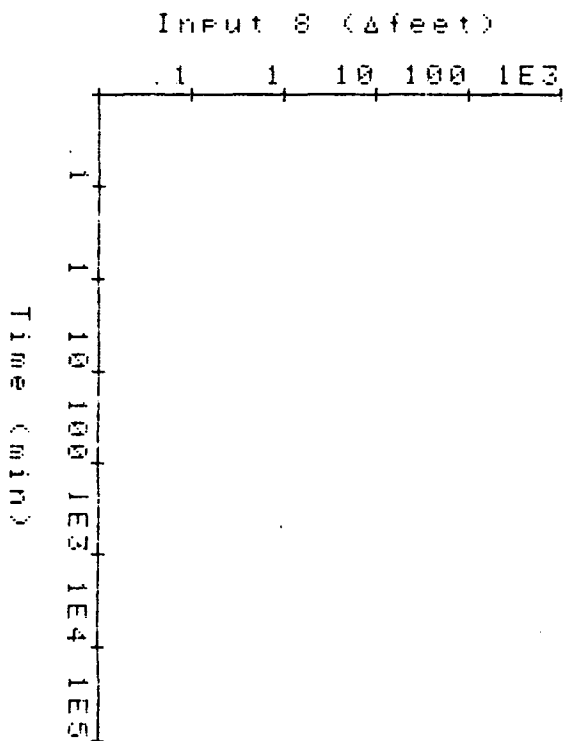
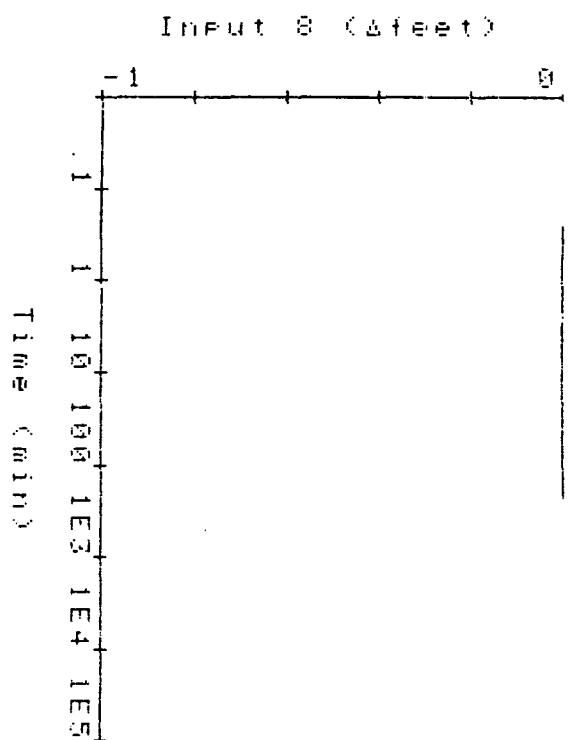


Input 8 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	38.82	0.00
1220	0.257	38.82	0.00
1220	0.341	38.83	-0.00
1220	0.424	38.82	0.00
1220	0.507	38.82	0.00
1220	0.591	38.82	0.00
1220	0.674	38.82	0.00
1220	0.757	38.82	0.00
1220	0.841	38.82	0.00
1220	0.924	38.82	0.00
1221	1.007	38.82	0.00
1221	1.417	38.82	0.00
1221	1.750	38.82	0.00
1222	2.084	38.82	0.00
1222	2.417	38.82	0.00
1222	2.750	38.82	0.00
1223	3.084	38.82	0.00
1223	3.417	38.82	0.00
1223	3.750	38.82	0.00
1224	4.084	38.83	-0.00
1224	4.417	38.82	0.00
1224	4.750	38.82	0.00
1225	5.084	38.82	0.00
1225	5.417	38.82	0.00
1225	5.750	38.82	0.00
1226	6.084	38.82	0.00
1226	6.417	38.82	0.00
1226	6.750	38.82	0.00
1227	7.084	38.83	-0.00
1227	7.417	38.82	0.00
1227	7.750	38.82	0.00
1228	8.084	38.82	0.00
1228	8.417	38.82	0.00
1228	8.750	38.82	0.00
1229	9.084	38.82	0.00
1229	9.417	38.82	0.00
1229	9.750	38.82	0.00
1230	10.084	38.82	0.00
1232	12.111	38.82	0.00
1234	14.111	38.82	0.00
1236	16.099	38.82	0.00
1238	18.098	38.82	0.00
1240	20.098	38.82	0.00
1242	22.098	38.82	0.00
1244	24.098	38.82	0.00
1246	26.098	38.82	0.00
1248	28.098	38.82	0.00

1250	30.098	38.82	0.00
1252	32.098	38.82	0.00
1254	34.098	38.82	0.00
1256	36.123	38.82	0.00
1258	38.265	38.82	0.00
1300	40.108	38.82	0.00
1302	42.292	38.82	0.00
1304	44.160	38.82	0.00
1306	46.160	38.82	0.00
1308	48.160	38.82	0.00
1310	50.188	38.82	0.00
1312	52.113	38.82	0.00
1314	54.113	38.82	0.00
1316	56.113	38.82	0.00
1318	58.113	38.82	0.00
1320	60.113	38.82	0.00
1322	62.238	38.82	0.00
1324	64.113	38.82	0.00
1326	66.113	38.82	0.00
1328	68.113	38.82	0.00
1330	70.113	38.82	0.00
1332	72.113	38.82	0.00
1334	74.113	38.82	0.00
1336	76.133	38.82	0.00
1338	78.113	38.82	0.00
1340	80.113	38.82	0.00
1342	82.212	38.82	0.00
1344	84.113	38.82	0.00
1346	86.105	38.82	0.00
1348	88.113	38.82	0.00
1350	90.113	38.82	0.00
1352	92.245	38.82	0.00
1354	94.113	38.82	0.00
1356	96.113	38.82	0.00
1358	98.113	38.82	0.00
1420	120.110	38.82	0.00
1440	140.250	38.82	0.00
1500	160.110	38.83	-0.00
1520	180.030	38.82	0.00
1540	200.120	38.82	0.00
1559	219.980	38.83	-0.00

Average level: 38.82



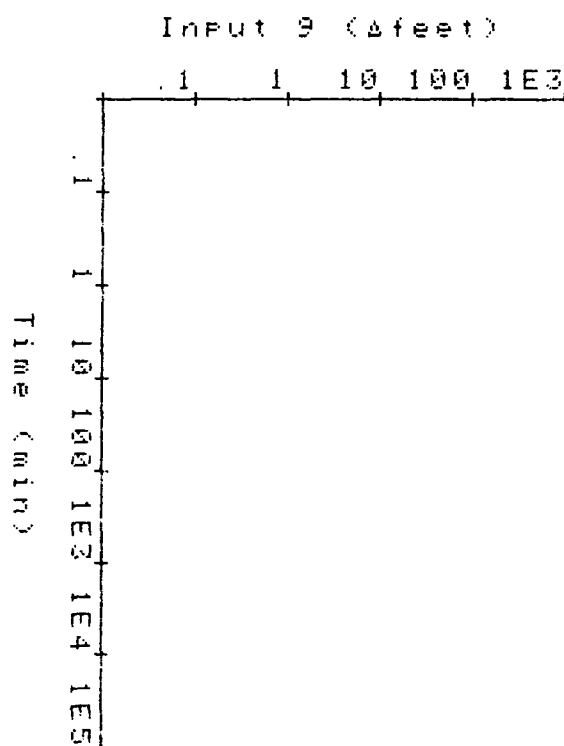
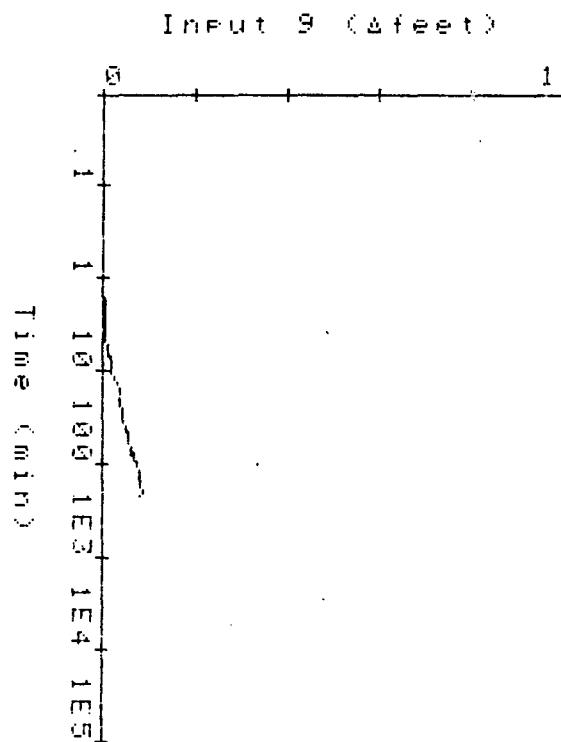
Input 9 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	5.67	0.00
1220	0.257	5.67	0.00
1220	0.341	5.67	0.00
1220	0.424	5.67	0.00
1220	0.507	5.67	0.00
1220	0.591	5.67	0.00
1220	0.674	5.67	0.00
1220	0.757	5.67	0.00
1220	0.841	5.67	0.00
1220	0.924	5.67	0.00
1221	1.007	5.67	0.00
1221	1.417	5.67	0.00
1221	1.750	5.66	0.01
1222	2.084	5.66	0.01
1222	2.417	5.66	0.01
1222	2.750	5.66	0.01
1223	3.084	5.66	0.01
1223	3.417	5.66	0.01
1223	3.750	5.66	0.01
1224	4.084	5.66	0.01
1224	4.417	5.66	0.01
1224	4.750	5.66	0.01
1225	5.084	5.66	0.01
1225	5.417	5.66	0.01
1225	5.750	5.66	0.01
1226	6.084	5.66	0.01
1226	6.417	5.66	0.01
1226	6.750	5.66	0.01
1227	7.084	5.65	0.02
1227	7.417	5.65	0.02
1227	7.750	5.65	0.02
1228	8.084	5.65	0.02
1228	8.417	5.65	0.02
1228	8.750	5.65	0.02
1229	9.084	5.65	0.02
1229	9.417	5.65	0.02
1229	9.750	5.65	0.02
1230	10.084	5.65	0.02
1232	12.111	5.64	0.03
1234	14.111	5.64	0.03
1236	16.099	5.64	0.03
1238	18.098	5.64	0.03
1240	20.098	5.63	0.04
1242	22.098	5.63	0.04
1244	24.098	5.63	0.04
1246	26.098	5.63	0.04
1248	28.098	5.63	0.04
1250	30.098	5.63	0.04
1252	32.098	5.62	0.05
1254	34.098	5.62	0.05
1256	36.123	5.62	0.05



1258	38.265	5.62	0.05
1300	40.100	5.62	0.05
1302	42.202	5.62	0.05
1304	44.160	5.62	0.05
1306	46.160	5.62	0.06
1308	48.160	5.62	0.06
1310	50.188	5.62	0.06
1312	52.113	5.61	0.06
1314	54.113	5.61	0.06
1316	56.113	5.61	0.06
1318	58.113	5.61	0.06
1320	60.113	5.61	0.06
1322	62.238	5.61	0.06
1324	64.113	5.61	0.06
1326	66.113	5.61	0.06
1328	68.113	5.61	0.06
1330	70.113	5.61	0.06
1332	72.113	5.61	0.06
1334	74.113	5.61	0.06
1336	76.133	5.60	0.07
1338	78.113	5.61	0.06
1340	80.113	5.60	0.07
1342	82.212	5.60	0.07
1344	84.113	5.60	0.07
1346	86.105	5.60	0.07
1348	88.113	5.60	0.07
1350	90.113	5.60	0.07
1352	92.245	5.60	0.07
1354	94.113	5.60	0.07
1356	96.113	5.60	0.07
1358	98.113	5.60	0.07
1420	120.110	5.59	0.08
1440	140.250	5.59	0.08
1500	160.110	5.59	0.08
1520	180.030	5.59	0.08
1540	200.120	5.58	0.09
1559	219.980	5.59	0.08

Average level: 5.60

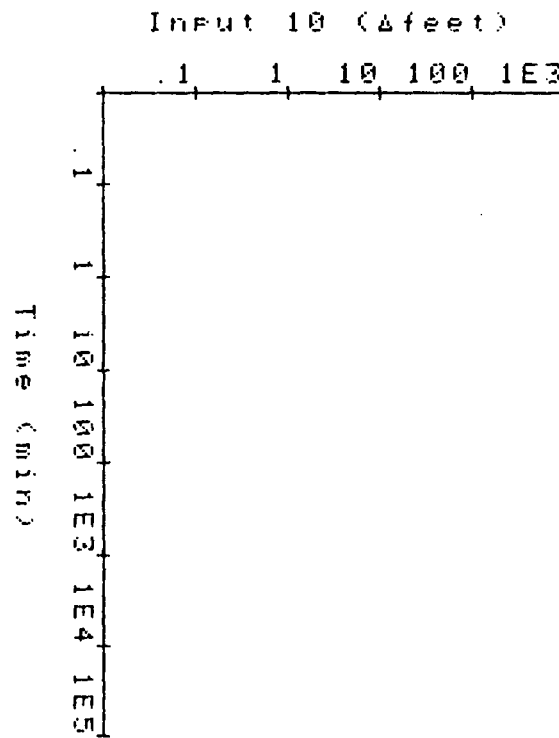
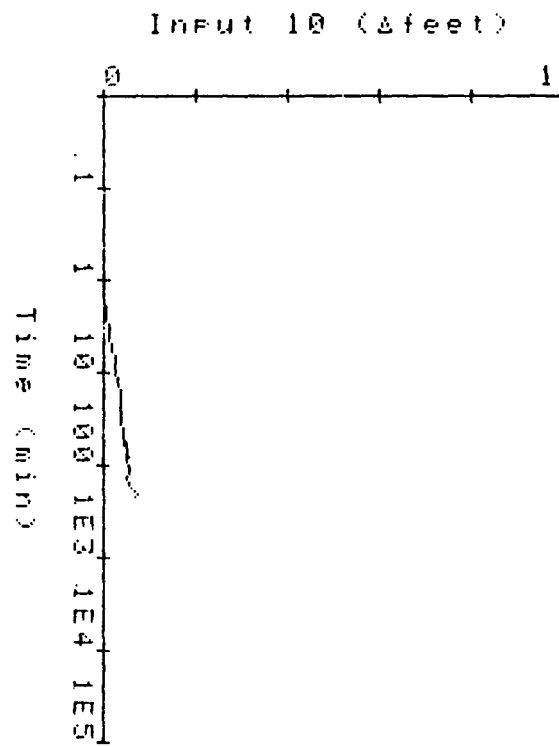


Input 10 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	7.05	0.00
1220	0.017	7.05	0.00
1220	0.034	7.05	0.00
1220	0.050	7.05	0.00
1220	0.067	7.05	0.00
1220	0.084	7.05	0.00
1220	0.100	7.05	0.00
1220	0.117	7.05	0.00
1220	0.134	7.05	0.00
1220	0.150	7.05	0.00
1220	0.167	7.05	0.00
1220	0.257	7.05	0.00
1220	0.341	7.05	0.00
1220	0.424	7.05	0.00
1220	0.507	7.05	0.00
1220	0.591	7.05	0.00
1220	0.674	7.05	0.00
1220	0.757	7.05	0.00
1220	0.841	7.05	0.00
1220	0.924	7.05	0.00
1221	1.007	7.05	0.00
1221	1.417	7.05	0.00
1221	1.750	7.05	0.00
1222	2.084	7.04	0.01
1222	2.417	7.04	0.01
1222	2.750	7.04	0.01
1223	3.084	7.04	0.01
1223	3.417	7.04	0.01
1223	3.750	7.04	0.01
1224	4.084	7.04	0.01
1224	4.417	7.04	0.01
1224	4.750	7.03	0.02
1225	5.084	7.03	0.02
1225	5.417	7.03	0.02
1225	5.750	7.03	0.02
1226	6.084	7.03	0.02
1226	6.417	7.03	0.02
1226	6.750	7.03	0.02
1227	7.084	7.03	0.02
1227	7.417	7.03	0.02
1227	7.750	7.03	0.02
1228	8.084	7.03	0.02
1228	8.417	7.03	0.02
1228	8.750	7.02	0.03
1229	9.084	7.02	0.03
1229	9.417	7.02	0.03
1229	9.750	7.02	0.03
1230	10.084	7.02	0.03
1232	12.111	7.02	0.03

1234	14.111	7.02	0.03
1236	16.099	7.01	0.04
1238	18.098	7.01	0.04
1240	20.098	7.01	0.04
1242	22.098	7.02	0.03
1244	24.098	7.01	0.04
1246	26.098	7.01	0.04
1248	28.098	7.01	0.04
1250	30.098	7.01	0.04
1252	32.098	7.01	0.04
1254	34.098	7.01	0.04
1256	36.123	7.01	0.04
1258	38.265	7.01	0.04
1300	40.108	7.01	0.04
1302	42.202	7.01	0.04
1304	44.160	7.01	0.04
1306	46.160	7.01	0.04
1308	48.160	7.00	0.05
1310	50.188	7.00	0.05
1312	52.113	7.00	0.05
1314	54.113	7.00	0.05
1316	56.113	7.00	0.05
1318	58.113	7.00	0.05
1320	60.113	7.00	0.05
1322	62.238	7.00	0.05
1324	64.113	7.00	0.05
1326	66.113	7.00	0.05
1328	68.113	7.00	0.05
1330	70.113	7.00	0.05
1332	72.113	7.00	0.05
1334	74.113	7.00	0.05
1336	76.133	7.00	0.05
1338	78.113	7.00	0.05
1340	80.113	7.00	0.05
1342	82.212	7.00	0.05
1344	84.113	7.00	0.05
1346	86.105	7.00	0.05
1348	88.113	7.00	0.05
1350	90.113	7.00	0.05
1352	92.245	7.00	0.05
1354	94.113	7.00	0.05
1356	96.113	7.00	0.05
1358	98.113	7.00	0.05
1420	120.110	7.00	0.05
1440	140.250	7.00	0.05
1500	160.110	6.99	0.06
1520	180.030	6.99	0.06
1540	200.120	6.97	0.08
1559	219.980	6.98	0.07

Average level: 7.00

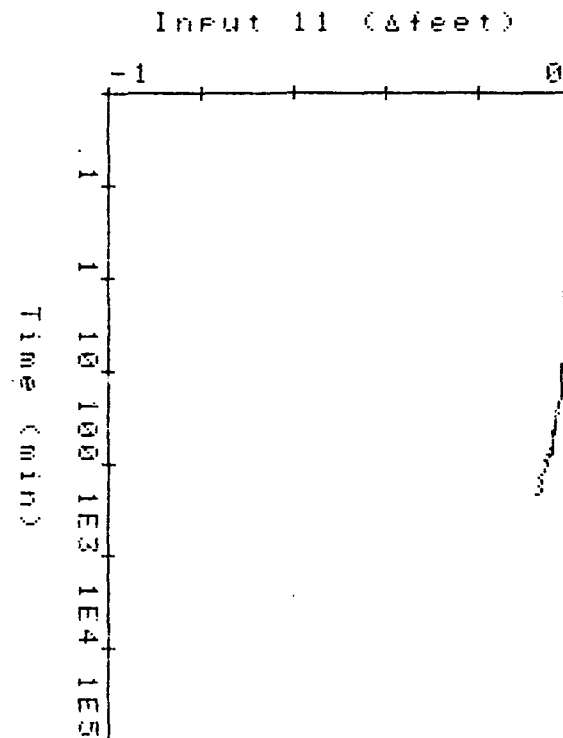


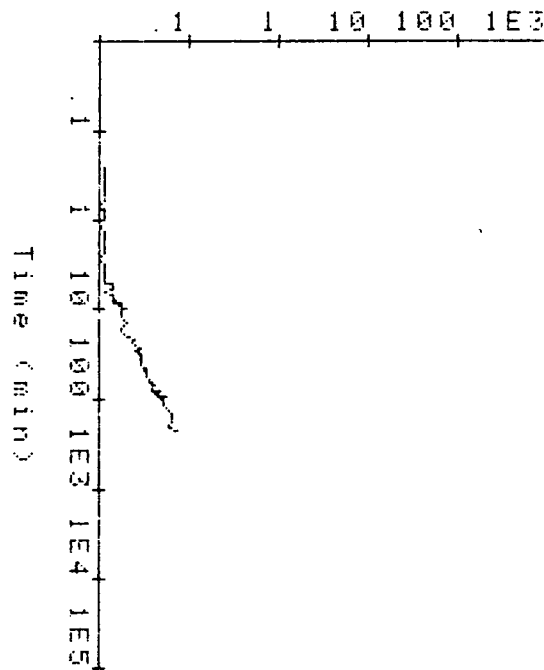
Input 11 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	7.05	0.00
1220	0.257	7.06	-0.01
1220	0.341	7.06	-0.01
1220	0.424	7.06	-0.01
1220	0.507	7.06	-0.01
1220	0.591	7.06	-0.01
1220	0.674	7.06	-0.01
1220	0.757	7.06	-0.01
1220	0.841	7.06	-0.01
1220	0.924	7.06	-0.01
1221	1.007	7.06	-0.01
1221	1.417	7.06	-0.01
1221	1.750	7.06	-0.01
1222	2.084	7.06	-0.01
1222	2.417	7.06	-0.01
1222	2.750	7.06	-0.01
1223	3.084	7.06	-0.01
1223	3.417	7.06	-0.01
1223	3.750	7.06	-0.01
1224	4.084	7.06	-0.01
1224	4.417	7.06	-0.01
1224	4.750	7.06	-0.01
1225	5.084	7.06	-0.01
1225	5.417	7.06	-0.01
1225	5.750	7.06	-0.01
1226	6.084	7.06	-0.01
1226	6.417	7.06	-0.01
1226	6.750	7.06	-0.01
1227	7.084	7.06	-0.01
1227	7.417	7.06	-0.01
1227	7.750	7.06	-0.01
1228	8.084	7.06	-0.01
1228	8.417	7.07	-0.02
1228	8.750	7.06	-0.01
1229	9.084	7.07	-0.02
1229	9.417	7.07	-0.02
1229	9.750	7.07	-0.02
1230	10.084	7.07	-0.02
1232	12.111	7.07	-0.02
1234	14.111	7.07	-0.02
1236	16.099	7.07	-0.02
1238	18.098	7.07	-0.02
1240	20.098	7.07	-0.02
1242	22.098	7.08	-0.03
1244	24.098	7.07	-0.02
1246	26.098	7.08	-0.03
1248	28.098	7.08	-0.03
1250	30.098	7.08	-0.03
1252	32.098	7.08	-0.03
1254	34.098	7.08	-0.03
1256	36.123	7.08	-0.03
1258	38.265	7.08	-0.03
1300	40.108	7.08	-0.03
1302	42.202	7.08	-0.03
1304	44.160	7.08	-0.03
1306	46.160	7.08	-0.03
1308	48.160	7.08	-0.03
1310	50.188	7.08	-0.03
1312	52.113	7.08	-0.03
1314	54.113	7.08	-0.03
1316	56.113	7.08	-0.03
1318	58.113	7.08	-0.03

1320	60.113	7.09	-0.04
1322	62.238	7.09	-0.04
1324	64.113	7.09	-0.04
1326	66.113	7.09	-0.04
1328	68.113	7.09	-0.04
1330	70.113	7.09	-0.04
1332	72.113	7.09	-0.04
1334	74.113	7.09	-0.04
1336	76.133	7.09	-0.04
1338	78.113	7.09	-0.04
1340	80.113	7.09	-0.04
1342	82.212	7.10	-0.05
1344	84.113	7.10	-0.05
1346	86.105	7.10	-0.05
1348	88.113	7.09	-0.04
1350	90.113	7.10	-0.05
1352	92.245	7.10	-0.05
1354	94.113	7.10	-0.05
1356	96.113	7.11	-0.06
1358	98.113	7.10	-0.05
1420	120.110	7.11	-0.06
1440	140.250	7.12	-0.07
1500	160.110	7.11	-0.06
1520	180.030	7.12	-0.07
1540	200.120	7.11	-0.06
1559	219.980	7.12	-0.07

Average level: 7.10





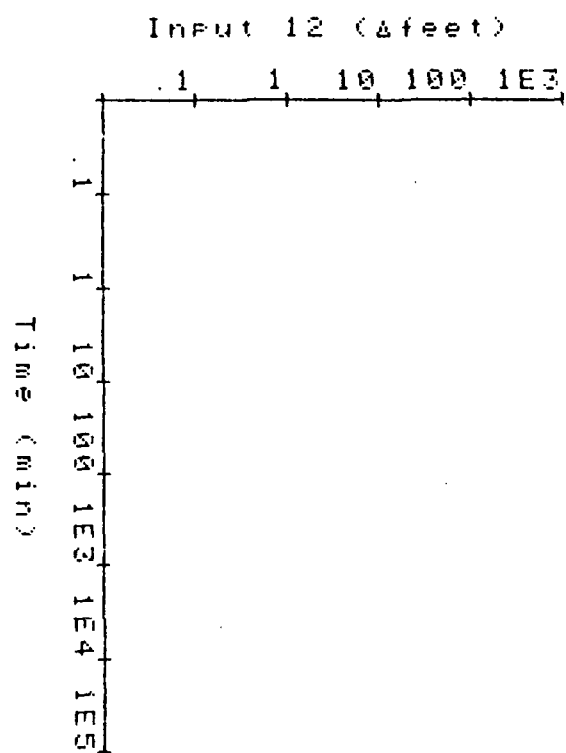
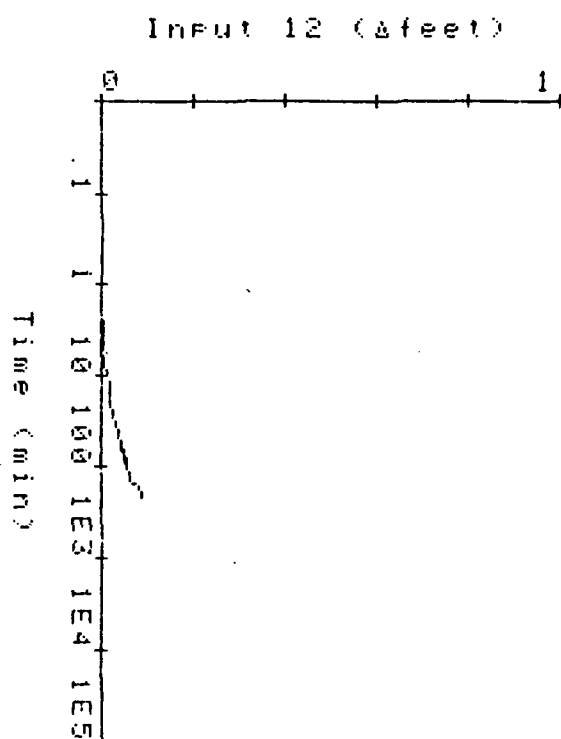
Input 12 (feet):

Time	ET (min)	level	Δlevel
1220	0.000	7.56	0.00
1220	0.257	7.56	0.00
1220	0.341	7.56	0.00
1220	0.424	7.56	0.00
1220	0.507	7.56	0.00
1220	0.591	7.56	0.00
1220	0.674	7.56	0.00
1220	0.757	7.56	0.00
1220	0.841	7.56	0.00
1220	0.924	7.56	0.00
1221	1.007	7.56	0.00
1221	1.417	7.56	0.00
1221	1.750	7.56	0.00
1222	2.084	7.56	0.00
1222	2.417	7.56	0.00
1222	2.750	7.55	0.01
1223	3.084	7.55	0.01
1223	3.417	7.55	0.01
1223	3.750	7.55	0.01
1224	4.084	7.55	0.01
1224	4.417	7.55	0.01
1224	4.750	7.55	0.01
1225	5.084	7.55	0.01
1225	5.417	7.55	0.01
1225	5.750	7.55	0.01
1226	6.084	7.55	0.01
1226	6.417	7.55	0.01
1226	6.750	7.55	0.01



1227	7.084	7.55	0.01
1227	7.417	7.55	0.01
1227	7.750	7.55	0.01
1228	8.084	7.55	0.01
1228	8.417	7.55	0.01
1228	8.750	7.55	0.01
1229	9.084	7.55	0.01
1229	9.417	7.55	0.01
1229	9.750	7.55	0.01
1230	10.084	7.55	0.01
1232	12.111	7.54	0.02
1234	14.111	7.54	0.02
1236	16.099	7.54	0.02
1238	18.098	7.54	0.02
1240	20.098	7.54	0.02
1242	22.098	7.54	0.02
1244	24.098	7.54	0.02
1246	26.098	7.54	0.02
1248	28.098	7.53	0.03
1250	30.098	7.53	0.03
1252	32.098	7.53	0.03
1254	34.098	7.53	0.03
1256	36.123	7.53	0.03
1258	38.265	7.53	0.03
1300	40.100	7.53	0.03
1302	42.202	7.53	0.03
1304	44.160	7.52	0.04
1306	46.160	7.52	0.04
1308	48.160	7.52	0.04
1310	50.188	7.52	0.04
1312	52.113	7.52	0.04
1314	54.113	7.52	0.04
1316	56.113	7.51	0.05
1318	58.113	7.52	0.04
1320	60.113	7.51	0.05
1322	62.238	7.51	0.05
1324	64.113	7.51	0.05
1326	66.113	7.51	0.05
1328	68.113	7.51	0.05
1330	70.113	7.51	0.05
1332	72.113	7.51	0.05
1334	74.113	7.51	0.05
1336	76.133	7.51	0.05
1338	78.113	7.51	0.05
1340	80.113	7.50	0.06
1342	82.212	7.50	0.06
1344	84.113	7.50	0.06
1346	86.105	7.50	0.06
1348	88.113	7.51	0.05
1350	90.113	7.50	0.06
1352	92.245	7.50	0.06
1354	94.113	7.50	0.06
1356	96.113	7.51	0.05
1358	98.113	7.50	0.06
1420	120.110	7.50	0.06
1440	140.250	7.50	0.06
1500	160.110	7.48	0.08
1520	180.030	7.48	0.08
1540	200.120	7.47	0.09
1559	219.980	7.47	0.09

Average level: 7.50

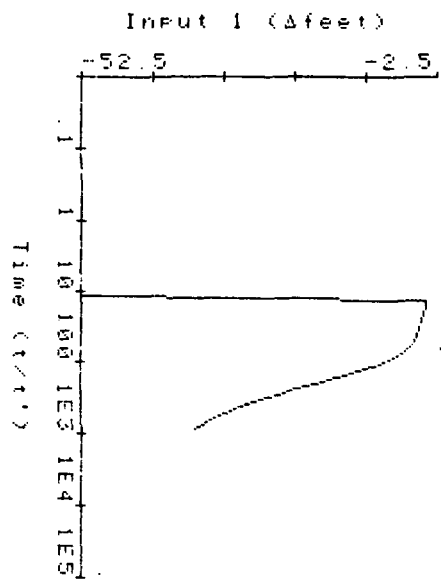
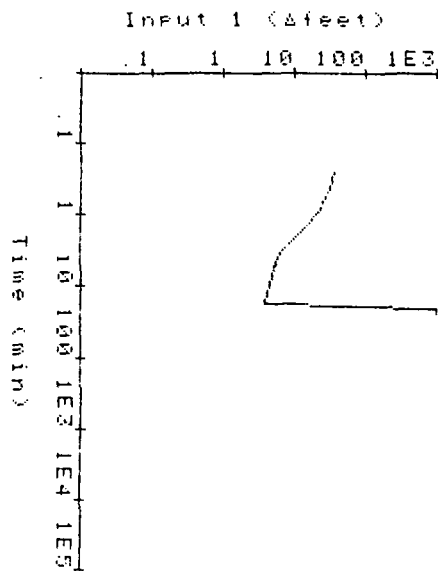
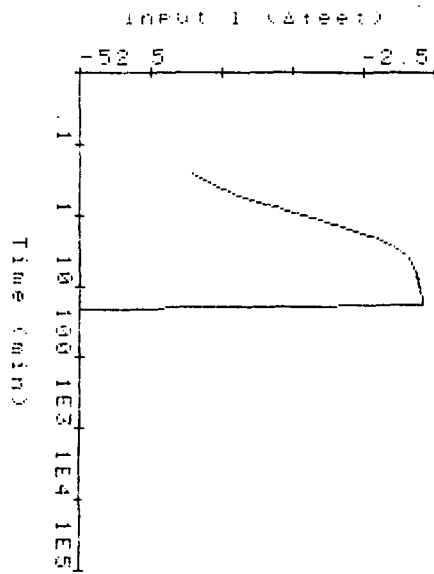


-----RECOVERY REPORT-----

Started at 1559  
Lasted 23.735 min

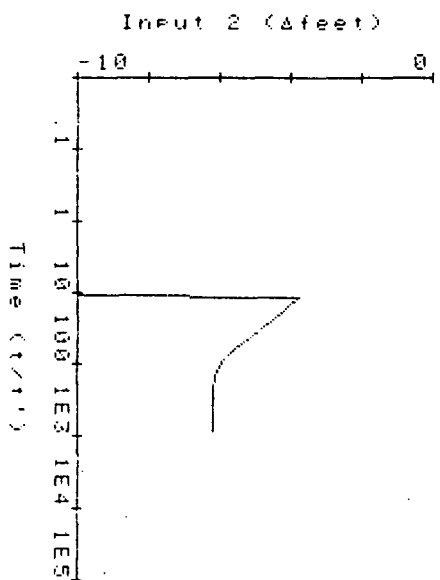
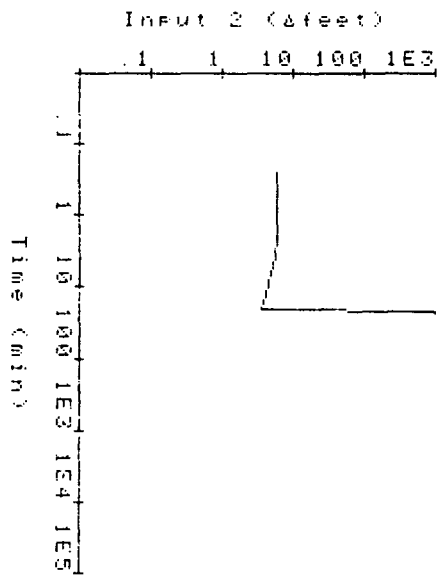
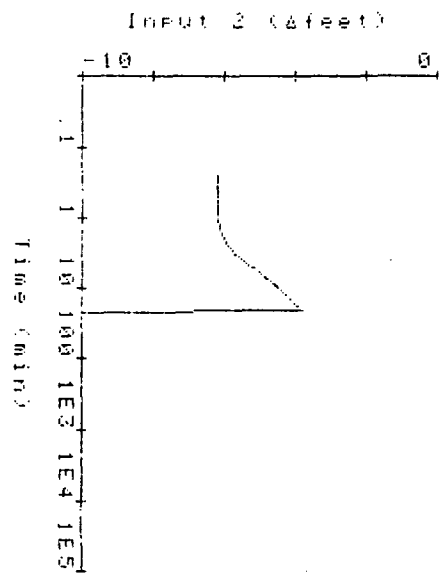
Input 1 (feet):

Time	ET (min)	level	Δlevel
1600	0.257	117.55	-36.55
1600	0.341	115.20	-34.20
1600	0.424	113.04	-32.04
1600	0.507	111.01	-30.01
1600	0.591	109.13	-28.13
1600	0.674	107.37	-26.37
1600	0.757	105.72	-24.72
1600	0.841	104.22	-23.22
1600	0.924	102.80	-21.81
1600	1.007	101.50	-20.50
1601	1.417	96.39	-15.39
1601	1.750	93.51	-12.51
1602	2.084	91.47	-10.47
1602	2.417	90.01	-9.01
1602	2.750	88.98	-7.98
1603	3.084	88.22	-7.22
1603	3.417	87.69	-6.69
1603	3.750	87.29	-6.29
1604	4.084	86.99	-5.99
1604	4.417	86.76	-5.76
1604	4.750	86.58	-5.58
1605	5.084	86.43	-5.43
1605	5.417	86.30	-5.30
1605	5.750	86.20	-5.20
1606	6.084	86.12	-5.12
1606	6.417	86.05	-5.05
1606	6.750	85.98	-4.98
1607	7.084	85.90	-4.90
1607	7.417	85.85	-4.85
1607	7.750	85.80	-4.80
1608	8.084	85.75	-4.75
1608	8.417	85.69	-4.69
1608	8.750	85.65	-4.65
1609	9.084	85.62	-4.62
1609	9.417	85.58	-4.58
1609	9.750	85.53	-4.53
1610	10.084	85.49	-4.49
1612	12.117	85.32	-4.32
1614	14.117	85.16	-4.16
1616	16.117	85.03	-4.03
1618	18.117	84.92	-3.92
1620	20.117	-999.99	-999.99
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99



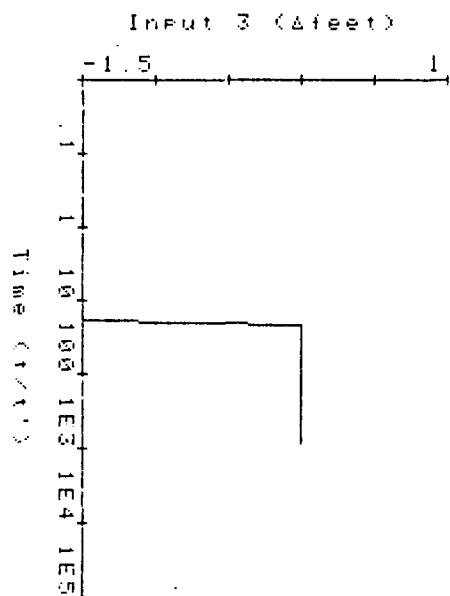
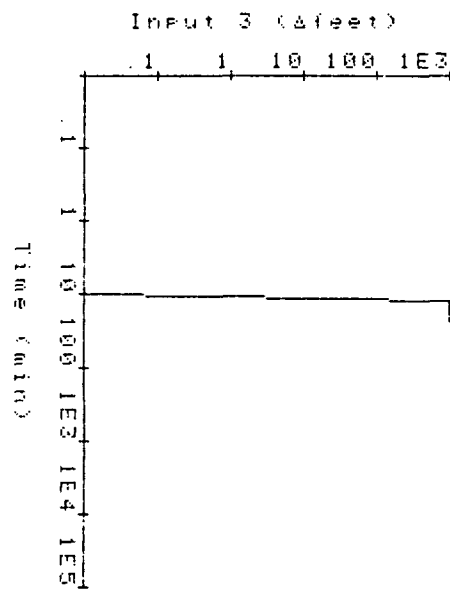
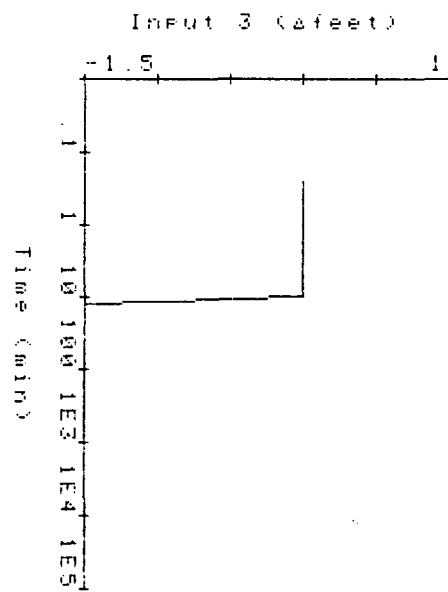
Input 2 (feet):

Time	ET (min)	level	Δlevel
1600	0.257	90.83	-6.19
1600	0.341	90.83	-6.19
1600	0.424	90.85	-6.21
1600	0.507	90.85	-6.21
1600	0.591	90.85	-6.21
1600	0.674	90.85	-6.21
1600	0.757	90.85	-6.21
1600	0.841	90.85	-6.21
1600	0.924	90.83	-6.19
1600	1.007	90.83	-6.19
1601	1.417	90.79	-6.15
1601	1.750	90.73	-6.09
1602	2.084	90.66	-6.02
1602	2.417	90.57	-5.93
1602	2.750	90.48	-5.84
1603	3.084	90.38	-5.74
1603	3.417	90.29	-5.65
1603	3.750	90.21	-5.57
1604	4.084	90.10	-5.46
1604	4.417	90.02	-5.38
1604	4.750	89.94	-5.30
1605	5.084	89.86	-5.22
1605	5.417	89.78	-5.14
1605	5.750	89.71	-5.07
1606	6.084	89.65	-5.01
1606	6.417	89.58	-4.94
1606	6.750	89.52	-4.88
1607	7.084	89.48	-4.84
1607	7.417	89.42	-4.78
1607	7.750	89.38	-4.74
1608	8.084	89.33	-4.69
1608	8.417	89.28	-4.64
1608	8.750	89.23	-4.59
1609	9.084	89.20	-4.56
1609	9.417	89.16	-4.52
1609	9.750	89.13	-4.49
1610	10.084	89.09	-4.45
1612	12.117	88.90	-4.26
1614	14.117	88.75	-4.11
1616	16.117	88.62	-3.98
1618	18.117	88.52	-3.89
1620	20.117	88.40	-3.76
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99



Input 3 (feet):

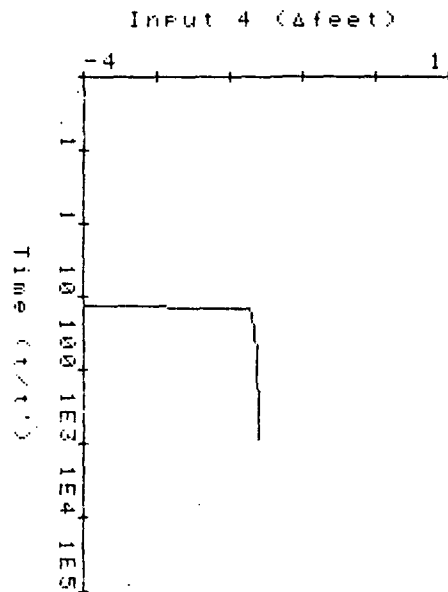
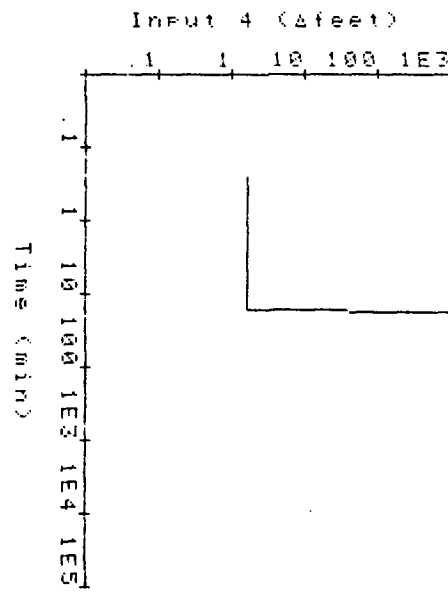
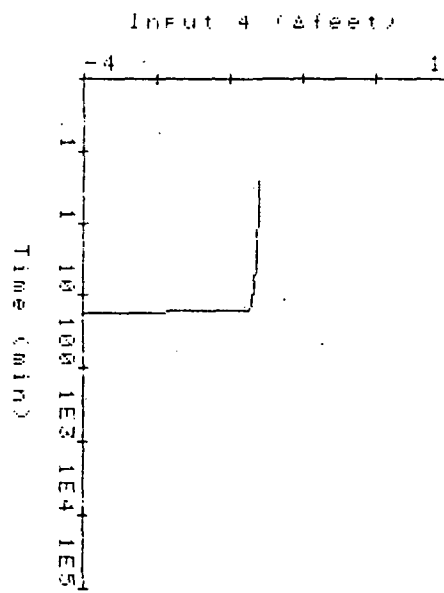
Time	ET (min)	level	Δlevel
1600	0.257	0.00	-0.00
1600	0.341	0.00	-0.00
1600	0.424	0.00	0.00
1600	0.507	-0.00	0.00
1600	0.591	0.00	0.00
1600	0.674	-0.00	0.00
1600	0.757	-0.00	0.00
1600	0.841	0.00	0.00
1600	0.924	-0.00	0.00
1600	1.007	0.00	0.00
1601	1.417	0.00	-0.00
1601	1.750	-0.00	0.00
1602	2.084	0.00	-0.00
1602	2.417	0.00	-0.00
1602	2.750	0.00	0.00
1603	3.084	0.00	0.00
1603	3.417	0.00	0.00
1603	3.750	0.00	-0.00
1604	4.084	0.00	0.00
1604	4.417	-0.00	0.00
1604	4.750	0.00	0.00
1605	5.084	0.00	0.00
1605	5.417	0.00	0.00
1605	5.750	0.00	0.00
1606	6.084	0.00	0.00
1606	6.417	-0.00	0.00
1606	6.750	0.00	0.00
1607	7.084	-0.00	0.00
1607	7.417	0.00	0.00
1607	7.750	-0.00	0.00
1608	8.084	0.00	0.00
1608	8.417	-0.00	0.00
1608	8.750	-0.00	0.00
1609	9.084	0.00	-0.00
1609	9.417	0.00	0.00
1609	9.750	0.00	0.00
1610	10.084	0.00	0.00
1612	12.117	-999.99	-999.99
1614	14.117	-999.99	-999.99
1616	16.117	-999.99	-999.99
1618	18.117	-999.99	-999.99
1620	20.117	-999.99	-999.99
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99





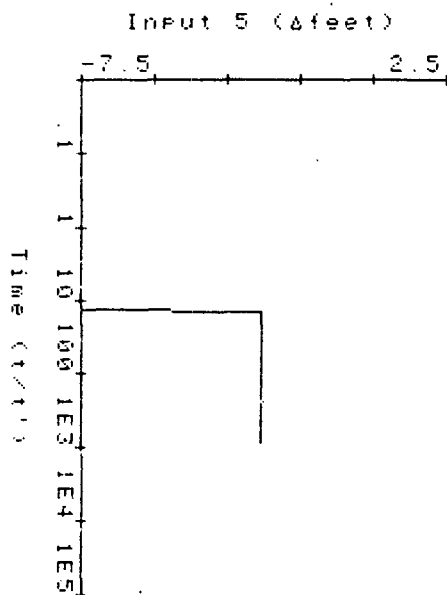
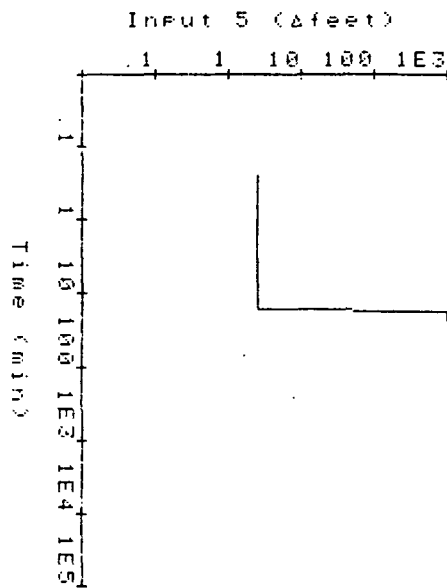
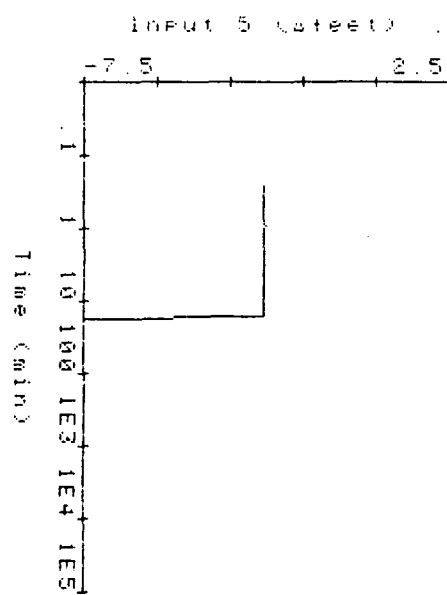
Input 4 (feet):

Time	ET (min)	level	Δlevel
1600	0.257	83.91	-1.60
1600	0.341	83.91	-1.60
1600	0.424	83.92	-1.61
1600	0.507	83.92	-1.61
1600	0.591	83.92	-1.61
1600	0.674	83.92	-1.61
1600	0.757	83.92	-1.61
1600	0.841	83.92	-1.61
1600	0.924	83.92	-1.61
1600	1.007	83.92	-1.61
1601	1.417	83.92	-1.61
1601	1.750	83.93	-1.61
1602	2.084	83.93	-1.62
1602	2.417	83.93	-1.62
1602	2.750	83.93	-1.62
1603	3.084	83.93	-1.62
1603	3.417	83.94	-1.63
1603	3.750	83.94	-1.63
1604	4.084	83.94	-1.63
1604	4.417	83.95	-1.64
1604	4.750	83.95	-1.64
1605	5.084	83.95	-1.64
1605	5.417	83.95	-1.64
1605	5.750	83.95	-1.64
1606	6.084	83.96	-1.65
1606	6.417	83.96	-1.65
1606	6.750	83.96	-1.65
1607	7.084	83.96	-1.65
1607	7.417	83.97	-1.66
1607	7.750	83.97	-1.66
1608	8.084	83.97	-1.66
1608	8.417	83.97	-1.66
1608	8.750	83.97	-1.66
1609	9.084	83.97	-1.66
1609	9.417	83.98	-1.67
1609	9.750	83.98	-1.67
1610	10.084	83.98	-1.67
1612	12.117	83.99	-1.68
1614	14.117	84.01	-1.70
1616	16.117	84.02	-1.71
1618	18.117	-999.99	-999.99
1620	20.117	-999.99	-999.99
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99



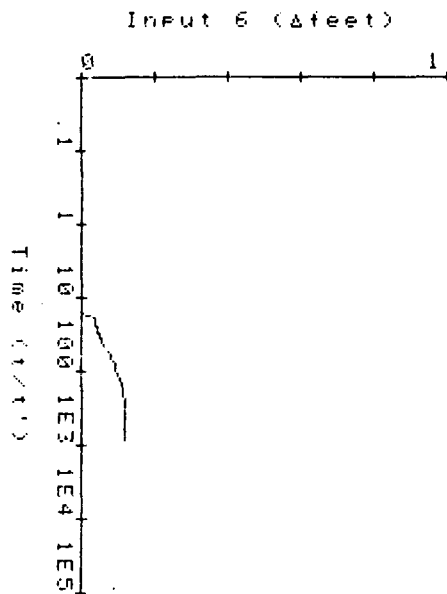
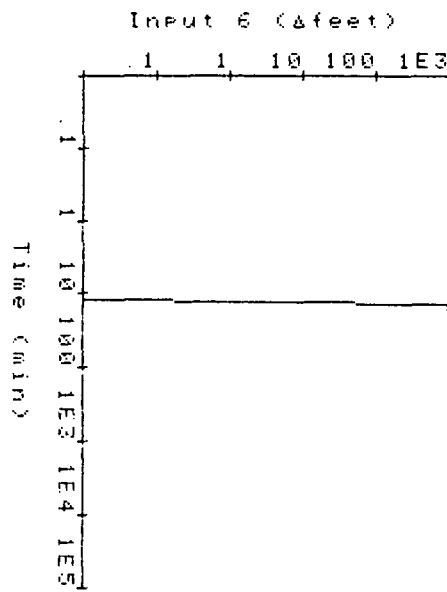
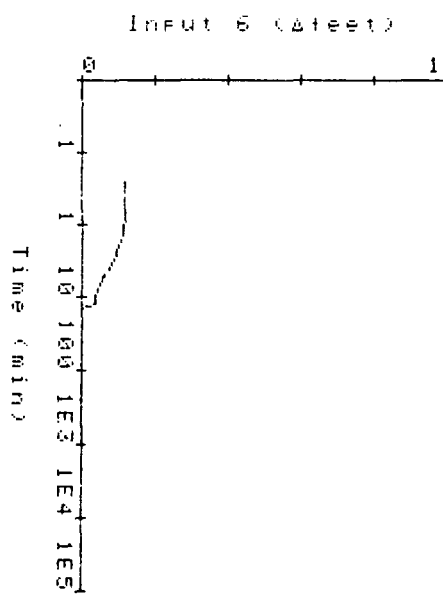
Input 5 (feet):

Time	ET (min)	level	Δlevel
1600	0.257	82.51	-2.54
1600	0.341	82.51	-2.54
1600	0.424	82.51	-2.54
1600	0.507	82.51	-2.54
1600	0.591	82.51	-2.54
1600	0.674	82.51	-2.54
1600	0.757	82.51	-2.54
1600	0.841	82.51	-2.54
1600	0.924	82.50	-2.53
1600	1.007	82.51	-2.53
1601	1.417	82.52	-2.54
1601	1.750	82.52	-2.55
1602	2.084	82.52	-2.55
1602	2.417	82.52	-2.55
1602	2.750	82.52	-2.55
1603	3.084	82.53	-2.56
1603	3.417	82.53	-2.56
1603	3.750	82.53	-2.56
1604	4.084	82.53	-2.56
1604	4.417	82.53	-2.56
1604	4.750	82.53	-2.56
1605	5.084	82.53	-2.56
1605	5.417	82.53	-2.56
1605	5.750	82.53	-2.56
1606	6.084	82.53	-2.56
1606	6.417	82.54	-2.56
1606	6.750	82.53	-2.56
1607	7.084	82.54	-2.56
1607	7.417	82.54	-2.56
1607	7.750	82.54	-2.56
1608	8.084	82.54	-2.56
1608	8.417	82.54	-2.56
1608	8.750	82.54	-2.57
1609	9.084	82.54	-2.57
1609	9.417	82.54	-2.57
1609	9.750	82.54	-2.57
1610	10.084	82.54	-2.57
1612	12.117	82.54	-2.57
1614	14.117	82.54	-2.57
1616	16.117	82.54	-2.57
1618	18.117	-999.99	-999.99
1620	20.117	-999.99	-999.99
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99



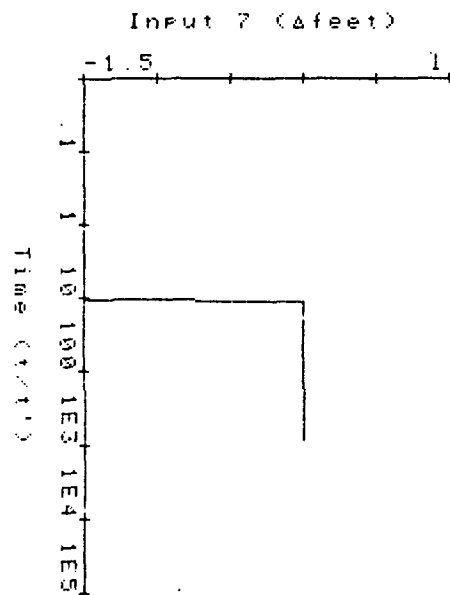
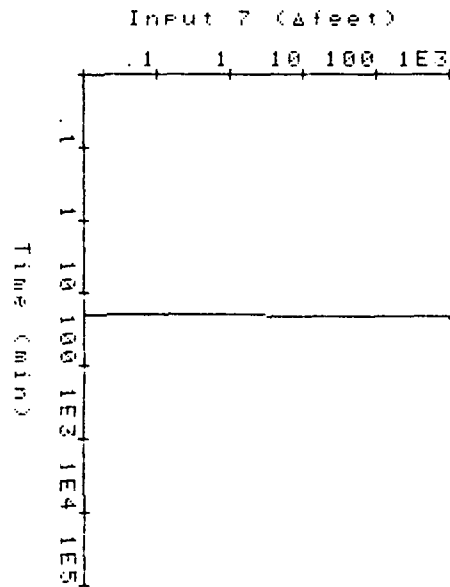
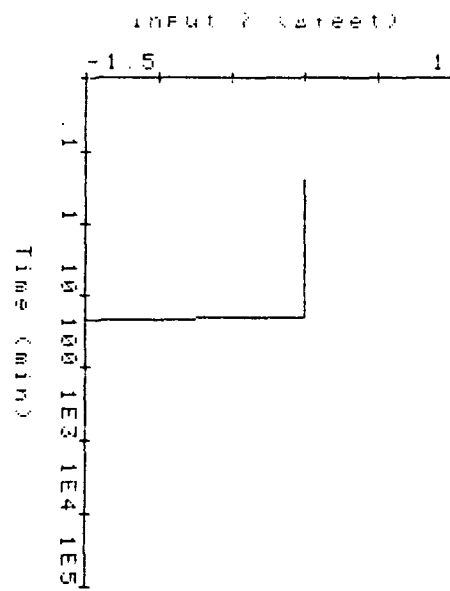
Input 6 (feet):

Time	ET (min)	level	Δlevel
1600	0.257	45.96	0.12
1600	0.341	45.96	0.12
1600	0.424	45.96	0.12
1600	0.507	45.96	0.12
1600	0.591	45.96	0.12
1600	0.674	45.96	0.12
1600	0.757	45.96	0.12
1600	0.841	45.96	0.12
1600	0.924	45.96	0.12
1600	1.007	45.96	0.11
1601	1.417	45.96	0.11
1601	1.750	45.97	0.11
1602	2.084	45.97	0.10
1602	2.417	45.98	0.10
1602	2.750	45.98	0.09
1603	3.084	45.99	0.09
1603	3.417	45.99	0.08
1603	3.750	46.00	0.08
1604	4.084	46.00	0.08
1604	4.417	46.00	0.07
1604	4.750	46.01	0.06
1605	5.084	46.01	0.06
1605	5.417	46.02	0.06
1605	5.750	46.02	0.06
1606	6.084	46.02	0.06
1606	6.417	46.02	0.05
1606	6.750	46.03	0.05
1607	7.084	46.03	0.05
1607	7.417	46.03	0.05
1607	7.750	46.03	0.05
1608	8.084	46.03	0.04
1608	8.417	46.03	0.04
1608	8.750	46.03	0.04
1609	9.084	46.04	0.04
1609	9.417	46.04	0.04
1609	9.750	46.04	0.04
1610	10.084	46.04	0.03
1612	12.117	46.04	0.03
1614	14.117	-999.99	-999.99
1616	16.117	-999.99	-999.99
1618	18.117	-999.99	-999.99
1620	20.117	-999.99	-999.99
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99



Input 7 (feet):

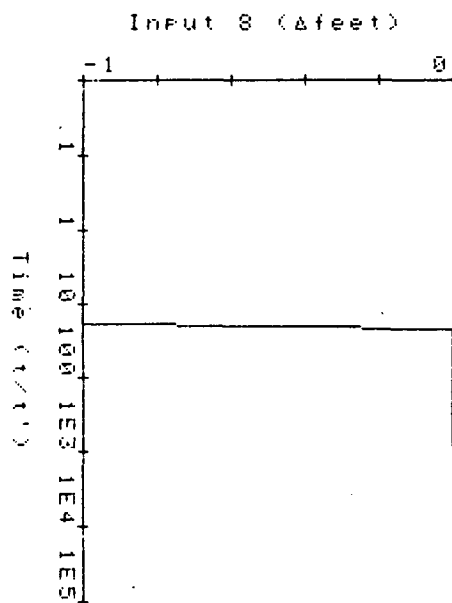
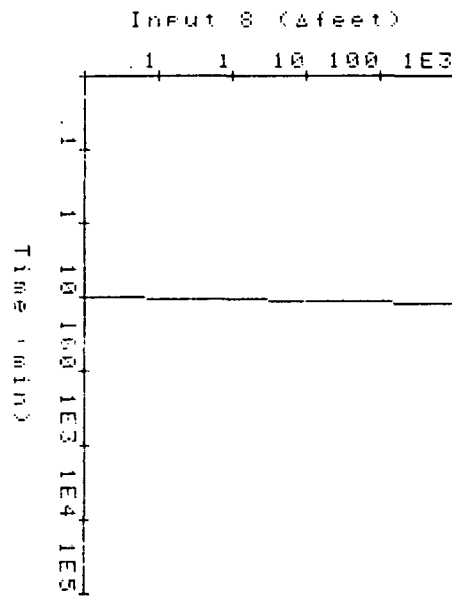
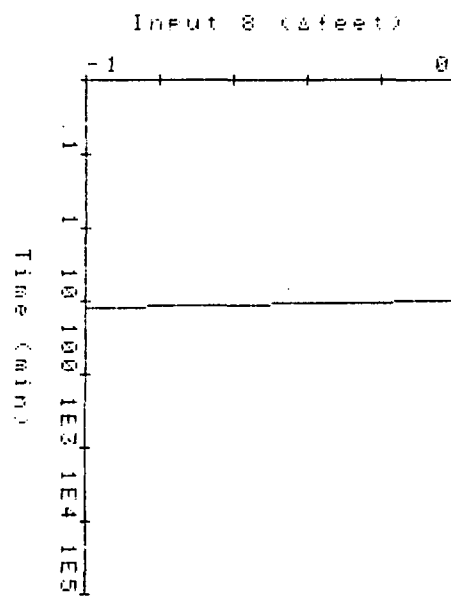
Time	ET (min)	level	Δlevel
1600	0.257	40.09	0.00
1600	0.341	40.09	0.00
1600	0.424	40.09	0.00
1600	0.507	40.09	0.00
1600	0.591	40.09	0.00
1600	0.674	40.09	0.00
1600	0.757	40.09	0.00
1600	0.841	40.09	0.00
1600	0.924	40.09	0.00
1600	1.007	40.09	0.00
1601	1.417	40.09	0.00
1601	1.750	40.09	0.00
1602	2.084	40.09	0.00
1602	2.417	40.09	0.00
1602	2.750	40.09	0.00
1603	3.084	40.09	0.00
1603	3.417	40.09	0.00
1603	3.750	40.09	0.00
1604	4.084	40.09	0.00
1604	4.417	40.09	0.00
1604	4.750	40.09	0.00
1605	5.084	40.09	0.00
1605	5.417	40.09	0.00
1605	5.750	40.09	0.00
1606	6.084	40.09	0.00
1606	6.417	40.09	0.00
1606	6.750	40.09	0.00
1607	7.084	40.09	0.00
1607	7.417	40.09	0.00
1607	7.750	40.09	0.00
1608	8.084	40.09	0.00
1608	8.417	40.09	0.00
1608	8.750	40.09	0.00
1609	9.084	40.09	0.00
1609	9.417	40.09	0.00
1609	9.750	40.09	0.00
1610	10.084	40.09	0.00
1612	12.117	40.09	0.00
1614	14.117	40.09	0.00
1616	16.117	40.09	0.00
1618	18.117	40.09	0.00
1620	20.117	40.09	0.00
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99





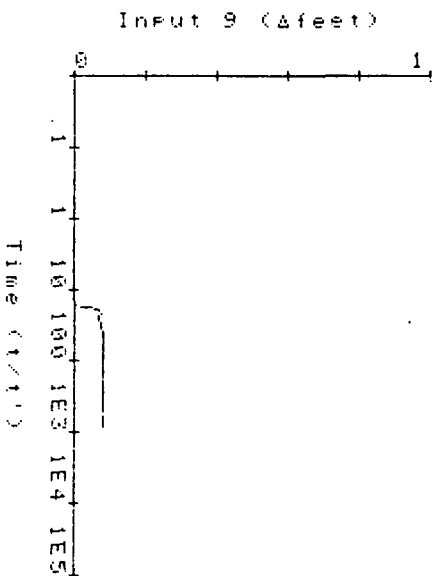
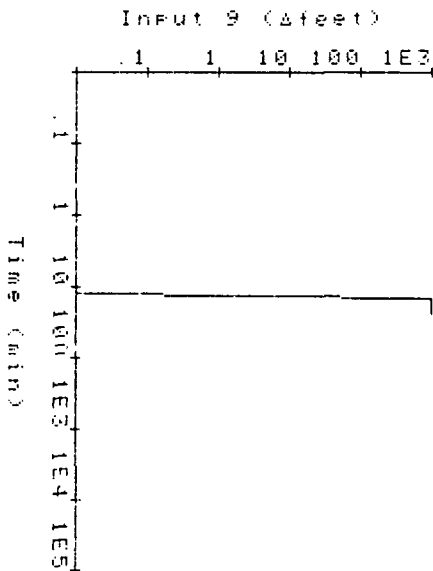
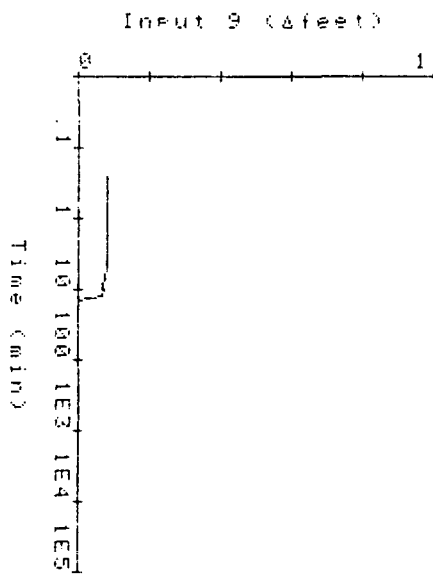
Input 8 (feet):

Time	ET (min)	level	Δlevel
1600	0.257	38.82	0.00
1600	0.341	38.83	-0.00
1600	0.424	38.83	-0.00
1600	0.507	38.83	-0.00
1600	0.591	38.83	-0.00
1600	0.674	38.82	0.00
1600	0.757	38.83	-0.00
1600	0.841	38.83	-0.00
1600	0.924	38.83	-0.00
1600	1.007	38.82	0.00
1601	1.417	38.83	-0.00
1601	1.750	38.83	-0.00
1602	2.084	38.83	-0.00
1602	2.417	38.82	0.00
1602	2.750	38.83	-0.00
1603	3.084	38.83	-0.00
1603	3.417	38.83	-0.00
1603	3.750	38.83	-0.00
1604	4.084	38.83	-0.00
1604	4.417	38.83	-0.00
1604	4.750	38.83	-0.00
1605	5.084	38.83	-0.00
1605	5.417	38.83	-0.00
1605	5.750	38.82	0.00
1606	6.084	38.83	-0.00
1606	6.417	38.83	-0.00
1606	6.750	38.82	0.00
1607	7.084	38.83	-0.00
1607	7.417	38.83	-0.00
1607	7.750	38.83	-0.00
1608	8.084	38.83	-0.00
1608	8.417	38.83	-0.00
1608	8.750	38.83	-0.00
1609	9.084	38.82	0.00
1609	9.417	38.83	-0.00
1609	9.750	38.83	-0.00
1610	10.084	38.83	-0.00
1612	12.117	-999.99	-999.99
1614	14.117	-999.99	-999.99
1616	16.117	-999.99	-999.99
1618	18.117	-999.99	-999.99
1620	20.117	-999.99	-999.99
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99



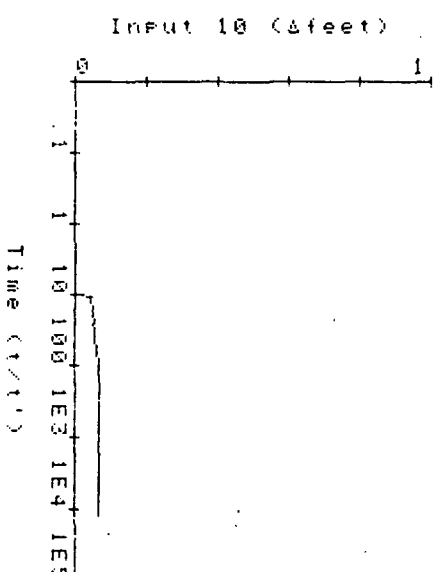
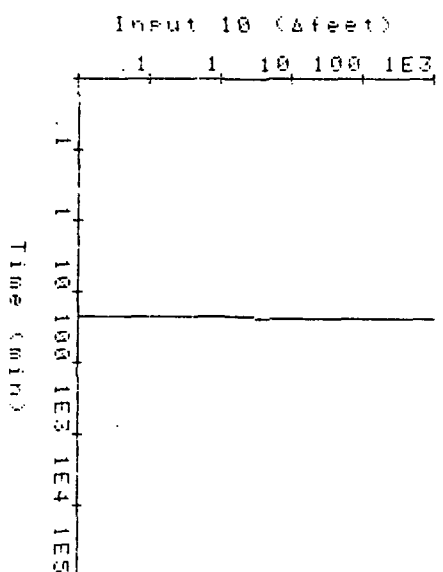
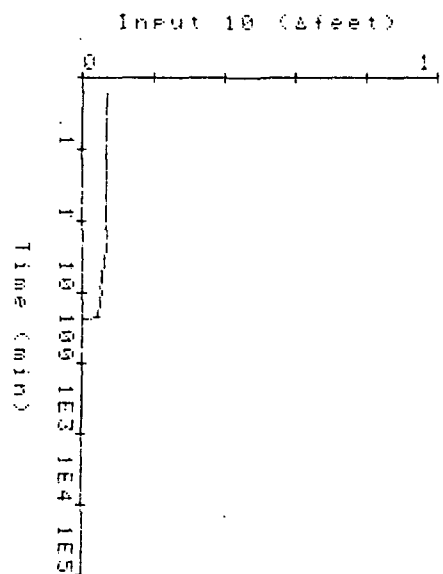
Input 9 (feet):

Time	ET (min)	level	Δlevel
1600	0.257	5.59	0.00
1600	0.341	5.59	0.00
1600	0.424	5.59	0.00
1600	0.507	5.59	0.00
1600	0.591	5.59	0.00
1600	0.674	5.59	0.00
1600	0.757	5.59	0.00
1600	0.841	5.59	0.00
1600	0.924	5.59	0.00
1600	1.007	5.59	0.00
1601	1.417	5.59	0.00
1601	1.750	5.59	0.00
1602	2.084	5.59	0.00
1602	2.417	5.59	0.00
1602	2.750	5.59	0.00
1603	3.084	5.59	0.00
1603	3.417	5.59	0.00
1603	3.750	5.59	0.00
1604	4.084	5.59	0.00
1604	4.417	5.59	0.00
1604	4.750	5.59	0.00
1605	5.084	5.59	0.00
1605	5.417	5.59	0.00
1605	5.750	5.59	0.00
1606	6.084	5.59	0.00
1606	6.417	5.59	0.00
1606	6.750	5.59	0.00
1607	7.084	5.60	0.07
1607	7.417	5.60	0.07
1607	7.750	5.60	0.07
1608	8.084	5.60	0.07
1608	8.417	5.60	0.07
1608	8.750	5.60	0.07
1609	9.084	5.60	0.07
1609	9.417	5.60	0.07
1609	9.750	5.60	0.07
1610	10.084	5.60	0.07
1612	12.117	5.60	0.07
1614	14.117	-999.99	-999.99
1616	16.117	-999.99	-999.99
1618	18.117	-999.99	-999.99
1620	20.117	-999.99	-999.99
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99



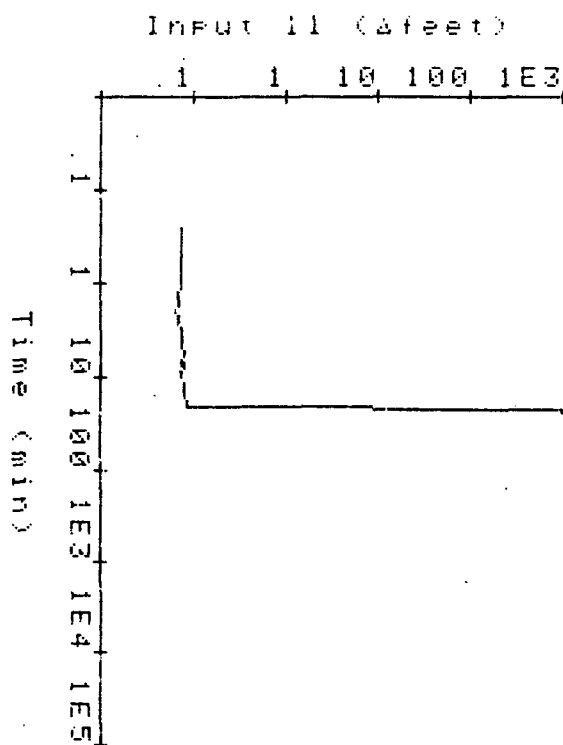
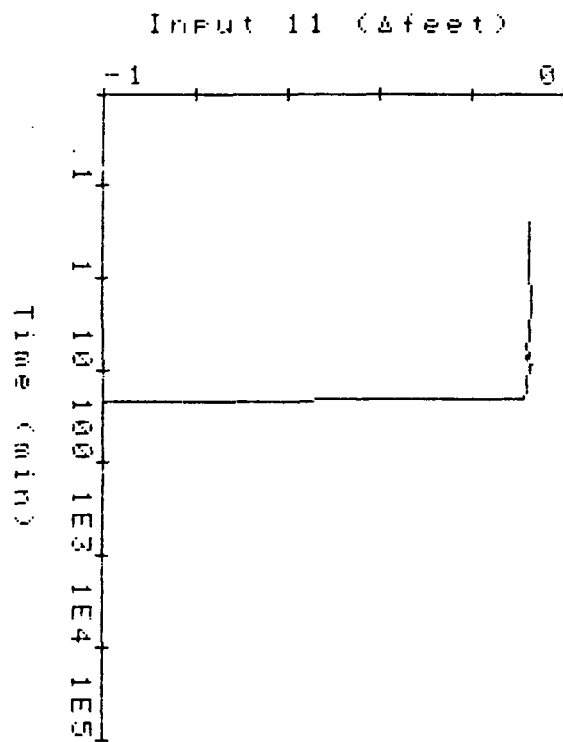
Input 10 (feet):

Time	ET (min)	level	Δlevel
1600	0.017	6.98	0.07
1600	0.034	6.98	0.07
1600	0.050	6.98	0.07
1600	0.067	6.98	0.07
1600	0.084	6.98	0.07
1600	0.100	6.98	0.07
1600	0.117	6.98	0.07
1600	0.134	6.98	0.07
1600	0.150	6.98	0.07
1600	0.167	6.98	0.07
1600	0.257	6.98	0.07
1600	0.341	6.98	0.07
1600	0.424	6.98	0.07
1600	0.507	6.98	0.07
1600	0.591	6.98	0.07
1600	0.674	6.98	0.07
1600	0.757	6.98	0.07
1600	0.841	6.98	0.07
1600	0.924	6.98	0.07
1600	1.007	6.98	0.07
1601	1.417	6.98	0.07
1601	1.750	6.98	0.07
1602	2.084	6.98	0.07
1602	2.417	6.98	0.07
1602	2.750	6.98	0.07
1603	3.084	6.99	0.06
1603	3.417	6.99	0.06
1603	3.750	6.99	0.06
1604	4.084	6.99	0.06
1604	4.417	6.99	0.06
1604	4.750	6.99	0.06
1605	5.084	6.99	0.06
1605	5.417	7.00	0.05
1605	5.750	7.00	0.05
1606	6.084	7.00	0.05
1606	6.417	7.00	0.05
1606	6.750	7.00	0.05
1607	7.084	7.00	0.05
1607	7.417	7.00	0.05
1607	7.750	7.00	0.05
1608	8.084	7.00	0.05
1608	8.417	7.00	0.05
1608	8.750	7.00	0.05
1609	9.084	7.00	0.05
1609	9.417	7.00	0.05
1609	9.750	7.00	0.05
1610	10.084	7.00	0.05
1612	12.117	7.00	0.05
1614	14.117	7.00	0.05
1616	16.117	7.00	0.05
1618	18.117	7.00	0.05
1620	20.117	7.00	0.05
1622	22.117	7.00	0.05
1623	23.735	-999.99	-999.99

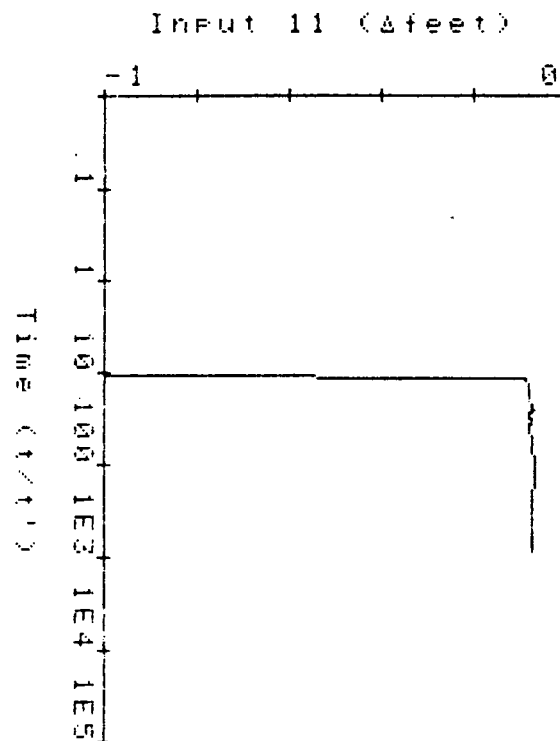


Input 11 (feet):

Time	ET (min)	level	Δlevel
1600	0.257	7.12	-0.07
1600	0.341	7.12	-0.07
1600	0.424	7.12	-0.07
1600	0.507	7.12	-0.07
1600	0.591	7.12	-0.07
1600	0.674	7.12	-0.07
1600	0.757	7.12	-0.07
1600	0.841	7.12	-0.07
1600	0.924	7.12	-0.07
1600	1.007	7.12	-0.07
1601	1.417	7.12	-0.07
1601	1.750	7.12	-0.07
1602	2.084	7.12	-0.07
1602	2.417	7.12	-0.07
1602	2.750	7.12	-0.07
1603	3.084	7.12	-0.07
1603	3.417	7.13	-0.08
1603	3.750	7.13	-0.08
1604	4.084	7.12	-0.07
1604	4.417	7.13	-0.08
1604	4.750	7.13	-0.08
1605	5.084	7.13	-0.08
1605	5.417	7.13	-0.08
1605	5.750	7.13	-0.08
1606	6.084	7.13	-0.08
1606	6.417	7.13	-0.08
1606	6.750	7.13	-0.08
1607	7.084	7.13	-0.08
1607	7.417	7.13	-0.08
1607	7.750	7.13	-0.08
1608	8.084	7.13	-0.08
1608	8.417	7.12	-0.07
1608	8.750	7.12	-0.07
1609	9.084	7.12	-0.07
1609	9.417	7.12	-0.07
1609	9.750	7.12	-0.07
1610	10.084	7.13	-0.08
1612	12.117	7.13	-0.08
1614	14.117	7.13	-0.08
1616	16.117	7.13	-0.08
1618	18.117	7.13	-0.08
1620	20.117	7.14	-0.09
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99



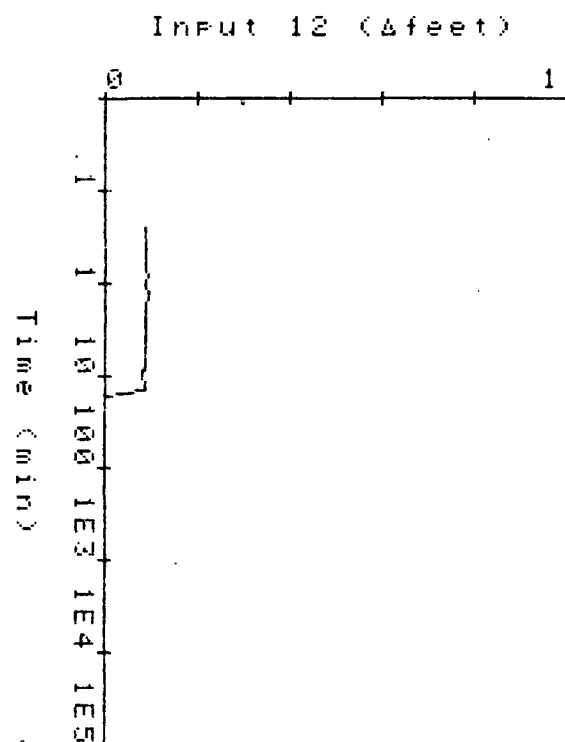


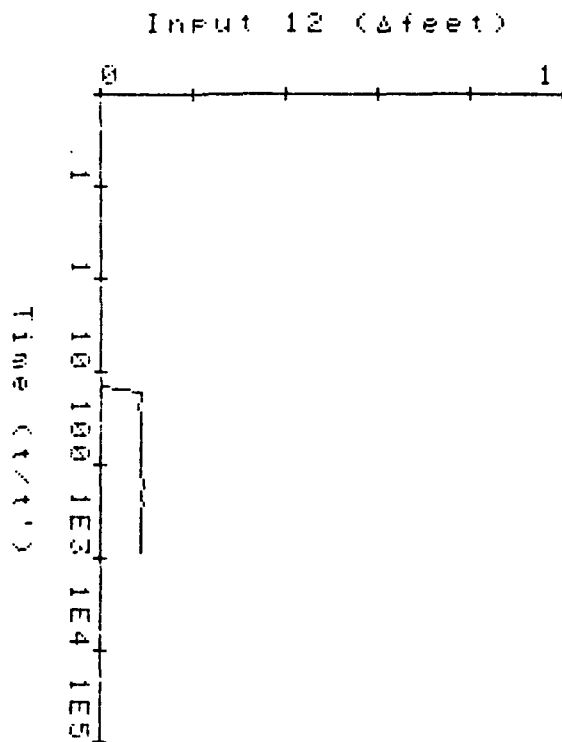
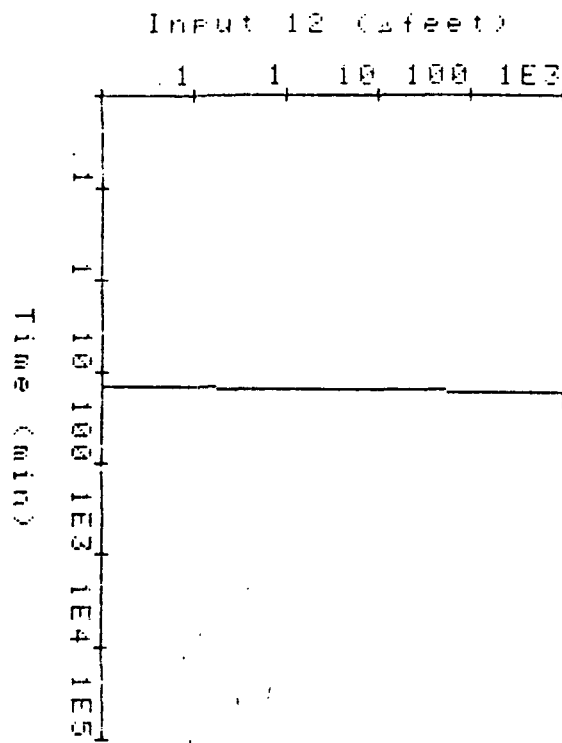


Input 12 (feet):

Time	ET (min)	level	$\Delta$ level
1600	0.257	7.47	0.09
1600	0.341	7.47	0.09
1600	0.424	7.47	0.09
1600	0.507	7.47	0.09
1600	0.591	7.47	0.09
1600	0.674	7.47	0.09
1600	0.757	7.47	0.09
1600	0.841	7.47	0.09
1600	0.924	7.47	0.09
1600	1.007	7.47	0.09
1601	1.417	7.47	0.09
1601	1.750	7.47	0.09

1602	2.084	7.47	0.09
1602	2.417	7.47	0.09
1602	2.750	7.47	0.09
1603	3.084	7.47	0.09
1603	3.417	7.47	0.09
1603	3.750	7.47	0.09
1604	4.084	7.47	0.09
1604	4.417	7.47	0.09
1604	4.750	7.47	0.09
1605	5.084	7.47	0.09
1605	5.417	7.47	0.09
1605	5.750	7.47	0.09
1606	6.084	7.47	0.09
1606	6.417	7.47	0.09
1606	6.750	7.47	0.09
1607	7.084	7.47	0.09
1607	7.417	7.47	0.09
1607	7.750	7.47	0.09
1608	8.084	7.47	0.09
1608	8.417	7.47	0.09
1608	8.750	7.48	0.08
1609	9.084	7.48	0.08
1609	9.417	7.48	0.08
1609	9.750	7.48	0.08
1610	10.084	7.48	0.08
1612	12.117	7.47	0.09
1614	14.117	7.47	0.09
1616	16.117	-999.99	-999.99
1618	18.117	-999.99	-999.99
1620	20.117	-999.99	-999.99
1622	22.117	-999.99	-999.99
1623	23.735	-999.99	-999.99





SE200B manufactured by  
In-situ, Inc.  
Laramie, Wyoming

# CALCULATIONS AND COMPUTATIONS

SHEET \_\_\_\_ OF \_\_\_\_

PROJECT: \_\_\_\_\_

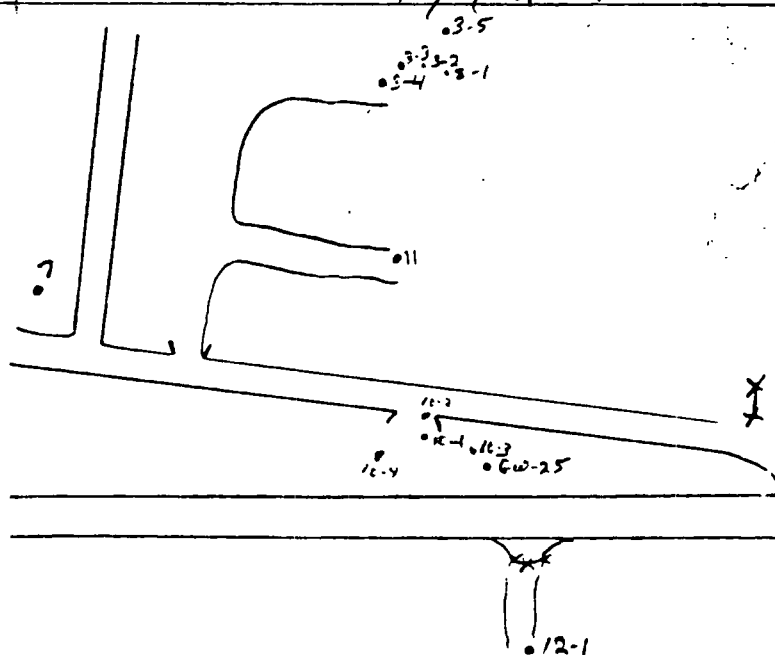
JOB NO.: \_\_\_\_\_

SUBJECT: FRENCH LTD WELLS

COMPUTED BY: \_\_\_\_\_ DATE: 9-19-86

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

MW #	CASING ELEVATION FEET MSL	INITIALS	TIME	WCL FROM NOTCH (FEET)	WCL FEET MSL
11		J.A.	8.15	79.97	
3-1		J.A.	8.24	5.38	
3-2		J.A.	8.21	4.87	
3-3		J.A.	8.23	5.97	
3-4		J.A.	8.19	82.31	
3-5		J.A.	8.25	4.46	
7		J.A.	8.32	81.17	
10-1			—	—	
10-2		J.A.	8.05	5.67	
10-3			—	—	
10-4		J.A.	8.03	7.56	
GW-25		J.A.	8.08	84.64	
PIC-2		—	—	—	—
PIC-3		—	—	—	—
PIC-4		—	—	—	—
12-1		J.A.	8.40	79.66	
RES-12-2 Mudlog		J.A.	8.42	4.31	



**REI**

# CALCULATIONS AND COMPUTATIONS

SHEET 1 OF 1

PROJECT: \_\_\_\_\_

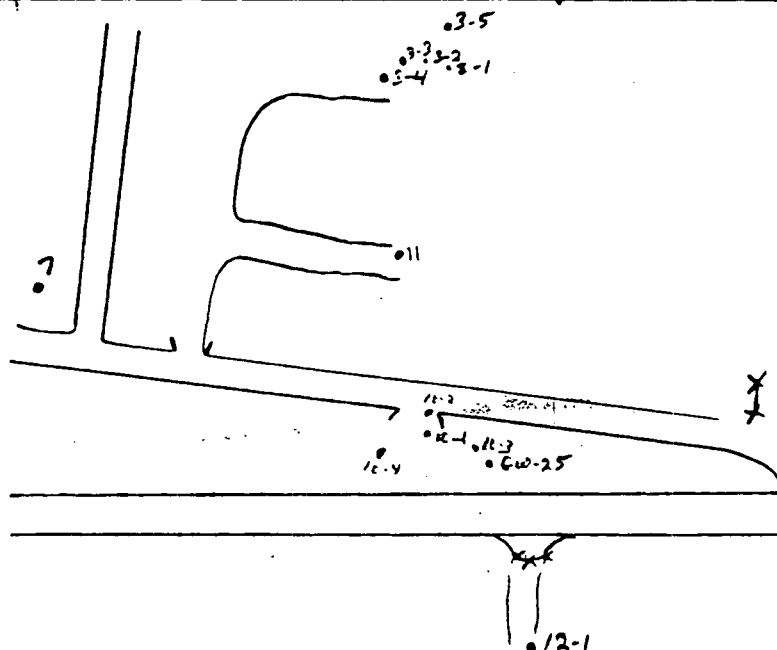
JOB NO.: 275-14

SUBJECT: FRENCH LTD WELLS

COMPUTED BY: \_\_\_\_\_ DATE: 9/16/86

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

MW #	CASING ELEVATION FEET MSL	INITIALS	TIME	WL FROM NOTCH (FEET)	WL FEET MSL
11		CWA	0814	85.15	
3-1		CWA	0809	5.31	
2-2		CWA	0808	4.78	
3-3		CWA	0807	5.86	
3-4		CWA	0805	86.43	
3-5		CWA	0810	4.36	
7		CWA	0800	81.15	
10-1		SEE INSTRUCTION			
10-2		CWA	0830	5.68	
10-3		CWA	0832	7.02	
10-4		CWA	0837	7.52	
GW-25		CWA	0833	92.85	
P10-2		_____	_____	_____	_____
P10-3		_____	_____	_____	_____
P10-4		_____	_____	_____	_____
12-1		CWA	0821	80.89	
12-2		CWA	0823	4.27	



REF